# 1 Development and application of a multi-scale modelling framework for

## 2 urban high-resolution NO<sub>2</sub> pollution mapping

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11 Abstract. Vehicle emissions have become a major source of air pollution in urban areas, especially for near-road environments, where the pollution characteristics are difficult to be captured by a single-scale air quality model 12 due to the complex composition of the underlying surface. Here we developed a hybrid model CMAO-13 RLINE URBAN to quantitatively analyse the effects of vehicle emissions on urban roadside NO<sub>2</sub> concentrations 14 at a high spatial resolution of 50 m  $\times$  50 m. To estimate the influence of various street canyons on the dispersion 15 of air pollutants, a Machine Learning-based Street Canvon Flow (MLSCF) scheme was established based on 16 17 Computational Fluid Dynamic and two machine learning methods. The results indicated that compared with the 18 CMAQ model, the hybrid model improved the underestimation of NO<sub>2</sub> concentration at near-road sites with MB 19 changing from -10  $\mu$ g/m<sup>3</sup> to 6.3  $\mu$ g/m<sup>3</sup>. The MLSCF scheme obviously increased upwind concentrations within 20 deep street canyons due to changes in the wind environment caused by the vortex. In summer, the relative contribution of vehicles to NO<sub>2</sub> concentrations in Beijing urban areas was 39% on average, similar to results from 21 22 CMAQ-ISAM model, but increased significantly with the decreased distance to the road centerline, especially reaching 75% on urban freeways. 23

## 25 Graphical abstract.



## 27 1 Introduction

The accelerated urbanization leads to severe air pollution in China. As one of the indicators of air pollution, nitrogen 28 29 dioxide (NO<sub>2</sub>) causes an adverse impact on human health and promotes the generation of ozone and particulate matter (Pandey et al., 2005; Khaniabadi et al., 2017). During the last decade, benefiting from the implementations 30 31 of several air pollution control strategies by the Chinese government, the air quality has improved (Jin et al., 2016; Zheng et al., 2018), and the vertical column densities of NO<sub>2</sub> displayed a decreasing trend after 2013 (Shah et al., 32 33 2020; Cui et al., 2021). However, the economic development and nitrogen oxides  $(NO_x)$  emissions are not 34 decoupled in China (Luo et al., 2022a). In some megacities of China, such as Chengdu, the daily averaged  $NO_2$  concentration could reach 200 µg/m<sup>3</sup> (Zhu et al., 2019), far exceeding the 24-h average air quality guideline 35 of 80  $\mu$ g/m<sup>3</sup> suggested by the Ministry of Environmental Protection of China. 36

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38 The improvement of  $PM_{2.5}$  in China was mainly due to the emission reduction and control measures of industrial and domestic sources (Zhang et al., 2019b), which also relieved the  $NO_2$  pollution, but the reduction potential of 39 these sources has been gradually declining. Meanwhile, as the population of vehicles is growing rapidly, vehicle 40 41 emissions have become a major source of  $NO_2$  pollution, especially in urban areas (Nguyen et al., 2018). Due to the low release height of vehicle emissions, combined with the negative dispersion condition caused by nearby 42 43 buildings, air pollutants will be significantly accumulated near the street. According to roadside observations, 44 within the distance of about 100-200 m near roads, the concentrations of CO, NO<sub>2</sub>, ultrafine particulate matter 45 (UFP), PM<sub>2.5</sub>, PM<sub>10</sub>, and other pollutants will increase with the decreased distance to the road centerline, especially for the pollution levels of NO<sub>2</sub> and UFP increasing exponentially. Therefore, the gradient of concentration around 46 the road changes dramatically (Naveb Yazdi et al., 2015; Hagler et al., 2012). Moreover, the dispersion of air 47 pollutants in the near-road environment is significantly affected by geometric characteristics of the street canyon. 48 For example, in a standard street canyon, when the external wind direction at the roof level is perpendicular to the 49 street axis, a clockwise vortex will be generated inside, resulting in the accumulation of pollutant concentrations at 50 51 the upwind grid receptors in the canyon (Oke, 1988; Manning et al., 2000). Consequently, how to quantitatively identify urban vehicle-induced air pollution around roads affected by complex underlying surface conditions has 52 become an urgent scientific issue. 53

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Regional-scaled air quality models, represented by Chemical Transport Models (CTMs) including Community
 Multi-scale Air Quality (CMAQ) model (Byun and Schere, 2006), Comprehensive Air quality Model with

extensions (CAMx), and Weather Research and Forecasting/Chemistry model (WRF-Chem) (Grell et al., 2005), have been used extensively in assessment on the impacts of vehicle emissions on the regional atmospheric environment, focusing on the source apportionment (Luo et al., 2022b; Vara-Vela et al., 2016; Kheirbek et al., 2016; Lv et al., 2020) and evaluation of control measures (Zhang et al., 2020; Yu et al., 2019; Cheng et al., 2019; Ke et al., 2017). However, the spatial resolution of CTMs is generally larger than 1 km×1 km, so the significant impacts of vehicle emissions on near-source air quality cannot be predicted by CTMs due to the grid homogenization on vehicle emissions.

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To avoid the aforementioned disadvantages, the local-scaled numerical models based on Gaussian diffusion theory 65 66 or computational fluid dynamic (CFD) are adopted by numerous researches to study at a finer spatial resolution 67 (Zhang et al., 2021b; Patterson and Harley, 2019; Soulhac et al., 2012), including Research LINE-source Dispersion Model (RLINE) (Snyder et al., 2013), Operational Street Pollution Model (OSPM), AERMOD (Cimorelli et al., 68 2005), and RapidAir® (Masey et al., 2018). However, the large uncertainties in predictions from Gaussian 69 dispersion models come from the provided meteorological conditions and background concentrations. The natural 70 logarithm function is usually used to characterize the vertical profile of wind speed in both the inertial and rough 71 sublayers, neglecting the influence of urban complex underlying surface compositions on the wind field (Cimorelli 72 73 et al., 2005; Masey et al., 2018; Snyder et al., 2013). Nevertheless, in standard and deep street canyons, the changes 74 of vertical wind profile cannot be described by the logarithmic form, otherwise the actual wind speed will be greatly 75 overestimated (Soulhac et al., 2008). Although the OSPM has performed a large number of comparisons with field observations in shallow or standard street canyons, the validation of model performance in deep street canyons 76 77 with a large aspect ratio was still inadequate (Kakosimos et al., 2010). Moreover, OSPM overestimated the bottom 78 wind speed in a deep street canyon by about 10 times compared with the predictions from CFD, resulting in greatly 79 underestimating pollutant concentrations (Murena et al., 2009). Comparatively speaking, CFD model can accurately simulate the air flow and pollutant concentration in complex street canyons, but the simulation domain 80 81 of CFD model is much smaller than the urban scale, and the influence of the long-term meteorological boundary conditions cannot be considered. 82

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Considering the respective strengths and limitations of regional models and local models, several studies have been
carried out on coupling of air quality models applicable to different scales (Ketzel et al., 2012; Stocker et al., 2012;
Lefebvre et al., 2013; Jensen et al., 2017; Kim et al., 2018; Mallet et al., 2018; Hood et al., 2018; Benavides et al.,
2019; Kamińska, 2019; Mu et al., 2022). Although these models performed accurately in near-road simulation, the

influence of street canvons is still hard to be considered. In some hybrid models (Stocker et al., 2012; Jensen et al., 88 89 2017; Mallet et al., 2018), OSPM was still applied to calculate concentration levels within the street, where the 90 application of logarithmic wind profile probably overestimated the bottom wind speed in a deep street canyon as abovementioned. Other models simply assumed that in street canyons, wind direction followed the street direction, 91 92 and wind speed was uniform, which was not sufficient to resolve the concentration gradient within street canyons (Kim et al., 2018; Benavides et al., 2019). Berchet et al. (2017) proposed a cost-effective method for simulating 93 94 city-scale pollution taking advantage of high-resolution accurate CFD, while the primary  $NO_x$  was predicted due 95 to the lack of a chemical module. Therefore, it is essential to build an integrated model to predict long-term and near-road air pollution suitable for the urban complex underlying surface environment. 96

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98 In this paper, we developed a hybrid model CMAQ-RLINE\_URBAN by offline coupling the local RLINE model 99 with the regional CMAQ model and some localized urban thermodynamic parameter schemes, to simulate the near-100 road NO<sub>2</sub> pollution and quantify the impacts of vehicle emissions at a high spatial resolution. Specifically, in order to predict the effects of urban street canyons on the diffusion of pollutants, we developed a Machine Learning-101 based Street Canyon Flow (MLSCF) parameterization scheme, which was based on two machine learning methods 102 using wind data from 1,600 CFD simulations. To evaluate the performance of CMAQ-RLINE\_URBAN, 103 simulations under several scenarios were conducted in Beijing urban areas from August 1st to 31th of 2019, and 104 105 validated through comparison with observations from monitoring sites. Furthermore, spatial distribution 106 characteristics of NO<sub>2</sub> concentrations in the near-road environment were also analysed in this study.

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#### 108 2 Materials and Methods

#### 109 2.1 Hybrid model framework

Here, we established the MLSCF scheme based on R language, and modified the code of RLINE model to add 110 other parameterization schemes with FORTRAN language. Finally, a multiscale air quality hybrid model was 111 112 developed to achieve a high-resolution NO<sub>2</sub> pollution mapping in urban areas. The framework of CMAQ-RLINE URBAN is shown in Figure 1. The hybrid model was established based on RLINE model, offline coupling 113 with the gridded meteorological field provided by WRF model and the pollutant background concentrations from 114 non-vehicle sources provided by CMAO model with the Integrated Source Apportionment Method (ISAM), 115 considering the thermodynamic effects caused by the complex underlying surface compositions of the city. In our 116 117 model, a NO<sub>2</sub> pollution map with a high temporal (1 h) and spatial resolution (50 m×50 m) can finally be obtained.

RLINE is a Gaussian line source dispersion model developed by Snyder et al. (2013) to predict pollutant 119 120 concentrations in near-road environments. In the RLINE model, the mobile source is considered as a finite line 121 source, from which the concentration is found by approximating the line as a series of point sources and integrating the contributions of point sources using an efficient numerical integration scheme. The number of points needed 122 123 for convergence to the proper solution is a function of distance from the source line to the receptor, and each point source is simulated using a Gaussian plume formulation. The RLINE model performs generally comparable results 124 125 when evaluated with other line source models for on-road traffic emissions dispersion (Snyder et al., 2013; Heist 126 et al., 2013; Chang et al., 2015), and has been successfully used in many studies to evaluate the impacts from traffic 127 emissions on air quality (Zhai et al., 2016; Valencia et al., 2018; Benavides et al., 2019; Filigrana et al., 2020; 128 Zhang et al., 2021a).

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130 The simulation for local meteorological conditions in CMAQ-RLINE\_URBAN included three steps: Estimation for areas above the top of Urban Canopy Layer (UCL), inside of UCL, and inside of the street canyon. (1) In this 131 study, the configuration of WRF model referred to our previous study (Lv et al., 2020). The height of midpoint in 132 the bottom layer to the ground was set as 22.5 m, which was close to the average height of buildings near street 133 canyons, similar to the settings in the previous study (Benavides et al., 2019). Therefore, the meteorological field 134 135 simulated by the WRF model was used as the wind field and atmospheric stability at the top of UCL. During the 136 hybrid model running, the meteorological conditions over buildings near each road were obtained separately from WRF model according to the road location. (2) Then, the surface roughness length  $(z_0)$  of each road was estimated 137 138 based on the surrounding building geometry and used to recalculate the localized meteorological parameters (e.g. 139 Monin-Obukhov length) within UCL according to the algorithm proposed by Benavides et al. (2019) ( $z_0$  scheme). 140 The atmospheric turbulence intensity in urban areas around sunset in the afternoon was obviously enhanced 141 considering the influence of the urban heat island effect based on methods in the AERMOD model (Cimorelli et 142 al., 2005) (UHI scheme). The UHI scheme would affect the turbulent intensity based on the evaluation for the 143 upward surface heat flux and the urban boundary layer height due to convective effects, and then the mixing height, 144 convective velocity scale, surface friction velocity, and Monin-Obhukov length were all recalculated (details in the 145 Supplement Section S1). (3) Finally, the wind field within UCL was calculated according to different types of road environments: open terrain and street canyon. The logarithmic wind profile based on Monin-Obhukov Similarity 146 147 Theory (MOST) (Foken, 2006) in the original RLINE model was still used when the grid receptor was located in 148 the open terrain (MOST scheme), while the MLSCF parameterization scheme was used for grid receptors within 149 the street canyon to quantitatively characterize the influence of the street canyon geometry and the external wind 150 environment at the top of the roof. The detailed introduction for street canyon geometry and the MLSCF scheme

151 was described in the following section.

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The real-time vehicle emission inventory based on Street-Level On-road Vehicle Emission (SLOVE) Model 153 154 developed in our previous study (Lv et al., 2020), which was based on the real-time traffic condition data from AMap, was used in both regional and local air quality models. In our simulation, the concentrations of NO, NO<sub>2</sub>, 155 156 and  $O_3$  excluding contributions from vehicle emissions were used as background concentrations at the roof level, 157 avoiding the double counting in the coupling process. These background concentrations were simulated by CMAQ-158 ISAM model, in which the emissions were divided into mobile and other four emission groups to trace their contributions separately, and details were presented in our previous study (Lv et al., 2020). In addition, the influence 159 160 of atmospheric turbulence and building geometry on the vertical mixing of background concentration was 161 considered (vertical mixing scheme). The ratios of wind speed at surface and roof levels were used as a proxy to calculate the contribution of background concentration over street canyons to the near-ground level (Benavides et 162 al., 2019). In this scheme, the surface wind was from MLSCF scheme when the gird receptor is located within the 163 street canyon, and otherwise the logarithmic wind profile was used to calculate the wind speed at the specified 164 height, and details were showed in the Supplement Section S2. Finally, combined with the vehicle-induced primary 165  $NO_x$  concentration calculated by the RLINE kernel, the high spatial resolution  $NO_2$  map could be simulated 166 167 considering the photochemical process of  $NO_x$ . In this study, a simplified two-reaction scheme, including the 168 photolysis of  $NO_2$  and the oxidation of NO, was incorporated into the model to characterize the photochemical process of NO<sub>x</sub> (details in the Supplement Section S3), which has been successfully applied in the SIRANE 169 170 dispersion model (Soulhac et al., 2017).

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#### 172 **2.2 Development for MLSCF scheme**

## 173 **2.2.1 The database of street canyon geometry**

We first established a database of street canyon geometry for 15,398 roads in urban areas of Beijing based on the three-dimensional building data obtained from our previous study (Lv et al., 2020) using Geographic Information System (GIS). Three typical parameters to represent street canyon geometry were investigated, including height ratio  $(H_l/H_r)$  ( $H_l$  is the building height on the left side, while  $H_r$  is the building height on the right side), aspect ratio (H/W) (H is set to be the average height, and W is the width of the street canyon), the canyon length to height ratio (L/H) (L is set to be the length of the street canyon). In this study, the extremely special geometry of canyons was not considered, and the typical street canyons were selected as the following conditions: (1) The proportion of actual street canyon length (the length of road where the buildings nearby) was greater than 0.5; (2) H/W was greater than 0.2; (3)  $H_l/H_r$  was between 0.3 and 3.3. Finally, the total number of the typical street canyon was 1,889, with a total length of 787 km. The spatial distributions of canyon geometry are shown in Figure S1 in the Supplement. In urban areas of Beijing, street canyon was generally wide with the averaged width of 50.3 m, and buildings on both sides were relatively low with a mean of 23.6 m. Most street canyons were obviously located in areas within the fourth ring road. The shallow ( $H/W \le 0.5$ ) canyons and long canyons (L/H>7) were dominated, accounting for 54% and 84% of the total number of street canyons.

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## 189 2.2.2 Description of CFD cases

Here, to predict air flow in street canyons comprehensively, CFD simulations were conducted under combinations of different values of controlling factors based on ANSYS FLUENT (v19.2). The controlling factors included the aforementioned three typical parameters to represent canyon geometry, the background wind speed at the height of H(V(H)) and the angle between wind direction and street axis ( $\alpha$ ) to describe the external wind environment. The selected values of each factor were listed in Table 1, and total 1600 (i.e.,  $5 \times 4 \times 4 \times 5 \times 4$ ) simulations were implemented.

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In this study, the computational domain of three-dimensional (3D) full-scale CFD simulations is shown in Figure 2. The average building height *H* of the street canyon was always set to 21 m in different simulations, which was similar to the mean street canyon height in Beijing. Other actual size of street canyons (e.g. street canyon width *W*) was calculated according to the ratio of each specific simulation. Distances between urban canopy layers (UCL) boundaries and the domain top, domain inlet and domain outlet were set as 5H, 6H, and 20H, respectively.

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The turbulence closure schemes for CFD include the Reynolds-Averaged Navier-Stokes (RANS) and the Large-Eddy Simulation (LES), and the choice of them depends on the computational cost, the accuracy required and the purpose of application. The RANS resolves the mean time-averaged properties with all the turbulence motions to be modelled, while LES adopts a spatial filtering operation and consequently resolves large-scale eddies directly and parameterizes small-scale eddies (Zhong et al., 2016). Compared with the LES, the RANS is more easily established and computationally faster (Xie and Castro, 2006). However, the LES can provide a better prediction of air flow than that from the RANS when handling complex geometries (Dejoan et al., 2010; Santiago et al., 2010). 210 In this study, considering the huge computational burden of a large number of simulations and the relatively simple

211 geometry of street canyons in our modelling, the RANS was selected to characterize the air flow.

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213 Following the CFD guideline (Tominaga et al., 2008; Franke et al., 2011), zero normal gradient conditions or 214 pressure outlet conditions were applied at the domain outlet, and symmetry boundary conditions were adopted at 215 the domain top and two lateral domain boundaries. For near-wall treatment, no-slip wall boundary conditions with 216 standard wall functions were used (Fluent, 2006). All governing equations for the flow and turbulent quantities 217 were discretized by the finite volume method with the second-order upwind scheme. The SIMPLE scheme was used for the pressure and velocity coupling. The residual for continuity equation, velocity components, turbulent 218 kinetic energy, and its dissipation rate were all below  $10^{-5}$ . Meanwhile, the CFD simulation would also stop when 219 220 the iteration steps exceeded 10,000, due to the large computing cost of so many simulations. The selected turbulence 221 model and grid arrangement are discussed in the following section.

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At the domain inlet, the power-law velocity profile (Brown et al., 2001), vertical profiles of turbulent kinetic energy  $k_{in}$  and its dissipation rate  $\varepsilon_{in}$  at the domain inlet (Lien and Yee, 2004; Zhang et al., 2019a), were described below:

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$$U_0(z) = U_{ref}\left(\frac{z}{H_{ref}}\right)$$

226 
$$k_{in}(z) = \left(I_{in} \times U_0(z)\right)^2$$

227 
$$\varepsilon_{in}(z) = \frac{C_{\mu}^{3/4} k_{in}^{3/2}}{\kappa z}$$

Here,  $U_0(z)$  stood for the stream-wise velocity at the height *z*.  $U_{ref}$  represented the reference speed. The reference height  $H_{ref}$  was 21m. The power-law exponent of  $\alpha$ =0.22 denoted underlying surface roughness above mediumdense urban area (Kikumoto et al., 2017). Turbulence intensity  $I_{in}$  was 0.1, Von Karman constant  $\kappa$  was 0.41 and  $C_{\mu}$  was 0.09.

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#### 233 2.2.3 The CFD validation

In this study, the stream-wise and vertical velocity predicted by CFD within street canyons was compared with wind tunnel data in previous researches. For buildings of the cube arrays model, wind tunnel data from Brown et al. (2001) was used to evaluate the reliability of CFD results by measuring vertical profiles of velocity. In this experiment, street canyon was perpendicular to the wind direction at the roof level. For long-street models, we predicted horizontal profiles of velocity along the street centerline at the height of z=0.11H or vertical profiles at some points and then validated CFD simulations using wind tunnel data from Hang et al. (2010). In this validation case, the wind direction at the roof level was parallel to the axis of street canyons. The description and validation results are shown in Figure S2-S3, and Table S1 in the Supplement, respectively.

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We identified the influence of different minimum sizes of hexahedral cells near wall surfaces (fine: 0.1m, medium: 243 0.2m, and coarse: 0.5m) and turbulence models (standard k-ɛ model and RNG k-ɛ model) on the predicted velocity, 244 245 to evaluate the grid independence and turbulence model accuracy (Figure S3 in the Supplement). The results 246 indicated that the predictions from the standard k- $\varepsilon$  model could well match the variations of observed velocity within the street canvon, of which performances were much better than that of the RNG model. In addition, different 247 grid resolutions used in simulations would not obviously affect the predicted results. We finally adopted the 248 249 standard k- $\varepsilon$  model to characterize turbulence, and the grid with an expansion ratio of 1.1 was applied in which the minimum size of hexahedral cells near wall surfaces was 0.5 m to save the computing cost. 250

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Moreover, the averaged wind speed from CFD in street canyons with different aspect ratios and external wind direction was compared with predictions from other empirical methods used in SIRANE model (Soulhac et al., 2012) and MUNICH model (Kim et al., 2018). Similar predictions using different methods also proved the reliability of CFD simulation in this study (Figure S4 in the Supplement).

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## 257 2.2.4 Machine learning

Data driven method, such as machine learning and deep learning, is now a successful operational geoscientific 258 processing schemes and has co-evolved with data availability over the past decade (Reichstein et al., 2019). 259 Specially, these models have been used as computationally efficient emulators of explicit mechanism models, to 260 explore uncertainties (Aleksankina et al., 2019) and sensitivities or replace complex gas-phase chemistry schemes 261 262 (Keller and Evans, 2019; Conibear et al., 2021). In addition, meta-models (Fang et al., 2005) such as neural networks and Gaussian process (Beddows et al., 2017) are also used to produce a quick to run model surrogate and 263 show reliable performance. Random Forest (RF) model algorithm is an ensemble learning method that generates 264 many decision trees and aggregates their results, which has been developed to solve the high variance errors typical 265 of a single decision tree (Breiman, 2001). Multivariate Adaptive Regression Splines (MARS) is a nonparametric 266 and nonlinear regression method, which can be regarded as an extension of the multivariate linear model (Friedman, 267 1991). RF and MARS are common machine learning methods which run efficiently on large data sets, and are 268

relatively robust to outliers and noise. Furthermore, they never require the specification of underlying data model and the complex parameter tuning, and they can still provide efficient alternatives and generally show a high accuracy in applications for predict air pollutant concentrations (Hu et al., 2017; Chen et al., 2018; Kamińska, 2019; Geng et al., 2020).

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Here, based on the database including 42,880 samples obtained from 1600 CFD simulations, the RF and MARS were both used to simulate the wind vector along X-axis ( $V_x$ ) and Y-axis ( $V_y$ ) at different heights within the street canyon respectively. The input predictor variables included H/W, L/W,  $H_l/H_r$ , the grid receptor relative height (z/H), the background wind vector at the height of H along X-axis ( $Vbg_x = V(H) \times \sin \alpha$ ) and Y-axis ( $Vbg_y =$  $V(H) \times \cos \alpha$ ). We finally combined the advantages of these two machine learning models and developed the MLSCF scheme to predict wind environment in street canyons and incorporated into the hybrid model, which is discussed in the section 3.1.

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In RF model, the number of predictors randomly sampled at each split node in the decision tree  $(m_{trv})$  and the 282 283 number of trees to grow (NumTrees) are two important hyperparameters that determine the performance of the model. Similarly, in MARS model, the two important hyperparameters are the total number of terms (*nprune*) and 284 the maximum number of interactions (*degree*). By comparing the mean squared error (MSE) for testing datasets 285 across models with candidate parameter combinations, we set  $m_{try}$  and NumTrees as 6 and 200 in RF, 286 287 respectively, and *nprune* and *degree* as 23 and 3 in MARS, respectively. Additionally, the 10-fold crossvalidation (CV) repeated ten times were considered to evaluate the prediction performance of our models. The total 288 dataset was randomly divided into 10 subsets, where 9 subsets was used to train model and another was applied for 289 290 validation. The fitted coefficients of MARS are shown in Table S2-S3 in the Supplement.

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In order to identify the sensitivity and response relationship between prediction variables and results in RF model, we used the MSE for out-of-bag (OOB) to evaluate the relative importance of each feature to  $V_x$  and  $V_y$ , by randomly replacing the value of a single prediction variable one by one (Liaw, 2002). Higher values of increase in MSE indicated that the predictor was more important. In addition, Partial Dependence Plots (PDPs) was applied to establish the response relationship between the change of a single predictive variable and the predicted results, considering the average influence of other variables (Greenwell, 2017).

#### 299 2.3 Configuration of CMAQ-RLINE URBAN

The near-ground NO<sub>2</sub> concentrations were simulated from August 1st to 31th in 2019 when the average of daily 300 high temperatures was higher than 30 °C and sunlight duration was longer than 13 hours, leading to strong 301 photochemical reactions. The simulation domain for the hybrid model covered the core urban areas within and 302 303 surrounding the fifth ring road, shown in Figure 3. The receptors included both grid receptors and monitor receptors. The grid receptors were set at a spatial resolution of 50 m×50 m, and the height above the ground was 1.5 m, which 304 was equivalent to the height of the human breathing. We used data from 10 observation stations (monitor receptors) 305 306 located in the normal urban environment and 5 near-road monitoring sites for validation (Beijing Ecological 307 Environment Monitoring Center, available at http://zx.bjmemc.com.cn/) (DSH, NSH, OM, XZM, and YDM) in the simulation domain (Figure 3), which were 10 meters and 3 meters above the ground respectively. The OM and 308 309 XZM sites were located in shallow street canyons, and details for the morphometric of near-road measurement sites 310 were shown in Table S4 in the Supplement.

311

312 In general, compared to the RLINE model, CMAQ-RLINE URBAN has the following improvements:

313 (a) The gridded meteorological parameters provided by WRF model were used.

(b) Gridded non-vehicle-related concentrations provided by CMAQ-ISAM model were used as backgroundconcentrations.

316 (c) A simple  $NO_x$  photochemical scheme was incorporated to simulate  $NO_2$  concentrations.

(d) Thermodynamic effects caused by the special underlying surface structures of the city were considered,
 including UHI effects, the influence of local buildings on turbulence intensity and vertical mixing of
 background concentrations.

320 (e) A newly developed MLSCF scheme was applied to predict wind environment in street canyons.

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In our simulation, the model configurations in the base scenario CMAQ-RLINE\_URBAN included all (a)-(e) schemes, and the other two control scenarios were set to investigate the sensitivity of urban schemes on predictions, where all input data was set to be the same. The scenario CMAQ-RLINE only including (a)-(c) schemes was set to analyze the impacts of urban thermodynamic schemes, and the scenario CMAQ-RLINE\_URBAN\_nc including (a)-(d) schemes was set to identify the impacts of the MLSCF scheme.

### 328 3 Results

#### 329 **3.1 Fitting results of machine learning**

In this study, the 10-fold cross-validation (CV) repeated ten times was considered to evaluate the prediction 330 performances of RF and MARS models. As shown in Figure 4 and Figure S5, both models performed acceptable 331 332 robustness in CV, indicating that neither RF nor MARS model overfitted the data. In general, the performances of both models in predicting  $V_v$  was better than that in  $V_x$  of which the absolute value was relatively small, especially 333 for MARS model. Since  $V_x$  was responsible for the formation of the vortex within street canyons and affected by 334 multiple factors, it was more difficult to be simulated. The averages of mean absolute error (MAE), root mean 335 square error (RMSE), and correlation coefficient (R) in the CV of the RF model for  $V_x$  and  $V_y$  were 0.04 m/s and 336 0.05 m/s, 0.02 m/s and 0.03 m/s, and 0.99, respectively. Although the average of the relative error (RE) were a little 337 high (42.5% and 43%), particularly when the predicted wind speed was low, the median RE were relatively low 338 with 9.8% and 2.7%, respectively, indicating an acceptable performance. Compared with the advanced non-linear 339 340 RF algorithm, the MARS model performed not very well, especially when the absolute value of  $V_r$  was greater than 1 m/s and  $V_{y}$  was less than 3 m/s. However, when the predicted wind speed by machine learning methods was 341 342 compared with observations from wind tunnel experiments, we found that the performance of the MARS model 343 was obviously better than that of RF model in one of validation cases (see Figure 5). The decision tree model like RF failed to respond to the parts beyond the range of prediction variables ( $Vbg_v = 17 \text{ m/s} >> 5 \text{ m/s}$ ), while the more 344 reasonable predictions can be obtained by the MARS model which used piecewise linear function essentially. 345 Therefore, the MLSCF scheme was established based on a method to combine the advantages of each model. The 346 347 RF model was used when the input value was within the range of predictors shown in Table 1, otherwise the 348 predictions from the MARS model were used.

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350 In addition, the importance of each predictor variable in the RF model was investigated to explain their impacts on 351 predictions. As shown in Figure 6, the background wind speeds on x and y axis played vital roles in predictions of  $V_x$  and  $V_y$ , respectively, followed by the relative height (z/H). Among the geometric parameters of the street 352 canyon, the impact of L/W was least. Since  $V_x$  was the main driving force for the formation of vortices in street 353 354 canyons, it was more affected by the geometry of street canyons especially  $H_l/H_r$ , comparing to  $V_v$ . This feature importance ranking was basically consistent with the conclusion in a previous study (Fu et al., 2017). Figure S6 in 355 the Supplement shows the PDPs of each predictor variable in RF model for  $V_x$  and  $V_y$ . As z/H grew,  $V_x$  and  $V_y$ 356 showed linear and logarithmic increase patterns, respectively. And the resistant effect of windward buildings on 357

wind speed enhanced with the increasing of  $H_l/H_r$ , resulting in a significant decrease in  $V_x$  particularly when  $H_l/H_r$  was lower than 1.25. The relationship between predictors and results in the model was consistent with the actual mechanism, indicating our model could provide an accurate description of the wind field in the street canyon.

#### 362 **3.2 Impacts of MLSCF on simulations in street canyons**

363 We compared the differences between monthly mean wind profile in different street canyons including OM (shallow canyon: H/W = 0.22), XZM (shallow canyon: H/W = 0.35), SZJ (standard canyon: H/W = 1) and 364 JTDL (deep canyon: H/W = 1.93), calculated by the default logarithmic function based on MOST in the original 365 RLINE model (Foken, 2006), and the MLSCF scheme developed in this study. As shown in Figure 7(a)-(d), the 366 wind profile estimated by MOST showed a logarithmic change at the height above displacement height  $(d_h)$  with 367 a decrease to 0 at  $d_h$ , and remained constant below  $d_h$  (the  $d_h$  is calculated by multiplying surface roughness length 368 369  $(z_0)$  times a factor which is recommended to be set as 5). Compared with the MOST, the simulated wind speeds 370 near the ground and at the top of canyons were generally lower based on the MLSCF scheme in shallow and 371 standard street canyons. In the deep street canyon, the significant reduction in ventilation volume led to the mean 372 wind speed simulated by the MLSCF scheme much lower than that of MOST at all heights. Although the aspect 373 ratios of the street canyon located in OM and XZM were similar, their orientations were quite different, resulting in significant differences under prevailing external winds in different directions. Since the prevailing northerly and 374 375 southerly wind was observed in Beijing during the study period, the resistance effect of the buildings on both sides 376 of the east-west street canyon located in QM was more obvious.

377

We also investigated the impacts of the MLSCF on hourly wind direction at the bottom (z = 3m) of different street 378 canyons by comparing the roof-level predictions from WRF model (see Figure 7(e)-(f)). In the shallow street 379 canyon like OM, the simulated wind direction at the bottom was consistent with the background on the whole, with 380 the R reaching 0.8. When the background wind direction was less than 180°, the averaged wind direction at the 381 bottom simulated by MLSCF was  $91.8^{\circ}$ , which was basically consistent with the angle between the street and the 382 south direction (84.5°). When the background wind direction was greater than 180°, the average wind direction 383 384 predicted by MLSCF ( $257.4^{\circ}$ ) was similar to that in the opposite direction of the street ( $264.5^{\circ}$ ), which was in line 385 with the theory proposed by Soulhac et al. (2008) that the average wind direction in street canyons was assumed to be consistent with the (opposite) orientation of the street. While in the deep street canyon of SZJ, when the external 386 wind perpendicularly blew to the street, the wind direction at the bottom was completely opposite to that at the top 387 388 due to the formation of vortex, with the R reaching -0.97. In conclusion, compared with the traditional MOST 389 method, the newly developed MLSCF scheme could well simulate the influence of the external wind environment 390 and geometry on the wind field inside the street canyon.

391

As shown in Figure 8, the impacts of the MLSCF scheme on simulated NO<sub>2</sub> concentration were identified by the 392 393 differences between CMAQ-RLINE\_URBAN and CMAQ-RLINE\_URBAN\_nc scenario during a clean day (August 24th). When the atmosphere was stable at night, in street canyons with a large aspect ratio, the wind 394 395 direction at the bottom changed to the opposite to that at the top, combined with the decreased wind speed affected 396 by the MLSCF scheme, the NO<sub>2</sub> concentrations at upwind grid receptors increased by up to 80  $\mu$ g/m<sup>3</sup>. Meanwhile, 397 the changes in wind direction would also decrease the concentrations at downwind grid receptors by up to  $20 \,\mu\text{g/m}^3$ . For example, in the SZJ standard canyon, the background wind direction over the street was  $79^{\circ}$  (easterly), and 398 399 the wind direction at the bottom changed to 291° affected by the MLSCF scheme (westerly). Therefore, the upwind 400  $NO_2$  concentrations increased, and the location of peak  $NO_2$  concentration shifted to the windward. Since the 401 changes in NO<sub>2</sub> concentrations were also influenced by the local on-road emissions, the increase was only up to 402  $2.1 \,\mu g/m^3$  in SJZ street, where the traffic flow and vehicle emissions were small at night. However, a little influence 403 was observed during the day in the convective boundary layer. During this period, although the wind direction at 404 the bottom was not changed obviously due to the parallel background wind in SZJ street, the increased surface 405 wind speed was beneficial for the dispersion, resulting in the decreased concentration in grid receptors within both 406 sides of the street canyon. In summary, the MLSCF scheme enabled the characterization of the concentration 407 distribution in street canyons.

408

#### 409 **3.3 Performance of near-road simulations from different models**

The performances in predicting NO<sub>2</sub> concentrations at all monitor receptors from different models were first compared, including CMAQ-RLINE\_URBAN, CMAQ-RLINE and CMAQ model. The mean bias (MB), RMSE, normalized mean bias (NMB), normalized mean gross error (NMGE), the fraction of predictions within a factor of two (FAC2), Index of agreement (IOA), and *R* between simulations and observations were all selected as statistical indicators for the evaluation (Table 2). In general, the performance of CMAQ-RLINE\_URBAN was the best at all urban sites. Compared to the CMAQ model, the averaged MB and NMB at urban sites in the hybrid model decreased from 8  $\mu$ g/m<sup>3</sup> to 1.3  $\mu$ g/m<sup>3</sup> and 27% to 4%, respectively.

417

418 Diurnal variations of observed and predicted hourly averaged NO<sub>2</sub> concentrations at near-road sites from different 419 models were mainly compared and shown in Figure 9. The comparison of hourly and daily averaged concentrations

is shown in Figure 10. Overall, the CMAO-RLINE URBAN performed best with the smallest deviations. By 420 comparing the performances of the CMAO and CMAO-RLINE scenario, we found the direct coupling between the 421 422 CMAQ and RLINE models could reproduce the high  $NO_2$  concentrations at near-road sites in daytime, and significantly improve the underestimation of near-source concentrations due to grid dilution on emissions in 423 CMAO model. The averaged MB and NMB at all sites changed from -10 µg/m<sup>3</sup> to 25.6 µg/m<sup>3</sup>, and from -20% to 424 51%, respectively. However, a significant overestimation was found in the CMAQ-RLINE at night (0:00-6:00) and 425 426 around sunset in the afternoon (16:00-23:00), of which the peak could exceed the observed concentrations by more 427 than 1 times. This overestimation was reduced in the CMAQ-RLINE URBAN, where the urban thermodynamic 428 schemes were implemented. The averaged MB and NMB decreased to 6.3  $\mu$ g/m<sup>3</sup> and 12%, respectively, due to the following reasons: (1) The increased surface roughness length slightly enhanced local turbulence intensity near 429 430 roads; (2) The UHI scheme enhanced the intensity of atmospheric turbulence in urban areas before and after sunset 431 in the afternoon; (3) The effect of turbulence intensity on the local vertical mixing of background concentrations was considered, significantly reducing the mixing ratio of concentrations over UCL and near the ground at nights 432 in the stable boundary layer (Figure S7 in the Supplement), which was probably the main driving force of decreased 433 predictions in the hybrid model (Benavides et al., 2019). However, the CMAO-RLINE URBAN slightly 434 overestimated the nighttime NO<sub>2</sub> concentration of all observation stations except the DSH, which was probably 435 436 caused by overestimations of background concentrations from CMAQ-ISAM and vehicle emissions.

437

The accuracy of model performances at each traffic site showed a little difference affected by the variations in the 438 traffic flow and emissions of nearby roads, as well as the geometry of surrounding buildings and street canyons. At 439 DSH and NSH sites, which were adjacent to ring roads as the main urban freight corridors with a high traffic flow 440 441 including a large proportion of trucks, the high  $NO_x$  emissions led to the highest roadside  $NO_2$  observations among all sites. The CMAQ model would significantly underestimate the high NO<sub>2</sub> concentration at sites nearby ring roads, 442 with MB and NMB lower than -15  $\mu$ g/m<sup>3</sup> and -28% (Table S5 in the Supplement), respectively, which was 443 improved using CMAQ-RLINE\_URBAN. However, the hybrid model performed a minor overestimation at the 444 NSH site, since the monitor was actually positioned in the road centerline but assumed to be located downwind in 445 the model, resulting in a relatively large systematically error (Snyder et al., 2013). In total, CMAQ-446 RLINE URBAN performed best among all models, especially improving the estimation of NO<sub>2</sub> concentrations 447 448 near roads by the original regional model.

Additionally, Figure S8 in the Supplement shows the comparison between simulated and observed roadside hourly and daily maximum 8-hour average  $O_3$  concentrations by different models, and their diurnal variations are shown in Figure S9. Generally, the hybrid model significantly improved the overestimation of daytime  $O_3$  concentrations by the CMAQ model when considering the titration effect of high NO concentration near roads on  $O_3$ . In the hybrid model, the peak time was delayed to about 15:00, which was closer to the observation, but still 1-2 hours earlier than the actual time, which may be related to the uncertainty in NO<sub>2</sub> photolysis rate.

456

## 457 **3.4 Spatial distribution characteristics of simulated concentrations**

458 We investigated the differences between the spatial distribution of the monthly averaged  $NO_2$  concentration simulated by the CMAO and CMAO-RLINE URBAN models, as shown in Figure 11. Since the urban 459 thermodynamic schemes were considered in the hybrid model, the overestimation of most urban environmental 460 461 grid receptors by CMAO model was relieved. Within the fourth ring road and its surrounding areas, the mean concentration of NO<sub>2</sub> from CMAQ-RLINE URBAN was 30.1 µg/m<sup>3</sup>, lower than that from the CMAO model (39.5 462  $\mu g/m^3$ ). The overall spatial distribution characteristics of NO<sub>2</sub> predictions from both models showed that the 463 concentrations in south regions were high due to the pollution transport from Hebei province (An et al., 2019). 464 However, near-road hotspots for the NO<sub>2</sub> pollution were identified in the hybrid model where the spatial resolution 465 of results increased to 50 m $\times$ 50 m. The NO<sub>2</sub> concentrations nearby ring roads with high traffic flow and emissions 466 were up to 120  $\mu$ g/m<sup>3</sup>, much higher than the maximum prediction from CMAO model (52.4  $\mu$ g/m<sup>3</sup>). In addition, 467 the simulated near-road concentrations from the hybrid model during traffic peak hours (18:00-19:00) were 468 significantly higher than those at noon (12:00-13:00), while there were few changes in results from CMAQ model 469 (Figure S10 in the Supplement). 470

471

The NO<sub>2</sub> concentrations estimated by CMAQ-RLINE\_URBAN at all grid receptors grids followed a two-mode Gaussian distribution (Figure S11 in the Supplement), which was similar to Zhang's results (Zhang et al., 2021b). The NO<sub>2</sub> concentrations as a result of vehicle emissions were further calculated by the differences between the total and background concentrations. In general, the vehicle-induced NO<sub>2</sub> concentrations in urban areas was 11.8  $\mu$ g/m<sup>3</sup>, accounting for 39% of the total concentrations, which was similar to the predicted contribution from the CMAQ-ISAM model (42.5%).

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Figure 12 shows the changes in  $NO_2$  concentrations simulated by the hybrid model with distance from the grid receptors to its nearest road centerline. The concentrations at grid receptors within 200 m from road were

significantly affected by vehicle emissions. Within 50 m around the road, as the distance from grid receptors to the 481 road centerline gradually increased, the NO<sub>2</sub> concentrations decreased exponentially. The total NO<sub>2</sub> concentrations 482 decreased from 53.1  $\mu$ g/m<sup>3</sup> to 30  $\mu$ g/m<sup>3</sup>, and the vehicle-induced concentrations also dropped from 34.7  $\mu$ g/m<sup>3</sup> to 483 12.6  $\mu$ g/m<sup>3</sup>. The concentrations near roads with different types were highly dependent on the emission intensity. 484 The NO<sub>2</sub> concentration was highest in the center of the urban freeway, which was 76  $\mu$ g/m<sup>3</sup> and about 1.9 times 485 higher than that on local roads. The relative contribution of vehicle emissions to NO<sub>2</sub> concentration reached up to 486 487 75.3% on urban freeways, as well as 71.9% and 65.5% on artery roads and freeways, but only 51.1% on local roads. 488 It was worth noting that although the  $NO_2$  concentrations at far grid receptors to the road on highways were slightly 489 higher than those on other road types, the contribution of vehicle emissions was the least. It was since the  $NO_x$ emission intensity of freeways was as high as that on artery roads, but the density and height of buildings around 490 491 freeways were usually low, resulting in a high vertical flux of background concentrations from the top of UCL to 492 the ground. In conclusion, the results from the hybrid model accurately reflected not only the impacts of local onroad emissions, but also the pollution characteristics affected by non-vehicle sources at the regional scale. 493

494

## 495 4 Conclusion and Discussions

In this study, we developed a hybrid model CMAQ-RLINE\_URBAN to quantitatively analyse the effects of vehicle emissions on urban roadside NO<sub>2</sub> concentrations at a high spatial resolution of  $50 \text{ m} \times 50 \text{ m}$ . The main conclusions of this study are as follows:

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The developed MLSCF scheme revealed that affected by the geometry of buildings on both sides of the road, the 500 501 wind filed in the street canyon sometimes was quite different from that in the environmental background. In deep 502 street canyons, the wind speed at the bottom decreased obviously due to the resistant effect of buildings, and the 503 directions of horizontal flow at bottom and top of the canyon were completely opposite due to the formation of vortex. The application of MLSCF scheme in the hybrid model led to increase NO<sub>2</sub> concentrations at upwind grid 504 505 receptors within deep street canyons due to changes in the wind environment. However, the influence of the turbulence induced by street canyon effects on the mixing of air pollution was not considered on which we will 506 make effort in the future. 507

508

509 The comparison between observations and predictions showed that the hybrid model significantly improved the 510 underestimation of near-source concentrations due to grid dilution on emissions in CMAQ model. The 511 implementation of the urban thermodynamic schemes in the hybrid model also relieved the overestimation in nighttime NO<sub>2</sub> concentrations from the CMAQ directly coupled with RLINE model. The predictions from CMAQ-RLINE\_URBAN model could accurately reflect not only the impact of road local emissions, but also the pollution characteristics of non-vehicle sources at regional level. It revealed that in summer, the average contribution of vehicle emission to NO<sub>2</sub> concentrations in urban areas of Beijing was 11.8  $\mu$ g/m<sup>3</sup>, and the relative contribution accounted for approximately 39%. Moreover, the vehicle-induced NO<sub>2</sub> pollution increased significantly with the decreased distance to the road centerline, especially reaching 76  $\mu$ g/m<sup>3</sup> (75%) on urban freeways.

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519 On the basis of this study, the following perspectives are proposed for future research: (1) At present, considering 520 the running cost, the grid resolution of area in Beijing 5th ring road and its surroundings can reach 50 m $\times$ 50 m. We will make efforts to develop a parallel computing method to reduce the computing time, in order to improve the 521 522 grid resolution of a relatively large-scale simulation. (2) In our study, a simplified two-reaction scheme was 523 incorporated into the model to characterize the photochemical process of NO<sub>x</sub>, since it performed similar predictions and less computational time compared with those of the complicated CB05 gas phase chemical 524 mechanism (Kim et al., 2018). However, another study pointed that the impact of nonlinear  $O_3$ -NO<sub>x</sub>-VOC 525 chemistry on NO<sub>2</sub> concentrations in the deep canyon was nonnegligible (Zhong et al., 2017). The influence of 526 different chemistry schemes on near-road simulation will be investigated in the future. (3) The long-term site-527 observation of wind environment and pollutant concentrations in various street canyons were suggested to be 528 529 compared with modelling results, especially in deep street canyons with large aspect ratio. The navigation 530 monitoring technology would be applied in the model verification, which can carry out large-scale observation of concentration along streets. (4) Here, we considered the dynamic impact of idealized building structure on wind 531 532 environment in street canyons. However, there are many other influencing factors, such as building layout and 533 arrangement, roof shape, green vegetation, and thermodynamic effect, which are suggested to be considered in 534 future studies. (5) In this study, we mainly focused on the  $NO_2$  concentrations. In fact, the concentration of particulate matter, especially UFP, will also have an obvious peak near the road centerline. In the future, the process 535 536 of physical and chemical changes of particulate matter near the vehicle exhaust outlet should be further investigated.

537

## 538 Data availability

539 Data are available upon request from the corresponding author Huan Liu (<u>liu\_env@tsinghua.edu.cn</u>).

## 541 Code availability

- 542 The RF and MARS model for MLSCF are both available on Github (https://github.com/claus0224/MLSCF-RF-
- 543 MARS), and other codes are available from the corresponding author on reasonable request.

544

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551

## 552 Author contributions

553 Z. Lv and Z. Luo contributed equally. Z. Lv and Z. Luo designed the research and wrote the manuscript. H.L., Y.Z. 554 and K.H. provided guidance on the research and revised the paper. Z. Lv, Z. Luo, and F.D. provided multiple 555 analytical perspective on this research. X.W., J.Z., and L.X. helped collect and clean the data. T.H. helped on 556 language modification.

557

## 558 Competing interests

- 559 The authors declare that they have no conflict of interest.
- 560

## 561 Additional information

- 562 The supplement is available for this paper at online resources.
- 563 Correspondence and requests for materials should be addressed to H.L.
- 564

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780 Figure 1: The framework of multiscale hybrid model CMAQ-RLINE\_URBAN.



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783 Figure 2: Computational domain (a) and grid arrangement (b) in all CFD test case.



Figure 3: Study domain (© OpenStreetMap contributors 2020. Distributed under the Open Data Commons
Open Database License (ODbL) v1.0) and location of monitoring sites (© Microsoft). A. DSH; B. NSH; C.
QM; D. XZM; E. YDM.



792 Figure 4: Cross validations of machine learning models for Vx (a, c) and Vy (b, d): (a)-(b) RF model; (c)-(d)

MARS model. 





Figure 5: Performances of machine learning on velocity profile in wind tunnel experiments. The street
canyon was perpendicular (a) or parallel (b) to the wind direction at the roof level in different experiments.
The detailed description of each experiment was introduced in Section 2.2.3.





801 Figure 6: Variable importance ranking in the RF model for (a)  $V_x$  and (b)  $V_y$ .



Figure 7: Influence of MLSCF on wind filed in the street canyon. Monthly averaged vertical profile of wind speed from MOST and MLSCF method in different street canyons: (a) QM (H/W=0.22); (b) XZM (H/W=0.35); (c) SZJ (H/W=1); (b) JTDL (H/W=1.93). The gray shade represents the standard deviation in results of all hours. Hourly wind direction from WRF model (at roof level) and MLSCF method (at ground level) in different street canyons: (e) QM (H/W=0.22); (f) SZJ (H/W=1). As the gray and green shade shown, the background wind over the street canyon provided by WRF model was divided into four main directions: east, west, south and north.



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813 Figure 8: Differences in NO<sub>2</sub> concentrations at the height of 1.5 m impacted by MLSCF scheme (a, c) over

- 814 the study domain (CMAQ-RLINE\_URBAN CMAQ-RLINE\_URBAN\_nc) (© Microsoft) and (b, d) near
- 815 SZJ in 2019-08-24 at 0:00-1:00 (a, b) and 10:00-11:00 (c, d).



Figure 9: Diurnal variations of observed and predicted hourly averaged NO<sub>2</sub> concentrations from different
models at near-road monitoring sites: (a) DSH; (b) NSH; (c) QM; (d) XZM; (e) YDM.



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Figure 10: Observed and predicted hourly (a-c) or daily averaged (d-f) NO2 concentrations from different models at near-road sites: (a, d) CMAQ model; (b, e) CMAQ-RLINE model; (c, f) CMAQ-RLINE\_URBAN model.





Figure 11: Spatial distribution of monthly averaged NO<sub>2</sub> concentrations from (a) CMAQ model and (b)

830 CMAQ-RLINE\_URBAN model.



833 Figure 12: Monthly averaged NO<sub>2</sub> concentrations attributed to all emission sources or vehicles with distance

834 from the receptor to its nearest road centerline. (a) NO<sub>2</sub> attributed to all emission sources near all roads; (b)

835 NO<sub>2</sub> attributed to all emission sources near different road types; (c) Relative contribution of vehicles to NO<sub>2</sub>

836 near different road types. The shade area in (a) represents the standard deviation in results of all receptors.

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Controlling factor	Value						
$H_l/H_r$ (unitless)	0.50	0.75	1.00	1.33	2.00		
<i>H</i> / <i>W</i> (unitless)	0.25	0.50	1.00	2.00	-		
<i>L/H</i> (unitless)	3	5	10	20	-		
<b>V</b> ( <b>H</b> ) (m/s)	1	2	3	4	5		
<b>α</b> (°)	0	30	60	90	-		

## 838 Table 1: Values of controlling factors used in the simulations.

Sites	Scenario	MB	RMSE	NMB	NMGE	FAC2	IOA	R
All	CMAQ	3.1	25.6	9	53	0.65	0.45	0.52
	CMAQ-RLINE	18.5	46.6	53	77	0.67	0.19	0.55
	CMAQ-RLINE_URBAN	4.6	25.8	13	49	0.75	0.49	0.57
Urban	CMAQ	8.0	24.3	27	58	0.68	0.40	0.59
	CMAQ-RLINE	12.3	35.8	43	76	0.64	0.20	0.50
	CMAQ-RLINE_URBAN	1.3	23.1	4	51	0.71	0.47	0.49

## 841 Table 2: Model performances under different scenarios

\*MB: Mean bias; RSME: Root mean squared error; NMB: Normalized mean bias; NMGE: Normalized mean gross
error; FAC2: Fraction of predictions within a factor of two; IOA: Index of agreement; R: correlation coefficient.