Response to the comments of reviewer #4

This review covers the 2nd revised version of the manuscript ACP-0218

"Influence of aerosol copper on HO2 uptake: A novel parameterized equation" by Huang et al

We thank the reviewer for the helpful comments. The referee's comments are first given in black type, followed by our response to each in turn in blue type. Any changes to the manuscript in response to the comments are then given in quotation marks in red type.

The first author of this manuscript is Huan Song, not Huang.

- This manuscript reports an explicit model of uptake of HO2 radicals to deliquesced inorganic aerosol particles to partially reconcile previous inconsistencies among experimental measurements and parameterizations. This includes a detailed treatment of the aqueous phase chemistry of HO2 and superoxide with Cu ions, as well as considering effects of Setchenov salting and ionic strength. The model is also used to interpret data from a field campaign. The previous review rounds already covered the general aspects regarding scientific relevance and significance the topic, which are undoubted. In response to previous comments related to a dataset also included to fit a parameterization, the authors of that dataset have joined the revised version of the paper and this version now includes an updated description of experimental details and revised data analysis related to that dataset. In response to another review, the authors have expanded the model description and the discussion related to sensitivity and uncertainty. Overall, this work provides valuable new information, especially the fact that taking into account the properties of the concentrated solutions of deliquesced aerosol particles allows to calculate HO2 uptake coefficients using known and well documented aqueous peroxy radical chemistry involving Cu ions. While the model includes some complexity by involving links to nitrogen oxides and and sulfur, it lacks inclusion of the interaction with the Fe(II)/Fe(III) redox couple, which usually is associated with the presence of Cu in atmospheric particles and may have important impacts. Nevertheless, the manuscript provides progress in understanding uptake of HO2 to aerosol particles.
- In spite of this being the 2nd revised version of this manuscript, still a number of deficiencies exist that should be addressed. In the comment below, I list the line numbers of the pdf file of the revised manuscript version. In principle, these concerns are rather minor in character, but still numerous. They should be addressed before the manuscript may be accepted for ACP.
 - 1) Language: the new text additions are sometimes misleading, mostly due to deficiencies in the English language. This should be fixed by a thorough work-through by the authors.
 - 2) Abstract line 24: the IUPAC website provides a recommendation for a number of different deliquesced aerosol systems, not only cloud droplets. See also comment further below on the same aspect in the manuscript.

We made the modifications to this aspect in the manuscript. In the abstract line 24, we deleted "for cloud droplets". On line 253, we change the words to "deliquesced aerosol particles" and on line 262, we added the words "proposed for HO₂ uptake for deliquesced aerosol particles" as recommended by the (24) opinion.

And the classical parameterized equation was confirmed by researches of reactive gas molecular uptake on dilute solution droplets (Magi et al., 1997) and on aqueous surfaces (Utter et al., 1992; Müller and Heal, 2002; Hu et al., 1995).

- 3) Line 26: not sure whether it is useful to have the parameterization in the abstract without explanation of symbols.
- 40 We added an instruction in the double brace in the abstract saying the explanations for the symbols are in the Appendix.
 - 4) Line 27: The Wangdu campaign is not something the reader understands without introduction. Either explain in more detail, 'data from a campaign in the Wangdu region', or just 'data from a field campaign'.

We deleted the name of the field campaign on line 27.

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 - 5) Lines 42-45: these sentences should be split up, and the reason for the lower reactivity in absence of transition metals should be explained, including the self reaction of HO2 that has been parameterized by Thornton et al. In addition, a language issue here: The impact of HO2 uptake is not depending on a parameterization. It is the model output, or the calculated response of some parameters to HO2 uptake that changes. This is different.
- We changed this part as:

"The model results of HO_2 uptake influence is lowered when a parameterized equation of γ_{HO_2} is used without considering the influence of transition metal ions (TMIs) (Thornton et al., 2008). The reasons for the lower reactivity in absence of TMI including the lower reaction rate of aqueous HO_2/O_2^- reactions(Thornton et al., 2008). However, in spite of the lower HO_2 uptake coefficient used a significant impact on the calculated [OH] and O_3 production rate are suggested for air masses over Chinese megacity areas (Macintyre and Evans, 2011)."

6) Line 73: symbols used in eq. (1) and (2) need to be explained

We added an instruction in the first of the paragraph saying the explanations for the symbols are in the Appendix.

7) Same paragraph: it does not become clear enough how the uptake coefficient was retrieved from the model output. This should be briefly described here.

We changed the sentences on line 73 as:

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"The model directly calculates the averaged quasi-first order gas phase HO₂ uptake loss rate at steady state, k_{het} (s⁻¹), in Eq. (1). γ_{HO_2} is retrieved by Eq.(2) considering the influence of aerosol liquid water content (ALWC) [g cm⁻³] rather than surface density because of the influence of the *RH* on the uptake process (Kuang et al., 2018; Bian et al., 2014)."

8) Line 106: some numbers should be given here. What is the ratio between H^cc and H_0 over the RH range considered in this study? Same sentence: why does H^cc depend strongly on the Cu concentration? The dominant solute is ammonium sulfate, which should be the main driver of salting and ionic strength, isn't it.

We gave the ratio of H^{cc} to H_0 of HO_2 in the revised MS as follows on the line 106:

"According to this correction, H^{cc} of HO₂ increases with RH. The ratio of H^{cc} to H_0 ranges from 0.03 (40% RH, I=16.7) to 0.34 (80% RH, I=5.5). Although the slating effect and the ionic strength are mainly driven by [NH₄⁺] and [SO₄²⁻], ionic strength increases quickly from 5.9 to 9.5 with [Cu²⁺] from 0.1 M to 1 M and limits the solubility of HO₂ gas molecules."

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- 9) Line 115: Two things here: the solubility of Fe is not a defined quantity, the authors may refer to the solubility of Fecontaining minerals. There are literature reports about what fraction of Fe is typically in dissolved form. In addition, there is a language issue here (many similar cases throughout the manuscript), the sentence reads like the solubility of Fe is related to its ratio to Cu, which is certainly not true.
- 10) Line 118: Neglecting the presence of Fe should lead to a stronger caveat for this work. The authors cite the Mao et al. (2013) work a few times, which clearly indicates a strong impact of the Cu/Fe ratio on the fate of HO2 products in the aqueous phase. Fe may reduce the contribution of recycling of peroxy radicals to lower the effective HO2 loss rate, and Fe might be relevant for the interpretation of the effect of HO2 uptake on the HOx budget in conjunction with the field data.
 - There is no direct evidence of the impact of the Cu/Fe ratio on the fate of HO2 products as proposed by Mao, so in this MS we used the model mechanisms for HO2 uptake to produce H2O as many other papers (Mozurkewich et al., 1987; Hanson et al., 1992; Thornton and Abbatt, 2005; Thornton et al., 2008; Taketani et al., 2009; Macintyre and Evans, 2011). On line 118, we change this part as:

"Since there is no direct evidence of the existence of Cu/Fe redox reactions of HO₂ which produce H₂O rather than H₂O₂ as proposed by (Mao et al., 2013), in the scope of this paper, HO₂ uptake produce H₂O separately by Cu and Fe free ions as proposed by many researches (Mozurkewich et al., 1987; Hanson et al., 1992; Thornton and Abbatt, 2005; Thornton et al., 2008; Taketani et al., 2009; Macintyre and Evans, 2011) and the mechanism summarized by IUPAC. Fe free ions can be seen as the equivalent Cu free ions in the application of the MARK model or the parameterized equation mentioned below."

- 11) Line 135: in eq. (10) and (11), the subscript 'equ' is misleading, since it should refer to 'effective' and not 'equilibrium' or 'equation'. So 'eff' would be better.
- We changed 'equ' to 'eff' in this part and updated the meaning of $[Cu^{2+}]_{eff}$ which is now the sum of effective copper concentration and other TMI equivalent copper concentrations.
- 12) Line 148: this paragraph is not sufficiently clear. k_eff seems to be the apparent first order loss rate coefficient of HO2 in the aqueous phase (not involving solubility). Typical numbers should be provided; otherwise it would not be understandable,

why a 1 M Cu(II) solution would not lead to a very short reacto-diffusive length and thus strong concentration gradients in HO2. Also the reasons for the apparently low values should be explained, as this must result from complex recycling occurring, since the first reaction of Cu(II) with HO2 is very fast.

k_{eff} is the comprehensive liquid phase reaction rate coefficient which encompasses both HO₂ dissolution equilibrium reactions
 and liquid phase chemical-physical reactions during HO₂ uptake process. It is calculated by Eq.19 and include the influence of the salting out effect of HO₂. Typical value is about 2.9×10⁶ M s⁻¹ with 1 M Cu²⁺ and 3.25×10⁴ M s⁻¹ with 0.001M Cu²⁺.
 k_{eff} will change dramatically according to the concentration of equivalent copper ions and the diameter of particles.
 We changed the relevant sentences and recalculated the ratio considering the high copper concentration on line 148 and

We changed the relevant sentences and recalculated the ratio considering the high copper concentration on line 148 and following part:

- "and D_{aq} is the aqueous phase diffusion coefficient [cm²s⁻¹], k_{eff} is the comprehensive liquid phase reaction rate coefficient which encompasses both HO₂ dissolution equilibrium reactions and liquid phase chemical-physical reactions during HO₂ uptake process. k_{eff} is calculated by Eq.19 and includes the influence of the salting out effect of HO₂ and the ionic strength effects on TMI. k_{eff} will change dramatically according to the concentration of equivalent copper ions and the diameter of particles. Higher Cu concentration will make the ratio smaller and cause larger uncertainties, however, in the copper-doped aerosol particle, because of the high value of k_{eff} (typical value is 2.9×10⁶ M s⁻¹ with 1 M Cu²⁺ and 3.25×10⁴ M s⁻¹ with 0.001 M Cu²⁺) and small Count Median Diameter (R_d) (usually smaller than 1 μm), the ratio [[HO₂]/[HO₂(r)] is close to 1. At a diameter of 100nm, and a relative humidity between 40% and 90%, the condensed phase copper ion concentration varies from 10⁻⁵ to 1 M, the average ratio of the surface HO₂ concentration and the condensed phase HO₂ concentration is beyond 0.87 at every Cu concentration. The ratios are calculated by simulation of k_{eff} and the accordingly calculations by Equation (12) and (13).
 Thus, in this model, we assume the surface concentration of HO₂ equals to the condensed phase average HO₂ concentration."
 - 13) Line 158: the value of the accommodation coefficient is not related to the amount of Cu. The amount of Cu may control the uptake regime, with large amounts leading to uptake becoming accommodation limited. But the value of alpha is independent of Cu, unless it is involved in the process of surface to bulk transfer of HO2. Are the authors confusing accommodation coefficient with uptake coefficient? Also Table 1 is misleading, as the data in column seem to be uptake coefficient, as indicated in the Table caption, but inconsistent with the column header.
 - 14) Line 162: probably related to the previous, the high accommodation coefficient for HO2 does not automatically mean it has a high loss rate. It only means that gamma may get large, if a strong sink is available in the condensed phase.
 - 15) Line 164: language: The MARK model probably does not make the selection of alpha, but the authors selected it.

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130 16) Line 167: as mentioned before, please clarify the column header of the table and the caption (alpha or gamma)

The accommodation coefficient is surely not influenced by the concentration of Cu ions if the viscosity of particles maintains.

While the accurate accommodation coefficient can be only measured with no limitation of aqueous mass transfer flux in which

situation, a high aqueous reaction rate. We changed this part in section 2.3 to avoid misleading. We also changed the column header.

- "The accommodation coefficient of HO₂ (α_{HO₂}) is independent of the concentrations of free Cu ions if the viscosity of particles maintains. While the more accurate accommodation coefficient can be only measured with no limitation of aqueous mass transfer flux, in which situation, α_{HO₂} equals to γ_{HO₂}. HO₂ uptake coefficients are summarized for copper-doped inorganic aerosol particles from various previous laboratory studies. The uptake coefficient of HO₂ is approximately 0.5 in sulfate aerosol and even higher for chlorine or nitrate aerosol because of the catalytic effect of Cu²⁺ on aqueous HO₂/O₂- (Table 1). In this situation, the aqueous reactions are fast enough for the uptake process be limited primarily by the mass transport process (accommodation) and the uptake coefficient equals to the accommodation coefficient. Thus, the MARK model typically uses α_{HO₂} as 0.5. We also tested the influence of the accommodation coefficient on calculated HO₂ uptake coefficient in a field campaign, details please see the Supplementary Information."
- 145 17) Line 172: first sentence: language!

We changed the word as "included".

- 18) Line 178: SMPS = Scanning Mobility Particle Sizer or Scanning Mobility Particle Spectrometer
- 19) Line 179: aerosol particles were produced using a ...
- We changed this part as:

- "...and the total aerosol surface area was determined with a Scanning Mobility Particle Sizer (SMPS) at the end of the flow tube. Aerosol particles were produced using a constant output atomizer..."
- 20) Line 198 and following: while the model is indeed used to explore the RH dependence of HO2 uptake and associated aqueous phase chemistry, the comparison to experimental data is not really covering a substantial RH range. So that is essentially limited to the effect of the Cu(II) concentration.
 - At present, there are experimental measurements of γ_{HO_2} at different RH but there is no experimental systematic study of this dependence where only RH is changed. Many researches proposed that γ_{HO_2} is higher for aqueous inorganic aerosol than for dry inorganic aerosol. Although the previous experiments did not directly measure the RH s dependence, the change of the experimental uptake coefficients met the simulation trend (see Figure 2). Ambient RH would affect the activity coefficients of reactant ions in the aerosol particle condensed phase and the solubility of the gas phase reactant such as OH, HO₂ and H₂O₂. The MARK model was presented to simulate the change of the uptake coefficient with RH in Figure 1.
- 21) Line 230: HO2 uptake at low Cu content: the figure should be plotted in log y-scale to demonstrate that the remaining uptake at low Cu content is driven by self reaction of HO2 (should be second order in HO2).

The aim of this MS is to explore the influence of TMI and RH on HO₂ uptake rather than HO₂ aqueous self-reaction mechanism. For this reason, we believe Figure 2 is better now to demonstrate the trend of HO₂ uptake coefficient under different copper ions gradient.

22) Line 231: What does the sentence 'The threshold is also consist in ...' mean? What are droplets?

On line 231 the word should be 'consistent' and the droplets refer to cloud or rain droplets.

determined by the solubility?

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- 23) Line 233: I understand that increasing Cu content drives uptake to the accommodation limit; but why should that be
- We changed the last sentence in the paragraph: "As the copper concentration increasing, the solution ionic strength increases and γ_{HO_2} rapidly rises to the limit of the accommodation coefficient and the limitation of the HO₂ solubility."
 - 24) Line 254: the Thornton et al. (2008) parameterization was developed for deliquesced aerosol particles, not cloud droplets. This repetitively comes up below again.
- 180 25) Line 262 and following: as mentioned above, the Thornton et al. and IUPAC recommendation has not been suggested for dilute aqueous droplets but actually for deliquesced aerosol particles. As discussed in Thornton et al. but also in the comments accompanying the IUPAC recommendations, the fact that k_TMI is lower than the actual known rate coefficient of HO2 or O2- with Cu(II), is assumed to likely result from the combined effects of solute strength effects. It is indeed the added value of this work to make this aspect more quantitative. The authors could emphasize this somewhat more to detail the individual contributions of Setchenov salting, of ionic strength and of the recycling efficiency among the cupper and peroxy species to the reduction of the effective rate coefficient. The advantage of eq 15 is that it correctly represents the transition between the reacto-diffusive regime (when k_eff is higher) to the homogeneous bulk reaction regime covered by the parameterization suggested in this work (eqs 18-21)

Corrections about the word "droplets" to "deliquesced aerosol particles" are done in the revised MS mentions in the response to opinion (2).

We deleted the discussion of the rate constant of Cu^{2+} with HO_2/O_2^- and added the sentence:

"The low reaction rates used here in the *CEq*. are assumed to likely result from the combined effects of solute strength effects as discussed by Lakey et al. (2016)."

The individual contributions are mentioned in the last paragraph of Section 3.3 as:

"The MARK model uses the same framework with the CEq and considers the Setchenov salting out and ionic strength effects on HO₂ uptake more comprehensively and detailly and proposes k_{eff} as the effective reaction coefficient (Eq.19). Considering the small RMSE between the MARK model and the laboratory studies, we proposed a novel parameterized equation (NEq.) to better describe the influence of [Cu²⁺] and RH on γ_{HO_2} .

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26) Line 310 and following: the authors should clearly state that this parameterization is only reasonable as long k_eff remains sufficiently small, such that no HO2 gradients within particles develop. While they seem to show that this is valid with the mechanism involving Cu only, it is not granted that this is still true when for instance including Fe ions in the mechanism which could leading to an increasing sink for HO2 if the recycling efficiency is shut off; similar effects may occur in presence of organics.

In the section 3.5.4 the MS discussed the possible sources of uncertainties of the novel equation including the approximate calculation of HO₂ concentration gradients and the influence of organics. We added the words: "or high copper equivalent concentration." in the first paragraph in this section.

About the influence of Fe ions is answered above.

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Influence of aerosol copper on HO₂ uptake: A novel parameterized equation

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Abstract. Heterogeneous uptake of hydroperoxyl radicals (HO₂) onto aerosols has been proposed to be a significant sink of HOx hence impacting the atmospheric oxidation capacity. Accurate calculation of the HO₂ uptake coefficient γ_{HO_2} is key to quantifying the potential impact of this atmospheric process. Laboratory studies show that γ_{HO_2} can vary by orders of magnitude due to changes in aerosol properties, especially aerosol soluble copper (Cu) concentration and aerosol liquid water content (ALWC). In this study we present a state-of-the-art model called MARK to simulate both gas and aerosol phase chemistry for the uptake of HO₂ onto Cu-doped aerosols. Moreover, a novel parameterization of HO₂ uptake was developed that considers changes in relative humidity (*RH*) and condensed phase Cu ion concentrations and which is based on a model optimization using previously published laboratory and new laboratory data included in this work. This new parametrization would be applicable to wet aerosols and it would complement current IUPAC recommendation—for cloud droplets. The new parameterization is as follows (the explanations for symbols- are in the Appendix):

$$\frac{1}{\gamma_{HO_2}} = \frac{1}{\alpha_{HO_2}} + \frac{3 \times v_{HO_2}}{4 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^{0.65}} + \frac{v_{HO_2} l}{4 RT H_{org} D_{org} \varepsilon} = \frac{1}{2 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^{0.65}} + \frac{v_{HO_2} l}{4 RT H_{org} D_{org} \varepsilon} = \frac{1}{2 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^{0.65}} + \frac{v_{HO_2} l}{4 RT H_{org} D_{org} \varepsilon} = \frac{1}{2 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^{0.65}} + \frac{v_{HO_2} l}{4 RT H_{org} D_{org} \varepsilon} = \frac{1}{2 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^{0.65}} + \frac{v_{HO_2} l}{4 RT H_{org} D_{org} \varepsilon} = \frac{1}{2 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^{0.65}} + \frac{v_{HO_2} l}{4 RT H_{org} D_{org} \varepsilon} = \frac{1}{2 \times 10^6 \times R_d H_{corr} RT \times (5.87 + 3.2 \times \ln(\text{ALWC/[PM]} + 0.067)) \times [\text{PM}]^{-0.2} \times [Cu^{2+}]_{eff}^{0.65} [Cu^{2+}]_{eff}^$$

All parameters used in the paper are summarized in Table A1. Using this new equation, field data from Wangdu-a field campaign were used to evaluate the impact of the HO₂ uptake onto aerosols on the ROx (=OH + HO₂+RO₂) budget. Highly variable values for HO₂ uptake were obtained for North China Plain (median value <0.1).

1 Introduction

The atmospheric cleaning capacity of the troposphere is largely determined by the concentrations of the hydroxyl radical, which are closely linked with the concentrations of the hydroperoxyl (HO₂) radical. In the established chemical mechanism, the coupling of OH and HO₂ is strongly determined by the reaction of OH + VOCs (volatile organic compounds)/CO/HCHO/CH₄/H₂/SO₂ and HO₂ + NO (Seinfeld, 1986). The reactivity from aerosol uptake cannot compete with the known gas phase reactivity of OH, whereas it may compete with the reactivity of NO toward HO₂ under some conditions such as low NO (Tang et al., 2017). For high aerosol mass load, the reaction rate of HO₂ with aerosol particles could be fast enough to influence the concentration of HOx radicals, and consequently, reduce ozone production from HO₂+NO (Kanaya et al., 2009; Li et al., 2019b).

From a global perspective, the impact of HO_2 uptake on the calculated HOx concentrations is diagnosed to be about $10\sim40$ % (Jacob, 2000; Whalley et al., 2015; Whalley et al., 2010; Mao et al., 2010; Li et al., 2019b; Li et al., 2019a) and often the value of γ_{HO_2} (the heterogeneous uptake coefficient (Schwartz, 1984; Schwartz, 1986)) is assumed to be a single value, 0.2 (Tie et al., 2001; Martin et al., 2003). The model results of- impact of-HO₂ uptake influence is lowered when a parameterized equation of γ_{HO_2} is used without considering the influence of transition metal ions (TMIs) (Thornton et al., 2008). The reasons for the lower reactivity in absence of TMI including the lower reaction rate of aqueous HO_2 / O_2 - reactions (Thornton et al., 2008). However, in spite of the lower HO₂ uptake coefficient usedhowever, still, a significant impact on the calculated [OH] and O_3 production rate are suggested for air masses over Chinese megacity areas (Macintyre and Evans, 2011). A model study (Xue et al., 2014) considering the aerosol uptake of HO_2 showed an impact on the simulated HO_2 concentrations and local O_3 production rates in Chinese urban regions: Beijing, Shanghai, and Guangzhou. Furthermore, researchers have proposed that in the North China Plain (Li et al., 2019a; Li et al., 2019b), the reduced HO_2 uptake owing to reduction of aerosol surface area is considered to be the key reason for the increased surface ozone concentration over the last few years when a value of 0.2 was used for γ_{HO_2} .

Previous studies show that the value of γ_{HO_2} from the laboratory, field, and modeling studies spans several orders of magnitude, ranging from <0.002 for dry aerosols (Cooper and Abbatt, 1996; Taketani et al., 2008; George et al., 2013) to 0.2 for liquid deliquesced aerosols. Much higher values of γ_{HO_2} have been measured and calculated for Cu-doped aerosols (Mozurkewich et al., 1987; Taketani et al., 2008; Thornton et al., 2008; Cooper and Abbatt, 1996; Lakey et al., 2016b; George et al., 2013). For fine particles, the reactions of HO₂ with soluble Cu ions may be fast enough, thus the uptake coefficient is limited by the mass accommodation coefficient α . Due to the widespread distribution of Cu²⁺ ion in ambient particles, the absence of an accurate evaluation of γ_{HO_2} is one of the largest uncertainties for the determination of the impact of HO₂ uptake on pressing atmospheric issues such as ozone formation.

In this study, we reanalyzed several datasets of the aerosol uptake of HO_2 from laboratory studies reported in the literature, a new dataset for HO_2 uptake coefficient onto Cu-dopped ammonium sulphate aerosols at 43% relative humidity and proposed a novel parameterized equation (abbreviated as NEq. in the paper) for the prediction of γ_{HO_2} that best fits all the laboratory

results. Furthermore, for Wangdu field campaign, we also calculated γ_{HO_2} according to the NEq. and the impact of HO_2 uptake on HOx (=OH + HO_2) budget was evaluated.

2 Materials and Methods

2.1 The Model

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A Multiphase Reaction Kinetic Model (MARK) is developed in this study for the simulation of γ_{HO2} for the laboratory experiments. The reaction mechanism and reaction rate constants are summarized in Table S.1 – S.4 in the Supplementary Information (SI). The MARK model is currently capable of simulating inorganic deliquescent aerosol at ambient pressure and temperature. The model directly calculates the <u>averaged quasi-first order gas phase HO2</u> uptake loss rate <u>at steady state</u>, k_{het}(s⁻¹), in Eq. (1). γ_{HO2} is retrieved by Eq.(2) considering the influence of In this model, aerosol liquid water content (ALWC) [g cm⁻³] is more pertinent rather than surface density because of the influence of the RH on the uptake process (Kuang et al., 2018; Bian et al., 2014).

$$\frac{d[HO_2]}{dt} = -k_{het} \times [HO_2] \tag{1}$$

$$k_{het} = \left(\frac{R_d}{D_g} + \frac{4}{\gamma v_{HO_2}}\right)^{-1} \times \frac{3ALWC}{\rho R_d}$$
 (2)

The meanings of the symbols are summarized in the Appendix. The units of aqueous reagents are converted to [molecule cm⁻] in the model by k_{mt} . To combine both gas phase molecular diffusion and liquid phase interface mass transport processes the approach adopted is using one variable called k_{mt} (Schwartz, 1984; Schwartz, 1986), which is used in the calculation for gas-liquid multiphase reactions in many modelling studies (Lelieveld and Crutzen, 1991; Chameides and Stelson, 1992; Sander, 1999; Hanson et al., 1994). The definition of k_{mt} is given by equation (3):

$$k_{mt} = \left(\frac{R_d^2}{3D_g} + \frac{4R_d}{3v_{HO_2}\alpha}\right)^{-1} \tag{3}$$

The rate of gas phase reactants (X) diffusing and dissolving to the condensed phase can be calculated in the framework of aqueous phase reactions as $k_{mt_X} \times ALWC$ (where X is the reactant molecule). Moreover, the conversion rate of aqueous phase reactants to gas phase can be calculated as $\frac{k_{mt_X}}{H^{cc} \times RT}$. The unit of k_{mt} is s^{-1} , as k_{mt} contains the conversion from m_{air}^{-3} of the gas phase molecule concentrations to m_{aq}^{-3} of the aqueous phase molecule concentrations and in the other direction. For larger particles (radius >1 μ m), k_{mt} is mainly determined by gas phase diffusion of HO₂. For smaller particles (radius <1 μ m) k_{mt} is mainly determined by the accommodation process. The MARK model can simultaneously simulate gas and liquid two-phase reaction systems in the same framework.

The aerosol particle condensed phase is not an ideal solution. Consequently, an effective Henry's law constant H^{cc} should be applied in the model calculation, that takes into account the effects of solution pH and "salting out" effect in the small gas phase molecule (such as HO₂, OH, O₂ ect.) due to the existence of electrolytes in the solution (Ross and Noone, 1991). This study uses the ISORROPIA II thermodynamic model (Fountoukis and Nenes, 2007) to calculate the ALWC and components

concentrations for metastable deliquescent aerosols. The effective Cu²⁺ concentration in the aqueous phase, which is strongly influenced by non-ideal solution ionic strength, is also calculated following Ross and Noone (Ross and Noone, 1991).

2.2 Corrections to γ_{HO_2} in the MARK model

2.2.1 Henry's law of gas phase reactants

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The aerosol particle condensed phase solution is not an ideal solution as commented before. The addition of an electrolyte to water interferes with the gas dissolution and the organization of water molecules around the gas. This frequently results in a decrease in the solubility, or a "salting out" effect. This salting out effect is frequently a linear function of the molar ionic strength *I. H*₀ is estimated to be about 3900 M atm⁻¹ at 298K for HO₂ (Thornton et al., 2008; Golden et al., 1990; Hanson et al., 1992) and its temperature dependence is given accordingly to the IUPAC recommendation (Ammann et al., 2013;IUPAC Task Group on Atmospheric Chemical Kinetic Data Evaluation, http://iupac.pole-ether.fr.). *H*₀ should be corrected by the solution pH and the "salting out" effect. In the MARK model, these two corrections are incorporated as *H*^{cc}:

$$H^{cc} = H_0 \times \left(1 + \frac{\kappa_{eq}}{|H+1|}\right) \times A_{HO_2} = 9.5 \times 10^{-6} \exp\left(\frac{5910}{T}\right) \times \left(1 + \frac{\kappa_{eq}}{|H+1|}\right) \times A_{HO_2}$$
 (4)

The activity coefficient A for HO_2 and other neutral small molecules such as H_2O_2 and O_2 can be expressed as (Ross and Noone, 1991):

$$A = 10^{-0.1 \times I} \tag{5}$$

According to this correction, H^{cc} of HO₂ increases with RH. The ratio of $-H^{cc}$ to H_0 ranges from 0.03 (40% RH, I=16.7) to 0.34 (80% RH, I=5.5). Although the slating effect and the ionic strength are mainly driven by $[NH_4^+]$ and $[SO_4^{2^-}]$, ionic strength increases quickly from 5.9 to 9.5 with $[Cu^{2+}]$ from 0.1 M to 1 M and limits the solubility of HO₂ gas molecules.

and decreases quickly after [Cu²⁺] reaches 0.1M in aerosol liquid phase, which limits

 γ_{HO_2} at high Cu²⁺ concentration.

2.2.2 Aerosol particle condensed phase Cu²⁺ molality calculation

Inorganic species in ambient aerosol particles may be in the form of aqueous ions, or in the form of precipitated solids in thermodynamic equilibrium with atmospheric gases and water vapor. The salts in the metastable aerosol are all dissolved in the aqueous phase. For meta-stable aerosols, this paper uses thermodynamic models to calculate ALWC and aerosol particle condensed phase component concentrations. In this work ISORROPIA II (Fountoukis and Nenes, 2007; Capps et al., 2012) thermodynamic equilibrium model for inorganic aerosol systems is used to take into account this.

At low relative humidity, the aqueous phase is highly concentrated (i.e. with a high ionic strength), and the solution is strongly non-ideal, consequently the activity coefficient and "salting out" effect must be taken into account for calculation of aerosol chemistry. The ion activity coefficient refers to the effective concentration of ions participating in an electrochemical reaction in an electrolyte solution.

Since there is no direct evidence of the existence of Cu/Fe redox reactions of HO₂ which produce H₂O rather than H₂O₂ as proposed by (Mao et al., 2013), in the scope of this paper, HO₂ uptake produce H₂O separately by Cu and Fe free ions as proposed by many researches (Mozurkewich et al., 1987; Hanson et al., 1992; Thornton and Abbatt, 2005a; Thornton et al., 2008; Taketani et al., 2009; Macintyre and Evans, 2011). Fe free ions can be seen as the equivalent Cu free ions in the application of the MARK model or the parameterized equation mentioned below.

Based on Ross and Noone (Ross and Noone, 1991), for an ion (x_i) of charge z_i (i=x,y,z...), the activity coefficient (φ_x) is

$$\log \varphi_x = -z_x^2 D - \sum_{v} \varepsilon(x, y, I) m_v \tag{6}$$

where D is given by equation (7):

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$$375 \quad D = \frac{0.5109\sqrt{I}}{1+1.5\sqrt{I}} \tag{7}$$

I is the ionic strength of a solution [M], which can be calculated as following equation:

$$I = \frac{1}{2} \cdot \sum m_i \cdot z_i^2 \tag{8}$$

 $\varepsilon(x, y, I)$ is referred to as "interaction coefficients", and the summation extends over all ions (y) in the solution at a molality of m_y . For ions of similar charge, $\varepsilon(x, y, I)$ is set to zero. For ions of unequal charge, $\varepsilon(x, y, I)$ may be calculated from the logarithm solution mean activity coefficient $log(A_{\pm})$ (Clegg et al., 1998) of the single electrolyte at the same I according equation (9):

$$\varepsilon(x,y,I) = \frac{(\log(A_{\pm}) + z_x z_y D)(z_x + z_y)^2}{4I} \tag{9}$$

In the condensed phase of aerosol particle, the effective molality of an ion x_i ($[x_i]_{equif}$) can be calculated as:

$$[x_i]_{equif} = [x_i] \times \varphi_{xi} \tag{10}$$

In the aerosol particle condensed phase, an effective concentration rather than the total concentration of Cu ion should be calculated in catalytic aqueous reactions with HO_2 . The effective concentration of Cu ion TMI can be calculated as:

$$[Cu^{2+}]_{equeff} = ([Cu^{2+}] + [Cu^{2+}]_{equ}) \times \varphi_{Cu}$$
(11)

 $[Cu^{2+}]_{eff}$ is the <u>effective</u> aerosol condensed phase soluble copper concentration. In this paper, $[Cu]_{equ}$ represents the equivalent copper concentrations from other TMI such as Fe and Mn.

390 2.2.3 The conversion formula of $[\overline{\textit{HO}_2}]$ and $[\textit{HO}_{2(r)}]$

Gas phase HO_2 molecules dissolve in the particle condensed phase and diffuse from the surface of a particle toward the center in parallel with aqueous phase reactions. We need to evaluate $[\overline{HO_2}]$, the assumed averaged steady-state HO_2 concentration over the volume of the particle. $[HO_{2(r)}]$ is HO_2 concentration at the surface of particles. The ratio of these two concentrations can be calculated as (Schwartz, 1986; Schwartz, 1984):

$$395 \quad \frac{[\overline{HO_2}]}{[HO_{2(r)}]} = 3 \times (\frac{\coth(q)}{q} - \frac{1}{q^2}) \tag{12}$$

where q is given by equation (13):

$$q = R_d \times \left(\frac{k_{eff}}{p_{ag}}\right)^{0.5} \tag{13}$$

and D_{aq} is the aqueous phase diffusion coefficient [cm²s⁻¹], k_{eff} is the comprehensive liquid phase reaction rate coefficient which encompasses both HO₂ dissolution equilibrium reactions and liquid phase chemical-physical reactions during HO₂ uptake process. k_{eff} is calculated by Eq.19 and includes the influence of the salting out effect of HO₂ and the ionic strength effects on TML k_{eff} will change dramatically according to the concentration of equivalent copper ions and the diameter of particles. Higher Cu concentration will make the ratio smaller and cause larger uncertainties, however, iIn the copper-doped aerosol particle, because of the high value of k_{eff} (typical value is 2.9×10^6 M s⁻¹ with 1 M Cu²+ and 3.25×10^4 M s⁻¹ with 0.001 M Cu²+) and small Count Median Diameter (R_d) (usually smaller than 1 µm), the ratio $\frac{[HO_2]}{[HO_{2(r)}]}$ is close to 1. At a diameter of 1 µm 100nm, and a relative humidity between 40% and 90%, the condensed phase copper ion concentration varies from 10⁻⁵ to 1 M, the average ratio of the surface HO₂ concentration and the condensed phase HO₂ concentration is beyond 0.87 at every Cu concentration.0.89. At 400_nm diameter particles for RH = 40% to 90%, the ratio is larger than 0.95. The ratios are calculated by simulation of k_{eff} and the accordingly calculations by Equation (12) and (13). Thus, in this model, we assume the surface concentration of HO₂ equals to the condensed phase average HO₂ concentration.

410 2.3 Laboratory results for the HO₂ accommodation coefficient

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The accommodation coefficient of $HO_2(\alpha_{HO_2})$ used in the model-is independent of the concentrations of free Cu ions if the viscosity of particles maintains. While the more accurate accommodation coefficient can be only measured with no limitation of aqueous mass transfer flux, in which situation, α_{HO_2} equals to γ_{HO_2} . HO_2 uptake coefficients are summarized was determined for copper-doped inorganic aerosol particles using values taken from various previous laboratory studies. The uptake coefficient of HO_2 is accommodation coefficient of HO_2 (α_{HO_2}) is approximately 0.5 in sulfate aerosol and even higher for chlorine or nitrate aerosol because of the catalytic effect of Cu^{2+} on aqueous HO_2/O_2 . (Table 1). In this situation, the aqueous reactions are fast enough for the uptake process be limited primarily by the mass transport process (accommodation) and the uptake coefficient equals to the accommodation coefficient. τ With the wide distribution of Cu^{2+} in aerosol particles, a high accommodation coefficient of HO_2 presents the possibility of HO_2 uptake as an important sink of HO_3 radicals. According to existing research results, the upper limitation of α_{HO_2} with aqueous sulfate aerosol particles is around 0.5. Thus, the MARK model typically selects uses the accommodation coefficient α_{HO_2} as 0.5. We also tested the influence of the accommodation coefficient on calculated HO_2 uptake coefficient in a field campaign, details please see the Supplementary Information.

Table 1: γ_{HO_2} determined under laboratory conditions for copper-doped inorganic aerosols.

Aerosol type	RH/%	Estimation of [Cu] in aerosol (mol L-1)	$\gamma_{HO_2} \alpha_{\overline{HO_2}}$	Ref.
NH ₄ HSO ₄	75%	0.0059-0.067*	0.40+0.21	(Mozurkewich et al., 1987)
(NH ₄) ₂ SO ₄	45%	0.5	0.53±0.13	(Taketani et al., 2008)
(NH ₄) ₂ SO ₄	42%	0.16	0.5 ± 0.1	(Thornton and Abbatt, 2005b)
$(NH_4)_2SO_4$	53-65%	0.5-0.7*	0.4±0.3	(George et al., 2013)
$(NH_4)_2SO_4$	65%	0.57	0.26 ± 0.02	(Lakey et al., 2016b)
$(NH_4)_2SO_4$	51%	0.0027	0.096±0.024	(Zou et al., 2019)
$(NH_4)_2SO_4$	43%	0.38	0.355 ± 0.023	This work
NaCl	53%	~0.5	0.65 ± 0.17	(Taketani et al., 2008)
KCl	75%	5% of KCl solution	0.55 ± 0.19	(Taketani et al., 2009)
LiNO ₃	75%	0.03-0.0063*	0.94 ± 0.5	(Mozurkewich et al., 1987)

^{*}Cu concentration is in molality (M).

2.4 The experimental setup and methodology of the latest results of γ_{HO_2}

In this study, we also conclude included the latest results which measured at Leeds. The experimental setup and methodology used to make the new measurements of $\gamma(HO_2)$ reported here have been described in detail elsewhere (Moon et al., 2018; Lakey et al., 2016b; George et al., 2013) and so only brief details are given here. In summary, the experiments were performed by moving an HO₂ injector backwards and forwards along the concentric axis of a laminar aerosol flow tube hence changing the contact time between HO₂ and the aerosols. Measurements of [HO₂] were performed using laser induced fluorescence (LIF) spectroscopy at low-pressure (the fluorescence assay by gas expansion (FAGE) technique (Heard and Pilling, 2003)) and the total aerosol surface area was determined with a Size-Scanning Mobility Particle Sizer (SMPS) at the end of the flow tube. Aerosol particless-were formed produced using a constant output atomiser (TSI, 3076) and the aerosol concentration and hence surface area could be varied, being controlled using a high efficiency particulate air (HEPA) filter in a bypass arrangement. Atomiser solutions were prepared by dissolving 0.01 moles of ammonium sulphate (AS) (Fisher scientific, >99%) with varying amounts of copper (II) sulphate (Fisher scientific, >98%) in 500 mL of Milli-Q water. The data were analysed as described in George et al 2013. The pseudo first-order loss rate coefficient (k') was obtained from the gradient of a plot of ln(HO₂ signal) against the interaction time between HO₂ and the aerosol before sampling by the FAGE detector. The uptake coefficient $(\gamma(HO_2))$ was obtained from the linear least-squares gradient of the plot of k' against the surface area concentration of aerosols in the flow tube. The error given on all measurements of $\gamma(HO_2)$ represents 2σ of the uncertainty of the fitted gradient. A correction to k' was applied to taking into account non-plug flow conditions in the flow tube using the Brown method.

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3 Results and Discussion

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3.1 Parameter sensitivity analysis of the MARK model

Hygroscopic inorganic particles are one of the most important components of PM_{2.5} in ambient air. The annual average contribution of inorganic aerosol to PM_{2.5} is between 25% and 48% across China (Tao et al., 2017), especially NH₄⁺, SO₄²⁻, NO₃⁻ and other inorganic ions. In laboratory studies of radical heterogeneous reactions, (NH₄)₂SO₄ aerosol is most widely studied because of its simple components, easy way to generate and as they are important component for urban aerosols (Cheng et al., 2012; Yin et al., 2005). A simplified approach was used to explore the mechanism of HO₂ heterogeneous uptake to derive a parameterized equation for the uptake coefficient, γ_{HO_2} .

In this study, (NH₄)₂SO₄ aerosol uptake reactions of HO₂ are simulated by the MARK model, and good correlation between simulation results and experimental results are obtained especially considering the influence of both [Cu²⁺] and RH (for the lack of measured data the parameterized equation is only valid in the range of 40% to 90% RH).

Figure 1 shows the influences of both factors, RH and condensed phase pH together with Cu^{+2} concentration on the heterogeneous process of HO_2 . As the RH rises, the γ_{HO_2} exhibits a logarithmic growth. Higher RH means a higher water content which dilutes the bulk phase ions thus promotes the activity coefficients of reactant ions in the aerosol particle condensed phase and the solubility of the gas phase reactant such as OH, HO_2 and H_2O_2 .

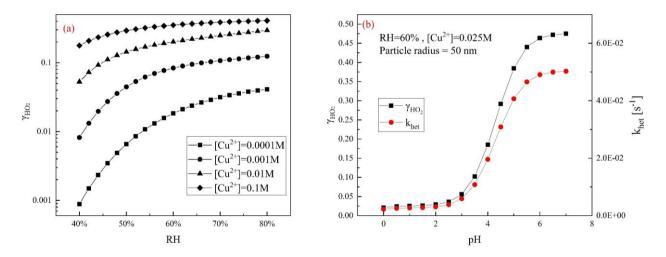


Figure 1: Influence of various parameters upon γ_{HO_2} predicted by the MARK model. (a) γ_{HO_2} increases with the *RH* at different [Cu²⁺]; (b) γ_{HO_2} denoted by black squares and black line and k_{het} in red circles and red line increase with aerosol particle condensed phase pH.

 γ_{HO_2} presents a sigmoid-shaped growth with aerosol particle condensed phase pH. In the model, it is found that as the pH rises, the uptake coefficient rises rapidly because HO₂ is a weak acid (pKa = 4.7) and has a low solubility in an acidic environment. The higher condensed phase pH is favorable for the dissolution equilibrium of the gas phase HO₂. This trend is consistent with the observed second-order rate constant of HO₂/O₂⁻ reviewed by Bielski et al. 1985 (Bielski et al., 1985). Moreover, aqueous phase reaction rates of HO₂/O₂⁻ and Cu²⁺/Cu⁺ increase with the increasing of condensed phase pH because in an alkaline environment HO₂ is more dissociated to O₂⁻ which has quicker reaction rate with Cu²⁺/Cu⁺. The pH of the ambient atmospheric aerosol is measured generally below 5 even when the concentration of NH₃ is high as in Beijing and Xi'an (Ding et al., 2019; Guo et al., 2017) with a range of 3-5. At this range, γ_{HO_2} is highly affected by aerosol condensed phase pH mainly because of the change of HO₂ solubility.

3.2 Model Validation

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Although the MARK model simulation results in this paper are not obtained by adjusting parameters to fit the experimental data points, the MARK model fitted well with these results under different ambient RH and Cu^{2+} concentrations.

At present, there are experimental measurements of γ_{HO_2} at different RH (Thornton et al., 2008; Taketani et al., 2008, 2009; Taketani and Kanaya, 2010; Taketani et al., 2012; Matthews et al., 2014; Thornton and Abbatt, 2005b) but there is no an experimental systematic study of this dependence where only RH is changed and not other parameters. Many researches proposed that γ_{HO_2} is higher for aqueous inorganic aerosol than for dry inorganic aerosol. Although the previous experiments did not directly measure the dependence of RH, the change of the uptake coefficient met the simulation trend (see Figure 2). For hygroscopic inorganic aerosols, *RH* significantly affects the aerosol liquid water content, changing its ionic strength, aqueous reagent activity coefficients, and the solubility of the gas phase reactant such as OH, HO₂ and H₂O₂.

Aerosol condensed phase copper ion concentration is another important factor of HO_2 uptake by adjusting the aqueous reaction rates between HO_2/O_2^- and Cu. As shown in Fig. 2. when the condensed phase copper ion concentration is less than $1-2\times10^{-4}$ M, the heterogeneous uptake of HO_2 is not significant and may mainly be driven by the self-reation of HO_2 . This threshold is consistent with the results of previous researches (Mozurkewich et al., 1987; Lakey et al., 2016b). The threshold is also consistent in different heterogeneous media of aerosol and cloud or rain droplets. As the copper concentration increasinges, the solution ionic strength increases and γ_{HO_2} rapidly rises to the limit of the accommodation coefficient-and determined by the limitation of the HO_2 solubility.

What is more, laboratory measurement uncertainties will directly influence the evaluation of the deviation between the modelled HO₂ uptake coefficient and the measured results because all the parameters inputted in the MARK model are in reference to the measurement conditions. However, it is difficult to calculate the detailed uncertainties from all factors that influence γ_{HO_2} because of the nonlinear reaction system. Uncertainties of the experimental conditions such as RH and particle diameters are combined into the reported values of γ_{HO_2} . Taking all these into account, we calculated an averaged uncertainty for the experimental values of γ_{HO_2} in different ranges of Cu ions concentration. Laboratory measurement uncertainty has the

largest value of 35.1% in the range of 1×10^{-4} to 0.01 M soluble copper concentration, 14.9% below 1×10^{-4} M and 9.3% higher than 0.01 M. In general, good agreement is achieved between the MARK model results and the results of the previous laboratory studies, which were also classified based on a statistical parameter: root mean square error (RMSE) (Figure 2). In this paper, the relative error of each measured data point is considered to calculate the weighted average in RMSE:

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n} (\left(\log_{10}^{u_{i}^{i}_{measured}} - \log_{10}^{u_{i}^{i}_{model}}\right)^{2} (\omega_{i})^{2})}{\sum_{i=1}^{n} (\omega_{i})^{2} \cdot n}}$$
(14)

 $u_{i_{model}}$ is the MARK model result at each Cu²⁺ concentration and RH, $u_{i_{measured}}$ is the central value of each measurement result and ω_i is its corresponding relative error.

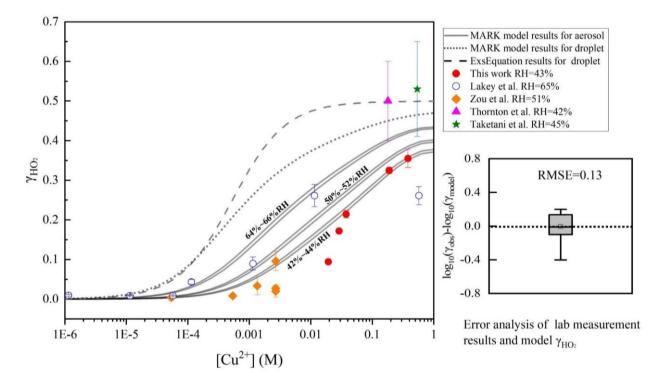


Figure 2: Dependence of γ_{HO_2} on aerosol copper concentration. Red filled circles denote the results at 43% RH measured at Leeds included in this paper. Blue hollow circles at 65% RH (Lakey et al., 2016b). Yellow filled diamonds denote results at 51% RH (Zou et al., 2019), filled purple triangle at 42% RH (Thornton and Abbatt, 2005b) and filled green star at 45% RH (Taketani et al., 2008). The grey dashed line denotes the results of the classical parameterized equation- (named as CEq. in this paper) γ_{HO_2} with <u>deliquesced aerosol particles dilute solution droplets</u> (Thornton et al., 2008; Hanson et al., 1992; Hanson et al., 1994; Jacob, 2000; Kolb et al., 1995), which was confirmed by researches of reactive gas molecular uptake on dilute solution droplets (Magi et al., 1997) and on aqueous surfaces (Utter et al., 1992; Müller and Heal, 2002; Hu et al., 1995). The

solid grey lines represent the model results of the MARK model in this study at various *RH* (two lines represent the range of *RH* from 64% to 66%, 50% to 52% and 42% to 44%) and the short dotted line represents the result in the MARK model of HO₂ with dilute solution droplets. The root mean square error (RMSE) between the MARK modelled values and the full dataset is 0.13. The aerosol pH is set as 4.5 based on the aqion 7.0.8 interface considering the participation of Cu ion (for details please see https://www.aqion.de/).

3.3 Comparison of the classical parameterized equation and the MARK model

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The classical parameterized equation (*CEq.*) (Thornton et al., 2008; Hanson et al., 1992; Hanson et al., 1994; Jacob, 2000; Kolb et al., 1995; Ammann et al., 2013; IUPAC Task Group on Atmospheric Chemical Kinetic Data Evaluation, http://iupac.pole-ether.fr.) proposed for HO₂ uptake for deliquesced aerosol particles—has been proved to provide good estimation of reactive gas molecular uptake coefficient on dilute solution droplets (Magi et al., 1997) and on aqueous surfaces (Utter et al., 1992; Müller and Heal, 2002; Hu et al., 1995). ÷

$$\frac{1}{\gamma_{HO_2}} = \frac{1}{\alpha_{HO_2}} + \frac{v_{HO_2}}{4H_{corr}RT\sqrt{D_{aq}k_{TMI}[TMI]}[coth(\frac{R_d}{l_{rd}} - (\frac{l_{rd}}{R_d}))]}}$$
(15)

$$l_{rd} = \sqrt{\frac{D_{aq}}{k_{TMI}[TMI]}} \tag{16}$$

When the classical parameterized equation (*CEq*.) is applied to the calculate HO₂ uptake coefficient with copper-doped aerosol, *CEq* has higher deviation of γ_{HO₂} between the measured results compared to the MARK model. All input parameters are the same except that the MARK model involved more liquid phase reactions instead of only considering the second order rate coefficient (*k*_{TMI}) of HO₂ and O₂⁻ with transition metal ions as the *CEq*. did. *k*_{TMI} is the most important parameter in the calculation of uptake coefficient. Based on the research by Bielski in 1985 (Bielski et al., 1985), we used the effective rate constant of HO_{2_total} (=HO_{2(aq)}+ O_{2^-(aq)}) with Cu ions as 1.5×10⁷ M⁻¹ s⁻¹ rather than the more commonly used value of 1×10⁹ M⁻¹ s⁻¹ considering the pH limitation (pH is about 3-5 in ambient aerosol particle condensed phase as discussed above). The prior value (1.5×10⁷ M⁻¹ s⁻¹) reflects the rate of reaction between HO₂ and Cu²⁺, more prevalent in acidic aerosol such as ammonium sulfphate, and the latter (1×10⁹ M⁻¹ s⁻¹) between O₂- and Cu²⁺ ions, which is more prevalent in aerosols with a pH greater than the *pK_a* of HO₂, such as NaCl (Bielski et al., 1985). This treatment within the calculation can bring predictions more in line with experimental results in the *CEq*. as shown in the dashed line in Figure 2.

IUPAC (Ammann et al., 2013;IUPAC Task Group on Atmospheric Chemical Kinetic Data Evaluation, http://iupac.pole-ether.fr.) proposed the effective rate coefficient k^1 for the reaction of HO_{2_total} (= $HO_{2(aq)}$ + $O_{2^-(aq)}$) with Cu ions as $5x10^5$ M⁻¹ s⁻¹ to achieve the best fit based on the calculation results from Lakey et al. (2016b). This assumption is not in accordance with the aqueous reaction rate coefficient from other databases mentioned below and needs further laboratory measurements to confirm it. According to the aqueous reaction rate coefficient from NIST and the latest measurement result (Lundström et al., 2004;

Huie, 2003), the rate coefficient of HO₂ with Cu²⁺ is 1×10^8 or 1.2×10^9 M⁻¹ s⁻¹ at pH= 2 and pH=1, respectively. These two rate coefficients were quantified in a low pH environment (pH=2 for 1.2×10^9 M⁻¹ s⁻¹ and pH=1 for 1×10^8 M⁻¹ s⁻¹). At the same time, the reaction rate of O₂⁻ with Cu²⁺ is 8×10^9 M⁻¹ s⁻¹ for pH in the range 3 6.5 (Huie, 2003). At higher pH, the reaction rate of HO₂ with Cu²⁺ may change, but it is unknown whether it will decrease by four orders of magnitude. Further kinetics experiments are needed at varying pH to verify the reaction rate coefficient of Cu²⁺ ions with HO₂ and O₂⁻ in aqueous solution. The low reaction rates used here in the *CEq*, are assumed to likely result from the combined effects of solute strength effects as discussed by Lakey et al. (2016b). The MARK model uses the same framework with the *CEq* and zonsiders the Setchenov salting out and ionic strength effects on HO₂ uptake more comprehensively and detailly and proposes k_{eff} as the effective reaction coefficient (Eq.19).

The rate constants used in the MARK model are shown in the Table S. 1 in the SI. The reaction rate of Cu²⁺ with HO₂/O₂ is 1×10⁸ and 8×10⁹ M⁻¹ s⁻¹ in the MARK model. We also test the MARK model with dilute solution droplets as shown in Figure 2 the short dotted line.

The classical parameterized equation (CEq.) is more applicable to calculate uptake coefficient of reactive gas molecular with diluted solution droplets such as cloud or rain droplets. The MARK model uses the same framework with the CEq, and considered more parameters influencing uptake process such as the activity coefficients of reactive reagents and the effects of valence states in aerosol particle condensed phase. Considering the small RMSE between the MARK model and the laboratory studies, we proposed a novel parameterized equation (NEq.) to better describe the influence of [Cu^{2+}] and RH on γ_{HO_2} .

3.4 A novel parameterized equation of γ_{HO_2}

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When the full reaction system reaches steady-state, the reaction of HO₂ in the aqueous particle phase can be expressed as the following reaction scheme (Schwartz, 1984; Schwartz and Freiberg, 1981; Schwartz, 1987):

$$HO_{2(q)} \rightleftharpoons HO_{2(r)} \rightleftharpoons HO_{2(q)} \xrightarrow{k_{eff}} Products$$
 (17)

Gas phase $HO_{2(g)}$ molecule transports onto the surface of the aerosol particles, $HO_{2(r)}$ then dissolves at the condensed phase to give $HO_{2(a)}$. The reactions between Cu^{2+}/Cu^{+} and HO_{2} can be seen as catalytic reactions, because in the model simulations, the total amount of $[Cu^{2+}]_{+}[Cu^{+}]$ does not change with reaction time. The rate of HO_{2} aqueous reaction with copper ions is noted as k_{eff} . For fine particles, we can safely assume that the interface concentration $[HO_{2(r)}]$ is equal to the condensed phase average $[HO_{2}]$ concentration due to rapid diffusion in the liquid phase (details have been discussed in section 2.2.3). For the submicrometer aerosol particles with which most uptake reaction occurs, the influence of the gas phase diffusion limitation can be neglected. Hanson et al. (1994) proposed the definition of the uptake coefficient as $\gamma = \alpha(1 - \frac{c_{a,surf}}{H^{cc}c_{g,surf}})$ where $c_{a,surf}$ is the suface concentration of the reactant, $c_{g,surf}$ is the gas phase concentration. In the process of HO_{2} uptake, we deduce the

parameterized equation (NEq.) of γ_{HO_2} in the framework of the resistance model:

$$\frac{1}{\gamma} = \frac{1}{\alpha_{HO_2}} + \frac{3 \times \nu_{HO_2}}{4 \times R_d \times H_{corr} \times RT k_{eff}} \tag{18}$$

$$k_{eff} = f(ALWC, PM) \times [Cu^{2+}]_{eff}^{0.65}$$
(19)

$$f(ALWC, PM) = 10^6 \times (5.87 + 3.2 \times ln\left(\frac{ALWC}{[PM]} + 0.067\right)) \times [PM]^{-0.2}$$
 (20)

$$580 \quad \frac{|Cu^{2+}|_{equ} - |Cu^{2+}|^{\varphi} - |Cu^{2+}|^{0.65}}{(21)}$$

From Eq.–(18), it can be deduced that γ_{HO_2} can be calculated by optimizing k_{eff} under different ambient environmental conditions from the MARK model results. The MIPFIT model (Markwardt, 2009; Lewis et al., 2009) in the IDL software program is used to optimize k_{eff} using the Levenberg-Marquardt algorithm. Because the equation is empirical, the initial value of k_{eff} is set as 1. k_{eff} is related to the $[Cu^{2+}]_{eff}$ which is the sum of condensed phase soluble copper concentration $[Cu^{2+}]_{eff}$ and other equivalent copper –concentrations mentioned Eq.11 with an exponential relationship to the parameterization of the catalytic reactions, which is denoted in Eq. (19). The exponent of $[Cu^{2+}]_{eff}$ is globally fitted using the MIPFIT method. It is found that the overall R^2 is higher than 0.97 and the residual is minimized when the exponent is 0.65. f(ALWC, [PM]) has a negative exponential relationship to [PM], and has a positive linear relationship to RH.

We further calculated the RMSE of the modeled data and NEq. (Eq.15) data under different RH conditions. The range of values shows the difference between the modeled data and NEq. data at different Cu^{2+} concentration.— At low RH and consequently relatively low ALWC, γ_{HO_2} is more sensitive to $[Cu^{2+}]$ especially at low $[Cu^{2+}]$. This sensitivity cannot be fully represented in the parameterized equation. What is more, at low $[Cu^{2+}]$ and low RH, the value of γ_{HO_2} is smaller than in other conditions, so that the uncertainty of γ_{HO_2} becomes larger.

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All the RMSE values are smaller than 0.2, which indicates a minor deviation from the laboratory results in our γ_{HO_2} equation. In the typical ambient urban atmospheric environment, with an aerosol mass concentration of 10-300 µg m⁻³, aqueous Cu²⁺ concentration of 10^{-5} -1 molar concentration, and a relative humidity between 40%-90%, the *NEq*. can be used. Beyond the range, the application of the *NEq*. may cause a large deviation. The HO₂ uptake under dry conditions needs further investigation in the future, but probably it is not of high priority because the effective reaction volume becomes 10% or less of the aerosol volume for dry conditions and the HO₂ uptake may then be neglected for typical tropospheric conditions (Taketani et al., 2008; Kanaya et al., 2009; Taketani and Kanaya, 2010; Thornton et al., 2008; George et al., 2013).

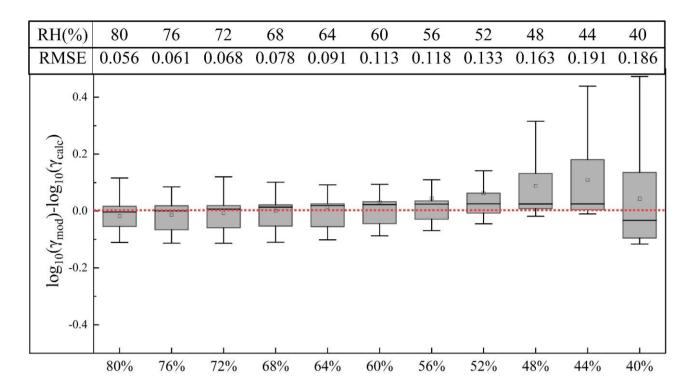


Figure 3: Comparison of the MARK modeled γ_{HO_2} to the corresponding calculated values from the $NEq.\ log_{10}(\gamma_{mod})$ is the logarithmic value of modeled γ_{HO_2} and $log_{10}(\gamma_{cal})$ is the calculated value from the NEq.

3.5 Evaluation of the impact of the new HO₂ uptake parametrization in the Wangdu campaign

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Many model studies (Lakey et al., 2015; Martinez et al., 2003; Tie et al., 2001; Whalley et al., 2015) suggest that heterogeneous uptake of HO₂ radical affects the global distribution of trace gases and the atmospheric oxidant capacity especially in regions with high aerosol loading or low NOx concentration. The importance of aerosol chemistry as a sink for ozone precursors in North China Plain has been suggested in many model studies (Li et al., 2019b; Lou et al., 2014). The competition of HO₂ with aerosol and gas phase reactants is crucial when evaluating the influence of heterogeneous reactions on the atmospheric oxidant capacity.

Based on the results of a comprehensive field campaign performed in summer 2014 in a rural site (Wangdu) in the North China Plain(Tan et al., 2020), the HO₂ uptake coefficient and the ratios of the HO₂ uptake loss rates ($TR_{HO2uptake}$) to the sum of the ROx termination rates ($TR_{ROxsinks}$) are calculated with direct measurements of the ROx radicals, trace gas species, ALWC and the aerosol condensed phase component concentrations (please see the SI for details). The experimental determined ROx termination rates include reaction channels from OH + NO₂, OH + NO, HO₂ + HO₂, HO₂ + RO₂ and RO₂ + NO. Considering

the solubility and size distribution of particle metal copper (Fang et al., 2017; Hsu et al., 2010a; Mao et al., 2013) we can estimate γ_{HO_2} in daytime and night.

3.5.1 Average results of observed meteorological parameters and trace gases concentration in the Wangdu campaign

Wangdu is located in the center of the Beijing-Tianjin-Hebei area and it is a regional site. The observations were carried out in the summer with serious photochemical smog pollution events (Tan et al., 2017; Tan et al., 2020). Table 2 summarizes the meteorological and chemical conditions in this field campaign. In terms of parameters such as temperature, pressure and relative humidity, the Wangdu area is a high-temperature and high-humidity environment with a monsoon climate.

Table 2: Average daytime results of observed meteorological parameters and trace gases concentration in Wangdu campaign from June 10th, 2014 to July 6th, 2014.

Parameters	Average values	1σ Accuracy
Temperature /°C	27 ±4	±0.05%
Pressure /hPa	1000 ± 5	$\pm 0.05\%$
RH/%	61 ±18	$\pm 0.05\%$
O ₃ /ppb	55.6±9.0	<u>±</u> 5%
NO _x /ppb	10±13.6	±20%
HONO/ppb	0.8 ± 0.24	±20%
CO/ppm	0.6 ± 0.19	<5%
Isoprene/ppb	0.5 ± 0.11	±15%-20%
HCHO/ppb	7±0.69	±5%

3.5.2 Calculation of soluble copper ion concentration

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During this campaign, the total concentration of heavy metal ions in fine particles (smaller than 2.5μ m) was measured using a commercial instrument based on non-destructive X-ray fluorescence technique (Xact 625, Cooper Environmental). Since the concentration of soluble copper concentration rather than total copper concentration is used in the model, it is necessary to analyze the ratio of soluble copper to total copper in the aerosol particles. For particle radius smaller than 2.5μ m, which are the most contributing bins of aerosols in HO₂ uptake, the mass fraction of Cu is about 33% –100% compared with other two size bins in ambient aerosols ($2.5-10 \mu$ m, $>10\mu$ m) (Mao et al., 2013). According to previous research results, the dissolution ratio of copper in aerosol particles varies from 20% to 70% in different regions, being solubility lower in smaller particles (Fang et al., 2017; Hsu et al., 2004; Hsu et al., 2010b). Therefore, when using the *NEq.* to calculate the HO₂ heterogeneous uptake coefficient, it is necessary to reduce the copper concentration considering the solubility and the distribution in the

accumulation mode of aerosol particles. We take 50% copper is soluble in the particle condensed phase and 50% copper is in the accumulation mode. Thus, we assume 25% of total aerosol metal copper concentration is soluble in the accumulation mode when calculating γ_{HO_2} in Wangdu campaign. The hourly resolution total copper concentration (ng m⁻³) is divided by the aerosol volume concentration and the atomic mass of copper (64) to obtain the total copper molar concentration in the aerosol (mol L⁻¹). γ_{HO_2} rather depends on copper concentration so we also evaluate the influence of copper solubility on the uptake coefficient. What is more, the unequally distribution of copper ions will also influence the HO₂ uptake coefficient (details in the SI).

$3.5.3 \, \gamma_{HO_2}$ estimated at Wangdu field campaign

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By inputting the soluble copper concentration, aerosol mass concentration, aerosol particle geometric mean diameter and the corresponding relative humidity and temperature into the *NEq.*, we can obtain an estimation of γ_{HO_2} in suburban Wangdu, which is shown in Fig. 4 (a) and (b). The time resolution is 1 hour. The aerosol pH is calculated using the thermodynamic model ISORROPIA-II (Fountoukis and Nenes, 2007) and the averaged value is 3.41 ± 0.69 (1σ). Average aerosol mass concentration is $67.2 \pm 39.7 \,\mu \text{g m}^{-3}$, the average Cu concentration is $35.8 \pm 57.7 \,\text{ng m}^{-3}$. The results of a fit to a Gaussian function results in a γ_{HO_2} value of 0.116 ± 0.086 (1σ) the Wangdu campaign (γ_{HO_2} will increase from 0.065 ± 0.051 (1σ) at 10% solubility to 0.196 ± 0.142 (1σ) at 70% solubility for the summary of day and night data).

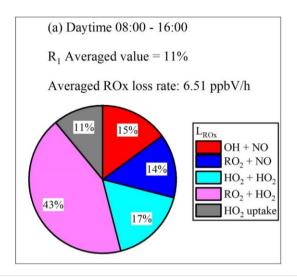
Tan et al. (2017) had compared the measured and modelled OH, HO₂ and RO₂ radicals in the Wangdu campaign. However, in this paper, they did not discuss the influence of HO₂ uptake. A very recent publication (Tan et al., 2020) calculated γ_{HO_2} in the Wangdu campaign based on the comparison of field measurement data for HO₂ and concentrations calculated by the box model. The paper proposes that all γ_{HO_2} calculated in this way from the Wangdu campaign can be fitted to a Gaussian distribution around the value of 0.08 \pm 0.13 (1 σ). This value isin the range of our estimation in this paper considering the influence of aerosol morphology and the indirect measurement uncertainty (please see the SI).

The experimentally determined ROx termination rates include reaction channels from OH + NO₂, OH + NO, HO₂ + HO₂, HO₂ + RO₂, RO₂ + NO. The ratio (R_1) of HO₂ uptake loss rate ($L_{HO2uptake}$) to the whole RO_x loss rate (L_{ROx}) is calculated by Equation-Eq. (212) and Eq. (223).

$$L_{HO2uptake} = 0.25 \cdot v_{HO_2} \cdot [ASA] \cdot [HO_2]$$
 (212)

$$R_1 = \frac{L_{HO2uptake}}{L_{ROX}} \tag{223}$$

[ASA] is the aerosol surface area $[\mu m^2 cm^{-3}]$.



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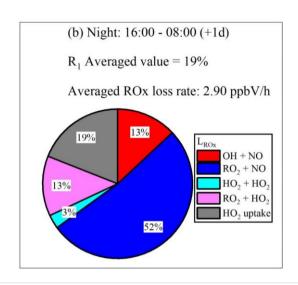


Figure 4: R_1 calculated by the *NEq.*. Pie charts show the values of R_1 and the loss rates for ROx during daytime (a) and nighttime (b). The averaged daytime (08:00–16:00) ROx radical loss rate is 6.5 ppbV/h and that for nighttime (16:00–08:00 (+1d)) is 2.9 ppbV/h.

No significant difference of γ_{HO_2} is observed during daytime and night. The HO₂ uptake coefficient is slightly higher at night due to the higher RH (57.6% at day and 67.4% at night). However, because of the high uncertainty of the uptake coefficient, such a high trend cannot be concluded to other cases. HO₂ heterogeneous uptake reactions with aerosol particles have small impact on ROx radical termination at daytime as shown in Fig. (4 a). However, HO₂ uptake may be important in the termination of ROx radicals at night shown in Fig. (4 b). The daytime ratio R_1 is lower than it is at night because of the lack of photochemical reactions, thus a longer HO₂ lifetime at night. The high proportion of RO₂+NO during night is due to high [NO] at dawn.

The RO_2 concentration is also important when evaluating the impact of HO_2 uptake. Using the modeled value of RO_2 concentration in Wangdu campaign, a higher proportion of HO_2 uptake to about 21% of ROx sinks in daytime can be calculated. However, using the modified field measured RO_2 concentration in Wangdu campaign, HO_2 uptake is less important in the budget of ROx as shown in Fig (4 aa), which is in line with the results from Tan et al. (2020).

3.5.4 Discussion of uncertainties of γ_{HO_2} estimated at Wangdu field campaign

The impact of HO_2 aerosol uptake on the ROx budget is complicated by large uncertainties in the HO_2 uptake coefficient under ambient conditions. The NEq is applicable under the assumption of steady-state concentrations and with metastable or liquid aerosol particles (if the ambient RH over a completely liquid aerosol decreases below the deliquescence RH, the aerosol may not crystalize immediately but may constitute a supersaturated aqueous solution (i.e., in the metastable state) (Song et al.,

2018)). The approximate calculation of HO₂ concentration gradients within the aerosol particle condensed phase also cause deviations for larger particles or high copper equivalent concentration.

Organic content of an aerosol particle may affect several important parameters in the uptake model (Lakey et al., 2016b; Lakey et al., 2015). For example, the aerosol pH, hygroscopic properties of the aerosol, the rate of diffusion of HO₂ within the aerosol and a reduction in the concentration of Cu^{2+} via the formation of complexes that could affect the ability of Cu to undergo redox reactions with HO₂ and O₂⁻. Hence, it is expected that the presence of organic matter would change the value of γ_{HO_2} . We tested the core-shell morphology of aerosol particles influence on HO₂ uptake in the Wangdu campaign (details in the SI). Organic matter will lower the uptake coefficient about 25% to 40% under the assumption of 20%-50% PM_{2.5} mass is organic matter.

Another uncertainty comes from aerosol particles morphology. The bulk diffusion coefficient of HO_2 and other reactive molecules should be lower in the situation of semi-solid particles (Berkemeier et al., 2016; Shiraiwa et al., 2010; Mikhailov et al., 2009) and would change with the water activity and the organic components (Price et al., 2015). For crystalline or amorphous solid aerosol particles, HO_2 will undergo surface reactions and diffuse across the surface rather than be accommodated within the aerosol bulk. The MARK model has limitations in the calculation of γ_{HO_2} with semi-solid aerosol particles. In the Wangdu campaign, κ_{sca} (optical aerosol hygroscopicity parameter) ranges from 0.05 to 0.35 with an average of 0.22. The ambient RH during the Wangdu campaign shows significant diurnal variations and varies greatly from 15% to 97%, with an average value of 61% (Kuang et al., 2019) indicating that the percentage of solid aerosol particles is relatively low and hence do not significantly influence γ_{HO_2} . Anyway, aerosol particles morphology relative to an aqueous phase will influence the uptake coefficient of HO_2 . The uptake process would vary with mixing state of the particles, thus the predicted γ_{HO_2} values here may be biased as a result but represents an average over bulk aerosols.

The interaction between organics and soluble copper and the influence of organics on aerosol properties will lead to further uncertainty in the calculation of the uptake coefficient. Lakey et al., 2016a; Lakey et al., 2015; Lakey et al., 2016b) have also shown that the addition of an organic compound to Cu^{2+} doped aerosols such as oxalic acid, which forms oxalate ions $(C_2O_4)^{2-}$ in the aerosol, results in a lower value of γ_{HO_2} as such ions forms a complex with the TMI.

As noted above, the value $(0.116 \pm 0.086 \, (1\sigma))$ estimated by the *NEq*. represents the upper limitation of γ_{HO_2} in the Wangdu field campaign.

4 Summary and conclusions

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Taketani et al. collected the filter samples of aerosol in Mts. Tai and Mts. Mang, North China (Taketani et al., 2012) and re-aerosolized from the water extracts of sampled particles. The measured uptake coefficients for Mt. Tai samples ranged between 0.09 and 0.40, while those at Mt. Mang were between 0.13 and 0.34. Li et. al (Li et al., 2019b) suggest that the rapid decrease of PM_{2.5} in China has slowed down the reactive uptake rate of HO₂ radicals by aerosol particles and could have been

the main reason for the increase in ozone in the North China Plain in the recent years. They apply a value of the uptake coefficient of 0.2 in their model calculations. However, the results of the MARK model and of the NEq. in this paper suggest that the HO₂ uptake coefficient could be smaller and highly variable for typical conditions in the North China Plain. Further research is needed to study the effects of heterogeneous uptake of HO₂ on gas phase and heterogeneous physicochemical reactions under different environmental conditions in different regions. The novel parameterized equation proposed in this paper provides an effective way for more detailed calculation of the effects of HO₂ heterogeneous reactions on the atmospheric radical budget, ozone production and particulate matter generation. This is the first attempt to parameterize the heterogeneous uptake coefficient of HO₂ with aerosol particles in China campaign. This equation estimates the γ_{HO_2} in a comprehensive field campaign which is in agreement with the simulation results from the comparison of gas phase radical concentrations (Tan et al., 2020). Overall, we can conclude that the HO₂ uptake process needs to be considered in photochemical box models for the study of the HOx radical budget. The exact value is highly variable with respect to the change of copper concentrations in the aerosol particle condensed phase and other factors. The measurement of condensed phase soluble copper and other TMIs, organic content, as well as the aerosol liquid water should be added for future field campaigns for the study of the HOx radical budget.

Appendix A

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Table A1 Description and units of parameters used in the MARK model and the parameterized equations

Parameter	Description	Unit
	Used in the parameterized equation	
γ_{HO_2}	HO ₂ uptake coefficient	-
$lpha_{HO_2}$	Mass accommodation coefficient of HO_2 which is the probability that a HO_2	-
	molecule colliding with the aerosol surface leads to dissolution, reaction or	
	volatilization	
v_{HO_2}	Mean molecular speed of HO ₂	$\mathrm{cm}\mathrm{s}^{\text{-1}}$
R_d	Count Median Radius of the aerosols	cm
R_c	radius of the aqueous core	cm
H_{corr}	Henry's constant corrected for solution pH	mol cm ⁻³ atm ⁻¹
	$H_{corr} = H_0 \times \left(1 + \frac{K_{eq}}{[H^+]}\right)$	
H_0	physical Henry's law constant	mol cm ⁻³ atm ⁻¹
H^{cc}	effective Henry's law constant	mol cm ⁻³ atm ⁻¹

H_{org}	Henry's law constant of HO2 for organic coating	mol cm ⁻³ atm ⁻¹
R	gas constant	$cm^3atmK^{-1}mol^{-1}$
T	temperature	K
RH	relative humidity ranging from 0.4 to 0.9	0-1
ALWC	aerosol liquid water content	g cm ⁻³
[PM]	Mass concentration of PM _{2.5}	μg cm ⁻³
D_g	gas phase diffusion coefficient of HO2	$\mathrm{cm}^2\mathrm{s}^{-1}$
D_{aq}	aqueous phase diffusion coefficient	$\mathrm{cm}^2\mathrm{s}^{\text{-1}}$
D_{org}	solubility and diffusivity of HO2 in the organic coating	$\mathrm{cm}^2\mathrm{s}^{\text{-1}}$
arepsilon	ratio of the radius of the aqueous core (R_c) and the particle (R_d) .	-
l	Thickness of organic coating which is calculated from the volume ratio of	cm
	the inorganics to total particle volume with the assumption of a hydrophobic	
	organic coating (density, 1.27 g cm ⁻³) on the aqueous inorganic core (with a	
	density of 1.77 g cm^{-3}).	
	Used in the corrections in the MARK model or the classical parameterized eq	uation
ρ	density of the aerosol particles	g cm ⁻³
I	Solution molar ionic strength	M
A	activity coefficient for gas phase HO2 and other neutral small molecules	-
φ_{x}	activity coefficient of ion in solution	-
m_y	molality of an ion in solution	M
$\varepsilon(x,y,I)$	"interaction coefficients", the summation extends over all ions (y) in the	-
	solution at a molality of m_y	
$[x_i]_{effqu}$	effective molality of an ion x_i	M
$[\overline{HO_2}]$	averaged steady-state HO2 concentration over the volume of the particle	M
$[HO_{2(r)}]$	HO ₂ concentration at the surface of particles	M
K_{eq}	solution equilibrium constant for HO ₂ in the gas phase	$M^{-1} s^{-1}$
k_{eff}	comprehensive liquid phase reaction rate coefficient which encompasses	$M^{-1} s^{-1}$
,,	both HO ₂ dissolution equilibrium reactions and liquid phase chemical-	
	physical reactions during HO ₂ uptake process	
k_{TMI}	second order rate coefficient (k_{TMI}) of HO ₂ and O ₂ ⁻ with transition metal	$M^{-1} s^{-1}$
	ions used in the classical equation	
k^1	effective rate coefficient used in the classical equation proposed by IUPAC	M ⁻¹ s ⁻¹

Author Contribution

Keding Lu conceived the study. Huan Song and Keding Lu developed the MARK model for multiphase simulations. Xiaorui Chen and Qi Zou improved the codes of the MARK model. Zhaofeng Tan, Hendrik Fuchs, Keding Lu, Alfred Wiedensohler, Mei Zheng, Andreas Wahner, Astrid Kiendler-Scharr, Yuanhang Zhang contributed to the related measurements of the Wangdu field campaign. Dwayne E. Heard, Daniel R. Moon and Mar á-Teresa Baeza-Romero contributed the laboratory studies of HO₂ uptake coefficients, and they have contributed to writing the manuscript. Huan Song performed the model simulations and prepared the manuscript with Keding Lu and Zhaofeng Tan which was enhanced by contributions from all the co-authors.

Competing Interest

The authors have no conflict of interests.

Data Availability

745 Data supporting this publication are available upon request for the corresponding author (k.lu@pku.edu.cn).

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