Authors' Response:

Manuscript Title: Development and application of a multi-scale modelling framework for urban high-resolution NO₂ pollution mapping

Discussion Link: https://acp.copernicus.org/preprints/acp-2022-371/#discussion

Revision notes:

Reviewers' comments are in blue italic type.

Authors' responses are in indent and in black normal font.

Revisions in the manuscript are in indent red normal font.

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Response to Reviewers #1's Comments *Summary*

The study of Lv et al. presents a multi-scale modelling framework for the simulation of urban scale NO2 and potentially other primary pollutants at high spatial resolution with a focus on traffic-related air pollution. The method combines several different types of models and approaches, a regional chemistry-transport-model (CMAQ), a dispersion model (RLINE), an urban heat island scheme, and machine-learning based simulation of street-canyon flows trained with a CFD model. The overall framework is referred to as CMAQ-RLINE URBAN.

The overall approach is interesting, but the publication has major deficiencies, is difficult to follow, and leaves many questions unanswered. In my view it cannot be published in the present form but will need substantial improvements.

Response:

Thank you very much for spending time to give us many constructive comments, and they have great importance in improving our manuscript. We have revised our manuscript and we believe that all the concerns are now fully addressed in this revision. In general, as you suggested, a more detailed review on multi-scale air quality models was added in the Introduction, and more descriptions on various parameterization schemes were provided in the Method and Supplement Materials. In addition, more explanations and expectations in the future were added in the Results and Discussions, respectively.

Major comments

Question 1

The individual model components as well as their interplay are very poorly described. Examples:

The RLINE model is never explained. It remains unclear whether this is Gaussian dispersion or any other type of model. Providing only references without any further details is not sufficient given the fact that this model plays a central role in this study.

How are emissions released into the model? Is traffic a line source? How are the emissions transported forward and dispersed by the (RLINE) model?

Response:

Thanks for your advice. We apologized that the introduction of RLINE was missing in our

original manuscript so that the details of our model is not sufficient. In general, the RLINE is a Gaussian dispersion model specially for the line source simulation. In this revision, we have added the description of RLINE model including its mechanism and application in **Section 2.1**.

The traffic emission is treated as a line source in RLINE. The concentration from the traffic emission is found by approximating the line as a series of point sources and integrating the contributions of point sources using an efficient numerical integration scheme.

Revisions in Manuscript:

(1) Materials and Methods, Line 119-128.

RLINE is a Gaussian line source dispersion model developed by Snyder et al. (2013) to predict pollutant concentrations in near-road environments. In the RLINE model, the mobile source is considered as a finite line source, from which the concentration is found by approximating the line as a series of point sources and integrating the contributions of point sources using an efficient numerical integration scheme. The number of points needed for convergence to the proper solution is a function of distance from the source line to the receptor, and each point source is simulated using a Gaussian plume formulation. The RLINE model performs generally comparable results when evaluated with other line source models for on-road traffic emissions dispersion (Snyder et al., 2013; Heist et al., 2013; Chang et al., 2015), and has been successfully used in many studies to evaluate the impacts from traffic emissions on air quality (Zhai et al., 2016; Valencia et al., 2018; Benavides et al., 2019; Filigrana et al., 2020; Zhang et al., 2021a).

Question 2

An UHI scheme is implemented, which "increases atmospheric turbulence intensity around sunset in the afternoon", but it is never explained how this increased turbulence affects the simulation or what is meant by "afternoon". Is the UHI scheme only triggered around sunset? Does it affect the turbulent intensity in RLINE? If so, how exactly? Which localized meteorological parameters are recalculated and how? Is the UHI scheme of Cimorelli et al. (2005) different from the algorithm proposed by Benavides et al., or is the Benavides algorithm based on Cimorelli et al.? The text remains extremely vague despite the fact that, again, this UHI scheme is an essential component of the final model system. Please note that WRF can be run with an urban canopy module (e.g. Barlage et al., 2016; doi:10.1002/2015JD024450), which would alleviate the necessity of implementing an UHI scheme in such a complicated (and unclear) way as done here. Why was this scheme not used to drive CMAQ and to compute the winds and stability above roof level?

Response:

Thanks for your questions. We apologize for misleading the reviewer about the UHI scheme, and the detailed description for UHI scheme were added in this revision. In this response, we will give a response to each question as follows:

- The impacts of UHI effect in the hybrid model is considered not only in the afternoon but also over the whole day. However, based on previous studies, the UHI effect is more significant in the afternoon around sunset.
- The UHI scheme will affect the turbulent intensity in RLINE. First, the upward surface heat flux and the urban boundary layer height due to convective effects was estimated. And then the mixing height Z_{mix}, convective velocity scale w^{*}, surface friction velocity u^{*}, and Monin-Obhukov length L_{MO} were recalculated. The UHI scheme was never considered in Benavides's study (Benavides et al., 2019), and in this study, it was built based on the algorithm used in the AERMOD model (Cimorelli et al., 2005). We have also added a brief introduction of UHI scheme in the Section S1. Urban heat island scheme and details in Supplement Materials.
- The WRF model can actually be coupled with urban canopy models (UCMs) to quantify the changes in meteorological conditions caused by special underlying surface structures in cities, where the UHI effect is included. However, the WRF model was applied for mesoscale meteorological simulation (not smaller than an urban scale), so it is too large to consider the impact on each road. The hybrid model in this study mainly focuses on local meteorology at the street level. In addition, if WRF coupled with UCMs and the UHI scheme are both used in the hybrid model, it will cause a double-counting problem of UHI effects.

Revisions in Manuscript:

(1) Materials and Methods. Line 140-145.

The atmospheric turbulence intensity in urban areas around sunset in the afternoon was obviously enhanced considering the influence of the urban heat island effect based on methods in the AERMOD model (Cimorelli et al., 2005) (UHI scheme). The UHI scheme would affect the turbulent intensity based on the evaluation for the upward surface heat flux and the urban boundary layer height due to convective effects, and then the mixing height, convective velocity scale, surface friction velocity, and Monin-Obhukov length were all recalculated (details in the Supplement Section S1).

(2) Supplement Materials. Section S1 Urban heat island scheme.

The Urban Heat Island effect refers to a phenomenon that the temperature of urban atmosphere and surface is higher than that of nearby rural areas, of which intensity can be quantified by using the temperature difference. UHI is caused by the thermodynamic effect of the special underlying surface structure induced by urbanization and the influence of human activities. In past decades, the intensity of UHI in Beijing has been increasing at a rate of $1.35 \,^{\circ}$ C every decade, and has gradually expanded from within the 2nd Ring Road to the 6th Ring Road and its surrounding areas (Ge et al., 2016). When the UHI intensity is high, the circulation between urban and suburban areas will enhance the boundary layer height and turbulence intensity in urban areas, and reduce the concentration of primary pollutants such as NO_x which are easily affected by the local climate. After adding the UHI scheme to the model, the overestimation of the simulation can be reduced, and the simulation is more consistent with the observed concentration (Sarrat et al., 2006).

Here, based on the algorithm used in AERMOD (Cimorelli et al., 2005), we estimated the influence of UHI on turbulence in urban areas, especially in the afternoon (16:00-23:00), to reduce the over-predicted pollutant concentrations caused by the overestimation of atmospheric stability in this period. During this period, due to the large amount of anthropogenic heat generated by transportation, cooking and other human activities, as well as the gradual release of solar radiation stored by buildings in daytime, the UHI intensity in Beijing increase to the peak (Wang et al., 2017). In the calculation, we still regarded each road as a basic unit for the calculation, and first estimated the sensible heat flux $H_{u,UHI}$ (W/m²) caused by UHI and the height of the mixing layer $Z_{mix,c}$ (m) formed by thermal turbulence. And then the mixing height Z_{mix} , convective velocity scale w^* , surface

friction velocity u^* , and Monin-Obhukov length L_{MO} were recalculated, as follows,

$$\begin{pmatrix} H_{u,UHI} = \alpha \rho c_p \Delta T_{u-r} u^* \\ Z_{mix,c} = Z_{mix,ref} (P/P_{ref})^{0.25} \end{cases}$$

where, α is the empirical coefficient, with a value of 0.03. ρ is air density (kg/m³) and calculated by air pressure and temperature. c_p is the specific heat capacity of air at constant pressure, with a value of 1004 J/kg·K. ΔT_{u-r} is the temperature difference between urban and suburban areas, which is set with the value of 3°C according to the observation of several meteorological ground observation stations and satellite remote sensing data (Wang et al., 2017). $Z_{mix,ref}$ and P_{ref} are the reference boundary layer height and urban population, with values of 400 m and 2 million, respectively (Cimorelli et al., 2005). P is the total population of urban areas in the research region, with the value of 9.2 million in our study domain for 2020 based on the WorldPop dataset (Bondarenko et al., 2020).

Question 3

CFD simulations were performed to train a machine-learning based street-canyon flow model (MLSCF) in order to predict airflow in street canyons efficiently. This part of the publication is quite clear, but how the results of the MLSCF are finally applied to compute the dispersion of NO2 is never explained. It should also be noted that the MLSCF model only predicts wind speeds at different locations in the street canyon (in along-canyon and perpendicular direction), but not turbulence, which also varies depending on wind speeds and angle between wind and canyon. The publication mentions the importance of the buildup of a vortex in certain situations, but it remains unclear how the mixing of air pollution induced by this vortex affects the mixing in RLINE. If RLINE is a simple Gaussian dispersion model, how would it be able to represent such a vortex?

Response:

Thanks for questions. The MLSCF is developed to estimate the wind velocity and direction at different height in the street canyon. In other words, outputs from the MLSCF model are wind vectors. Therefore, the impact of turbulence induced by street canyon effect on wind environment is considered. As shown in the Figure 8, the impacts of the MLSCF scheme on simulated NO₂ concentration were identified by the differences between modeling scenarios with and without MLSCF. For example, in the SZJ standard canyon, the application of MLSCF led to the wind direction at the bottom in street canyon opposite to that at the roof, increasing the upwind concentrations (Figure 8b and Section 3.2 in the manuscript).

However, as you mentioned that since the RLINE is a Gaussian model, we cannot directly calculate the impact of vortex in specific situations on the mixing of concentrations in street canyons. We will make effort on developing another empirical method to estimate effects of the vortex on the mixing of concentrations in the future research, and this is discussed in the **Conclusions** now.

Revisions in Manuscript:

(1) Conclusion and Discussions, Line 505-507.

However, the influence of the turbulence induced by street canyon effects on the mixing of air pollution was not considered on which we will make effort in the future.

Question 4

NOx is released by emission sources mainly in the form of NO and then converted to NO2 by reaction of O3. The paper mentions that a "two-reaction scheme" was incorporated into RLINE, but it is not explained which photochemical reactions exactly were considered, how this reaction scheme was implemented in RLINE, or in what form NOx was emitted. Figure 1 suggests that concentrations from vehicles and from background are combined within the "NOx photochemical scheme". Is the scheme applied separately to the two components? How exactly are they combined?

Response:

Thank you for questions. We apologized those unclear descriptions on the NOx photochemical reactions in the original manuscript. In general, we used the two-reaction method applied in other studies, such as the SIRANE model (Soulhac et al., 2017). The NO_x photochemical scheme includes two main chemical reactions, namely the photolysis of NO₂ and the oxidation of NO as follows:

$$\begin{cases} NO_2 + hv \rightarrow NO + O_3 \\ NO + O_3 \rightarrow NO_2 \end{cases}$$

During simulation, the NOx (NO+NO₂) emitted from vehicles is first regarded as an inert gas and only the primary concentration after diffusion is simulated. Then, assuming a

photo-stationary equilibrium condition, the concentrations of NO, NO_2 and O_3 are calculated as follows:

$$\begin{cases} [NO_2] = (b - \sqrt{b^2 - 4c})/2 \\ [NO] = [NO]_b + [NO_2]_b + [NO_x]_d - [NO_2] \\ [O_3] = [O_3]_b + [NO_2]_b + \zeta [NO_x]_d - [NO_2] \\ b = k1/k2 + [O_3]_b + [NO]_b + 2[NO_2]_b + (1 + \zeta)[NO_x]_d \\ c = ([O_3]_b + [NO_2]_b + \zeta [NO_x]_d)([NO]_b + [NO_2]_b + [NO_x]_d) \end{cases}$$

where, $[NO_x]_d$ is the primary concentration of NO_x directly simulated by RLINE model when taken as an inert gas. $[NO]_b$, $[NO_2]$, and $[O_3]_b$ are the background concentrations of NO, NO₂ and O₃ from non-vehicle sources, respectively, which are provided by CMAQ-ISAM model. ζ is the ratio of NO₂ to NO_x in vehicle emissions, with a value of 0.2 (Benavides et al., 2019; Valencia et al., 2018).

We have added a brief introduction of the "two-reaction scheme" in Materials and Methods and details in Supplement Materials (Section S3. NOx photochemical parameter scheme).

Revisions in Manuscript:

(1) Materials and Methods. Line 167-170.

In this study, a simplified two-reaction scheme, including the photolysis of NO_2 and the oxidation of NO, was incorporated into the model to characterize the photochemical process of NO_x (details in SI. Section S2), which has been successfully applied to the SIRANE dispersion model (Soulhac et al., 2017).

(2) Supplement Section S3. NOx photochemical parameter scheme.

The NO_x photochemical parameter scheme applied in this study includes two reactions:

$$\begin{cases} NO_2 + hv \rightarrow NO + O_3 \\ NO + O_3 \rightarrow NO_2 \end{cases}$$

Kim et al. compared two-reaction scheme with CB05 gas phase chemical mechanism by incorporated them into SinG model to estimate roadside NO₂ concentration, and found a similar results, while the computing time cost of two-reaction scheme was significantly less than that of the CB05 mechanism (Kim et al., 2018). Therefore, the simplified two-reaction scheme was incorporated into the model in this study to characterize the NO_x photochemical process. During simulation, the NOx (NO+NO₂) emitted from vehicles is first regarded as an inert gas and only the primary concentration after diffusion is simulated.

Then, assuming a photo-stationary equilibrium condition, the concentrations of NO, NO_2 and O_3 are calculated using the two-reaction scheme, as follows:

$$\begin{cases} [NO_2] = (b - \sqrt{b^2 - 4c})/2 \\ [NO] = [NO]_b + [NO_2]_b + [NO_x]_d - [NO_2] \\ [O_3] = [O_3]_b + [NO_2]_b + \zeta [NO_x]_d - [NO_2] \\ b = k1/k2 + [O_3]_b + [NO]_b + 2[NO_2]_b + (1 + \zeta)[NO_x]_d \\ c = ([O_3]_b + [NO_2]_b + \zeta [NO_x]_d)([NO]_b + [NO_2]_b + [NO_x]_d) \end{cases}$$

where, $[NO_x]_d$ is the primary concentration of NO_x directly simulated by RLINE model when taken as an inert gas. $[NO]_b$, $[NO_2]$, and $[O_3]_b$ are the background concentrations of NO, NO₂ and O₃ from non-vehicle sources, respectively, which are provided by CMAQ-ISAM model. The unit of concentrations in these formulas is mol/m³. ζ is the ratio of NO₂ to NO_x in vehicle emissions, with a value of 0.2 (Benavides et al., 2019; Valencia et al., 2018). The reaction rates of the photolysis of NO₂ and the oxidation of NO were set to be *k1* and *k2* respectively, and calculated as follows (Hurley, 2005):

$$\begin{cases} k1 = 10^{-4} \times \delta \times \text{TSR} \\ k2 = 9.24 \times 10^5 \times \exp(-1450/T) / T \\ \delta = \begin{cases} 4.23 + 1.09 / \cos Z, & 0 \le Z \le 47 \\ 5.82, & 47 < Z \le 64 \\ -0.997 + 12(1 - \cos Z), & 64 < Z \le 90 \end{cases}$$

where, all parameters were from the WRF model. TSR is the total solar radiation (W/m²). *Z* is the solar zenith angle (°). *T* is the ambient temperature (K).

Question 5

A "vertical mixing scheme" is mentioned on page 6, which accounts for the "influence of atmospheric turbulence and building geometry on the vertical mixing" and seems to mix background air from roof level into the street canyons. The scheme requires wind speeds at the surface and at roof level, but it is not entirely clear which winds are used here. From the MLSCF scheme? What is the motivation for using the ratio between wind speeds at roof level and street level to compute the contribution of background air? I can only guess, but decisions like this need to be motivated thoroughly.

Response:

Thanks for your suggestions. For motivation of this scheme, since the settings of vertical pressure layer in the CMAQ and the WRF model are the same, the concentrations from

non-vehicle sources provided by the CMAQ-ISAM model are regarded as the background concentration at the top of the urban canopy layer. If the influence of turbulence changes on the mixing of background concentration is not taken into account, the pollutant concentrations near surface at night stable boundary layer is easy to be significantly overestimated (Benavides et al., 2019).

In this scheme, the wind speed at the roof level is from the WRF model. The surface wind is from MLSCF scheme when the gird receptor is located in the street canyon, and otherwise the logarithmic wind profile is used to calculate the wind speed at the specified height. We have added a brief introduction of the "vertical mixing scheme" in **Materials and Methods** and details in **Supplement Materials (Section S2. Vertical mixing scheme)**.

Revisions in Manuscript:

(1) Materials and Methods. Line 163-165.

In this scheme, the surface wind was from MLSCF scheme when the gird receptor is located within the street canyon, and otherwise the logarithmic wind profile was used to calculate the wind speed at the specified height, and details were showed in the Supplement Section S1.

(2) Supplement Section S2. Vertical mixing scheme.

Since the settings of vertical pressure layers in the CMAQ and the WRF model are same, the concentrations induced by non-vehicle sources provided by the CMAQ-ISAM model can be regarded as the background concentration at the top of the urban canopy layer (UCL). If the influence of turbulence changes on the mixing of background concentration is not taken into account, the pollutant concentration at night stable boundary layer is easy to be significantly overestimated (Benavides et al., 2019). Therefore, we assumed that the concentration relationship between the top of UCL and the near surface is affected by atmospheric stability, local street canyons and building morphology.

In this study, based on the method proposed by Benavides et al. (2019), the ratio of wind speed between the near surface of the road and the top of surrounding buildings was used as a proxy parameter in the model to characterize the turbulence intensity which affects the vertical concentration mixing between the top of UCL and near surface. However,

Benavides et al. assumed that the average wind speed in the street canyon was proportional to the angel between the top wind direction and the central axis of the road, and the logarithmic wind profile to was still used to represent the change of wind speed within UCL, resulting in the influence of the street canyon effect on vertical mixing of background concentration was not considered. In this study, when the grid receptor is located in the street canyon, the MLSCF scheme was used to describe the wind profile within UCL. Otherwise, the logarithmic wind profile was used to calculate the wind speed at the specified height. This parameter scheme mainly calculated the background concentration mixing ratio (fac_{bg}), which was multiplied by the background concentration provided by the CMAQ-ISAM model to estimate the background concentration at the specified height near the ground. Based on the estimated sensible heat flux (H_u , W/m²) from the WRF model, convective boundary layer (H_u >0) and stable boundary layer (H_u <0) were distinguished, and the effect of building density around the receptor site on fac_{bg} was also considered, as follows:

$$\operatorname{fac}_{\operatorname{bg}} = \begin{cases} 1 - F + F \times \frac{\operatorname{WS}_{\operatorname{sfc}}}{\operatorname{WS}_{\operatorname{bh}}}, & \operatorname{bd} > 0.1 \& H_{\operatorname{u}} > 0\\ \\ \frac{\operatorname{WS}_{\operatorname{sfc}}}{\operatorname{WS}_{\operatorname{bh}}}, & \operatorname{bd} > 0.1 \& H_{\operatorname{u}} \le 0\\ 1 - 5\operatorname{bd} + 5\operatorname{bd} \times \frac{\operatorname{WS}_{\operatorname{sfc}}}{\operatorname{WS}_{\operatorname{bh}}}, & \operatorname{bd} \le 0.1 \& H_{\operatorname{u}} > 0\\ 1 - 10\operatorname{bd} + 10\operatorname{bd} \times \frac{\operatorname{WS}_{\operatorname{sfc}}}{\operatorname{WS}_{\operatorname{bh}}}, & \operatorname{bd} \le 0.1 \& H_{\operatorname{u}} \le 0 \end{cases}$$

where, F=m+abs(0.25-bd), where *m* is an empirical parameter with value of 0.1.

Question 6

Why was a resolution of 50 m x 50 m chosen? Note that in Section 2.1 it is suggested that the resolution is only 100 m x 100 m. As mentioned on line 152, the average width of streets in Beijing is about 50 m. Thus, a resolution of 50 m is by far not sufficient to resolve gradients within street canyons.

Response:

Thanks for your reminding, and the original description was misleading. The grid spatial resolution of the hybrid model was 50 m x 50 m rather than 100 m x 100 m. This grid resolution over the whole urban area is limited due to the long computing time at present.

Since the addition parameterization schemes applied into the hybrid model, especially for the MLSCF, the meteorological field of each street needs to be calculated separately, leading to the large computational burden. However, when we focus on the distribution of concentration gradient near the street, the resolution of grid receptors will be improved to several meters level. For example, in Figure 8b and d, the grid resolution near SJZ street was improved to be 2 m. We will make efforts to develop a parallel computing method to reduce the computing time, in order to improve the grid resolution of a relatively largescale simulation. We have modified the writing and added this discussion in **Conclusions**.

Revisions in Manuscript:

(1) Materials and Methods. Line 116-117.

In our model, a NO₂ pollution map with a high temporal (1 h) and spatial resolution (50 m×50 m) can finally be obtained.

(2) Conclusion and Discussions. Line 519-522.

At present, considering the running cost, the grid resolution of area in Beijing 5th ring road and its surroundings can reach 50 m \times 50 m. We will make efforts to develop a parallel computing method to reduce the computing time, in order to improve the grid resolution of a relatively large-scale simulation.

Question 7

The machine-learning model is rather simple and little convincing. Complex models are often replaced by artificial intelligence methods using neural networks or Gaussian process models, see for example Beddows et al. (2017, doi:10.1021/acs.est.6b05873). A good summary of methods applied in the context of air quality simulations is presented in Conibear et al. (2021, doi: doi.org/10.1029/2021GH000391). Here, a random forest (RF) regression and a MARS approach are used, but these choices are not motivated at all. The RF approach seems to generate quite noisy wind profiles (see Figure 5), but in most cases performs better than MARS The combination of RF and MARS is referred to as "ensemble learning", but according to page 11, there RF and MARS models have been trained completely independently and there is only a simple switch between the two methods depending on whether the input values are within the range of the predictors used in the

training or not. There is a long way from such a simple approach to "ensemble learning".

Response:

Thanks for your suggestions. As your suggested, the applications of machine learning models on air quality predictions were investigated. In general, Random Forest (RF) and Multivariate Adaptive Regression Splines (MARS) are common machine learning methods which run efficiently on large data sets, and are relatively robust to outliers and noise. Furthermore, compared with other models (e.g. ANN), RF and MARS never require the specification of underlying data model and the complex parameter tuning (Kühnlein et al., 2014), and they can still provide efficient alternatives and generally show a high accuracy in many applications of predicting air pollutant concentrations (Chen et al., 2018; Geng et al., 2020; Hu et al., 2017; Kamińska, 2019). Therefore, RF and MARS are selected in this study, and the validation results with a little deviation (R was 0.99 and median of RE was less than 10%) indicated a good performance of our model (details see Section 3.1). A brief review of the applications of machine learning models, and the advantages of RF and MARS models have been both discussed in the revised Materials and Methods.

As for another question about the "ensemble learning" used in the manuscript, we agreed that we just combined the results of two different models depends on whether the input value was within the range of predictors or not. We realized that it is not appropriate to name this kind of combination as "ensemble learning", so the description about our model has been modified in the manuscript.

Revisions in Manuscript:

(1) Abstract. Line 16-17.

A Machine Learning-based Street Canyon Flow (MLSCF) scheme was constructed based on Computational Fluid Dynamic and two machine learning methods.

(2) Introduction. Line 101-103.

We developed a Machine Learning-based Street Canyon Flow (MLSCF) parameterization scheme, which was based on two machine learning methods using wind data from 1,600 CFD simulations.

(3) Materials and Methods. Line 258-272.

Data driven method, such as machine learning and deep learning, is now a successful

operational geoscientific processing schemes and has co-evolved with data availability over the past decade (Reichstein et al., 2019). Specially, these models have been used as computationally efficient emulators of explicit mechanism models, to explore uncertainties (Aleksankina et al., 2019) and sensitivities or replace complex gas-phase chemistry schemes (Keller and Evans, 2019; Conibear et al., 2021). In addition, metamodels (Fang et al., 2005) such as neural networks and Gaussian process (Beddows et al., 2017) are also used to produce a quick to run model surrogate and show reliable performance. Random Forest (RF) model algorithm is an ensemble learning method that generates many decision trees and aggregates their results, which has been developed to solve the high variance errors typical of a single decision tree (Breiman, 2001). Multivariate Adaptive Regression Splines (MARS) is a nonparametric and nonlinear regression method, which can be regarded as an extension of the multivariate linear model (Friedman, 1991). RF and MARS are common machine learning methods which run efficiently on large data sets, and are relatively robust to outliers and noise. Furthermore, they never require the specification of underlying data model and the complex parameter tuning, and they can still provide efficient alternatives and generally show a high accuracy in applications for predict air pollutant concentrations (Hu et al., 2017; Chen et al., 2018; Kamińska, 2019; Geng et al., 2020).

Question 8

The introduction section does a fairly poor job in citing relevant literature. Quite many multi-scale air pollution models have been developed recently and also machine learning methods are increasingly used. It is important to place the present study in context and explain where it is different or better than other approaches.

Response:

Thanks for your comments. As mentioned in the above response, a brief review of the applications of machine learning models has been added in the Materials and Methods. We have also added a review on multi-scale model in the Introduction. Compared with previous studies, the innovation of our model lies in its comprehensiveness, which takes the influence of street canyons, the chemical process, and background schemes into

consideration. In addition, the MLSCF scheme built here is a machine learning based scheme which is suitable for a wide range of street canyon wind environment simulation without huge computational cost.

Revisions in Manuscript:

(1) Introduction. Line 84-96.

Considering the respective strengths and limitations of regional models and local models, several studies have been carried out on coupling of air quality models applicable to different scales (Ketzel et al., 2012; Stocker et al., 2012; Lefebvre et al., 2013; Jensen et al., 2017; Kim et al., 2018; Mallet et al., 2018; Hood et al., 2018; Benavides et al., 2019; Kamińska, 2019; Mu et al., 2022). Although these models performed accurately in nearroad simulation, the influence of street canyons is still hard to be considered. In some hybrid models (Stocker et al., 2012; Jensen et al., 2017; Mallet et al., 2018), OSPM was still applied to calculate concentration levels within the street, where the application of logarithmic wind profile probably overestimated the bottom wind speed in a deep street canyon as abovementioned. Other models simply assumed that in street canyons, wind direction followed the street direction, and wind speed was uniform, which was not sufficient to resolve the concentration gradient within street canyons (Kim et al., 2018; Benavides et al., 2019). Berchet et al. (2017) proposed a cost-effective method for simulating city-scale pollution taking advantage of high-resolution accurate CFD, while the primary NO_x was predicted due to the lack of a chemical module. Therefore, it is essential to build an integrated model to predict long-term and near-road air pollution suitable for the urban complex underlying surface environment.

Minor comments Question 9

I was confused by the usage of the term "receptor". It seems that a receptor can be a grid point but it can also be any other point in the domain, e.g. the location of a measurement station. This needs to be explained much more clearly and earlier in the manuscript. Note that receptor modelling has quite a distinct meaning in air quality modelling and is usually associated with source-apportionment modeling like chemical mass balance or positive

matrix factorization.

Response:

Thanks for your reminding. As you mentioned, the term "receptor" in our manuscript referred to the location where the concentration was predicted by the model. The receptors included both grid receptors and monitor receptors. The grid receptors were set at a spatial resolution of 50 m×50 m, and the monitor receptors were 10 observation stations located in the normal urban environment and 5 near-road monitoring sites. We have revised the writing in the manuscript to avoid misleading. Due to too many revisions, these revisions are not shown in this response. **Please see the word with red color in the manuscript**.

Question 10

The workflow illustrated in Figure 1 is not entirely clear to me: First of all, the arrow between the boxes "receptors in street canyon?" and "receptor information" likely points in the wrong direction. The most confusing thing is that there is a distinction between "Is a street canyon" and "Receptor in a street canyon". How is it possible that a point can be in a street canyon and at the same time not be inside? Why is there only "road information" needed as input to decide whether we are in a street canyon or not? Shouldn't there also be 3D building data? How the first decision "is a street canyon" is applied is not clear to me at all. Do you choose a road segment and then decide if it is inside a canyon or not? What about points between roads? How do you decide to which road a given point in the city belongs? What about other areas of the city without roads, e.g. parks?

Response:

Thank you very much for suggestion. We apologize for misleading the reviewer about the workflow figure. The box "Is a street canyon" was actually not correct in the workflow and removed in this revision. However, the arrow between the boxes "receptors in street canyon?" and "receptor information" points is in the right direction. In fact, the first criterion is "Receptor in a Street Canyon?", which is depended on the receptor information (e.g. coordinates of the receptor) and road information (e.g. coordinates and geometry parameters). The 3D building data was processed into the geometry parameters of each road segment as stated in the Section 2.2.1. The coordinates and road width were used to

decide whether the receptor is within a street canyon or not. If the receptor is not located within a street canyon, it will be regarded as located in the open terrain area, where the logarithmic wind profile will be used rather than MLSCF scheme. Now the corrected workflow is shown in Figure 1 in the revised manuscript.

Revisions in Manuscript:

(1) Figures.



Figure 1: The framework of multiscale hybrid model CMAQ-RLINE_URBAN.

Question 11

At many instances in the paper, references to figures, tables and other sections are made in past tense (".. was shown in Figure 1", ".. were discussed in the following section", etc.) but should be in present tense (" .. are shown in Figure 1", " .. are discussed in the following section", etc.)

Response:

Thanks for your advice. We have corrected the tense in Results. Due to too many revisions,

these revisions are not shown in this response. **Please see the word with red color in the manuscript**.

Question 12

Data and code availability: Both are only available upon request. Code is only available upon "reasonable request". What is reasonable? Why is the code not made accessible more easily? Advancements in science critically depend on open science and open data.

Response:

Thanks for your question. We agreed that advancements in science critically depend on open science and open data. Now the code of MLSCF scheme is open to the public. We have added the expressions and coefficients of MARS model in the **Supplement Materials (Table S2 and S3)**, and the code of both RF and MARS models in the R language are now available on the Github website. We are pleased to share our data and code for the purpose of a scientific research.

Revisions in Manuscript:

(1) Code availability. Line 541-543.

The RF and MARS model for MLSCF are both available on Github (https://github.com/claus0224/MLSCF-RF-MARS), and other codes are available from the corresponding author on reasonable request.

(2) Supplement Materials. Tables

Terms	Expression	Coefficients
1	Intercept	0.532
2	$\max(0.5-Vbg_{\rm x},0)$	-0.623
3	$\max(Vbg_{x}-0.5, 0)$	0.111
4	$\max(2.5-Vbg_{y},0)$	-0.131
5	$\max(Vbg_y-2.5, 0)$	-0.010
6	$\max(0.5-H/W, 0)$	2.315
7	$\max(H/W-0.5, 0)$	-0.259
8	$\max(0.774 - z/H, 0)$	-0.812
9	max(<i>z</i> / <i>H</i> -0.774, 0)	2.774
10	$\max(2.5-Vbg_{x}, 0) \times \max(0.5-H/W, 0)$	-1.103
11	$\max(Vbg_x-2.5, 0) \times \max(0.5-H/W, 0)$	0.249
12	$\max(0.87-Vbg_x, 0) \times \max(0.774-z/H, 0)$	0.481

Table S2. Coefficients in V_x fitting of Multivariate Adaptive Regression Splines

13	$\max(Vbg_x-0.87, 0) \times \max(0.774-z/H, 0)$	-0.444
14	$\max(2.5-Vbg_x, 0) \times \max(z/H-0.774, 0)$	-1.151
15	$\max(Vbg_x-2.5, 0) \times \max(z/H-0.774, 0)$	-1.139
16	$\max(0.5-Vbg_y, 0) \times \max(0.5-H/W, 0)$	-3.536
17	$\max(Vbg_y-0.5, 0) \times \max(0.5-H/W, 0)$	0.028
18	$\max(0.5-H/W, 0) \times \max(0.774-z/H, 0)$	0.897
19	$\max(H/W-0.5, 0) \times \max(0.774-z/H, 0)$	0.664
20	$\max(Vbg_x-2.5, 0) \times \max(H_1/H_r-1.33, 0) \times \max(z/H-0.774, 0)$	-2.054
21	$\max(Vbg_x-2.5, 0) \times \max(1.33-H_1/H_r, 0) \times \max(z/H-0.774, 0)$	6.242

Table S3. Coefficients in V_y fitting of Multivariate Adaptive Regression Splines

Terms	Expression	Coefficients		
1	Intercept	2.117		
2	$\max(2.5\text{-}Vbg_{y},0)$	-0.812		
3	$\max(Vbg_y-2.5, 0)$	0.624		
4	max(1- <i>H</i> / <i>W</i> , 0)	0.455		
5	max(<i>H</i> / <i>W</i> -1, 0)	-0.335		
6	$\max(0.75 - H_l/H_r, 0)$	-0.081		
7	$\max(H_{\rm l}/H_{\rm r}$ -0.75, 0)	-0.690		
8	max(0.079- <i>z</i> / <i>H</i> , 0)	-14.220		
9	max(<i>z</i> / <i>H</i> -0.079, 0)	0.200		
10	$\max(0.5-Vbg_x, 0) \times \max(H_1/H_r-0.75, 0)$	0.428		
11	$\max(Vbg_x-0.5, 0) \times \max(H_1/H_r-0.75, 0)$	-0.036		
12	$\max(2.5-Vbg_y, 0) \times \max(H/W-1, 0)$	0.152		
13	$\max(2.5-Vbg_y, 0) \times \max(1-H/W, 0)$	-0.265		
14	$\max(2.5-Vbg_y, 0) \times \max(H_1/H_r-0.75, 0)$	0.230		
15	$\max(Vbg_y-2.5, 0) \times \max(H_1/H_r-0.75, 0)$	0.109		
16	$\max(2.5-Vbg_y, 0) \times \max(z/H-0.079, 0)$	-0.090		
17	$\max(2.5-Vbg_y, 0) \times \max(0.079-z/H, 0)$	5.602		
18	$\max(Vbg_y-2.5, 0) \times \max(z/H-0.226, 0)$	0.536		
19	$\max(Vbg_y-2.5, 0) \times \max(0.226-z/H, 0)$	-2.361		
20	$\max(1-H/W, 0) \times \max(H_1/H_r-0.75, 0)$	0.480		
21	$\max(H/W, 0) \times \max(H_1/H_r-0.75, 0)$	-0.052		

Question 13

Parts of the code seem to be written in Fortran, other parts in R, but it is not clear which. If only CMAQ and WRF are written in Fortran and all other parts in R, then it is not justified to state that a multiscale hybrid model was developed based on Fortran (and R), because there was no development but only application of Fortran code. Whether the model was implemented on Linux (page 5, line 96) or another platform seems irrelevant to me.

Response:

Thanks for your question. The MLSCF scheme is written in R language. Other parameterization schemes, including surface roughness scheme, UHI scheme, vertical mixing scheme and NOx photochemical scheme, were all written in Fortran language and then added in to the original RLINE source code. We have revised the description about the development language in the manuscript to make it clearer. And as you suggested, the statement about Linux platform was removed.

Revisions in Manuscript:

(1) Materials and Methods. Line 110-112.

Here, we established the MLSCF scheme based on R language, and modified the code of RLINE model to add other parameterization schemes with FORTRAN language. Finally, a multiscale air quality hybrid model was developed to achieve a high-resolution NO₂ pollution mapping in urban areas.

Question 14

The wind profiles predicted by the MOST scheme presented in Figure 7 look very strange. Apparently, wind speeds reduce to zero at the displacement height, but then jump back to a non-zero value below. Why is this kink in the profile at lower altitude in Figure 7c than in Figures 7a and 7b (despite the higher aspect ratio H/W in case (c) than in (a) and (b)) and why is it not present at all in Figure 7d? Why are the winds at z/H = 1 different between the MOST and the MLSCF schemes? Shouldn't the wind at this level be constrained by the same WRF model output?

Response:

Thanks for your question. The differences in kink altitude among Figure 7a-d refer to the calculation of displacement height (d_h). In RLINE model, the d_h is calculated by multiplying surface roughness length (z_0) times a factor which is recommended to be set as 5. Due to the great differences in z_0 (highly depends on the local geometry of buildings) of each street, d_h is also different. Moreover, the height of each street is also different, and

the y axis of Figure 7a-d represented z/h, so the kink altitudes (d_h/h) in different streets of these figures are not comparable. And the Figure 7 mainly illustrates the different predictions of wind speed between MOST and MLSCF schemes. We added the calculation method of d_h in the manuscript to make the statement clearer.

The differences in winds at z/H = 1 between the MOST and the MLSCF schemes are mainly because the influence of turbulence in the street canyon on wind at the roof level is considered in the MLSCF scheme. However, in the MOST and MLSCF schemes, the wind environment higher than the roof level (z/H>1) were both from WRF model and remained the same.

Revisions in Manuscript:

(1) Results. Line 366-369.

As shown in Figure 7(a)-(d), the wind profile estimated by MOST showed a logarithmic change at the height above displacement height (d_h) (the d_h is calculated by multiplying surface roughness length (z_0) times a factor which is recommended to be set as 5) with a decrease to 0 at d_h , and remained constant below d_h .

Question 15

Figure 8 shows differences between simulations with and without the MLSCF scheme. Why are these differences limited to very narrow lines? It is very difficult to see details in this figure. It would be useful to see a zoom into a subregion.

Response:

Thanks for your question. It is because MLSCF scheme only affects the concentration of grid receptors inside the street canyon. The concentrations of grid receptors outside the street canyon are not affected, so the difference shown in Figure8 is a narrow strip visually. The detailed differences in the spatial distribution of concentrations within in a street canyon has already been described in Figure 8b and d, where the SJZ street was taken as an example.

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Response to Reviewers #2's Comments *Summary*

The regional to urban coupling allows the consideration of regional weather effects in local models and plays an important role in the improved prediction of local air pollution. The development of such multiscale modelling framework is interesting. This paper developed a hybrid CMAQ-RLINE_URBAN, which coupled the regional CMAQ Chemical Transport Model, RLINE local dispersion model and urban thermodynamic scheme. Intensive CFD street canyon simulations have been conducted for the application of Machine Learning. The hybrid model has been applied to one month simulation in Summer for Beijing as a case study. It performed better than the regional CMAQ model in predicting NO2 concentrations for roadside sites. However, there are still a number of major comments to be addressed.

Response:

Thank you very much to give us constructive comments. Upon learning through them, we greatly improved our manuscript. We believe all the concerns you mentioned at this time were addressed in this revision.

Major comments Question 1

Literature review: Lack of discussion about the computational fluid dynamic (CFD). CFD can be classified into two categories: Reynolds-averaged Navier-Stokes (RANS) and Large-Eddy Simulation (LES), based on turbulence closure schemes (e.g. https://doi.org/10.1016/j.envpol.2016.04.052). Discussion about the comparison between RANS and LES is needed, and to justify the use of RANS in the present study (e.g. computationally faster than LES, but only resolve the mean time-averaged properties).

Response:

Thanks for your advice. Considering the topic of this paper is "coupled model", the description of CFD method and its turbulence closure schemes was not included in the Introduction. As you mentioned, we agreed that it was necessary to discussion about the comparison between RANS and LES. We have added the review of turbulence closure schemes in the CFD method section (Section 2.2.2). Furthermore, we clarified the reason for the use of the RANS, as follows:

a. A total of 1600 simulations are implemented in this study. Due to such a huge computation cost, we must choose the RANS which is much faster than the LES.

b. The geometry of street canyons in our modelling is uncomplicated, so the RANS can meet our experimental accuracy requirements.

Revisions in Manuscript:

(1) Materials and Methods. Line 203-211.

The turbulence closure schemes for CFD include the Reynolds-Averaged Navier-Stokes (RANS) and the Large-Eddy Simulation (LES), and the choice of them depends on the computational cost, the accuracy required and the purpose of application. The RANS resolves the mean time-averaged properties with all the turbulence motions to be modelled, while LES adopts a spatial filtering operation and consequently resolves large-scale eddies directly and parameterizes small-scale eddies (Zhong et al., 2016). Compared with the LES, the RANS is more easily established and computationally faster (Xie and Castro, 2006). However, the LES can provide a better prediction of air flow than that from the RANS when handling complex geometries (Dejoan et al., 2010; Santiago et al., 2010). In this study, considering the huge computational burden of a large number of simulations and the relatively simple geometry of street canyons in our modelling, the RANS was selected to characterize the air flow.

Question 2

Literature review: there is not enough information about local RLINE model, and also the coupled CMAQ-RLINE model. Then to justify the need of the further development of CMAQ-RLINE_URBAN in the present study. Also, the literature about the current status of regional-to-urban coupling is missing (e.g. https://doi.org/10.5194/acp-18-11221-2018, 2018).

Response:

Thanks for your advice. We apologized that the detailed introduction of RLINE was missing in our original manuscript. In general, the RLINE is a Gaussian dispersion model specially for the line source simulation. In this revision, we have added the description of RLINE model including its mechanism and application in **Method Section 2.1**.

Although RLINE has been successfully used in many studies to evaluate the impacts from traffic emissions on air quality, there are still large uncertainties in predictions from induced by the provided meteorological conditions and background concentrations, especially the application in urban areas. It is similar with other Gaussian dispersion models, where the natural logarithm function is still used to characterize the vertical profile of wind speed in both the inertial and rough sublayers, neglecting the influence of urban complex underlying surface compositions on the wind field. Thus, it is essential to develop a coupled model, such as CMAQ-RLINE_URBAN in our study. The detailed discussions about this weakness have been already presented in the **Introduction** section in the original manuscript.

In this revision, as you suggested, we have also added a review on about the current status of regional-to-urban coupling in the **Introduction** section to further describe the innovation of our model.

Revisions in Manuscript:

(1) Introduction. Line 84-96.

Considering the respective strengths and limitations of regional models and local models, several studies have been carried out on coupling of air quality models applicable to different scales (Ketzel et al., 2012; Stocker et al., 2012; Lefebvre et al., 2013; Jensen et al., 2017; Kim et al., 2018; Mallet et al., 2018; Hood et al., 2018; Benavides et al., 2019; Kamińska, 2019; Mu et al., 2022). Although these models performed accurately in nearroad simulation, the influence of street canyons is still hard to be considered. In some hybrid models (Stocker et al., 2012; Jensen et al., 2017; Mallet et al., 2018), OSPM was still applied to calculate concentration levels within the street, where the application of logarithmic wind profile probably overestimated the bottom wind speed in a deep street canyon as abovementioned. Other models simply assumed that in street canyons, wind direction followed the street direction, and wind speed was uniform, which was not sufficient to resolve the concentration gradient within street canyons (Kim et al., 2018; Benavides et al., 2019). Berchet et al. (2017) proposed a cost-effective method for simulating city-scale pollution taking advantage of high-resolution accurate CFD, while the primary NO_x was predicted due to the lack of a chemical module. Therefore, it is

essential to build an integrated model to predict long-term and near-road air pollution suitable for the urban complex underlying surface environment.

(2) Materials and Methods. Line 119-128.

RLINE is a Gaussian line source dispersion model developed by Snyder et al. (2013) to predict pollutant concentrations in near-road environments. In the RLINE model, the mobile source is considered as a finite line source, from which the concentration is found by approximating the line as a series of point sources and integrating the contributions of point sources using an efficient numerical integration scheme. The number of points needed for convergence to the proper solution is a function of distance from the source line to the receptor, and each point source is simulated using a Gaussian plume formulation. The RLINE model performs generally comparable results when evaluated with other line source models for on-road traffic emissions dispersion (Snyder et al., 2013; Heist et al., 2013; Chang et al., 2015), and has been successfully used in many studies to evaluate the impacts from traffic emissions on air quality (Zhai et al., 2016; Valencia et al., 2018; Benavides et al., 2019; Filigrana et al., 2020; Zhang et al., 2021a).

Question 3

Resolution for the hybrid model CMAQ-RLINE_URBAN. The resolution of 50 m x 50 m is still coarse to resolve the street scale dispersion of road sources. Could such resolution be flexible (i.e. further to higher resolutions) in the hybrid model? The justification of the use of 50 m x 50 m in the present study is needed

Response:

Thanks for your question. Actually, the grid resolution in our hybrid model is flexible. However, the grid resolution over the whole urban area is limited to $50 \text{ m} \times 50 \text{ m}$ due to the long computing time for such a large domain at present. Since the addition developed parameterization schemes were applied in the hybrid model, especially for the MLSCF, the meteorological field of each street needs to be calculated separately, leading to the large computational burden. However, when we focus on the distribution of concentration gradient near the street, the resolution of grid receptors will be improved to several meters level. For example, in Figure 8b and d, the grid resolution near SJZ street was improved to be 2 m. In the future, we will make efforts to develop a parallel computing method with multi cores to reduce the computing time, in order to improve the grid resolution of a relatively large-scale simulation. We have modified the writing and added this discussion in the **Conclusions** section.

Revisions in Manuscript:

(1) Materials and Methods. Line 116-117.

In our model, a NO₂ pollution map with a high temporal (1 h) and spatial resolution (50 m×50 m) can finally be obtained.

(2) Conclusion and Discussions. Line 519-522.

At present, considering the running cost, the grid resolution of area in Beijing 5th ring road and its surroundings can reach 50 m×50 m. We will make efforts to develop a parallel computing method to reduce the computing time, in order to improve the grid resolution of a relatively large-scale simulation.

Question 4

Machine learning is for air flow (wind speed) only. How is it linked to the pollutant dispersion? Would it be better than a traditional street canyon model (e.g. https://doi.org/10.1080/10962247.2020.1803158)?

Response:

Thanks for questions. In this study, the MLSCF is developed to estimate the wind velocity and direction at different height in the street canyon. In other words, outputs from the MLSCF model are wind vectors. Therefore, the impact of turbulence induced by street canyon effect on wind environment is considered. When the receptor is located within a street canyon, the wind field within the UCL was simulated by MLSCF scheme and used to calculate the pollutant dispersion, which has been already shown in Figure 1 and discussed in section 2.1. As shown in the Figure 8, the impacts of the MLSCF scheme on simulated NO₂ concentration were identified by the differences between modeling scenarios with and without MLSCF. For example, in the SZJ standard canyon, the application of MLSCF led to the wind direction at the bottom in street canyon opposite to that at the roof, increasing the upwind concentrations (Figure 8b and Section 3.2 in the manuscript).

Compared with the traditional street canyon model, such as the OSPM, the MLSCF in our model considered the influence of geometry of buildings on the air flow with high aspect ratio up to 2 (see Table 1), and the wind profile is affected by the geometry of buildings instead of a logarithmic wind profile. However, when compared with research of a "box model" simulation you mentioned (Hood et al., 2021), it is hard to compare which one is better due to different computation framework and mode. However, we are committed to comparing our model with other researches through real cases in the future.

Question 5

It is not clear how NOx photochemical scheme works? Does it explicitly resolve the simple NOx-O3 cycle? If VOCs chemistry is further considered, then it would likely make a substantial difference in predicting NO2 concentration (e.g. https://doi.org/10.1016/j.envpol.2017.01.076). It is suggested to add some discussion on this aspect.

Response:

Thank you for questions. We apologized those unclear descriptions on the NOx photochemical reactions in the original manuscript. In general, we used the two-reaction method applied in other studies, such as the SIRANE model (Soulhac et al., 2017). The NO_x photochemical scheme includes two main chemical reactions, namely the photolysis of NO₂ and the oxidation of NO as follows:

$$\begin{cases} NO_2 + hv \rightarrow NO + O_3 \\ NO + O_3 \rightarrow NO_2 \end{cases}$$

During simulation, the NOx (NO+NO₂) emitted from vehicles is first regarded as an inert gas and only the primary concentration after diffusion is simulated. Then, assuming a photo-stationary equilibrium condition, the concentrations of NO, NO₂ and O_3 are calculated.

We have added a brief introduction of the "two-reaction scheme" in Materials and Methods and details in Supplement Materials (Section S3. NOx photochemical parameter scheme).

For the question about VOCs chemistry, Kim has already compared a simple mechanism

only involving NOx and O_3 (Leighton mechanism), with the CB05 gas phase chemical mechanism including VOCs chemistry by incorporated them into SinG model to estimate roadside NO₂ concentration respectively, and found a very similar predictions (Kim et al., 2018b). Therefore, the Leighton mechanism was selected in an operational version of SinG due to the halved computational time. However, Zhong et al. found the NO₂ and O_x inside the canyon was enhanced by 30–40% via OH/HO2 chemistry in the canyon (Zhong et al., 2017). The difference of the influence of VOCs chemistry on concentrations in these studies mainly due to the differences in local meteorological conditions, emissions and other factors (e.g. geometry of canyons). Considering that the input emission data of two-reaction scheme are more accessible and the computational cost is lower compared with those in the O₃-NOx-VOC chemistry, we chose two-reaction scheme in this study. We will make effort on investigate the influence of chemistry scheme on simulation in the future, and this is added in the **Conclusions** now.

Revisions in Manuscript:

(1) Materials and Methods. Line 167-170.

In this study, a simplified two-reaction scheme, including the photolysis of NO_2 and the oxidation of NO, was incorporated into the model to characterize the photochemical process of NO_x (details in the Supplement Section S3), which has been successfully applied in the SIRANE dispersion model (Soulhac et al., 2017).

(2) Conclusion and Discussions. Line 522-527.

In our study, a simplified two-reaction scheme was incorporated into the model to characterize the photochemical process of NO_x , since it performed similar predictions and less computational time compared with those of the complicated CB05 gas phase chemical mechanism (Kim et al., 2018). However, another study pointed that the impact of nonlinear O₃-NO_x-VOC chemistry on NO₂ concentrations in the deep canyon was nonnegligible (Zhong et al., 2017). The influence of different chemistry schemes on near-road simulation will be investigated in the future.

(3) Supplement Materials Section S3. NOx photochemical parameter scheme.

The NO_x photochemical parameter scheme applied in this study includes two reactions:

$$\begin{cases} NO_2 + hv \rightarrow NO + O_3 \\ NO + O_3 \rightarrow NO_2 \end{cases}$$

Kim et al. compared two-reaction scheme with CB05 gas phase chemical mechanism by incorporated them into SinG model to estimate roadside NO₂ concentration, and found a similar results, while the computing time cost of two-reaction scheme was significantly less than that of the CB05 mechanism (Kim et al., 2018). Therefore, the simplified two-reaction scheme was incorporated into the model in this study to characterize the NO_x photochemical process. During simulation, the NOx (NO+NO₂) emitted from vehicles is first regarded as an inert gas and only the primary concentration after diffusion is simulated. Then, assuming a photo-stationary equilibrium condition, the concentrations of NO, NO₂ and O₃ are calculated using the two-reaction scheme, as follows:

$$\begin{cases} [NO_2] = (b - \sqrt{b^2 - 4c})/2 \\ [NO] = [NO]_b + [NO_2]_b + [NO_x]_d - [NO_2] \\ [O_3] = [O_3]_b + [NO_2]_b + \zeta [NO_x]_d - [NO_2] \\ b = k1/k2 + [O_3]_b + [NO]_b + 2[NO_2]_b + (1 + \zeta)[NO_x]_d \\ c = ([O_3]_b + [NO_2]_b + \zeta [NO_x]_d)([NO]_b + [NO_2]_b + [NO_x]_d) \end{cases}$$

where, $[NO_x]_d$ is the primary concentration of NO_x directly simulated by RLINE model when taken as an inert gas. $[NO]_b$, $[NO_2]$, and $[O_3]_b$ are the background concentrations of NO, NO₂ and O₃ from non-vehicle sources, respectively, which are provided by CMAQ-ISAM model. The unit of concentrations in these formulas is mol/m³. ζ is the ratio of NO₂ to NO_x in vehicle emissions, with a value of 0.2 (Benavides et al., 2019; Valencia et al., 2018). The reaction rates of the photolysis of NO₂ and the oxidation of NO were set to be *k1* and *k2* respectively, and calculated as follows (Hurley, 2005):

$$\begin{cases} k1 = 10^{-4} \times \delta \times \text{TSR} \\ k2 = 9.24 \times 10^5 \times \exp(-1450/T) / T \\ \delta = \begin{cases} 4.23 + 1.09 / \cos Z, & 0 \le Z \le 47 \\ 5.82, & 47 < Z \le 64 \\ -0.997 + 12(1 - \cos Z), & 64 < Z \le 90 \end{cases}$$

where, all parameters were from the WRF model. TSR is the total solar radiation (W/m^2) .

Z is the solar zenith angle (°). T is the ambient temperature (K).

Minor comments Question 6

Line 39: Which pollutant does these measures of industrial and domestic sources aim to tackle?

Is it for PM2.5, rather than NO2?

Response:

Thanks for your reminding. This research (Zhang et al., 2019) is aim to track $PM_{2.5}$. However, the main air pollution control measures on industrial, domestic and mobile sources mentioned in this study will also relieve the NO₂ pollution, such as the strengthen industrial emissions standards, upgrades and phase out on industrial capacities. We have revised the statement now for better understanding.

Revisions in Manuscript:

(1) Introduction. Line 38-40.

The improvement of PM_{2.5} in China was mainly due to the emission reduction and control measures of industrial and domestic sources (Zhang et al., 2019), which also relieved the NO₂ pollution, but the reduction potential of these sources has been gradually declining.

Question 7

Lines 42-43: The poor dispersion caused by buildings along the street would also play a key role in it. High pollutant concentrations in street canyon environment are caused by combined effects of poor dispersion, increased traffic emissions and chemistry processes.

Response:

Thanks very much for your advice. We agreed that this statement should be more precise. We have revised the original description.

Revisions in Manuscript:

(1) Introduction. Line 41-43.

Due to the low release height of vehicle emissions, combined with the negative dispersion condition caused by nearby buildings, air pollutants will be significantly accumulated near the street.

Question 8

Line 58: "has" should be "have".

Response:

Thanks for your comments. We have revised it now.

Revisions in Manuscript:

(1) Introduction. Line 55-59.

Regional-scaled air quality models, represented by Chemical Transport Models (CTMs) including Community Multi-scale Air Quality (CMAQ) model (Byun and Schere, 2006), Comprehensive Air quality Model with extensions (CAMx), and Weather Research and Forecasting/Chemistry model (WRF-Chem) (Grell et al., 2005), have been used extensively in assessment on the impacts of vehicle emissions on the regional atmospheric environment.

Question 9

Line 96: "Based on FORTRAN and R languages", it is not clear. Which part is based on R? Is it for a post-processing tool?

Response:

Thanks for your reminding. The MLSCF scheme (including RF and MARS) was established based on R language, and we further modified the code of RLINE model to add other parameterization schemes with FORTRAN language. We added more description to make it clearer in the manuscript.

Revisions in Manuscript:

(1) Materials and Methods. Line 110-111.

Here, we established the MLSCF scheme based on R language, and modified the code of

RLINE model to add other parameterization schemes with FORTRAN language.

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Response to Reviewers #3's Comments Summarv

In this work, a hybrid model has been developed and evaluated to analyse the effects of vehicle emissions on urban roadside concentrations of NO2 in Beijing. The article is well written and raises an important topic, the link between the simulations done using regional chemistry transport models and the simulations at the urban level done using gaussian/dispersion models. However, there are a few points that should be clarified in order to make clearer the evaluation of the model and the scenarios tested.

Response:

Thank you very much for spending time to give us so many constructive comments. Upon learning through them, we improved our manuscript. We try our best to address all the concerns in this revision.

Major comments

Question 1

The introduction clearly shows the differences between chemistry transport models and dispersion/gaussian models highlighting the difficulties of the former in predicting the roadside concentrations. However, there isn't a clear link between regional models and urban models. Few works have been published and few models have been already developed to couple regional and urban models and these should be mentioned in the introduction.

Response:

Thanks for your advice. In recent years, considering the respective strengths and limitations of chemistry transport models and dispersion/gaussian models, several studies have been carried out on coupling of air quality models applicable to different scales. And we apologized that the introduction of coupled model was missing in our original manuscript. Now we have added a review about the current status of coupled model in the Introduction to further describe the innovation of our model.

Revisions in Manuscript:

(1) Introduction. Line 84-96.

Considering the respective strengths and limitations of regional models and local models,

several studies have been carried out on coupling of air quality models applicable to different scales (Ketzel et al., 2012; Stocker et al., 2012; Lefebvre et al., 2013; Jensen et al., 2017; Kim et al., 2018; Mallet et al., 2018; Hood et al., 2018; Benavides et al., 2019; Kamińska, 2019; Mu et al., 2022). Although these models performed accurately in nearroad simulation, the influence of street canyons is still hard to be considered. In some hybrid models (Stocker et al., 2012; Jensen et al., 2017; Mallet et al., 2018), OSPM was still applied to calculate concentration levels within the street, where the application of logarithmic wind profile probably overestimated the bottom wind speed in a deep street canyon as abovementioned. Other models simply assumed that in street canyons, wind direction followed the street direction, and wind speed was uniform, which was not sufficient to resolve the concentration gradient within street canyons (Kim et al., 2018; Benavides et al., 2019). Berchet et al. (2017) proposed a cost-effective method for simulating city-scale pollution taking advantage of high-resolution accurate CFD, while the primary NOx was predicted due to the lack of a chemical module. Therefore, it is essential to build an integrated model to predict long-term and near-road air pollution suitable for the urban complex underlying surface environment.

Question 2

The methodology highlights only part of the process defined in Figure 1. The authors focus their discussion on the urban model but WRF and CMAQ configuration and outputs should also be mentioned and discussed.

Response:

Thanks for your advice. The configuration of WRF and CMAQ model was introduced in detail in our previous study (Lv et al., 2020), where each input data and parameterization schemes are discussed. This information has been already provided in the Method section. The prediction of CMAQ model has also already shown and discussed in Figure 9-11 and Table 2, including the outputs of CMAQ, the comparison of different models and the validation of CMAQ. In this revision, we added the validation of predictions from WRF model compared with observations in **Table S6 in in Supplement Materials**.

Revisions in Manuscript:

^			^					
Variables	Sample size	Observed Average	Simulated Average	MB	NMB	RMSE	R	
WS10 (m/s)	732	2.5	3.7	1.2	46	1.9	0.6	
WD10 (°)	456	190.4	169.0	-8.0	-4	49.5	0.4	
T2 (°C)	742	25.8	29.0	3.2	12	3.5	0.9	
RH (%)	741	64.3	50.4	-13.9	-22	17.4	0.9	

(1) Supplement Materials. Table S6. Table S6. The performance of WRF model compared with observations.

*WS10: wind speed at the height of 10 m; WD10: wind direction at the height of 10 m; T2: Temperature at the height of 2 m; RH: Relative humidity; MB: Mean bias; RSME: Root mean squared error; NMB: Normalized mean bias; R: correlation coefficient.

Question 3

The simulations are run for a period of high photochemical activity. This is surely dependent on weather conditions that are completely absent from the article?

Response:

Thanks for your advice. We apologized that the description about weather conditions in simulation period is missing. In this study, we choose summer (August 1st to 31th in 2019) as simulation period since the strong photochemical reactions, induced by the high temperature (the average of daily high temperatures higher than 30 °C) and strong solar radiation conditions (sunlight hours longer than 13 hours). Now we revised this statement to make it clearer.

Revisions in Manuscript:

(1) Materials and Methods. Line 300-302.

The near-ground NO₂ concentrations were simulated from August 1st to 31th in 2019 when the average of daily high temperatures was higher than 30 °C and sunlight duration was longer than 13 hours, leading to strong photochemical reactions.

Question 4

The NOx-O3 system include also VOCs. There is no mention of this in the methodology or in the results. Are VOCs included in the simulations? It would be good to add the chemical mechanism somewhere in the supplementary material?

Response:

Thanks for your advice. We apologized those unclear descriptions on the NOx photochemical reactions in the original manuscript. In general, the VOCs is not included in our study, where a simple mechanism only involving NOx and O_3 was used. We used the two-reaction method applied in other studies, such as the SIRANE model (Soulhac et al., 2017). The NO_x photochemical scheme includes two main chemical reactions, namely the photolysis of NO₂ and the oxidation of NO as follows:

$$\begin{cases} NO_2 + hv \rightarrow NO + O_3 \\ NO + O_3 \rightarrow NO_2 \end{cases}$$

During simulation, the NOx (NO+NO₂) emitted from vehicles is first regarded as an inert gas and only the primary concentration after diffusion is simulated. Then, assuming a photo-stationary equilibrium condition, the concentrations of NO, NO₂ and O_3 are calculated.

Following your suggestions, we have added a brief introduction of the "two-reaction scheme" in Materials and Methods and details in Supplement Materials (Section S3. NOx photochemical parameter scheme).

For comments about VOCs chemistry, Kim has already compared a simple mechanism only involving NOx and O₃ (Leighton mechanism), with the CB05 gas phase chemical mechanism including VOCs chemistry by incorporated them into SinG model to estimate roadside NO₂ concentration respectively, and found a very similar predictions (Kim et al., 2018). Therefore, the Leighton mechanism was selected in an operational version of SinG due to the halved computational time. However, Zhong et al. found the NO₂ and O_x inside the canyon was enhanced by 30–40% via OH/HO2 chemistry in the canyon (Zhong et al., 2017). The difference of the influence of VOCs chemistry on concentrations in these studies mainly due to the differences in local meteorological conditions, emissions and other factors (e.g. geometry of canyons). Considering that the input emission data of two-reaction scheme are more accessible and the computational cost is lower compared with those in the O₃-NOx-VOC chemistry, we chose two-reaction scheme in this study. We will make effort on investigate the influence of chemistry scheme on simulation in the future, and this is added in the **Conclusions** now.

Revisions in Manuscript:

(1) Materials and Methods. Line 167-170.

In this study, a simplified two-reaction scheme, including the photolysis of NO_2 and the oxidation of NO, was incorporated into the model to characterize the photochemical process of NO_x (details in the Supplement Section S3), which has been successfully applied in the SIRANE dispersion model (Soulhac et al., 2017).

(2) Conclusion and Discussions. Line 522-527.

In our study, a simplified two-reaction scheme was incorporated into the model to characterize the photochemical process of NO_x , since it performed similar predictions and less computational time compared with those of the complicated CB05 gas phase chemical mechanism (Kim et al., 2018). However, another study pointed that the impact of nonlinear O₃-NO_x-VOC chemistry on NO₂ concentrations in the deep canyon was nonnegligible (Zhong et al., 2017). The influence of different chemistry schemes on near-road simulation will be investigated in the future.

(3) Supplement Materials Section S3. NOx photochemical parameter scheme.

The NO_x photochemical parameter scheme applied in this study includes two reactions:

$$\begin{cases} NO_2 + hv \rightarrow NO + O_3 \\ NO + O_3 \rightarrow NO_2 \end{cases}$$

Kim et al. compared two-reaction scheme with CB05 gas phase chemical mechanism by incorporated them into SinG model to estimate roadside NO₂ concentration, and found a similar results, while the computing time cost of two-reaction scheme was significantly less than that of the CB05 mechanism (Kim et al., 2018). Therefore, the simplified two-reaction scheme was incorporated into the model in this study to characterize the NO_x photochemical process. During simulation, the NOx (NO+NO₂) emitted from vehicles is first regarded as an inert gas and only the primary concentration after diffusion is simulated. Then, assuming a photo-stationary equilibrium condition, the concentrations of NO, NO₂ and O_3 are calculated using the two-reaction scheme, as follows:

$$\begin{cases} [NO_2] = (b - \sqrt{b^2 - 4c})/2 \\ [NO] = [NO]_b + [NO_2]_b + [NO_x]_d - [NO_2] \\ [O_3] = [O_3]_b + [NO_2]_b + \zeta [NO_x]_d - [NO_2] \\ b = k1/k2 + [O_3]_b + [NO]_b + 2[NO_2]_b + (1 + \zeta)[NO_x]_d \\ c = ([O_3]_b + [NO_2]_b + \zeta [NO_x]_d)([NO]_b + [NO_2]_b + [NO_x]_d) \end{cases}$$

where, $[NO_x]_d$ is the primary concentration of NO_x directly simulated by RLINE model when taken as an inert gas. $[NO]_b$, $[NO_2]$, and $[O_3]_b$ are the background concentrations of NO, NO₂ and O₃ from non-vehicle sources, respectively, which are provided by CMAQ-ISAM model. The unit of concentrations in these formulas is mol/m³. ζ is the ratio of NO₂ to NO_x in vehicle emissions, with a value of 0.2 (Benavides et al., 2019; Valencia et al., 2018). The reaction rates of the photolysis of NO₂ and the oxidation of NO were set to be *k1* and *k2* respectively, and calculated as follows (Hurley, 2005):

$$\begin{cases} k1 = 10^{-4} \times \delta \times \text{TSR} \\ k2 = 9.24 \times 10^5 \times \exp(-1450/T) / T \\ 4.23 + 1.09 / \cos Z, \quad 0 \le Z \le 47 \\ 5.82, \quad 47 < Z \le 64 \\ -0.997 + 12(1 - \cos Z), \quad 64 < Z \le 90 \end{cases}$$

where, all parameters were from the WRF model. TSR is the total solar radiation (W/m²). *Z* is the solar zenith angle (°). *T* is the ambient temperature (K).

Minor comments

Question 5

Line 32: the reference (Cui et al., 2021), (Shah et al., 2020) should be (Cui et al., 2021; Shah et al., 2020).

Response:

Thanks for your reminding. We apologized that the citation format is wrong and corrected it now in this revision.

Revisions in Manuscript:

(1) Introduction. Line 30-33.

During the last decade, benefiting from the implementations of several air pollution control strategies by the Chinese government, the air quality has improved (Jin et al., 2016; Zheng et al., 2018), and the vertical column densities of NO₂ displayed a decreasing trend after 2013 (Shah et al., 2020; Cui et al., 2021).

Question 6

Line 33: delete that: it is still much more severe than that in developed.

Response:

Thanks for your advice. We apologized that this statement is not appropriate and deleted it now in this revision.

Question 7

Line 40 - 42: The comparison with the emission in Lyon is quite specific. I suggest explaining a bit more or in an alternative to make a more general case of "other urban areas.

Response:

Thanks for your suggestion. We agreed that the case in Lyon introduced here was too specific and deleted it now in this revision.

Revisions in Manuscript:

(1) Introduction. Line 40-41.

Meanwhile, as the population of vehicles is growing rapidly, vehicle emissions have become a major source of NO₂ pollution, especially in urban areas (Nguyen et al., 2018).

Question 8

Line 102: the spatial resolution should be precise: please substitute < 100 m x 100 m with the real spatial resolution.

Response:

Thanks for your reminding, and the original description was misleading. The grid spatial resolution of the hybrid model over the urban area was 50 m x 50 m. We revised the statement to be precise.

Revisions in Manuscript:

(1) Materials and Methods. Line 116-117.

In our model, a NO₂ pollution map with a high temporal (1 h) and spatial resolution (50 m×50 m) can finally be obtained.

Question 9

Line 107 -108: The choice of the midpoint height of 22.5m suggests that the CMAQ has a first vertical layer at 45m of height. In the first instance, this would be in my opinion too high. Generally, CTMs have the first 9-10 vertical layers below the boundary layer but, to improve the prediction on the ground level, keep the 1st layer around 20m from the ground.

Could the authors enforce their statements with one or more references that justify this choice.

Response:

Thanks for your question. We agreed that in traditional CTMs, it is useful to improve the prediction when the first layer was set to be lower. However, in our hybrid model, we planned to get the wind environment and the background concentrations at the top of the canyon, so the midpoint height of the first layer in both WRF and CMAQ model must be similar with the height of street canyon. In Beijing, the average height of street canyon is 23.6 m, so we set 22.5 m as the midpoint height of the first layer. This setting is similar with that in Benavides's study (Benavides et al., 2019), where the bottom layer in the model was set to be 40.6 m, of which midpoint height was similar to the average building height. Now we added the reference in the **Materials and Methods** section to enforce our statements.

Revisions in Manuscript:

(1) Materials and Methods. Line 132-134.

The height of midpoint in the bottom layer to the ground was set as 22.5 m, which is close to the average height of buildings near street canyons, similar to the settings in the previous study (Benavides et al., 2019).

Question 10

Line 277 - 279: The authors describe the performance of the model in terms of "high" and "low" RE. It would be good to provide a more quantitative description or a reference value for this particular metric.

Response:

Thanks for your question. We have already provided a quantitative description about the "high" and "low" RE. The "high" RE referred to the value of 42.5% and 43% in previous sentence. And the "low" RE referred to the value of 9.8% and 2.7% in this sentence. There is not a quantitative criterion to judge whether the RE is high or low, which generally depends on the specific requirement of the experiment. Now we revised our statement and put the quantitative description in this one sentence.

Revisions in Manuscript:

(1) Results. Line 337-339.

Although the average of the relative error (RE) were a little high (42.5% and 43%), particularly when the predicted wind speed was low, the median RE were relatively low with 9.8% and 2.7%, respectively, indicating an acceptable performance.

Question 11

Line 280 – 283: I'm not sure that the MARS model performs better than RD in Figure 5. I suggest clarifying this paragraph better. In the a) figure the CFD is the closest to the observations, followed by RF (red slope) and MARS (yellow slope). In figure b) again CFD is the closest to the observations, RF is completely underestimated and MARS is overestimated from values of z/H > 0.25.

Response:

Thanks for your question. Figure 5 was aimed to compare the performance of RF and MARS in two different cases, so we should find between MARS and RF which one is closer to the CFD and observations. In the first case (Figure 5a), the MARS model performed not very well when compared with the RF. However, in another uncommon case when $Vbg_y=17$ m/s >>5 m/s (Figure 5b), RF failed to respond to the parts beyond the range of prediction variables, and the predictions from MARS is closer to the CFD and observations. Therefore, by comparing the performance of two models in Figure 5, the MLSCF scheme was established based on a method to combine the advantages of each model. The RF model was used when the input value was within the range of predictors shown in Table 1, otherwise the predictions from the MARS model were used. We have corrected the description of x-lable in Figure 5b and revised the text under this figure for better understanding.

Revisions in Manuscript:

(1) Manuscript. Figure 5.



Figure 5: Performances of machine learning on velocity profile in wind tunnel experiments. The street canyon was perpendicular (a) or parallel (b) to the wind direction at the roof level in different experiments. The detailed description of each experiment was introduced in Section 2.2.3.

Question 12

Line 378 - 383: The authors mention NOx emissions leading to high NO2 observations among all sites. They also say that the CMAQ model underestimates the NO2 concentrations near ring roads (MB = -15μ g/m3). The NOx emissions account for NO+NO2, if this variable is NOx before being inserted in CMAQ, it has to be divided between NO and NO2. In roadside sites generally, the NO emissions are high, could the underestimation in CMAQ be related to a not precise division of the original emissions of NOX in NO and NO2?

Response:

Thanks for your question. The setting of the division of the original NOx emissions in NO and NO₂ depends on what emission source it is, rather than what model we use. For example, divisions of NOx emission from industry and vehicle are different, but the divisions of NOx emission from vehicles in both CMAQ or our hybrid model remained the same. In our study, the ratio of NO₂ to NOx in vehicle emission was set as 0.2 according to previous studies (Benavides et al., 2019; Valencia et al., 2018), which was introduced in the **Supplement Materials Section S3. NOx photochemical parameter scheme** now.

Revisions in Manuscript:

(1) Supplement Materials Section S3. NOx photochemical parameter scheme.
ζ is the ratio of NO₂ to NO_x in vehicle emissions, with a value of 0.2 (Benavides et al., 2019; Valencia et al., 2018).

Question 13

Line 390 – 394: The model actually improves the performance of O3 in comparison with CMAQ only model. This agrees with the underestimation in NO2 that the CMAQ only shows and was previously described by the authors. Being the O3 chemistry dependent not only on NO, and NO2 but also on VOCs I would spend some words introducing these pollutant classes and giving more details on them.

Response:

Thanks for your advice. In this study we focused on near-source process, where the O_3 was largely affected by the titration of NOx. As mentioned in the previous study (Biggart et al., 2020), roads with higher NOx emissions led to lower NO_2/NO_x concentration ratios within distances of 100m, indicating greater O_3 loss through its titration by NO. This is one of the reasons why a simple mechanism only involving NOx and O3 was used in this study. The influence of VOCs concentrations on pollutant concentrations have been discussed in several studies (Kim et al., 2018; Zhong et al., 2017), and in this study we didn't take it into consideration. Details about this has been described in the *Question 4*.

Revisions in Manuscript:

(1) Conclusion and Discussions. Line 522-527.

In our study, a simplified two-reaction scheme was incorporated into the model to characterize the photochemical process of NO_x , since it performed similar predictions and less computational time compared with those of the complicated CB05 gas phase chemical mechanism (Kim et al., 2018). However, another study pointed that the impact of nonlinear O₃-NO_x-VOC chemistry on NO₂ concentrations in the deep canyon was nonnegligible (Zhong et al., 2017). The influence of different chemistry schemes on near-road simulation will be investigated in the future.

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