



1 New Methodology Shows Short Atmospheric Lifetimes of 2 Oxidized Sulfur and Nitrogen due to Dry Deposition

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13

14 **Abstract**

15

16 The atmospheric lifetimes of pollutants determine their impacts on human health, ecosystems
17 and climate and yet, pollutant lifetimes due to dry deposition over large regions have not been
18 determined from measurements. Here, a new methodology based on aircraft observations is used
19 to determine the lifetimes of oxidized sulfur and nitrogen due to dry deposition over $(3-6) \times 10^3$
20 km^2 of boreal forest in Canada. Dry deposition fluxes decreased exponentially with distance
21 resulting in lifetimes of 2.2-26 hours. Fluxes were 2-14 and 1-18 times higher than model
22 estimates for oxidized sulfur and nitrogen, respectively, indicating dry deposition velocities
23 which were 1.2-5.4 times higher than those computed for models. A Monte-Carlo analysis with
24 five commonly used inferential dry deposition algorithms indicates that such model
25 underestimates of dry deposition velocity are typical. These findings indicate that deposition to
26 vegetation surfaces are likely under-estimated in regional and global chemical transport models
27 regardless of the model algorithm used. The model-observation gaps may be reduced if surface
28 pH, and quasi-laminar and aerodynamic resistances in algorithms are optimized as shown in the
29 Monte-Carlo analysis. Assessing the air quality and climate impacts of atmospheric pollutants
30 on regional and global scales requires improved measurement-based understanding of
31 atmospheric lifetimes of these pollutants.

32



33 **1 Introduction**

34 Deposition represents the terminating process for most air pollutants and the starting
35 point for ecosystem impacts. Understanding deposition is critical in determining the atmospheric
36 lifetimes and spatial scale of atmospheric transport of pollutants, which in turn, dictates their
37 ecosystem (WHO, 2016; Solomon et al., 2007) and climate (Samset et al., 2014) impacts. In
38 particular, atmospheric lifetimes (τ) of oxidized sulfur and nitrogen compounds influence their
39 concentrations and column burdens in air, which affect air quality and hence human exposure
40 (WHO, 2016). Furthermore, the lifetime of these species affects their contributions to
41 atmospheric aerosols, with a consequent influence on climate via changes to radiative transfer
42 through scattering and cloud formation (Solomon et al., 2007). In addition, their deposition can
43 exceed critical load thresholds causing aquatic and terrestrial acidification, and eutrophication in
44 the case of nitrogen deposition (Howarth, 2008; Bobbink et al., 2010; Doney, 2010; Vet et al.,
45 2014; Wright et al., 2018). Quantifying τ and deposition thus provides a crucial assessment of
46 these regional and global impacts.

47 Deposition occurs through wet and dry processes. While wet deposition fluxes can be
48 measured directly (Vet et al., 2014), there are few validated methods for dry deposition fluxes
49 (Wesley and Hicks, 2000), and none which estimates deposition over large regions. Dry
50 deposition fluxes (F) may be obtained using micrometeorological measurements for pollutants
51 for which fast response instruments are available. However, these results are only valid for the
52 footprints of the observation sites, typically hundreds of meters (Aubinet et al., 2012), and their
53 extrapolation to larger regions may suffer from representativeness issues. As a result,
54 atmospheric lifetimes τ with respect to dry deposition have not been determined through direct
55 observations. On a regional scale, dry deposition fluxes are typically derived by multiplying



56 network-measured or model-predicted air concentrations with dry deposition velocities (V_d)
57 (Sickles and Shadwick, 2015; Fowler et al., 2009; Meyers et al., 1991), which are derived using
58 resistance-based inferential dry deposition algorithms (Wu et al., 2018), and compared with
59 limited micrometeorological flux measurements (Wesley and Hicks, 2000; Wu et al., 2018;
60 Finkelstein et al., 2000; Matsuda et al., 2006; Makar et al., 2018) for validation. When applied to
61 a regional scale, an inferential-algorithm derived V_d may have significant uncertainties (Wesley
62 and Hicks, 2000; Aubinet et al., 2012; Wu et al., 2018; Finkelstein et al., 2000; Matsuda et al.,
63 2006; Makar et al., 2018; Brook et al., 1997). For example, inferred V_d for SO_2 , despite being
64 the most studied and best estimated, may be underestimated by 35% for forest canopies
65 (Finkelstein et al., 2000). Underestimated V_d for SO_2 and nitrogen oxides can contribute to
66 model over-prediction of regional and global SO_2 concentrations (Solomon et al., 2007; Christian
67 et al., 2015; Chin et al., 2000), or under-prediction of global oxidized nitrogen dry deposition
68 fluxes (Paulot et al., 2018; Dentener et al., 2006).

69 Here, a new approach is presented to determine τ with respect to dry deposition and F for
70 total oxidized sulfur (**TOS**, the sulfur mass in SO_2 and particle- SO_4 (pSO_4)) and total reactive
71 oxidized nitrogen (**TON**, the nitrogen mass in NO , NO_2 , and others designated as NO_x) on a
72 spatial scale of $(3-6) \times 10^3 \text{ km}^2$, using aircraft measurements. This approach provides a unique
73 methodology to determine τ and F over a large region. Coupled with analyses for chemical
74 reaction rates (for **TOS** compounds), the average V_d for **TOS** and **TON** over the same spatial
75 scale were also determined. The airborne measurements were obtained during an intensive
76 campaign from August to September 2013 in the AOSR (Gordon et al., 2015; Liggio et al., 2016;
77 Li et al., 2017; Baray et al., 2018; Liggio et al., 2019) in northern Alberta, Canada. Direct



78 comparisons with modelled dry deposition estimates are made to assess their uncertainties and
79 the spatial-temporal scales of air pollutant impacts.

80 **2 Methods**

81 **2.1 Lagrangian Flight Design**

82 Details of the airborne measurement program have been described elsewhere (Gordon et
83 al., 2015; Liggio et al., 2016; Li et al., 2017; Liggio et al., 2019; Baray et al., 2018). Briefly, an
84 instrumented National Research Council of Canada's Convair-580 research aircraft was flown
85 over the Athabasca oil sands region (AOSR) in Alberta, Canada from August 13 to September 7,
86 2013. The flights were designed to determine emissions, assess atmospheric transformation
87 processes and gather data for satellite and numerical model validation. Three flights were flown
88 to study transformation and deposition processes by flying a Lagrangian pattern so that the same
89 pollutant air mass was sampled at different time intervals downwind of emission sources for a
90 total of 4-5 hrs. Flights 7 (F7, Aug 19), 19 (F19, Sep 4) and 20 (F20, Sep 5) took place during
91 the afternoon when the boundary layer was well established. The flights were conducted in clear
92 sky conditions so wet deposition processes were insignificant. The aircraft flew tracks
93 perpendicular to the plume at multiple altitudes between 150 to 1400 m agl and multiple
94 intercepts of the plume downwind. Vertical profiles conducted as spirals were flown at the
95 centre of the plume which provided information on the boundary layer height and extent of
96 plume mixing. There were no other anthropogenic sources downwind of the AOSR.

97 **2.2 Aircraft Measurements**

98 A comprehensive suite of detailed gas- and particle-phase measurements were made from
99 the aircraft. Measurements pertaining to the analysis in this paper are discussed below.



100 **SO₂ and NO_y.** Ambient air was drawn in through a 6.35 mm (1/4") diameter PFA sampling line
101 taken from a rear-facing inlet located on the roof towards the rear of the aircraft. The inlet was
102 pressure-controlled to 770 mm Hg using a combination of a MKS pressure controller and a
103 Teflon pump. Ambient air from the pressure-controlled inlet was fed to instrumentation for
104 measuring SO₂ and NO_y. SO₂ was detected via pulsed fluorescence with a Thermo 43iTLE
105 (Thermo Fisher Scientific, Franklin, MA, USA). NO_y (also denoted as Total Oxidized Nitrogen
106 (TON)) was measured by passing ambient air across a heated (325°C) molybdenum converter
107 that reduces reactive nitrogen oxide species to NO. NO was then detected through
108 chemiluminescence with a Thermo 42iTL (Thermo Fisher Scientific). An inlet filter was used
109 for SO₂, but NO_y includes particulate nitrate (pNO₃), NO, NO₂, HNO₃ and other oxides of
110 nitrogen such as peroxy acetyl nitrate. The conversion efficiency of the heated molybdenum
111 converter and inlet transmission was evaluated with NO₂ and HNO₃ and found to be near 100%
112 and >90%, respectively. Other NO_y species are expected to be greater than that of HNO₃.
113 Species like NO₃ radical and N₂O₅ are expected to be low as they photolyze quickly during
114 daytime. Zeros were performed 3-5 times per flight for all instruments by passing ambient air
115 through an in-line Koby King Jr cartridge for ~5 minutes. Multiple calibrations were conducted
116 before, during and after the study using National Institute Standards and Technology reference
117 standards. Data were recorded at a time resolution of 1 second and corrected for a sampling time
118 delay of 1-3 seconds depending on the instrument.

119 **Aerosols.** Multiple aerosol instruments sub-sampled from a forward facing, shrouded, isokinetic
120 particle inlet (Droplet Measurement Technologies, Boulder, CO, USA). A Time-of-Flight High
121 Resolution Aerosol Mass Spectrometer (AMS) (Aerodyne Research Inc.) was used to measure
122 non-refractory submicron aerosol components including pSO₄, pNO₃, pNH₄, and p-organics.



123 Details of the AMS and its operations have been published elsewhere (DeCarlo et al., 2006).
124 The instrument was operated in mass spectrometry V-mode with a time resolution of 10 seconds.
125 Filtered measurements were taken 4-5 times per flight to determine background signals.
126 Ionization efficiency calibrations using monodisperse ammonium nitrate were performed during
127 the study with an uncertainty of $\pm 9\%$. Data were corrected for a sampling time delay of 10
128 seconds by comparing with faster response instruments e.g. a wing-mounted Forward Scattering
129 Spectrometer Probe Model 300 (FSSP-300) and an in-board Ultra High Sensitivity Absorption
130 Spectrometer (UHSAS) (both from Droplet Measurement Technologies). The AMS data were
131 processed using AMS data analysis software (Squirrel, version 1.51H and PIKA, version 1.10H).
132 A collection efficiency was applied to the data and determined by comparing the total AMS-
133 derived mass with the mass derived from the size distribution measurements from the UHSAS
134 assuming a density based on the chemical composition; the collection efficiency ranged from 0.5
135 to 1.

136 Measurements are discussed in terms of total oxidized sulfur (TOS, the sulfur mass in
137 SO_2 and particle- SO_4 (pSO_4)) and total reactive oxidized nitrogen (TON, the nitrogen mass in
138 reactive oxidized nitrogen species, often denoted NO_y).

139 **Volatile Organic Compounds (VOCs).** Selected VOCs were used to estimate the OH
140 concentrations used for determining oxidation rates for SO_2 . VOCs were measured with a proton
141 transfer reaction time-of-flight mass spectrometer (PTR-ToF-MS, Ionicon Analytik GmbH,
142 Austria) as well as through discrete canister grab samples. The PTR-ToF-MS and its operation,
143 along with the details of the canister sampling and lab analyses during the study were described
144 in detail previously (Li et al., 2017). Briefly, the PTR-ToF-MS used chemical ionization with
145 H_3O^+ as the primary reagent ion. Gases with a proton affinity greater than that of water were



146 protonated in the drift tube. The pressure and temperature of the drift tube region were
147 maintained at a constant 2.15 mbar and 60°C, respectively for an E/N of 141 Td. The protonated
148 gases were detected using a high-resolution time of flight mass spectrometer at a time resolution
149 of 2 seconds. Instrumental backgrounds were performed in flight using a custom-built zero-air
150 generating unit. The unit contained a catalytic converter heated to 350°C with a continuous flow
151 of ambient air at a flow rate of one litre per minute. The data were processed using Tofware
152 software (Tofwerk AG). Calibrations were performed on the ground using gas standard mixtures
153 from Ionicon, Apel-Reimer and Scott-Marrin for 22 compounds. The canister samples were
154 collected in pre-cleaned and passivated 3L stainless steel canisters that were subsequently sent to
155 an analytical laboratory for GC-FID/MS analyses for a suite of 150 hydrocarbon compounds.

156 **Meteorology and aircraft state parameters.** Meteorological measurements have been
157 described elsewhere (Gordon et al., 2015). In brief, 3-D wind speed and temperature were
158 measured with a Rosemount 858 probe. Dew point was measured with an Edgetech hygrometer
159 and pressure was measured with a DigiQuartz sensor. Aircraft state parameters including
160 positions and altitudes were measured with GPS and a Honeywell HG1700 unit.

161

162 **2.3 Mass transfer rates in the atmosphere**

163 Mass transfer rates (T) across flight screens (Figure 1) were determined using an
164 extension of the Top-down Emission Rate Retrieval Algorithm (TERRA) developed for emission
165 rate determination using aircraft measurements (Gordon et al., 2015). Briefly, at each plume
166 interception location, the level flight tracks were stacked to create a virtual screen. Background
167 subtracted pollutant concentrations and horizontal wind speeds normal to the screen were
168 interpolated using kriging. The background for SO₂ was ~0 ppb and pSO₄ was 0.2 – 0.3 μg m⁻³



169 which was subtracted from the pSO₄ measurements before mass transfer rates were calculated
170 (Liggio et al., 2016). Integration of the horizontal fluxes across the plume extent on the screen
171 yields the transfer rate T . Using SO₂ as an example,

$$172 \quad T_{SO_2} = \int_{s_1}^{s_2} \int_{z_1}^{z_2} C(s, z) u_n(s, z) ds dz \quad (1)$$

173 where $C(s, z)$ is the background subtracted concentration at screen coordinate s and z , which
174 represent the horizontal and vertical axes of the screen. The $u_n(s, z)$ is the horizontal wind speed
175 normal to the screen at the same coordinates.

176 Since the lowest flight altitude was 150 magl, it was necessary to extrapolate the data to
177 the surface as per the procedures described previously (Gordon et al., 2015). Extrapolation to the
178 surface methods were compared and differences were included in the uncertainty estimates.
179 Since the main source of SO₂ is from the elevated facility stacks, the uncertainty for a single
180 screen is estimated at 4% (Gordon et al., 2015). NO_y was also extrapolated linearly to the
181 surface and the mass transfer rates were similarly compared to other extrapolation methods. NO_y
182 sources include the elevated facility stacks and surface sources such as the heavy hauler trucks
183 operating in the surface mines. The uncertainty in the resulting T for a single screen is estimated
184 to be larger at 8%, as a larger fraction of the NO_y mass may be below the lowest measurement
185 altitude (Gordon et al., 2015). Sulfur and nitrogen data were also extrapolated linearly to
186 background values from the highest altitude flight tracks upwards to the mixed layer height,
187 which was determined from vertical profiles of pollutant mixing ratios, temperature and dew
188 point (Table 1). Two different approaches, a finite jump model and a gradient flux approach
189 (Stull, 1988; Degrazia et al., 2015), were used to estimate the potential upward loss across the
190 interface between the boundary layer and the free troposphere for sulfur. In both approaches, the



191 upward S flux was a minor loss at $< 45 \text{ g/km}^2/\text{hr}$, about 3 orders of magnitude lower than the
192 several to many $\text{kg/km}^2/\text{hr}$ horizontal advective transport that were determined using TERRA.

193 Changes in T (denoted ΔT) were then calculated as the differences in T between pairs of
194 virtual screens. The uncertainty in ΔT was estimated as 8% for **TOS** and 26% for **TON** as
195 supported by emission rate uncertainties determined for box flights (Gordon et al., 2015). The
196 uncertainty analysis for box flights is applicable to ΔT here, as both account for uncertainties
197 with an upwind and a downwind screen. The ΔT uncertainties were propagated through
198 subsequent calculations.

199 Knowing ΔT , and accounting for the net rates of chemical loss and formation between
200 screens for SO_2 and pSO_4 , the deposition rates (and subsequently the deposition flux in tonnes S
201 (or N) $\text{km}^{-2} \text{ hr}^{-1}$, Section 2.4 were determined as follows, using sulfur compounds as an example:

$$202 \quad \Delta T_{\text{SO}_2} = T_{\text{SO}_2}(t_2) - T_{\text{SO}_2}(t_1) = X_{\text{SO}_2} - D_{\text{SO}_2} \quad (2)$$

$$203 \quad \Delta T_{\text{pSO}_4} = T_{\text{pSO}_4}(t_2) - T_{\text{pSO}_4}(t_1) = X_{\text{pSO}_4} - D_{\text{pSO}_4} \quad (3)$$

$$204 \quad \Delta T_{\text{TOS}} = T_{\text{TOS}}(t_2) - T_{\text{TOS}}(t_1) = -D_{\text{TOS}} \quad (4)$$

205 where X_{SO_2} is the rate of chemical reaction loss of sulfur mass in SO_2 , X_{pSO_4} is the rate of
206 chemical formation of sulfur mass as pSO_4 , D_{SO_2} and D_{pSO_4} are deposition rates of sulfur mass in
207 SO_2 and pSO_4 respectively, and t_1 and t_2 are plume interception times at Screen 1 and Screen 2,
208 respectively. Reaction with the OH radical was considered to be the most significant chemical
209 loss of SO_2 and the most significant path for the formation of pSO_4 (further details in SI Section
210 S4. X_{SO_2} and X_{pSO_4} were determined using estimated OH radical concentrations, which were
211 determined using the methodology described in SI Section S4.



212 Dry deposition rates, D_{SO_2} and D_{pSO_4} , and their uncertainties were determined using Eq.
213 (2) and (3). For total oxidized sulfur **TOS** (i.e., sulfur in $SO_2 + pSO_4$) and total oxidized
214 nitrogen **TON** (i.e., nitrogen in NO_y) the chemistry term is not relevant, and thus, the dry
215 deposition rate D_{TOS} was directly determined from ΔT_{TOS} using equation (4), and respectively for
216 **TON**.

217

218 **2.4 Dry deposition fluxes and dry deposition velocities**

219 Average dry deposition fluxes (F) for **TOS** and **TON** were obtained by dividing the
220 deposition rates D with the footprint surface area of the plume between two adjacent screens
221 (Figure 1 grey shaded regions), as shown in Equation 5 for the dry deposition flux F_{TOS} of **TOS**
222 (in $t\ S\ km^2\ hr^{-1}$):

$$223 \quad F_{TOS} = \frac{D_{TOS}}{Area} \quad (5)$$

224 where the surface area, $Area$, was identified as the geographic area under the plume extending to
225 the edges of the plume where concentrations fell to background levels (i.e. SO_2 to ~ 0 ppb; SO_4
226 $\sim 0.2\ \mu g\ m^{-3}$). This approach was similarly used to derive deposition fluxes from an air quality
227 model, Global Environmental Multiscale – Modelling Air-quality and Chemistry (GEM-MaCH)
228 (Moran et al., 2010; also see SI Section S5 for details). The geographic surface area uncertainty
229 is estimated at 5%. Dry deposition fluxes between the sources and the first screen were also
230 estimated using ΔT based on the extrapolated transfer rates back to the source region ('extended'
231 region). The surface area boundaries for these 'extended' regions were determined using latitude
232 and longitude coordinates that were weighted by emissions. This was done by first using the
233 average wind direction from Screen 1 and creating a set of parallel back trajectories (~ 20)



234 starting at different parts of Screen 1 back across the source region. For **TON**, the NO_x emission
235 sources along each back trajectory were weighted by their NO_x emissions to obtain an emissions-
236 weighted center location with latitude and longitude coordinates for each back trajectory. The
237 line connecting these emissions-weighted center locations formed the boundary of the extended
238 surface area. The extended surface area was similarly determined for **TOS** based upon the
239 known locations of the major SO₂ point sources. The uncertainty of the ‘extended’ regions is
240 estimated at 10% based on repeated optimizations of the geographical area. Surface areas are
241 visualized as grey shaded regions between screens in Figure 1 and tabulated in SI Table S1.

242 Spatially-averaged dry deposition velocities, V_d , based on the aircraft measurements were
243 determined over the surface area between screens using average plume concentrations across
244 pairs of screens at about 40 meters above the ground for **TOS** and **TON** (e.g. Equation 6 for
245 SO₂).

$$246 \quad V_d = \frac{F_{SO_2}}{[SO_2]} \quad (6)$$

247 The largest source of uncertainty in V_d calculated this way was the determination of
248 concentration at 40 meters above the surface as the measurements were extrapolated from the
249 lowest aircraft altitude to the surface and interpolated concentrations were used. The
250 measurement-derived V_d are compared with those from GEM-MACH which uses inferential
251 methods.

252

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254



255 **2.5 Monte-Carlo simulations of dry deposition velocities using multiple resistance-based**
256 **parameterizations**

257 Parameterization of dry deposition in inferential algorithms is commonly based on a
258 resistance approach with dry deposition velocity depending on three main resistance terms as
259 below:

$$260 \quad V_d = \frac{1}{R_a + R_b + R_c} \quad (7)$$

261

262 where R_a , R_b and R_c represent the aerodynamic, quasi-laminar sublayer and bulk surface
263 resistances respectively. Although these resistance terms are common among many regional air
264 quality models (Wu et al., 2018), the formulae used (and inputs in to these formulae) to calculate
265 the individual resistance terms differ significantly among the inferential deposition algorithms.
266 To assess the potential for a general underestimation of V_d across different inferential deposition
267 algorithms, and to compare with the aircraft-derived V_d , five different inferential deposition
268 algorithms, including that used in the GEM-MACH model for calculating V_d (Wu et al., 2018)
269 were incorporated into a Monte-Carlo simulation for V_d for SO_2 . NO_y was not considered here,
270 as its measurement includes multiple reactive nitrogen oxide species with different individual
271 deposition velocities. We note that many of the inferential algorithms are based on observations
272 of SO_2 and O_3 deposition made at single sites, and the extent to which a chemical is similar to
273 SO_2 or O_3 features into its V_d calculation – the comparison thus has relevance for species aside
274 from SO_2 .

275 The five deposition algorithms considered are denoted ZHANG, NOAA-GEM, C5DRY,
276 WESLEY and GEM-MACH. To perform the simulations, formulae for the first four algorithms



277 were taken from Wu et al. (2018) and for GEM-MACH taken from Makar et al. (2018). The
278 stomatal resistance in the ZHANG algorithm was from Zhang et al. (2002). The GEM-MACH
279 formula (Equation 8.7 in the SI of Makar et al. (2018)) for mesophyll resistance R_{mx} contained a
280 typo (missing the Leaf Area Index (LAI)) and was corrected for as follows:

$$281 \quad R_{mx} = [LAI(H^*/3000 + 100 f_0)]^{-1} \quad (8)$$

282 Prescribed input values were constrained by the range of possible values consistent with the
283 conditions during the aircraft flights and are shown in SI Table S3 with associated references.
284 Calculations for the R_a term were based on unstable and dry conditions as observed during the
285 aircraft flights. The Monte-Carlo simulation generated a distribution of possible V_d values,
286 based on randomly generated values of the input variables to each algorithm and selected from
287 Gaussian distributions with a range of 3 sigma for all input parameters. All simulations were
288 performed with the same input values that were common between the algorithms.

289 **3 Results and Discussion**

290 **3.1 Meteorological and Emissions Conditions during the Transformation Flights**

291 During the experiments, the dry deposition rates (D) were quantified under different
292 meteorological conditions and emissions levels of **TOS** and **TON** (E_{TOS} and E_{TON}) for the three
293 flights (see Table 1). These differences played important roles in the observed pollutant
294 concentrations and resulting dry deposition fluxes for F7, F19 and F20. Mixed layer heights
295 (MLH) were derived from aircraft vertical profiles that were conducted in the centre of the
296 plume at each downwind set of transects. The profiles of temperature, dew point temperature,
297 relative humidity and pollutant mixing ratios were inspected for vertical gradients indicating a
298 contiguous layer connected to the surface. The highest MLH was determined for F7 at 2500



299 magl whereas F19 had the lowest MLH at 1200 magl (Table 1). In F20, the MLH was 2100
300 magl. The combination of a high MLH in F7 with the highest wind speeds resulted in the lowest
301 pollutant concentrations of the three flights. In F19, lower wind speeds and the lowest mixed
302 layer heights led to the highest pollutant levels. F20 had emissions and meteorological
303 conditions that were in between F7 and F19 resulting in pollutant concentrations between those
304 of F7 and F19.

305 Emission rates of SO₂ and NO_x (designated as *E_{TOS}* and *E_{TON}*) from the main sources in
306 the AOSR were estimated from the aircraft measurements and varied significantly between the
307 three flight days. The measurement-based emission rates of *E_{TOS}* and *E_{TON}* were taken from the
308 mass transfer rates of *T_{SO2}* and *T_{NOy}* (described in Methods) by extrapolating backwards to the
309 source locations in the AOSR using exponential functions (Figure 2, Section 3.2). For **TOS**, the
310 source location was set at 57.017N, -111.466W, where the main stacks for SO₂ emissions are
311 located. For **TON**, the source locations were determined from geographically weighted
312 locations. Emission rates *E_{TOS}* and *E_{TON}* for each flight are shown in Table 1.

313 Model-based *E_{TOS}* and *E_{TON}* were also obtained from the 2.5 km x 2.5 km gridded
314 emissions fields that were specifically developed for model simulations of the large AOSR
315 surface mining facilities (Zhang et al., 2018) i.e. Suncor Millenium, Syncrude Mildred Lake,
316 Syncrude Aurora North, Shell Canada Muskeg River Mine & Muskeg River Mine Expansion,
317 CNRL Horizon Project and Imperial Kearn Mine. The emissions fields have been used in GEM-
318 MACH (described in SI Section S5) to carry out a number of model simulations (Zhang et al.,
319 2018; Makar et al., 2018) including for the present study. In this work, emissions were summed
320 from various sources including offroad, point (Continuous Emissions Monitoring (CEMS)), and
321 point (non-CEMS) for the surface mines to obtain total AOSR hourly emission rates for the



322 flight time periods of interest (Table 2). The standard deviations reflect the emissions variations
323 during the simulated flight.

324 3.2 Mass Transfer Rates

325 The mass transfer rates T across the virtual flight screens for all three flights are shown
326 for **TOS** and **TON** in Figure 1 and plotted in Figure 2. In F20, two distinct **TON** plumes were
327 observed, allowing separate T calculations for **TON**. Monotonic decreases in T were observed
328 for both **TOS** and **TON** during transport downwind in all flights, clearly showing dry
329 depositional losses. The deposition rate D (Methods, Section 2.3) was used to estimate the
330 cumulative deposition of **TOS** and **TON** as a fraction of E_{TOS} or E_{TON} and is shown in Figure 3
331 for F7, F19 and F20 for transport distances of up to 107-135 km downwind of the sources.

332 Curves were fitted to the **TOS** and **TON** dry deposition cumulative percentages from which $d_{1/e}$
333 and τ were determined (SI Table S1). The transport e-folding distance ($d_{1/e}$) was determined
334 where 63.2% of E_{TOS} (or E_{TON}) was dry deposited, i.e., $\sum_{d=0}^{d_{1/e}} D(d) = 0.368E_{TOS}$. The
335 atmospheric lifetimes (τ) were derived as $\tau = d_{1/e}/u$, where u was the average wind speed across
336 the distance $d_{1/e}$. These estimates were compared with predictions from the regional air quality
337 model GEM-MACH (Makar et al., 2018; Moran et al., 2010; SI Section S5) using facility
338 emission rates (Table 2). For **TOS** during F19, (Figure 3b, e), the observed cumulative
339 deposition at the maximum distance accounted for $74 \pm 5\%$ vs. the modelled 21% of E_{TOS} , due
340 mostly to SO_2 dry deposition ($>92\%$). Fitting a curve to D and interpolating the cumulative
341 deposition fraction to the 63.2% E_{TOS} loss leads to a $d_{1/e}$ of 71 ± 1 km, versus 500 km for the
342 model prediction. Under the prevailing wind conditions, the observed distance indicates a τ for
343 **TOS** of approximately 2.2 hours, whereas the model prediction indicated 16 hours. Large
344 observation-based values and model prediction differences in lifetime were also evident for the



345 other flights (SI Table S1). Clearly, the model predictions significantly underestimated
346 deposition and vastly overestimated $d_{I/e}$ and τ . The observation-based values for τ are also lower
347 than average lifetimes of 1–2 days for SO₂ and 2–9 days for pSO₄ derived from global models
348 (Chin et al., 2000; Benkovitz et al., 2004; Berglen et al., 2004), which include the effects of wet
349 deposition and chemical conversion for SO₂, thus making their implicit residence times with
350 respect to dry deposition even longer.

351 For **TON** in F19 (Figure 3h, l), the observed cumulative deposition accounted for
352 $49\pm 11\%$ of E_{TON} at the maximum flight distance, versus 19% predicted by the model. Similar
353 model underestimates for cumulative deposition fractions were found for F7 and F20.
354 Extrapolating to the 63.2% cumulative deposition fraction, $d_{I/e}$ was estimated to be 190 ± 7 km for
355 F19 versus a predicted 650 km from the model, implying a τ of approximately 5.6 hours for the
356 measurement-based results and 23 hours for the model prediction. Again, analogous differences
357 for F7 and F20 were found (SI Table S1). Similar to TOS, the measurement-based $d_{I/e}$ and τ
358 values for TON were significantly smaller than commonly accepted lifetimes of a few days for
359 nitrogen oxides in the boundary layer (Munger et al., 1998).

360 **3.3 Dry Deposition Fluxes F**

361 Using D , the average dry deposition fluxes, F (in tonnes S or N km² hr⁻¹), were calculated
362 by dividing D by the plume footprint surface areas estimated by extending to the plume edges
363 where the concentrations fell to background levels (Methods, Section 2.4). These footprints are
364 shown as the gray shaded geographic areas in Figure 1, totaling 3500, 5700 and 4200km² for F7,
365 F19, and F20 plumes, respectively; see SI Table S1 for **TON** plume areas). Figure 4a shows
366 F_{TOS} values for all three flights, exhibiting exponential decreases with increasing distance away
367 from the sources and showing e-folding distances for F_{TOS} of 18, 27, and 55 km for F7, F19, and



368 F20, respectively. More than 90% of the decreases in F_{TOS} were accounted for by F_{SO_2} .
369 Similarly, F_{TON} decreased exponentially with increasing transport distances in all flights (Figure
370 4c), exhibiting e-folding distances of 18 and 33 km for F7 and F19, and 55 and 189 km for the
371 south and north TON plumes during F20, respectively. These e-folding distances were similar to
372 those for F_{TOS} , indicating similar rates of decreases in F_{TON} with transport distances.

373 As expected from the τ and transport e-folding distance $d_{1/e}$ comparisons, the GEM-
374 MACH model F_{TOS} were significantly lower than the measurement-based F_{TOS} results (Figure
375 4a), with the model F_{TOS} e-folding distances usually large: 133, 797, and 57 km for F7, F19, and
376 F20, respectively, or 7.4, 29.5, and 1.1 times longer than the corresponding measurement results.
377 Part of the differences between model and measurement F_{TOS} could be explained by differences
378 in actual versus model emissions, E_{TOS} (Tables 1 vs 2). To remove the influence of emissions,
379 an emission-normalized flux ($=F_{TOS}/E_{TOS}$ and F_{TON}/E_{TON}) was calculated for both measurement
380 and model (SI Figure S1). Figure 4b shows the ratios of measurement to model normalized
381 emissions for TOS. The model emission-normalized fluxes F_{TOS}/E_{TOS} were lower than the
382 measurement-based values by factors of 2.5-14, 1.8-3.4, and 2.0-3.0 for F7, F19, and F20,
383 respectively, decreasing with increased transport distances. However, they coalesce to a factor
384 of 2 at the furthest distances sampled by the aircraft, indicating that the model F_{TOS} estimates
385 were biased low by similar factors. The decreasing trends suggest that at distances further
386 downwind, model fluxes may exceed measurement-based fluxes, albeit at magnitudes lower than
387 those shown in Figure 4a, which is consistent with earlier study results (Makar et al., 2018). For
388 F_{TON} , the model-predicted values were also lower than the measurement results, especially near
389 the sources (Figure 4c), and showed little variation with transport distances for all flights, in
390 strong contrast to the exponential decays observed from the aircraft. However, the emission-



391 normalized fluxes ($=F_{TON}/E_{TON}$) for the model approached those from measurements within
392 maximum flying distances for F19 and F20, although still significantly lower for F7 ($>10x$)
393 (Figure 4d).

394 **3.4 Dry Deposition Velocities V_d**

395 The shorter $d_{1/e}$ and τ , and larger deposition fluxes F near the sources determined from
396 the aircraft measurements compared to predictions by the GEM-MACH model indicate that the
397 model V_d was underestimated. Gas-phase V_d in the model is predicted with a standard inferential
398 “resistance” algorithm (Wesley, 1989; Jarvis, 1976), with resistance to deposition calculated for
399 multiple parameters including aerodynamic, quasi-laminar sublayer and bulk surface resistances
400 (Baldocchi, 1987). To demonstrate the model underestimation in V_d , comparisons between the
401 measurement-based and model V_d were made where an evaluation of V_d for **TOS** and **TON** was
402 possible. All F_{SO_2} were converted into V_{d-SO_2} by dividing F_{SO_2} by interpolated SO_2
403 concentrations at 40 meters above ground, averaging 1.2 ± 0.5 , 2.4 ± 0.4 , and 3.4 ± 0.6 $cm\ s^{-1}$ for F7,
404 F19 and F20, respectively, across the plume footprints (Methods, Section 2.4 and SI Table S2).
405 The corresponding model V_{d-SO_2} derived in the same way as the observations was 0.72, 0.63, and
406 $0.58\ cm\ s^{-1}$, 1.7-5.4 times lower than observations (SI Section S5; SI Table S2). Interestingly,
407 the median V_d for SO_2 of $4.1\ cm\ s^{-1}$ determined using eddy covariance/vertical gradient
408 measurements from a tower in the AOSR is higher than the mass balanced method showing an
409 even larger discrepancy compared to the model (SI Section S3; Figure S4). Similarly, derived
410 V_{d-TON} averaged 2.8 ± 0.8 , 1.6 ± 0.5 , 4.7 ± 1.4 and $2.2\pm 0.7\ cm\ s^{-1}$ F7, F19, F20 south plume, and F20
411 north plume, respectively (SI Table S2), 1.2-5.2 times higher than the corresponding modelled
412 V_{d-TON} of 1.4, 1.3, 0.92, and $0.90\ cm\ s^{-1}$.

413



414 **3.5 Monte-Carlo simulations of V_d for SO₂**

415 To further demonstrate observation-model differences, V_d distributions of SO₂ from five
416 common inferential dry deposition algorithms (Wu et al., 2018; Makar et al., 2018) were
417 determined for the conditions encountered during the flights using a Monte-Carlo approach as
418 described in Methods, Section 2.5). Results for the V_d simulations algorithms are shown in
419 Figure 5a. Histograms for all five algorithms have peak V_d values at ~ 1 cm s⁻¹ or lower.
420 Probability distributions for the individual resistance terms, R_a , R_b , and R_c showed that the
421 dominant resistance driving V_d was the R_c term (SI Figure S2). Also shown in Figure 5a are the
422 measurement-derived V_d for Flights 7, 19 and 20, and that from the Oski-ôtin ground site. The
423 observed V_d values are larger than the V_d values for most of the simulations, with the exception
424 of Flight 7, where the Zhang et al. (2002), NOAA-GEM (Wu et al., 2018) and C5DRY (Wu et
425 al., 2018) algorithms' distributions agree with the observations. All algorithms are biased low
426 relative to the observations for the remaining flights, and the Oski-ôtin ground site. It is noted
427 that the ground-site observations that were derived using a standard flux tower methodology (SI
428 Section S3) at a single site, appeared to be higher than all other V_d ; nevertheless, these
429 observations are closer to the aircraft values than the algorithm estimates. These results indicate
430 that an underestimation of V_d relative to both aircraft and ground based measurements in the
431 AOSR region is not unique to the GEM-MACH model or its dry deposition algorithm; similar
432 results would occur with the other algorithms included in the Monte-Carlo simulations, all of
433 which are used within other regional models.

434 To investigate the possible reasons behind the low model V_d relative to the observations,
435 a series of sensitivity tests using SO₂ were conducted. Differences in model V_d have been shown
436 to be mainly due to differences in the calculated R_c (Wu et al., 2018), and sensitivity tests here



437 indicated that R_c is particularly sensitive to the cuticular resistance R_{cut} . Hence, factors causing
438 R_{cut} to change can have significant impact on model V_d . In some of the algorithms, R_{cut} and
439 other resistance terms are dependent on the effective Henry's Law constant K_H^* for SO_2 . The
440 Monte-Carlo simulations for Figure 5 assumed a surface pH= 6.68 resulting in a K_H^* of 1×10^5 for
441 SO_2 . Additional Monte-Carlo simulations were performed for the GEM-MACH dry deposition
442 algorithm by adjusting K_H^* assuming different pH with small variations from a pH=6.68
443 significantly changing R_c , R_{cut} , and V_d (SI Figure S3). In Figure 5b – red dashed line, with a
444 surface pH change from 6.68 to 8, consistent with possible alkaline surfaces in the AOSR
445 (Makar et al., 2018), in the GEM-MACH simulation, the V_d distribution is moved to larger
446 values) with its peak value shifting from 0.6 to 1.4 $cm\ s^{-1}$. These results show that model V_d may
447 be highly sensitive to assumed surface pH, at least when using some inferential dry deposition
448 algorithms which are pH-dependent. However, Figure 5b shows that this pH-associated increase
449 in V_d is still insufficient to encompass the range of measurement-derived V_d . Increasing pH to 8
450 for the GEM-MACH simulation reduces R_{cut} , hence R_c , to values much smaller than R_a and R_b ,
451 suggesting that model V_d cannot further increase without reductions in both R_a and R_b . In other
452 words, R_a and R_b were probably overestimated in the current deposition velocity algorithms. By
453 using the Zhang et al. (2002) R_a and the NOAA-GEM (Wu et al., 2018) R_b parameterizations in
454 the GEM-MACH algorithm, a further shift of the GEM-MACH V_d distribution to larger values
455 was found, with the range encompassing most of the observations (Figure 5b, pink dashed line).

456 Clearly, from the Monte-Carlo simulations for SO_2 V_d comparisons, inferential dry
457 deposition algorithms as used in regional and global chemical transport models need to be further
458 validated and improved, especially over large geographic regions. Here, the role of pH was
459 identified for improvement in some algorithms along with possible improvement in aerodynamic



460 and quasi-laminar sublayer resistance parameters. Yet, for other algorithms and for **TON**
461 compounds, the model low-biases in V_d remain to be investigated.

462 The underestimates suggest that the applications of these algorithms in regional or global
463 models may significantly underestimate model predictions of **TOS** dry depositional loss from the
464 atmosphere. Underestimates in V_d are the result of a combination of uncertainties in the
465 parameterizations of each algorithm. In the case of the algorithm used in GEM-MACH, by
466 adjusting the assumed surface pH from 6.68 to 8 (justifiable given the considerable dust
467 emissions in the region (Zhang et al., 2018)), the model V_d moved closer to the aircraft-derived
468 values (Figure 5b), reducing the model-observation gap by approximately 2/3. In addition,
469 substituting the aerodynamic resistance and quasi-laminar sublayer resistance parameterizations
470 in the GEM-MACH algorithm with that from Zhang et al. (2002) and NOAA-GEM (Wu et al.,
471 2018), respectively, resulted in a further increase in the model V_d distribution that encompasses
472 most of the observations (Figure 5b). Clearly, different algorithms respond differently to
473 changes in the parameterizations, and validation and adjustment to each algorithm needs
474 measurement-based results over large regions such as derived here.

475

476 **4 Conclusions**

477 The atmospheric transport distances and lifetimes $d_{1/e}$ and τ determined from the aircraft
478 measurements are substantially shorter than the GEM-MACH model predictions, and the dry
479 deposition fluxes and velocities F and V_d near sources are larger compared to the predictions by
480 GEM-MACH and five inferential dry deposition velocity algorithms, respectively. There are
481 important implications for these measurement-model discrepancies. Such discrepancies indicate
482 that regional or global chemical transport models using these algorithms are biased low for local



483 deposition and high for long-range transport and deposition, and **TOS** and **TON** loss from the
484 atmosphere are significantly under-predicted, resulting in overestimated lifetimes. Moreover,
485 emissions assessed through network measurements or budget analysis of atmospheric **TOS** and
486 **TON** (Sickles and Shadwick, 2015; Paulot et al., 2018; Berglen et al., 2004) may be
487 underestimated due to lower V_d used in these estimates, and may require reassessing the
488 effectiveness of control policies. Shorter τ for **TOS** and **TON** reduces their atmospheric spatial
489 scale and intensity of smog episodes, potentially reducing human exposures (Moran et al., 2010).
490 Importantly, shorter τ for **TOS** and **TON** reduces their contribution to atmospheric aerosols;
491 consequently, the negative direct and indirect radiative forcing from these sulfur and nitrogen
492 aerosols are reduced, reducing their cooling effects on climate (Solomon et al., 2007). These
493 impacts suggest that more measurements to determine τ and F for these pollutants across large
494 geographic scales and different surface types are necessary to better quantify their climate and
495 environmental impacts in support of policy. While in the past such determination was difficult
496 and/or impossible, the present study provides a viable methodology to achieve such a goal.

497

498



499 **Table 1.** Average observed meteorological conditions and facility emission rates of **TOS** (E_{TOS})
 500 and **TON** (E_{TON}), (determined from extrapolated (to distance=0) transfer rates; Figure 1) for
 501 **TOS** and **TON** during the F7, F19 and F20 flights. SP=south plume; NP=north plume.

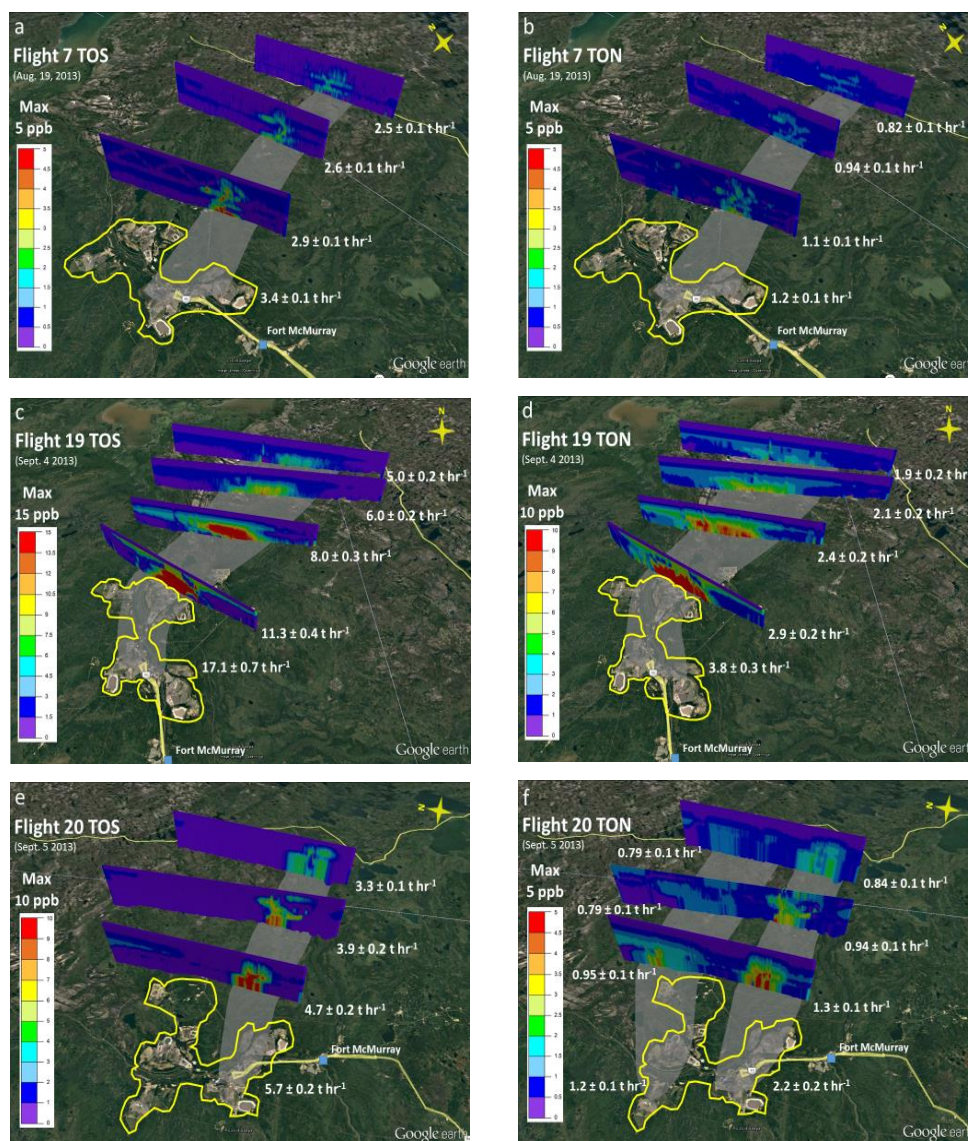
Flight	Date	Time (UTC)	Mean wind speed (m/s)	Mean wind direction (°)	Mixed layer height (m agl)	E_{TOS} (t/hr)	E_{TON} (t/hr)
7	Aug 19/13	2007–0108	13.0±1.0	256±11.7	2500±100	3.4	1.2
19	Sep 4/13	1854–2353	9.5±1.9	218±16	1200±100	18.5	3.9
20	Sep 5/13	1933–2436	8.9±1.2	281±11	2100±100	5.8	2.2 (SP) 1.2 (NP)

502

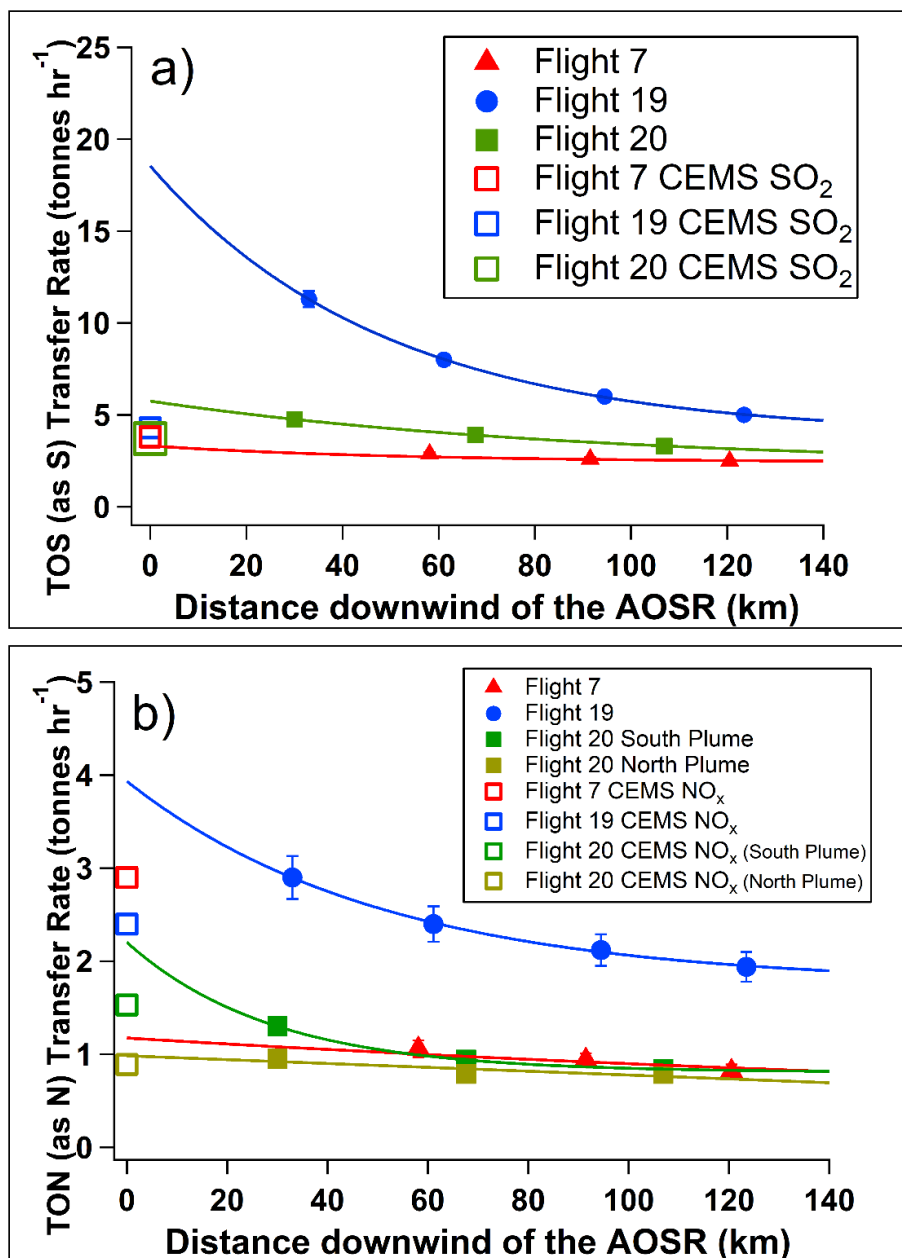
503 **Table 2.** Model average meteorological conditions and facility emission rates of **TOS** (E_{TOS}) and
 504 **TON** (E_{TON}) during the F7, F19 and F20 flights as described above. SP=south plume; NP=north
 505 plume.

Flight	Date	Time (UTC)	mean wind speed (m/s)	mean wind direction (°)	mixed layer height (m agl)	E_{TOS} (t/hr)	E_{TON} (t/hr)
7	Aug 19/13	2007–0108	12.6±0.3	253±5.0	1670±80	3.8	2.9
19	Sep 4/13	1854–2353	8.1±1.0	225±4.6	1450±43	4.3	2.4
20	Sep 5/13	1933–2436	9.1±0.7	275±1.6	1590±42	3.7	1.5 (SP) 0.9 (NP)

506



514 **Figure 1.** TOS and TON plumes downwind of the AOSR during three Lagrangian flights, F7,
515 F19 and F20. The AOSR facilities are enclosed by the yellow outline. The transfer rates T in
516 tonnes S or N hr^{-1} across each screen are shown. The grey shaded surface areas are identified as
517 the geographic footprint under the plumes. Data: Google, Image 2016 Digital Globe © Google
518 Maps.

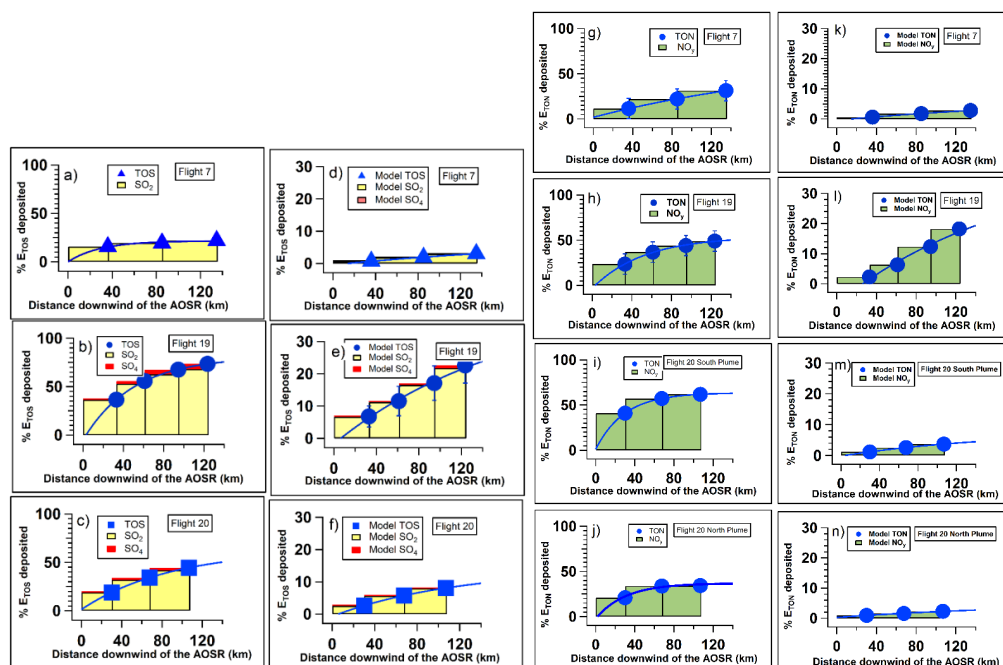


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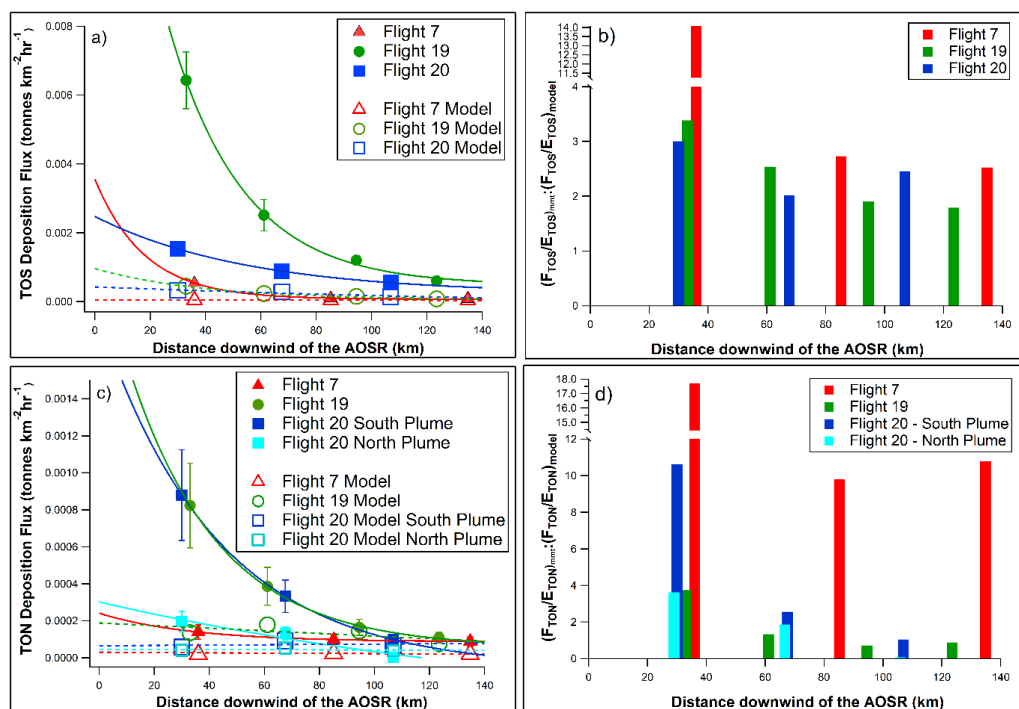
520 **Figure 2.** TERRA-derived transfer rates of (a) TOS and (b) TON for F7, F19 and F20. The
521 vertical bars indicate the propagated uncertainties. The model emission rates E_{TOS} and E_{TON} are
522 shown by the open symbols.



523



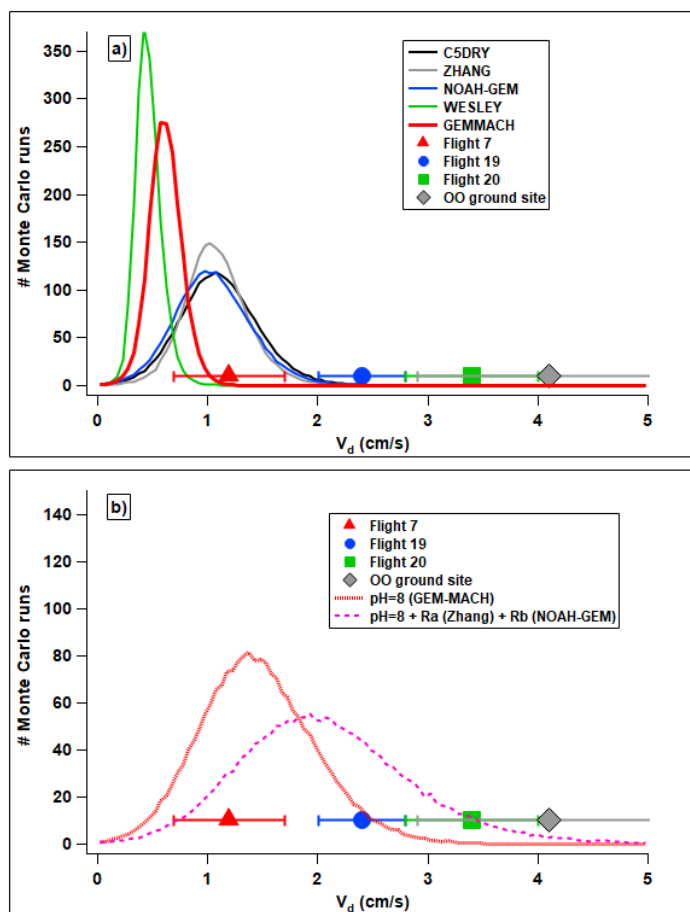
524 **Figure 3.** Cumulative dry deposition as a percentage of emissions of E_{TOS} E_{TON} for F7, F19 and
 525 F20 measurements and GEM-MACH model predictions. The bars show the dry deposition due
 526 to SO_2 and pSO_4 . The curves were fitted to the **TOS** and **TON** dry deposition percentages from
 527 which $d_{1/e}$ and τ were determined.



528

529 **Figure 4.** Dry deposition fluxes F_{TOS} and F_{TON} determined from measurements (solid symbols)
 530 and GEM-MACH model predictions (open symbols). (a) F_{TOS} , (b) ratios of measurement to
 531 model normalized emissions F_{TOS}/E_{TOS} , (c) F_{TON} , and (d) ratios of measurement to model
 532 normalized emissions F_{TON}/E_{TON} .

533



534

535 **Figure 5.** (a) Distributions of V_d for SO_2 from Monte-Carlo simulations using 5 different
536 deposition parameterizations (Wu et al., 2018; Makar et al., 2018) and (b) Monte-Carlo
537 simulations for the GEM-MACH algorithm using a pH=8 and using a pH=8 plus replacing the
538 GEM-MACH algorithm R_a and R_b formulae with that from Zhang et al. (2002) and NOAH-GEM
539 (Wu et al., 2018), respectively. Aircraft-derived V_d for F7, F19 and F20 as well as the median
540 value for the Oski-ôtin ground site (SI Figure S4) are shown in both (a) and (b) for comparison.
541



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704 **Author Contribution:**

705 KH, SML, JL, SM, RM, RS, JO, MW all contributed to the collection of aircraft observations in the field.
706 KH, RM and JO made the SO₂, NO_y and pSO₄ measurements and carried out subsequent QA/QC of data.
707 RM analyzed canister VOCs and provided OH concentration estimates. SM provided OH estimates from
708 MCM modelling as a comparison. AD contributed to the development of TERRA. JL wrote the Monte
709 Carlo code. PM and AA ran the model and provided model analyses. JZ provided emissions data. LZ and
710 RS provided deposition algorithm parameters. KH and SML wrote the paper input from all co-authors.

711 **Code availability**

712 All the computer code associated with the TERRA algorithm, including for the kriging of pollutant data, a
713 demonstration dataset and associated documentation is freely available upon request. The authors request
714 that future publications which make use of the TERRA algorithm cite this paper, Gordon et al., Liggio et
715 al., or Li et al. as appropriate.

716 **Data availability**

717 All data used in this publication are freely available on the Canada-Alberta Oil Sands Environmental
718 Monitoring Information Portal: [https://www.canada.ca/en/environment-climate-change/services/oil-
719 sands-monitoring/monitoring-air-quality-alberta-oil-sands.html](https://www.canada.ca/en/environment-climate-change/services/oil-sands-monitoring/monitoring-air-quality-alberta-oil-sands.html)
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728 The authors declare no competing interests.