A transition in atmospheric emissions of particles and gases from on-road heavy-duty trucks

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11 Abstract. The transition in extent and characteristics of atmospheric emissions caused by the modernisation of the heavy-duty 12 on-road fleet were studied utilising roadside measurements. Emissions of particle number (PN), particle mass (PM), black 13 carbon (BC), nitrogen oxides (NO_x), carbon monoxide (CO), hydrocarbon (HC), particle size distributions and particle 14 volatility were measured from 556 individual heavy-duty trucks (HDTs). Substantial reductions in PM, BC, NO_x, CO and to 15 a lesser extent PN were observed from Euro III to Euro VI HDTs by 99%, 98%, 93% and 57% for the average emissions 16 factors of PM, BC, NO_x, and CO respectively. Despite significant total reductions in NO_x emissions, the fraction of NO₂ in the 17 NO_x emissions increased continuously from Euro IV to Euro VI HDTs. Larger data scattering was evident for PN emissions 18 in comparison to solid particle number (SPN) for Euro VI HDTs, indicating a highly variable fraction of volatile particle 19 components. Particle size distributions of Euro III to EEV HDTs were bimodal, whereas those of Euro VI HDTs were 20 nucleation mode dominated. High emitters disproportionately contributed to a large fraction of the total emissions with the 21 highest-emitting 10% of HDTs in each pollutant category being responsible for 65% of total PM, 70% of total PN and 44% of 22 total NO_x emissions, respectively. Euro VI HDTs, which accounted for 53% of total kilometres driven by Swedish HDTs, were 23 estimated to only contribute to 2%, 6%, 12% and 47% of PM, BC, NO_x, and PN emissions. A shift to a Euro VI HDTs dominant 24 fleet would promote a transition of atmospheric emissions towards low PM, BC, NO_x and CO levels. Nonetheless, reducing 25 PN, SPN, and NO₂ emissions from Euro VI HDTs is still important to improve air quality in urban environments.

26 **1 Introduction**

Vehicular emissions contribute significantly to gaseous and particle pollutants in the urban atmosphere and description of their extent and characteristics are key input components for urban air quality modelling. As technology and traffic demands change, so do the characteristics of the emissions. In Europe, the introduction of new legislation, especially Euro VI, has aimed to 30 reduce emissions of many pollutants. Legislation exists for particles (mass and number) and selected gases, however, there are 31 also many components of the emissions that are not directly regulated but are potentially detrimental to human health. The 32 most notable example of a non-regulated pollutant is the abundance of ultrafine particles (UFP) (Campagnolo et al., 2019), 33 defined as particles with a diameter less than 100 nm (Zhu et al., 2002). UFPs can cause lung disease, an increase of blood 34 coagulability and cardiovascular disease and related mortality (Du et al., 2016). In the most recent Euro class, this has partly 35 been covered by introducing a limit on the solid particle number (SPN) while volatile particles and particles less than 23 nm 36 are not considered. Furthermore, the legislation has mainly been based on test cycles performed before introducing a new 37 engine into the market but only recently also off-cycle and in-service conformity testing has been introduced, hence the actual 38 performance in real-traffic is less constrained, where driving pattern, maintenance, and age of engine will vary. Here real-39 traffic studies may capture variability between vehicles and also put the effect of new legislation and parallel phase-out of 40 older technology into perspective for the abatement of urban air pollution.

41 Heavy-duty vehicles (HDVs) usually account for a smaller number fraction of on-road vehicles than light-duty vehicles 42 but they tend to contribute to a disproportionately high fraction of mobile source particulate matter emissions (Gertler, 2005; 43 Cui et al., 2017). Emissions from HDVs, often diesel, are significantly affected by the engine type, exhaust after-treatment 44 system (ATS), and driving conditions. The main purpose of ATS is the reduction of particulate and gaseous pollutants. Diesel 45 Oxidation Catalysts (DOC) are used for reducing hydrocarbon emissions, selective catalytic reduction (SCR) systems or 46 exhaust gas recirculation (EGR) are employed to mitigate NO_x emissions, and diesel particulate filters (DPF) can reduce 47 particulate matter mass emissions. The use of ATS can, however, bring undesired side effects. For example, conversion of SO₂ 48 to SO₃ and increased gaseous sulfuric acid formation have been reported from DOCs (Arnold et al., 2012). DPFs potentially 49 enhance the formation of UFP (Herner et al., 2011; Preble et al., 2017). Retrofitted DPF can slightly reduce the NO_x emissions 50 but significantly increase the direct emission of NO₂ by as much as a factor of 8 (Smith et al., 2019). Failure of the temperature-51 dependent SCR in eliminating the excess NO₂ leads to an elevated NO₂ to NO_x ratio (Herner et al., 2009; Bishop et al., 2010; 52 He et al., 2015).

53 The Euro standard regulates vehicle emission limits in Europe. The Euro III standard was established in 1999, and more 54 stringent Euro IV and Euro V standards were implemented in 2005 and 2008, respectively. The Enhanced Environmentally 55 Friendly Vehicle (EEV) is a voluntary environmental standard which lies between the levels of Euro V and Euro VI. The 56 currently enforced Euro VI standard has been implemented since 2013-2014 and introduced SPN limits into the regulation for 57 the first time. Generally, newer engines are expected to perform better in controlling pollutant emissions. Guo et al. (2014) 58 reported that Euro V diesel buses performed better than Euro IV and Euro III diesel buses in the emissions of all the pollutants, 59 except for the generation of more nucleation mode particles. The latest 2018 European Environmental Agency (EEA) report 60 confirms an overall improvement in the European air quality, while the road transport sector remains one of the major 61 contributors to pollutant emissions and the largest contributor to the total NO_x emission (Grigoratos et al., 2019; EEA, 2018). 62 A recent on-board sensor-based study pointed out that HDVs emitted more than three times the NO_x certification standard 63 during real-world hot-driving and idling operations (Tan et al., 2019). Published data regarding particle and gaseous pollutant

emissions from real-world on-road Euro VI heavy-duty vehicles are scarce and often limited by the small sample size (Giechaskiel et al., 2018; Grigoratos et al., 2019; Moody and Tate, 2017). Remote sensing sampling can measure a large sample size of vehicles but are usually restricted to gaseous pollutant emissions (Burgard and Provinsal, 2009; Burgard et al., 2006; Carslaw et al., 2011). From an air quality perspective, the particle emissions are crucial. The complexity and dynamics of atmospheric particles require detailed information of its emission for atmospheric modelling and for descriptions of their health impacts. For example, particle size is important to determine the effects on respiratory deposition in humans (Manigrasso et al., 2017; Lv et al., 2016).

71 Diesel exhaust particles are a complex mixture of numerous semi-volatile and non-volatile species, and the semi-volatile 72 compounds will experience gas-to-particle partitioning in the atmosphere (Robinson et al., 2007; Donahue et al., 2006). Biswas 73 et al. (2009) reported that the semi-volatile fraction in HDV emission is more oxidative than the refractory particles, which 74 may change the redox state in cells and cause oxidative stress. Semi-volatile organic compounds, such as PAHs and their 75 derivatives may possess genotoxic and carcinogenic characteristics (Bocchi et al., 2016; Vojtisek-Lom et al., 2015). 76 Giechaskiel et al. (2009) suggested using the volatile mass fraction as a metric to assess health effects as the volatile mass 77 dissolves in the lung fluid and thereby interacts with epithelial cells. Deploying a Volatility Tandem Differential Mobility 78 Analyzer in suburban Guangzhou, China, Cheung et al. (2016) found that 57–71 % of ambient particles between 40 and 300 nm 79 contain volatile components. Furthermore, the evaporated semi-volatile compounds from the particle phase can be further 80 oxidized to form secondary organic aerosols (SOA) (Hallquist et al., 2009; Gentner et al., 2017). To better quantify the health 81 effects and global and regional contributions of road traffic to the total particle burden in the atmosphere, information on the 82 volatility properties of vehicle particulate emissions is needed.

83 Different approaches have been applied to study the emissions from HDTs (Franco et al., 2013). Chassis dynamometer 84 tests provide relatively comprehensive emission characteristics of individual vehicles (Jiang et al., 2018; Chen et al., 2018; 85 Thiruvengadam et al., 2015), but the artificial driving cycles make it difficult to simulate the full range of real-world driving 86 conditions. Portable emission measurement systems (PEMS) (Grigoratos et al., 2019; Piriola et al., 2017) and plume chasing 87 studies (Lau et al., 2015; Pirjola et al., 2016) have been conducted in real-world environments but are often limited by small 88 sample sizes. Tunnel studies (Li et al., 2018) measure the average emission of all vehicles passing through the tunnel without 89 specific emission information of vehicle types. Roadside measurements, as presented in this study, provide an opportunity to 90 study real-world on-road traffic emissions on large sample sizes with individual vehicle information (e.g. Hallquist et al., 2013; 91 Dallmann et al., 2012; Carslaw and Rhys-Tyler, 2013; Watne et al., 2018).

In this work, we measured the gaseous and particle emissions from 556 on-road individual HDTs and quantified changes in emissions and the potential transition in characteristics caused by the reduction achieved by the introduction of more stringent Euro standards. Particle size distributions and particle volatilities were investigated with respect to Euro class, and pollutant emission characteristics were studied with respect to year of registration. Cumulative pollutant distributions were established to demonstrate the importance of controlling high-emitters in reducing total emissions. The typical contribution of air pollution emissions from each Euro class HDTs was estimated based on total vehicle kilometres driven. Results of the 98 presented pollutant emission factors in our study will be useful for both emission models and emission inventories. A clear

99 transition of atmospheric pollutant emission trends was evident and can provide useful guidance for policies regarding the 100 regulation of existing fleets.

101 **2 Methods**

102 **2.1 Field sampling site**

Pollutant emissions from HDTs were measured at a roadside location in Gothenburg, Sweden (Fig. 1). The HDTs passed the sampling location with an average speed of 27 km h^{-1} and acceleration of 0.7 km h^{-1} s⁻¹ on a slight uphill slope (~2°). Under such uphill driving conditions, vehicles are expected to emit higher levels of pollutants than during downhill and cruise driving. This will be further examined in Sect. 3.3.

107 2.2 Air sampling

108 The sampling of the emissions was conducted in line with Hallquist et al. (2013), i.e. extractive sampling of passing HDT 109 plumes. Air was continuously drawn through a flexible copper tube to the instruments inside a container. A similar 110 experimental set-up was previously applied to on-road bus emission measurements (Liu et al., 2019). Particles were measured 111 by an EEPS (Engine Exhaust Particle Sizer, Model 3090 TSI Inc.) in the size range of 5.6-560 nm with high time resolution 112 (10 Hz) while total particle number was measured by a butanol-based condensation particle counter (CPC Model 3775 TSI 113 Inc., 50 cut-off diameter 4 nm). Particle numbers measured by the two instruments showed a good correlation ($R^2=0.73$) 114 (Fig. S1). A second EEPS measured the outflow of a TD (thermodenuder, Dekati, Inc.), enabling estimations of particle 115 volatility. The data were corrected for size-dependent losses in the TD. The temperature inside the TD heating zone was set to 116 250° C with a residence time of ~ 0.6 s, which is generally sufficient to evaporate nearly all the organics and sulphates from 117 the particles (Huffman et al., 2008). However, organics with extremely low volatility (organic saturation mass concentration, 118 119 define the 'non-volatile components' as particle components that remain after passing through the TD operating at 250°C. 120 Differences in counting efficiencies between the two EEPS were accounted for by size-dependent correction factors (typically 121 less than 10%), which were retrieved by simultaneous sampling of ammonium sulphate particles by both EEPS and direct 122 comparison of their measured size distributions (Fig. S2). BC and the mixture of BC and brown carbon (BrC) were measured 123 by an Aethalometer at 880 nm and 370 nm respectively (Model AE 33, Magee Scientific Inc.). The determination of particle 124 mass concentrations by the integrated particle size distribution (IPSD) method requires information on particle density. Particle 125 sphericity and unit density were assumed due to a lack of detailed knowledge about the chemical composition of the emitted 126 particles. Figure S3 shows that there is a good linear relationship at EF_{PM} larger than 1 mg (kg fuel)⁻¹ between the BC mass 127 measured by the Aethalometer and the non-volatile particle mass measured by the EEPS but assuming sphericity and unit 128 density the EEPS mass is lower, which indicates a potential underestimation of the effective non-volatile particle density. 129 Compared to the EEPS, the detection limit of the Aethalometer is five times higher, which may influence the correlation 130 between BC and PM at low mass loading conditions (Fig. S3). There have been several studies on the morphology and density 131 of combustion generated particles and its detailed dependence on combustion and dilution condition (e.g. Maricq and Ning, 132 2004; Ristimaki et al., 2007; Liu et al., 2009; Zheng et al., 2011; Ouiros et al., 2015). However, to be consistent, avoid 133 assumptions and to compare with a majority of previously reported data, unity density was used for further discussion and 134 comparisons. CO₂ was measured by a non-dispersive infrared gas analyser (LI-840, LI-COR Inc.). NO₃ and NO were measured 135 simultaneously by two separate chemiluminescent analysers (Model 42i, Thermo Scientific Inc.), and the NO₂ concentration 136 was calculated from the difference between the NO_x and NO concentrations. SO₂ was measured by a pulsed fluorescence gas 137 analyser (Model 43c, Thermo Scientific Inc.). A Remote Sensing Device (RSD) (OPUS Inspection Inc.) was used to measure 138 the gaseous emission factors of CO, NO_x, and HC. Briefly, the instrument was set up with a transmitter and a receiver on the 139 same side of the truck passing lane and a reflector on the opposite side. Co-linear beams of IR and UV light are emitted and 140 cross-reflected through the plume and light attenuation related to respective pollutant concentrations are measured. Gas 141 pollutant concentrations were determined relative to CO₂ as measured by the RSD. NO_x and NO measured by the gas analysers 142 and the RSD were in agreement (R²=0.53 and 0.66 respectively, Figs. S4, S8a). The High-Resolution Time-of-Flight Chemical 143 Ionization Mass Spectrometer (HR-ToF-CIMS) shown in Fig. 1 was used to characterise the chemical composition of organic 144 and inorganic compounds in the gas and particle phase, emitted from the HDTs. However, the extensive chemical 145 characterisation is beyond the scope of this work and will be presented elsewhere.

146 A schematic of the experimental setup is given in Fig. 1 along with some examples of typical temporal profiles of pollutant 147 concentrations in the plumes from Euro III and Euro VI HDTs. A camera at the roadside recorded the HDT plate numbers, 148 which was used for identification and to obtain engine Euro type information. All the instruments were at least operated at 1Hz 149 of sampling frequency to capture rapidly changing concentrations during the passage of a HDT, which is sufficiently fast to 150 measure pollutant concentration peaks (typically 5 to 20 s in duration) as shown in Fig. 1c-e. In general, the duration of a peak 151 was around 5s, for NO_x slightly longer, limiting measurements of high-frequency passages. Euro III HDTs typically emitted a 152 significant amount of PN, PM, NO_x, and non-volatile components (Fig. 1c). More than 95% of Euro III, Euro IV, Euro V, and 153 EEV HDTs had measurable particle emission signals. Significant differences in low particle and gaseous emissions were 154 evident for Euro VI HDTs (Fig. 1d and e).

155 2.3 Data analysis

The exact time of individual HDTs passing the sampling inlet was determined from the camera recordings and the associated plume pollutant concentrations were integrated to calculate corresponding pollutant emission factors of individual HDTs as described by Hallquist et al. (2013). Emissions of gases and particles from individual HDTs were normalized by the CO₂ concentration to compensate for different degrees of dilution during sampling (Janhäll and Hallquist (2005)). CO₂ peak concentrations exceeding four times the standard deviation of the background signal were used as the base criterion for successful plume capture. Peaks in NO_x, PN, PM, and BC concentrations concurrent with that of CO₂ signify the presence of co-emitted pollutants in a HDT plume. Emission factors (EFs) of gaseous and particle emissions for individual HDTs can then be expressed in units of amount of pollutant emitted per kg fuel burned based on the carbon balance method (Ban-Weiss et al., 2009; Hak et al., 2009):

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$$EF_{pollutant} = \frac{\int_{t_1}^{t_2} ([pollutant]_t - [pollutant]_{t_1})dt}{\int_{t_1}^{t_2} ([co_2]_t - [co_2]_{t_1})dt} \times EF_{co_2} , \qquad (1)$$

166 where $EF_{pollutant}$ is the emission factor of the respective pollutant. The time interval of t_1 to t_2 represents the period when the 167 instruments measured the concentration of an entire pollutant peak from an individual HDT (see Fig. 1c-e). Dallmann et al. 168 (2011) and Preble et al. (2015) used the concepts of inflection points to identify t_1 and t_2 . In our study, t_1 and t_2 were determined 169 similarly: t_1 is the point before the pollutant concentration intensity increases abruptly and t_2 is when the intensity becomes 170 relatively flat and undistinguishable compared to background levels. It is noted that the integrated peak intensity is insensitive 171 to the exact location of t_2 since the added integrated signals at or beyond this point are fluctuating around zero. t_1 and t_2 were 172 determined independently of each pollutant peak to account for differences in the time response of individual instruments to the exhaust plume. $\int_{t_1}^{t_2} ([pollutant]_t - [pollutant]_{t_1}) dt$ and $\int_{t_1}^{t_2} ([CO_2]_t - [CO_2]_{t_1}) dt$ are the changes in concentration of a 173 174 pollutant and CO₂ during this time interval. EF_{CO2} of 3158 g (kg diesel fuel)⁻¹ was used as the emission factor of CO₂, assuming 175 complete combustion and a carbon content of 86.1% as given in Edwards et al. (2014). Emission factors for plumes with 176 pollutant concentrations lower than our set detection limit (four times the standard deviation of the pollutant background signal) 177 were replaced by the minimum value among all recorded emission factors (EF_{min}) rather than being omitted to avoid inflating 178 emissions from low-emitting HDTs.

179 **3 Results and Discussion**

180 **3.1 Fleet compositions**

181 A total of 675 resolved plumes from 556 individual HDTs for the carriage of goods with weights exceeding 12 tonnes were 182 identified. There were 330 Swedish HDTs with Euro type information, 46 Swedish HDTs from which Euro type information 183 was not available, and 180 foreign licensed non-Swedish HDTs. Among the 330 Swedish trucks, Euro III, Euro IV, Euro V, 184 EEV, and Euro VI HDTs accounted for 3%, 5%, 30%, 5%, and 57%, respectively (Fig. S5).

185 **3.2 Emissions variability**

Differences in operating and ambient conditions may lead to differences in pollutant emission factors for the same HDT. In this study, we utilized measurement data from 55 HDTs which passed the sampling location repeatedly, yielding a total of 137 plumes. The average pollutant emission factors of each HDT plotted against the individual plume measurements of the corresponding HDT are shown in Fig. S6. In general, the emission factors of PM, non-volatile PN, and NO_x showed little 190 variation ($R^2 \ge 0.77$) among multiple passages of the same HDT, however, higher variability was observed in the PN emissions.

191 This is likely related to variations in the formation of nucleation mode particles from volatile compounds which is more

sensitive to driving (Zheng et al., 2014) and dilution conditions. In the following discussion, for HDTs with multiple passages,

193 the average pollutant emission factors of all the detected plumes were used for that individual HDT.

194 **3.3 Emissions factors (EFs) of particles and gaseous pollutants**

195 Figure 2 a and b show the box-and-whisker plots of PM and PN emission factors (EFs) for different Euro classes. Generally, 196 both PM and PN emissions decreased with more stringent Euro emission standards, and especially for Euro VI where larger 197 changes in emission characteristics were evident. These decreasing trends are statistically significant at the 95% CI using the 198 Jonckheere-Terpstra test, a nonparametric test for trends in ordered groups. In addition to PM and PN, the emission trends of 199 BC, NO_x, CO and HC with respect to the level of stringency of Euro standards were statistically examined. Using Euro III 200 HDTs (median EF_{PM} =586 mg (kg fuel)⁻¹) as a baseline, the median EF_{PM} for Euro IV, Euro V, EEV, and Euro VI HDTs have 201 been reduced by 78.1%, 86.1%, 88.9%, and 99.8% respectively. In particular, Euro VI HDTs has a median EF_{PM} of only 1.4 202 mg (kg fuel)⁻¹ (Fig. 2a). While it is noted that Euro III to Euro VI standard certifications are based on chassis dynamometer 203 cycle measurements, the Euro VI regulations have started to include additional off-cycle and in-service conformity testing. 204 The Euro emission standard of transient testing for heavy-duty engines gives emission limits as brake specific emission factors, 205 as mass (g) or number (#) of a specific pollutant per kWh. In order to enable a comparison with the Euro emission standard, 206 the EFs in g (or #) per kg fuel were converted using a brake specific fuel consumption (BSFC) of 231.5 g kWh⁻¹. This is the 207 average value for the long haul and regional delivery cycles of chassis dynamometer tests of a typical rigid Euro VI 208 truck (Rexeis et al., 2018). The uncertainty of the BSFC for different Euro class HDTs operating over a wide range of engine 209 conditions is generally within 25% (Mahmoudzadeh Andwari et al., 2017; He et al., 2017; Dreher and Harley, 1998; Heywood, 210 1988). Note that our measurements represent points of time similar to those in a cycle where the particle emissions can be most 211 prominent. Looking at a whole cycle, this value will be averaged, hence the results from our instantaneous plume measurements 212 may represent an upper limit of the emissions. In Fig. 2a, the right y-axis gives the EFs converted into units of g kWh⁻¹ and 213 the Euro standards are shown as blue crosses.

214 In general, the measured median EF_{PM} are lower than the Euro standards for all HDT types. In particular, the median 215 EF_{PM} for Euro VI HDTs is more than one order of magnitude lower than the Euro standard regulation value since Diesel 216 Particulate Filters (DPFs) are required for these Euro VI HDTs to comply with PM and PN standards (Williams and Minjares, 217 2016). No information about potential retrofits of tested HDTs was available for the vehicles measured in this study. The 218 effectiveness of DPF in reducing particle emissions have been confirmed by various studies (Martinet et al., 2017; May et al., 219 2014; Mendoza-Villafuerte et al., 2017; Moody and Tate, 2017; Preble et al., 2015). For example, Bergmann et al. (2009) 220 illustrated that post-DPF PM concentrations decreased by 99.5% compared with pre-DPF for the New European Driving Cycle 221 (NEDC). In real-world measurements, at least ~90% reductions in PM emissions compared to typical pre-DPF levels have 222 been reported (Bishop et al., 2015). Euro emission standards for PM of Euro IV and Euro V heavy-duty diesel engine are the

223 same, while the measured median EF_{PM} of the Euro V fleet was around 1.5 times lower than that of the Euro IV fleet. The 224 control of diesel engine emissions typically requires a compromise between NO_x and particle emission reduction (Clark et al., 225 1999). The NO_x emission standard is more stringent for Euro V compared to Euro IV (a factor of 43% lower), and hence Euro 226 V HDTs are generally equipped with SCR or EGR to reduce NO_x . In contrast, Euro IV engines are rarely equipped with NO_x 227 after-treatment systems and thus must achieve the NO_x emission limits by tuning the engine performance parameters at the 228 expense of higher PM emissions (Preble et al., 2018; Van Setten et al., 2001). In each of the Euro III, Euro IV, Euro V, and 229 EEV classes, 25-50% of all the measured HDTs had an EF_{PM} higher than their corresponding Euro standards. As described 230 previously, this comparison with the Euro standard is relative and indicative. The higher emissions from individual HDTs may 231 indicate deterioration of engine performance due to wear caused by aging, mileage accumulation, or inadequate maintenance. 232 Our study shows that Euro VI HDTs generally have low PM emissions, but HDTs from older Euro classes frequently exceeded 233 their PM emission limits, suggesting that improved maintenance and suitable retrofitting of older engines are needed.

234 For PN emissions, EF_{PN} shows an overall trend similar to EF_{PM}. However, large data scatter was evident for Euro VI 235 HDTs, likely due to the sensitivity of nucleation mode particle formation to changes in driving conditions (Fig. 2b). Zheng et 236 al. (2014) reported high concentrations of nucleation mode particles under uphill driving conditions but low concentrations 237 under cruise and downhill driving conditions. It is important to note that the median EF_{PN} of Euro VI HDTs was significantly 238 lower than those from the other Euro type HDTs, which indicates efficient PM removal by the DPF without compromising on 239 total PN emission. Nonetheless, the decrease of particle number in the accumulation mode removes particle surface area 240 available for condensation and therefore favours nucleation of organics from fuel and lubrication oil. Le Breton et al. (2019) 241 confirmed the contribution of lubrication oil in bus emissions. Besides, DPFs can act as a sulphur reservoir and when excess 242 sulphur is released, SO₂ to SO₃ conversion can take place once the after-treatment temperature reaches a critical level (Herner 243 et al., 2011). In this case, total particle number emissions can increase due to nucleation from gas-phase sulphuric acid. Since 244 the fuel sulphur content is low, more than 90% of Euro VI HDTs had an EF_{SO2} lower than the threshold in this study, organics 245 would play a more important role in the formation of nucleation mode particles.

Figure 2c shows that the median EF_{BC} was reduced by more than 99% for Euro VI HDTs compared to Euro III HDTs, and the median EF_{BC} of Euro VI HDTs was even at the threshold (0.2mg (kg fuel)⁻¹). The BC emissions generally showed a decrease from Euro III to Euro VI HDTs (Jonckheere-Terpstra test, *p*<0.01), which is similar to the EF_{PM} trend with the exception of Euro IV HDTs. Compared with Euro V HDTs, the median EF_{BC} of Euro IV HDTs is 35% lower, however, the emission of the mixture of BC and BrC from Euro IV HDTs is higher (Fig. S7a). Euro IV HDTs had the highest BrC contribution to the total light-absorbing substances among all the Euro classes (Fig. S7b).

Figure 2d compares the emissions of NO_2 and NO_x from different Euro class HDTs. The vertical lines represent the different Euro standards. HDTs with either EF_{NO2} or EF_{NOx} lower than the detection limits of the instruments were removed in Fig. 2d for illustration purposes, while all the presented statistical analyse include all the data as outlined above. In general, Euro VI HDTs exhibit more than 90% reduction in both median and average EF_{NOx} compared to Euro III HDTs. This is consistent with Carslaw et al. (2011) who estimated a 93% NO_x reduction from Euro III to Euro VI for heavy goods vehicles

257 (HGV) in the United Kingdom. Relatively, the Euro V HDTs had a larger fraction exceeding its Euro standard, which may be 258 due to the combined effects of poor engine tuning and the inactivity (low temperature) or deterioration of SCR systems. Newer 259 engines tend to exhibit a higher NO₂ emission fraction at a similar NO_x level, and the Euro VI HDTs show a relatively low 260 median EF_{NO2} with a large range of data scatter and several high emitters. A continuous increase of EF_{NO2}/EF_{NOx} was evident 261 from Euro IV to Euro VI HDTs (Fig. S8b). This trend is consistent with Kozawa et al. (2014), who reported an increase in the 262 share of NO₂ to total NO_x from Euro III to Euro V vehicles. Euro VI HDTs have a higher NO₂ fraction because the DOC 263 upstream of the filter is used to convert NO to NO_2 to control the soot loading in the DPF and facilitate the passive 264 regeneration (Van Setten et al., 2001). A failure of the NO₂ reduction due to the inactivity of the SCR, resulting from low 265 exhaust gas temperature, may result in a higher NO₂ emission (Bishop et al., 2010; Heeb et al., 2010; Herner et al., 2009; May 266 et al., 2014; Thiruvengadam et al., 2015). A more significant decrease in NO_x than NO₂ emissions of Euro VI HDTs may cause 267 an increase of EF_{NO2}/EF_{NOx}.

268 Table 1 compares the average emission data of PM and PN of the current work with previous studies according to the 269 HDT type and gives information on used measurement methods and driving conditions. Generally, the EF_{PM} and EF_{PN} in this 270 study are within the reported ranges of HDV emissions in the literature. Our estimated EF_{PM} of Euro III HDTs are comparable 271 to those of Euro III buses in Hallquist et al. (2013) and Pirjola et al. (2016). HDTs and buses within the same Euro class emit 272 similar amounts of PM. Watne et al. (2018) show that DPF retrofitted Euro III buses have much lower particle EFs. While 273 EF_{PM} is highly dependent on driving conditions such as speed and acceleration, the average EF_{PM} of Euro IV, Euro V and EEV 274 HDTs of this study:172, 146, and 78 mg (kg fuel)⁻¹, respectively, are comparable to trends in previous studies (Hallquist et al., 275 2013; Pirjola et al., 2016; Watne et al., 2018). Average EF_{PM} of Euro VI HDTs (5 mg (kg fuel)⁻¹/ 1.1 mg km⁻¹) is within the 276 range of emissions from HDVs with DPFs, e.g., 0.6 - 20.5 mg km⁻¹ for a recent chassis dynamometer test (Jiang et al., 2018) 277 and 2.5 - 8.7 mg km⁻¹ for road measurements in California (Quiros et al., 2016). Note that size ranges and measurement 278 methodologies may differ among the studies as listed in Table 1. Since most of the particle emissions related to road traffic 279 combustion are below 560 nm (Fig. 4), the size range in our study is comparable to most other wider range PM measurements. 280 Larger particles from road measurements of total PM may include non-combustion-related particles, e.g. resuspended road 281 dust, tire and brake particles, and should be interpreted with caution. In contrast to EF_{PM} , a much less obvious decrease in 282 average EF_{PN} was observed across different Euro classes. The reason for the high average particle emission for EEV and Euro 283 VI is likely due to high emissions of nucleation mode particles from a number of HDTs.

In Figure 3a, EF_{PM} and EF_{PN} of individual HDTs in this study and selected previous studies are plotted. HDTs with either EF_{PM} or EF_{PN} lower than the detection limits of the instruments (0.07 mg (kg fuel)⁻¹ and 2.8×10¹¹# (kg fuel)⁻¹ respectively) were removed from the figure (24% of the data) for illustration purposes, while all the presented statistical analyse include all the data as outlined above. Generally, both EF_{PM} and EF_{PN} exhibited a decreasing trend from Euro III to Euro IV and from Euro V to EEV HDTs (Jonckheere-Terpstra test, *p*<0.01). Overall, Euro VI HDTs had drastically lower PM emissions but highly scattered PN emissions. Older Euro type buses retrofitted with DPF were shown to have reduced particle emissions, and some retrofitted Euro III buses (black open triangles in Fig. 3a) may perform as well as Euro VI HDTs, indicating the effectiveness of retrofitting older HDTs.

292 In more recent Euro standards, PN regulation has been introduced. The SPN as defined by the European Particle 293 Measurement Program (PMP) is the number of particles which remain after passing through an evaporation tube with a wall 294 temperature of 300-400°C (Zheng et al., 2011). The PMP only measures and regulates solid particles with a diameter larger 295 than 23 nm because measurements of smaller particles in the nucleation mode have poor repeatability (Martini et al., 2009). 296 SPN larger than 23 nm was integrated into the European emission regulation in 2013 for Euro VI heavy-duty 297 engines (Giechaskiel et al., 2012). A potential issue of evaporation measurements is that a fraction of the sub-23 nm particles 298 can also be formed downstream of the European PMP methodology through re-nucleation of semi-volatile precursors (Zheng 299 et al., 2012; Zheng et al., 2011). In our study, the TD temperature of 250°C is lower than the maximum temperature used by 300 the PMP (300-400°C) and does not follow the exact operation specifications of the PMP. However, Amanatidis et al. (2018) 301 summarised that TD is a suitable alternative approach for the removal of volatile particles. Particles larger than 23 nm 302 downstream of the TD were measured by the EEPS and we integrated the size bins from 23.5 nm to 560 nm to represent the 303 SPN. Figure 3b compares the EFPM and EFSPN of Euro VI HDTs. Generally, after-treatment control systems could not reduce 304 SPN emissions as effectively as PM emissions, indicating that more control of SPN emission of Euro VI HDTs may be 305 necessary.

306 Shown in Table 2 are the average EFs of gaseous pollutants (NO_x, CO, HC) in this study compared with other studies. 307 EF_{NOx} generally decreased from the Euro III (43.3 g (kg fuel)⁻¹) to Euro VI (3.1 g (kg fuel)⁻¹) class, and are in good agreement 308 with reported values for HDTs in the literature. EF_{NOx} of Euro III HDTs is moderately higher in this study. Note that the EF_{NOx} 309 and EF_{PM} of EEV were much higher in Pirjola et al. (2016), in which only a limited number (3-4) vehicles were tested and hard braking was common in approaching a 90° turn before accelerating again. The ratio of EF_{NO2} to EF_{NOx} generally agrees 310 311 with the projection in Kousoulidou et al. (2008), on-road plume chasing measurements in Lau et al. (2015) and remote sensing 312 studies in the UK (Carslaw and Rhys-Tyler, 2013). Carslaw et al. (2019) reported a decreasing trend of EF_{NO2}/EF_{NOx} with 313 vehicle mileage for Euro 6 light-duty diesel vehicles, while no significant trend was identified for Euro VI HDTs in this study. 314 There may be other parameters influencing the NO_x emission. For example, Ko et al. (2019) reported that the NO_x emissions 315 from Euro VI diesel vehicles were 29% higher in a traffic jam than in smooth traffic conditions. The temperature of the exhaust 316 and DPF regeneration may also influence the EF_{NOx} .

Compared with EF_{NOX} , EF_{CO} decreased less pronounced from Euro III to Euro VI HDTs (57%). Compared with newer Euro class HDTs, a larger fraction of HDTs in older Euro classes have an EF_{CO} exceeding the Euro standards, which indicates that engine deterioration may have a serious effect on the CO emissions (Fig. S8c). Hallquist et al. (2013) reported a positive relationship between EF_{CO} and EF_{PM} , i.e. high CO indicates incomplete combustion which favors soot formation. DPFs may also reduce CO in addition to PM (Hallquist et al., 2013), which is in agreement with the lowest CO emission of 15.5 g (kg fuel)⁻¹observed for DPF equipped Euro VI HDTs in this study. HC emission was relatively low for all HDT types, and no obvious decreasing trend was evident for EF_{HC} from Euro III to Euro VI HDTs (Jonckheere-Terpstra test, *p*=0.895) (Fig. S8d and Table 2). This does not reflect the more stringent Euro standard limit regarding HC where the Euro VI limit is more than

325 a factor of three lower than the preceding Euro V/IV standards.

The 46 Swedish HDTs without available Euro type information emitted similar levels of particle and gaseous pollutants to Euro VI HDTs and were thus likely equipped with newer Euro engines.

- Compared with the fleet of non-Swedish HDTs, the Swedish HDT fleet generally have a lower median and average EF_{NOx} but there are no significant differences in the EF of other pollutants (Fig. 2 and Tables 1 and 2). The differences in EF_{NOx} are significant at the statistical 95% CI using the Kolmogorov-Smirnov test, used in favour to typical student t-test to account for non-normality of the EF distributions. As information of Euro class, engine types and treatment technologies of non-Swedish HDTs is not available, we cannot further explore why there is a difference between the two fleets.
- 333 In addition to engine Euro type, pollutant emission trends were also investigated with respect to five different vehicle 334 manufacturers (M1, M2, M3, M4, and M5). EF_{PM}, EF_{PN}, EF_{BC} and EF_{NOx} of HDTs under the same Euro class but from different 335 manufacturers are compared in Fig. S9. Since EF data was not normally distributed, statistical significance is assessed with a 336 Kruskal–Wallis test. It is a non-paramedic analogue of the one-way ANOVA test. The p-values are calculated at the statistical 337 95% confidence level. No significant group difference (p>0.05) was observed in EF_{PM}, EF_{PN}, EF_{BC}, and EF_{NOx} for Euro V HDTs, i.e., HDTs from five different manufacturers show comparable emission characteristics. EF_{PM}, EF_{PN}, and EF_{NOx} of Euro 338 339 VI HDTs show no dependency on manufacturers, but a significant difference was observed between M2 and M5 in EF_{BC} of 340 Euro VI HDTs (p=0.016). (No analysis on Euro III, Euro IV, and EEV HDTs was conducted due to the limited vehicle number 341 from each manufacturer).

342 **3.4 Size-resolved EF**_{PN} of volatile and non-volatile particles

343 Figure 4a-e show the average size-resolved number emission factors (solid lines) simultaneously measured via the bypass and 344 TD lines for different Euro class HDTs. The EF_{PN} of the volatile components is calculated as the difference of EF_{PN} measured 345 after the bypass line and the non-volatile component EF_{PN} measured after the TD line. To differentiate between nucleation and 346 accumulation mode particles, a cut point particle diameter of 30 nm was used as defined by Kittelson et al. (2002). In general, 347 all Euro III, Euro IV, Euro V and EEV HDTs showed a bimodal particle number size distribution, with one mode peaking at 348 ~6-10 nm (nucleation mode) and another at ~50-80 nm (accumulation/soot mode) (Maricq, 2007). For Euro VI HDTs the 349 particle number size distributions were dominated by the nucleation mode. The EF_{PN} of the accumulation mode particles shows 350 a decreasing trend from Euro III to EEV HDTs. The accumulation mode of the Euro VI HDTs was insignificant. For heavy-351 duty diesel engines without a particulate filter, nucleation mode particles are mainly formed from organics. For vehicles with 352 DPF both organics and the fuel sulphur content might influence the formation of nucleation mode particles (Vaaraslahti et al., 353 2004). Thiruvengadam et al. (2012) found a direct relationship between exhaust nanoparticles in the nucleation mode and the 354 exhaust temperature of the DPF-SCR equipped diesel engine. These factors lead to high variability in the nucleation mode 355 fraction of EFPN. Figure 4f shows that HDVs with DPF (dashed lines) exhibited lower emissions of accumulation mode 356 particles, with no significant reduction in nucleation mode particles when compared to HDVs without DPF (solid lines). In

357 general, the absence of significant accumulation mode particles from Euro VI HDTs was consistent with observations made 358 from DPF equipped HDVs. High emissions of accumulation mode particles from Euro III HDTs were consistent with 359 measurements from HDVs without DPF in previous studies (Liu et al., 2019; Hallquist et al., 2009; Preble et al., 2015).

Most particles in the nucleation mode evaporate after passing through the TD. Sakurai et al. (2003b) reported that volatile compounds in diesel particles are mainly comprised of unburned lubrication oil. The non-volatile components in the nucleation mode may consist of metallic ash from lubrication oil or fuel additives (Sakurai et al., 2003a) or some organic compounds of extremely low volatility (Gkatzelis et al., 2016). In the accumulation mode, the particle mode diameter shifted towards lower sizes after passing the TD. In Fig. 4a-e, we also present the median size distribution (dashed lines). There is a small difference between mean and median size distributions in the accumulation mode while a bigger difference occurs in the nucleation mode. The latter mode is more dynamic and there are larger possibilities for extreme values skewing the averages.

367 To be consistent with previous studies which overwhelmingly report average size distributions, we choose to utilize the 368 average size distributions for the discussions below. The volatilities of particle emissions in the accumulation and nucleation 369 mode have been evaluated by calculating the average EF_{PN} and EF_{PM} fraction remaining (after heating) of particles emitted 370 from Euro III-VI HDTs (Fig. S10). In general, the EF_{PN} fraction remaining in the nucleation mode was lower than that in the 371 accumulation mode across all HDTs in all Euro classes. In terms of particle mass, the nucleation mode and accumulation mode 372 showed similar EF_{PM} fractions remaining from Euro III to EEV HDTs, while Euro VI HDTs had a much lower EF_{PM} fraction 373 remaining in the nucleation mode than in the accumulation mode. Compared with other Euro class HDTs, Euro VI HDTs had 374 the lowest EF_{PN} and EF_{PM} fraction remaining in both nucleation and accumulation mode. Around 94% of the particles by 375 number and 55% of the particles by mass (or volume) in total were evaporated. Alfoldy et al. (2009) reported that if the same 376 amount of volatile mass in the nucleation mode and accumulation mode were inhaled, 48% and 29% of the mass would deposit 377 in the lung respectively, implying that volatile mass in the nucleation mode would exert a 1.5 times stronger effect.

378 **3.5 Emissions from high emitters**

379 Figure 5 shows the cumulative emission distributions for PM, PN, NO_x and NO₂ emissions, with HDTs ranked in order from 380 dirtiest to cleanest. The plots show a significant skewedness towards a small fraction of HDTs with a high fraction of total 381 emissions (deviation from 1:1 line) for each pollutant, indicating the importance of "high emitters". The disproportionate 382 skewed distribution of pollutants is a common feature of on-road emission measurements (Preble et al., 2018; Preble et al., 383 2015; Dallmann et al., 2012). The highest-emitting 10% of HDTs in each pollutant were responsible for 65% of total PM, 70% 384 of total PN, 44% of total NO_x emissions and 69% of total NO₂, respectively. The distribution of NO_x has the least skewedness 385 compared with the other pollutants. If the 10% highest emitters for each pollutant were removed, the corresponding average 386 EF for PM, PN, NO_x and NO₂ would decrease by 62%, 67%, 38%, and 66% respectively. However, the high emitters for each 387 pollutant are different. For example, Euro III HDTs account for 70% and 67% of the top 3% emitters for PM and BC emissions, 388 while Euro VI HDTs account for 80% and 56% of the top 3% emitters for PN and NO₂ emissions. Here, top 3% emitters were 389 chosen as the reference because Euro III HDTs only accounted for 3% of the total number of HDTs. Lau et al., (Lau et al.,

390 2015) similarly reported that not all high-emitters were members of the lower Euro classes and that high-emitters for a 391 particular pollutant may not simultaneously be high-emitters for other pollutants.

392 **3.6 Fleet characteristics**

Figure 6a-d show the changes in average EFs of PM, PN, BC, and NO_x with respect to the registration year of the HDTs. Triennial average EFs were calculated, with truck registration years divided into 5 bins (2002-2005, 2006-2008, 2009-2011, 2012-2014 and 2015-2017). The black arrows in Fig. 6d show the years that the particular type of HDTs examined in this study was first registered. Coupled with the possible phase-out of older fleets, the HDTs with more advanced engines gradually accounted for a higher proportion of the total fleet. There is a significant improvement during the last years and the transition to widespread adoption of Euro VI will take real-world on-road emissions into a new era of much lower contributions to air pollution.

400 To estimate for each Euro class the typical contribution of air pollution emissions we utilised the number of kilometres 401 driven by HDTs on Swedish roads. During 2018, 4.1×10^9 and 9.2×10^8 kilometres were driven by Swedish and non-Swedish 402 diesel HDTs on Swedish roads, contributing to 82% and 18% to the total distances travelled by diesel HDTs respectively (Fig. 403 7a). The numbers of kilometres driven by Swedish Euro 0, Euro I, Euro II, Euro III, Euro IV, Euro V and Euro VI diesel HDTs 404 were 2.8×10^7 , 5.0×10^6 , 5.4×10^7 , 2.0×10^8 , 3.1×10^8 , 1.3×10^9 and 2.2×10^9 respectively (HBEFA 3.3, 2019). In Figure 7b, the 405 relative contributions of kilometers driven by Swedish Euro 0 to Euro VI HDTs are shown. Zhang et al. (2014) reported no 406 statistically significant difference in fuel consumption among Euro II to Euro IV buses under a real-world typical bus driving 407 cycle in Beijing. In this study, we assume the fuel consumption per kilometre and fuel density are the same across the different 408 Euro class HDTs and adopting the average fuel-based EFs calculated in this study (Tables 1 and 2), the approximation of 409 contributions of pollutants emitted from Swedish HDTs in each Euro class to the total PM, PN, BC and NO_x emissions are 410 depicted in Fig. 7c-f. Due to a lack of corresponding emission information, pollutant average EFs of Euro 0, Euro I and Euro 411 II HDTs were assumed to be at the same level as those of Euro III HDTs representing lower bound estimates. Euro 0-II HDTs 412 accounted for less than 2.2% of the grand total distance driven but totally contributed to 16%, 13%, 6% and 4% of BC, PM, 413 NO_x and PN emissions. Euro III HDTs only accounted for 5% (Fig. 7b) of the total fleet but disproportionally contributed to 414 37%, 30%, 16% and 10% of BC, PM, NO_x and PN emissions. Euro IV HDTs also exhibited disproportionally high PM and 415 NO_x emissions. A fraction of 32% of HDTs belonged to the Euro V category, they contributed to 53%, 42%, 34%, and 32% 416 of NO_x, PM, BC and PN emissions respectively. Upgrading, replacing or making obsolete Euro 0 to Euro V HDTs would be 417 necessary for mitigating a large part of the PM, PN, BC and NO_x emissions. Euro VI HDTs accounted for the highest fraction 418 of the total fleet (53%), but only contributed to 2%, 6%, 12% and 47% of PM, BC, NO_x, and PN emissions, indicating 419 successful overall pollution reduction with the introduction of more Euro VI HDVs. Using the median EFs as references, the 420 emission contributions from Euro VI HDTs to the total pollutant emissions would be even lower (Fig. S11). These data provide 421 useful information to predict future pollutant emission trends and to guide policy analysis and implementation. Since the 422 predicted transition in emissions from road transport would be significant, chemical transport model/cost-assessment models 423 need to get fast access to emission factors for new generation HDTs to be able to provide a better estimation of near future air

424 pollution levels.

425 4 Atmospheric implications and conclusions

426 The transition in the atmospheric emission of particles and gases from on-road HDTs caused by the modernisation of the fleet 427 is reported in this study. Particle emissions of PM, BC and to a lesser extent PN exhibited substantial reductions from Euro III 428 to Euro VI HDTs (Jonckheere-Terpstra test, p < 0.01). The gaseous emissions of NO_x and CO also showed a significant decrease 429 with respect to Euro class (Jonckheere-Terpstra test, p < 0.01), while the HC emission was relatively low for all the HDT Euro 430 class types. Compared with Euro III HDTs, Euro VI HDTs showed 99%, 98%, 93% and 57% reductions of the average 431 emissions factors of PM, BC, NO_x, and CO respectively. Although a significant reduction in NO_x emissions and a lower median 432 EF_{NO2} were evident, the fraction of NO₂ in the NO₃ emissions increased continuously from Euro IV to Euro VI HDTs, and 433 Euro VI HDTs were the dominant class of the top 3% emitters for NO₂. PN showed the largest data scattering for Euro VI 434 HDTs, though after evaporation of the volatile fraction, SPN became less scattered. A plausible reason for this large variability 435 in PN but not PM is the formation of nucleation mode particles containing more volatile compounds, which is more sensitive 436 to individual driving and plume dilution conditions. Reducing particle mass by DPF is clearly important but the consequence 437 in doing so removes particle surface area available for condensation and may therefore favour nucleation mode particle 438 formation if not the precursors of these are also reduced. Furthermore, due to the absence of larger particles, the coagulation 439 rate is decreased and produced nucleation mode particle can retain for a longer time in the atmosphere, which has a direct 440 influence on the evaluation of near-road human exposure.

Driving condition and engine technology affected the size distribution of particle number emissions. The average particle number size distributions of Euro III to EEV HDTs were bimodal with nucleation modes at ~6-10 nm and accumulation modes at ~50-80 nm. Euro VI HDTs displayed nucleation mode dominant size distributions. Measurements of particle volatility revealed that Euro VI HDTs had the highest volatile fraction in both nucleation mode and accumulation mode compared to the other Euro classes. More detailed chemical composition information of this volatile fraction is needed to assess their potential impacts for health and formation of SOA.

447 We also found that a small number of high emitters contributed to a large fraction of the total emissions. The top 10% 448 emitters in each pollutant category were responsible for 65% of total PM, 70% of total PN, 44% of total NO_x and 69% of total 449 NO_2 emissions, respectively. Euro III HDTs were the dominant top 3% emitters for PM and BC emissions, and Euro VI HDTs 450 were the dominant top 3% emitters for PN and NO_2 emissions.

In general, an overall pollution reduction has been achieved during the last years and the transition to Euro VI adoption will take real-world on-road emissions into a new era of much lower contributions to air pollution. The emissions of PM, BC and NO_x are predicted to further decrease in the future, while PN emissions may be subject to greater fluctuation and therefore be more challenging to control. Upgrading or phasing-out of existing Euro 0 to Euro V vehicles and introducing more Euro VI 455 HDTs would result in large pollution reductions. More intensive attentions need to be focused on SPN controls for Euro VI

456 HDTs. A careful and more detailed examination of the impacts of fleet upgrades in terms of ambient pollutant levels and

- 457 emission reduction targets for individual pollutants may be needed for further evaluation.
- 458
- 459 Data availability.
- 460 The data used in this publication are available to the community and can be accessed by request to the corresponding author.
- 461 *Author contributions.*
- 462 ÅMH designed the project; LZ, ÅMH, CMS, SMG, ÅS, MJ, HS, MH, and IW conducted the measurements; LZ, CMS, and
- 463 QL analysed data; LZ, ÅMH, MH, CKC and BPL wrote the paper. All co-authors contributed to the discussion of the
- 464 manuscript.
- 465 *Competing interests.*
- 466 The authors declare that they have no conflict of interest.
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Table 1. Comparison of the average emission data^a for PM and PN from the present study with literature data.

PM/PN						
Vehicle type	Speed km h ⁻¹	Dp range nm	Method	Instrument	EF _{PM} mg (kg fuel) ⁻¹	EF _{PN} # (kg fuel) ⁻¹ 10 ¹⁴
Euro III HDT in this study	26±6 ^b	5.6-560	roadside	EEPS	684±365	20.3±11.7
Euro III bus	acceleration	5.6-560	roadside	EEPS	6.7-2074	0.11-45
(Hallquist et al., 2013)	constant speed	5.6-560	roadside	EEPS	151-273	0.12-4.2
Euro III bus with DPF	acceleration	5.6-560	roadside	EEPS	62-2465	1.9-23
(Hallquist et al., 2013)	constant speed	5.6-560	roadside	EEPS	41-142	1.1-9.7
Euro III bus	≤25	PM_1	1	ELPI°	1240±220 ^b	
(Pirjola et al., 2016)	(bus depot)	$D_p \ge 2.5$	plume chasing	CPC		20.6 ± 3.2^{b}
	≤ 45 (bus line)	PM_1 D _p >2.5	plume chasing	ELPI ^c CPC	500	17.7
Euro III bus with DPF+SCR (Watne et al., 2018)	acceleration	5.6-560	roadside	EEPS	8.9±0.2	0.12±0.12
Euro III bus with DPF+SCR (Liu et al., 2019)	stop and go (bus stop)	5.6-560	roadside	EEPS	30±26 ^b	14.0±3.0 ^b
Euro III diesel bus and truck (Zavala et al., 2017)	driving cycle	35-1000	plume chasing & roadside	SP-AMS ^f	4300	-
Euro IV HDT in this study	23±8 ^b	5.6-560	roadside	EEPS	172±68	8.7±3.0
Euro IV bus with EGR	acceleration	5.6-560	roadside	EEPS	562-3089	13-44
(Hallquist et al., 2013)	constant speed	5.6-560	roadside	EEPS	91-489	5.8-47
Euro IV bus with EGR+DPF	acceleration	5.6-560	roadside	EEPS	177-650	5.1-13
(Hallquist et al., 2013)	constant speed	5.6-560	roadside	EEPS	58-61	2.6-3.1
Euro IV bus with EGR+DPF	≤25	PM_1		ELPIc	1190±520 ^b	
(Pirjola et al., 2016)	(bus depot)	$D_p \ge 2.5$	plume chasing	CPC		$8.9{\pm}1.6^{b}$
Euro IV bus with SCR (Watne et al., 2018)	acceleration	5.6-560	roadside	EEPS	145-560	3-13
Euro IV diesel bus and truck (Zavala et al., 2017)	driving cycle	35-1000	plume chasing and roadside	SP-AMS ^f	1800	-
Euro V HDT in this study	27±7 ^b	5.6-560	roadside	EEPS	146±49	9.7±2.7
Euro V bus+SCR	acceleration	5.6-560	roadside	EEPS	125-766	4.4-92
(Hallquist et al., 2013)	constant speed	5.6-560	roadside	EEPS	41-509	2.7-33
Euro V bus (Watne et al., 2018)	acceleration	5.6-560	roadside	EEPS	145±70	3.0±1.7
Euro V HDV with SCR (Rymaniak et al., 2017)	average at 45	PM/ 5.6-560	PEMS	MSS ^e EEPS	1840 ^d	0.09 ^d
Euro V bus with SCR (Liu et al., 2019)	stop and go (bus stop)	5.6-560	roadside	EEPS	180±15 ^b	6.5±2.9 ^b
Euro V diesel bus and truck (Zavala et al., 2017)	driving cycle	35-1000	plume chasing and roadside	SP-AMS ^f	720	-
EEV HDT in this study	25 ± 8^{b}	5.6-560	roadside	EEPS	78±35	16.5±23.6

EEV bus with EGR +DPF	≤25	$PM_1/$	nhuma ahaaina	ELPIc	400 ± 280^{b}	
(Pirjola et al., 2016)	(bus depot)	$D_p \ge 2.5$	plume chasing	CPC		2.1 ± 0.1^{b}
EEV bus with SCR	≤25	$\dot{P}M_1/$	nhuma ahaaina	ELPI ^c	280 ± 170^{b}	
(Pirjola et al., 2016)	(bus depot)	$D_p \ge 2.5$	plume chasing	CPC		7.0 ± 3.8^{b}
EEV with DOC+DPF+SCR	overage at 15	PM/	DEMS	MSS ^e	236 ^d	
(Rymaniak et al., 2017)	average at 45	5.6-560	LENIS	EEPS		0.02 ^d
EEV bus	stop and go	$PM_1/$	plumo chosing	ELPIc	200	
(Jarvinen et al., 2019)		$D_p \ge 3$	plume chasing	CPC		8.6
Euro VI HDT in this study	29 ± 8^{b}	5.6-560	roadside	EEPS	5±2	8.5 ± 4.6
Euro VI bus	stop and go	$PM_1/$	nluma abaging	ELPIc	70	
(Jarvinen et al., 2019)		$D_p \ge 3$	plume chasing	CPC		5
Euro VI HDGV	13.86		DEMS		28 33d	
(Moody and Tate, 2017)	15-00	-	I LIVIS	-	20-33	-
Euro VI HDT	65-74	_	PEMS	_	_	$0.002_{-}0.01^{d}$
(Grigoratos et al., 2019)	05-74		I LMB			0.002-0.01
HDT without available Euro	27+7b	5 6 560	roadside	FEDS	17+23	7 5+7 3
type information	21±1	5.0-500	Toausiue	EEF 5	47±23	7.5±7.5
Total Swedish HDT	28±7 ^b	5.6-560	roadside	EEPS	96±36	9.6±2.7
Total non-Swedish HDT	26±8 ^b	5.6-560	roadside	EEPS	117±42	11.1±4.2

Non-European HDV with different ATS HDV with DPF

(Wang et al., 2017; Quiros et al., 2016)	13-80	$\begin{array}{c} PM \\ D_p \geq 5 \end{array}$	PEMS	gravimetric CPC	12-41 ^d	0.006-13.2
Heavy-duty HDV with DPF+SCR (Thiruvengadam et al., 2015)	driving cycle	РМ	chassis dynamometer	gravimetric	6-29 ^d	-
HDV with DPF+SCR (Jiang et al., 2018)	driving cycle	PM _{2.5}	chassis dynamometer	gravimetric	3-97 ^d	-
(model year 2004- 2006) (Preble et al., 2015)	accelerating	$D_p \ge 2.5$	roadside	CPC	-	47.2±9.7
HDT with SCR+DPF (model year 2010- 2013) (Preble et al., 2015)	48	$D_p \ge 2.5$	roadside	CPC	-	15.9±11.5
HDV (mean model year 2005) (Bishop et al., 2015)	15.7-16.8	PM _{1.2}	OHMS ^g	digital mass monitor	650	-
HDV (mean model year 2009) (Bishop et al., 2015)	7.7-9.3	PM _{1.2}	OHMS ^g	digital mass monitor	31	-
HDV without after-treatment (Quiros et al., 2018)	driving cycle	PM _{2.5}	chassis dynamometer	gravimetric	1980 ^d	-
HDV+DPF (Quiros et al., 2018)	driving cycle	PM _{2.5}	chassis dynamometer	gravimetric	6-9 ^d	-

^a Given errors are at 95% CI. ^b Standard deviation. ^c ELPI, Electrical Low-Pressure Impactor.

- ^d Average fuel consumption of 0.26 L km⁻¹ for HDV during long haul and regional delivery tests (Rexeis et al., 2018), the
- density of 0.815 kg dm⁻³ (Swedish Environmental Protection Agency, 2013) of diesel particles were assumed for unit
- 756 conversion.
- ^e MSS, Micro Soot Sensor.
- ^fSP-AMS, Soot Particle Aerosol Mass Spectrometer.
- 759 ^gOHMS, On-Road Heavy-Duty Vehicle Emissions Monitoring System.

	Speed	Method	${\rm EF}_{\rm NOx}{}^{\rm b}$	EF _{NO2} / EF _{NOx} ^b	$\mathrm{EF_{CO}^{c}}$	$\mathrm{EF}_{\mathrm{HC}}^{\mathrm{c}}$
Vehicle type	$km h^{-1}$		g	mass ratio	g	g
			(kg fuel) ⁻¹	%	(kg fuel) ⁻¹	(kg fuel) ⁻¹
Euro III HDT in this study	26 ± 6^{d}	roadside	43.3±31.5	7.5 ± 4.1	36.0±13.2	0.8±1.3
Euro III bus	1		161.07		161.161	.12
(Hallquist et al., 2013)	acceleration	roadside	16.1±9.7	-	16.1±16.1	<13
	≤25	1	107.1 od			
Euro III bus	(bus depot)	plume chasing	$12.7\pm1.8^{\circ}$	-	-	-
(Pirjola et al., 2016)	≤45	-1	20.5			
-	(bus line)	plume chasing	20.3	-	-	-
Euro III bus						
with DPF+SCR	acceleration	roadside	-	-	13±10	0.02
(Watne et al., 2018)						
Euro III HDV	$64 + 13^{d}$	nlume chasing	_	24+4	_	_
(Lau et al., 2015)	04 ± 15	plune enasing		27		
Euro III &IV HDV	_	model	_	14	_	_
(Kousoulidou et al., 2008)		model				
Euro III HGV	Average at	remote sensing	16.2 ± 1.0^{f}	-	-	-
(Carslaw et al., 2011)	31	8				
Euro III HGV	28-60	remote sensing	-	24.1±4.7	-	-
(Carslaw and Rhys-Tyler, 2013)	22 od	1 · 1	10.0.10.1	27.20	22.1.10.2	0 7 1 1
Euro IV HDT in this study	23±8ª	roadside	19.8±10.1	2.7±2.9	22.1 ± 10.3	0.7 ± 1.1
Euro IV bus (Hellowist et al. 2012)	acceleration	roadside	12.9±6.5	-	16.1±16.1	<13
(Haliquist et al., 2015)						
with ECP DDE	≤25	nlumo chosing	23 4+6 1 ^d			
(Piriola et al. 2016)	(bus depot)	plume chasing	23.4 ± 0.1	-	-	-
Furo IV bus with SCR						
(Watne et al 2018)	roadside	acceleration	-	-	220-230	0.3-0.6
Euro IV HDV	,					
(Lau et al., 2015)	64 ± 13^{a}	plume chasing	-	28±5	-	-
Euro IV HGV	average at		10.0.1.1f			
(Carslaw et al., 2011)	31	remote sensing	10.3 ± 1.4^{1}	-	-	-
Euro IV HGV	29. (0	· · ·		21.07		
(Carslaw and Rhys-Tyler, 2013)	28-60	remote sensing	-	3.1±0.7	-	-
Euro V HDT in this study	27 ± 7^{d}	roadside	22.2±3.8	$6.0{\pm}2.8$	22.8±5.1	0.9 ± 0.4
Euro V bus	aggalaration	roadaida	25 5 10 7		07+22	~12
(Hallquist et al., 2013)	acceleration	Toauside	55.5±9.7	-	9.7±3.2	<15
Euro V bus with SCR	stop and go	roadside	0 8+3 5d	3 7+1 5d	28 e	2 2e
(Liu et al., 2019)	(bus stop)	Toausiue	9.8±3.5	5.7±1.5	20	2.2
Euro V HDV	$64 + 13^{d}$	nlume chasing	_	40 + 14	_	_
(Lau et al., 2015)	01 ± 10	rianic chubing		10-11		
Euro V HDV	_	model	_	18	-	_
(Kousoulidou et al., 2008)				10		
Euro V HGV	average at	remote sensing	13.3 ± 5.8^{f}	-	-	-
(Carslaw et al., 2011)	31					
Euro V HGV	28-60	remote sensing	-	3.7±0.7	-	-
(Carslaw and Rhys-Tyler, 2013)		ε				

Table 2. Comparison of the average emission data^a for NO_x, NO₂/NO_x, CO and HC from the present study with literature data.

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	EEV HDT in this study	25+8 ^d	roadside	13 6+6 7	63+37	18 0+10 1	0 2+0 4
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	EEV bus with EGR +DPF	<25	Toudstud	10.0_0.7	0.0_0.1	10.0_10.1	0.2_0.1
BEV bus with SCR (Pirjota et al., 2016) (bus depot) (235) (bus depot) plume chasing roadside 39.8 ± 4.2^4 - - Euro VI IBDT in this study (Grigoratos et al., 2019) 65.74 PEMS $0.3-31.3$ - $28.822.3$ $0.3-31.1$ Euro VI IBDV (Kousoulidou et al., 2008) - model - 35 - - Euro VI IBDV (Kousoulidou et al., 2008) - model - 35 - - HDT without available Euro type information Total wordsh HDT 28 ± 7^d roadside 7.8 ± 4.5 13.9 ± 6.3 20.7 ± 5.6 0.8 ± 0.6 Non-European HDV with different ATS roadside 13.0 ± 2.5 18.6 ± 1.9 0.9 ± 0.3 Total non-Swedish HDT 26 ± 8^d roadside 13.0 ± 2.5 18.6 ± 1.9 0.9 ± 0.3 Total avaita L, 2015 driving cycle chassis dynamometer 30.43 - $0.1-13.4^f$ $<0.64^f$ HDV with DC+DFF+SCR cycle mobile dynamometer 11 - - $-$ HDV (May et al., 2014) driving dynamometer 11 - - - $-$ HDV (May et al., 2018)	(Piriola et al. 2016)	(bus denot)	plume chasing	32.9±7.6 ^d	-	-	-
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	EEV bus with SCR	<25					
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	(Piriola et al. 2016)	(bus denot)	plume chasing	39.8±4.2 ^d	-	-	-
Euro VI HDT (Grigoratos et al., 2019) 65-74 PEMS 0.3-31.3 - 2.8-22.3 0.3-3.1 (Grigoratos et al., 2019) 65-74 PEMS 0.3-31.3 - 2.8-22.3 0.3-3.1 (Kousoulidou et al., 2008) - model - 35 PEMS 2.2 ^{cf}	Furo VI HDT in this study	29+8 ^d	roadside	3 1+1 0	22 5+4 2	15 5+2 2	1 0+0 5
Instruction Construction Construction <th< td=""><td>Euro VI HDT</td><td>2720</td><td>Toudside</td><td>5.1±1.0</td><td>22.3 ± 1.2</td><td>15.5±2.2</td><td>1.0±0.5</td></th<>	Euro VI HDT	2720	Toudside	5.1±1.0	22.3 ± 1.2	15.5±2.2	1.0±0.5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	(Grigoratos et al. 2019)	65-74	PEMS	0.3-31.3	-	2.8-22.3	0.3-3.1
Instruction of the second	Euro VI HDV						
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	(Kousoulidou et al. 2008)	-	model	-	35	-	-
Instruction PEMS 2.2^{i} $ -$ HDT without available Euro 27 ± 7^{d} roadside 7.8 ± 4.5 13.9 ± 6.3 20.7 ± 5.6 0.8 ± 0.6 Non-European HDV with different ATS 26 ± 8^{d} roadside 10.7 ± 1.8 15.9 ± 2.5 18.6 ± 1.9 0.9 ± 0.3 Non-European HDV with different ATS 26 ± 8^{d} roadside 13.0 ± 2.5 12.7 ± 3.0 19.1 ± 3.0 0.9 ± 0.6 Non-European HDV with different ATS 43.9 ± 2.5 18.6 ± 1.9 0.9 ± 0.6 Non-European HDV with different ATS 43.9 ± 2.5 18.6 ± 1.9 0.9 ± 0.6 Non-European HDV with different ATS 43.9 ± 2.5 18.6 ± 1.9 0.9 ± 0.6 HDV with DPF+SCR driving chassis 0.2 ± 6.4^{t} $0.1-13.4^{t}$ $<0.64^{t}$ HDV with DPF+SCR driving chassis 0.2 ± 6.4^{t} 0.006^{t} $(1.3^{t}$ HDV with SCR cycle driving chassis 0.2 ± 6.4^{t} $0.9-2.8^{t}$ $0.1-0.4^{t}$ HDV with SCR cycle chassis $0.2-5\pm0.9^{t}$ 0.2 ± 0.6^{t} $0.1-0.4^{t}$ $0.1-0.4^{t}$ 0	Euro VI HDV	driving		c			
HDT without available Euro type information Total Swedish HDT 27 ± 7^4 27 ± 7^4 roadside roadside 13.9 ± 6.3 15.9 ± 2.5 20.7 ± 5.6 18.6 ± 1.9 0.9 ± 0.3 13.0 ± 2.5 20.7 ± 5.6 18.6 ± 1.9 0.9 ± 0.3 Non-European HDV with different ATS Heavy-duty HDV with DPF+SCR (Diray et al., 2018) HDV with DOC+DPF+SCR (Quiros et al., 2016)driving cycle driving cycle $3.8\cdot27.8^{t}$ dynamometer dynamometer dynamometer $0.2-66.4^{t}$ $0.1-13.4^{t}$ 14.9^{t} $<0.64^{t}$ 14.9^{t} HDV with DOC+DPF+SCR (Quiros et al., 2016) $12.7\cdot85.6$ dynamometer dynamometer $0.2-66.4^{t}$ $1.7\cdot11.8^{t}$ $0.9-2.8^{t}$ $0.1-0.4^{t}$ 14.9^{t} HDV with SCR (May et al., 2014)cycle driving dynamometer $30-43$ dynamometer $-$ $-$ $-$ $-$ $-$ $-$ 	(Moody and Tate, 2017)	cvcle	PEMS	2.2 ^r	-	-	-
type information 27 ± 7^a roadside 7.8 ± 4.5 13.9 ± 6.3 20.7 ± 5.6 0.8 ± 0.6 Total Swedish HDT 28 ± 7^d roadside 10.7 ± 1.8 15.9 ± 2.5 18.6 ± 1.9 0.9 ± 0.3 Non-European HDV with different ATS Heavy-duty HDV driving chassis $3.8-27.8^t$ - $0.1-13.4^t$ $<0.64^t$ (Thirvengedam et al., 2015) driving chassis $0.2-66.4^t$ - $0.1-13.4^t$ $<0.64^t$ (DV with DPF+SCR driving chassis $0.2-66.4^t$ - $0.1-0.4^t$ $<14.9^t$ $<1.3^t$ HDV with DC+DPF+SCR driving chassis $0.2-66.4^t$ - $0.006^ <1.3^t$ (Quiros et al., 2016) $12.7-85.6$ mobile $1.7-11.8^t$ - $0.9-2.8^t$ $0.1-0.4^t$ HDV (May et al., 2014) driving chassis $30-43$ - - - HDV field average 22.5 ± 0.9 remote sensing 12.4 ± 0.6 8.9 5.9 ± 0.9 2.2 ± 0.4 HDV field average 22.5 ± 0.9 accelerating or adside 5.1 ± 1.2 $22.1\pm$	HDT without available Euro						
Total Swedish HDT Total non-Swedish HDT 28 ± 7^d 26 ± 8^d roadside roadside 10.7 ± 1.8 13.0 ± 2.5 15.9 ± 2.5 12.7 ± 3.0 18.6 ± 1.9 19.1 ± 3.0 0.9 ± 0.3 0.9 ± 0.6 Non-European HDV with different ATS Heavy-duty HDV with DPF+SCR (Thiruvengadam et al., 2015) driving cycle chassis dynamometer $3.8-27.8^{f}$ $ 0.1-13.4^{f}$ $<0.64^{f}$ HDV with DPF+SCR (Quiros et al., 2018) cycle driving dynamometer chassis dynamometer $0.2-66.4^{f}$ $ 0.1-0.4^{f}$ $<0.1-0.4^{f}$ HDV with DOC+DPF+SCR (Quiros et al., 2016) $12.7-85.6$ mobile dynamometer $0.2-66.4^{f}$ $ 0.9-2.8^{f}$ $0.1-0.4^{f}$ HDV (May et al., 2014) driving dynamometer $0.2-40.4^{f}$ $0.9-2.8^{f}$ $0.1-0.4^{f}$ HDV fleet average (Haugen et al., 2018) 22.5 ± 0.9 remote sensing 12.4 ± 0.6 8.9 5.9 ± 0.9 2.2 ± 0.4 HDT $del year 200.5$ $accelerating$ or cruise at (Preble et al., 2015) $accelerating$ or cruise at (model year 2001) $accelerating$ or cruise at (Burgard et al., 2006) $20-40$ $accelerating$ or cruise at (Burgard et al., 2006) $20-40$ $accelerating$ or cruise at (Burgard et al., 2006) $20-40$ $accelerating$ oreadside $accelerating$ or cruis	type information	27±7ª	roadside	7.8 ± 4.5	13.9±6.3	20.7 ± 5.6	0.8 ± 0.6
Total non-Swedish HDT 26 ± 8^d roadside 13.0 ± 2.5 12.7 ± 3.0 19.1 ± 3.0 0.9 ± 0.6 Non-European HDV with different ATS Heavy-duty HDV with DPF+SCR (Jaing et al., 2015)driving cyclechassis dynamometer $3.8-27.8^t$ $ 0.1-13.4^t$ $<0.64^t$ HDV with DPF+SCR (Quiros et al., 2016)driving cyclechassis dynamometer $0.2-66.4^t$ $ 0.1-13.4^t$ $<0.64^t$ HDV with DCF-DFF+SCR (Quiros et al., 2016)driving driving cyclechassis dynamometer $0.2-66.4^t$ $ 0.9-2.8^t$ $0.1-0.4^t$ HDV with SCR (May et al., 2014)driving driving (May et al., 2014) 22.5 ± 0.9 remote sensing 12.4 ± 0.6 8.9 5.9 ± 0.9 2.2 ± 0.4 HDT (model year 2004-2006) (Preble et al., 2015) 22.5 ± 0.9 roadside 16.5 ± 1.7 3.4 ± 1.8 $ -$ HDT (model year 2001) (Burgard et al., 2006) $20-40$ roadside $ 9.1\pm 0.5$ 26.0 ± 2.1 1.8 ± 0.6 HDT (model year 2000) (Burgard et al., 2006) $20-40$ roadside $ 6.1\pm 0.1$ 37.9 ± 1.6 3.3 ± 0.4 Fleet average (Dalman et al., 2012) $20-40$ $28-36$ roadside $2-5$ $ 17-24$ $1.9-2.3$ HDT (model year 2004) (Burgard et al., 2005) $20-40$ 22.2 ± 0.4 $ -$ HDT (model year 2000) (Burgard et al., 2006) $20-40$ $20-40$ $ -$ HDT (model year 2000) (Burgard et al., 2012) </td <td>Total Swedish HDT</td> <td>28 ± 7^{d}</td> <td>roadside</td> <td>10.7 ± 1.8</td> <td>15.9 ± 2.5</td> <td>18.6 ± 1.9</td> <td>0.9 ± 0.3</td>	Total Swedish HDT	28 ± 7^{d}	roadside	10.7 ± 1.8	15.9 ± 2.5	18.6 ± 1.9	0.9 ± 0.3
Non-European HDV with different ATS Heavy-duty HDV driving classis (Thiruvengadam et al., 2015) driving classis (Jang et al., 2018) cycle driving (During et al., 2018) cycle driving HDV with DOC+DPF+SCR cycle dynamometer (Quiros et al., 2016) 12.7-85.6 laboratory HDV with SCR cycle chassis (May et al., 2014) driving chassis HDV With SCR cycle chassis (May et al., 2014) driving chassis HDV With SCR cycle chassis (May et al., 2014) driving chassis HDV Ret average cycle chassis (May et al., 2014) driving crassis HDT cycle chassis (model year 2004- 2006) cycle roadside Preble et al., 2015) accelerating roadside 16.5±1.7 $3.4±1.8$ - HDT (model year 2000- 2013) 48 roadside 5.1 ± 1.2 22.1 ± 8.4 - - (Burgard et al., 2005)	Total non-Swedish HDT	26 ± 8^{d}	roadside	13.0 ± 2.5	12.7 ± 3.0	19.1 ± 3.0	0.9 ± 0.6
Non-European HDV with different ATS Heavy-duty HDV with DPF+SCR (Thiruvengadam et al., 2015) driving cycle chassis dynamometer $3.8-27.8^{f}$ - $0.1-13.4^{f}$ $<0.64^{f}$ HDV with DPF+SCR (Darget al., 2018) cycle chassis dynamometer $0.2-66.4^{f}$ - 0.006^{-} 14.9^{f} $<1.3^{f}$ HDV with DOC+DPF+SCR (Quiros et al., 2016) 12.7-85.6 laboratory chassis dynamometer $3.0-43$ - - - HDV (May et al., 2014) driving (May et al., 2014) driving dynamometer $3.0-43$ - - - HDV with SCR (May et al., 2014) driving dynamometer $30-43$ - - - HDV Ret average (Haugen et al., 2018) 22.5±0.9 remote sensing 12.4 ± 0.6 8.9 5.9 ± 0.9 2.2 ± 0.4 HDT (model year 2004- 2005) (Preble et al., 2015) accelerating or cruise at 48 roadside 5.1 ± 1.2 22.1 ± 8.4 - - HDT (model year 2000) (Burgard et al., 2006) $5-25$ roadside $ 9.1\pm0.5$ 26.0 ± 2.1 1.8 ± 0.6 HDT (model year 2000) (Burgard et al., 2006) $20-40$ roadside 2.5 -							
Non-European HDV with different ATSHeavy-duty HDV with DPF+SCR (Thiruvengadam et al., 2015)driving cyclechassis dynamometer $3.8-27.8^{f}$ - $0.1-13.4^{f}$ $<0.64^{f}$ HDV with DPF+SCR (Jaing et al., 2018)driving cyclechassis dynamometer HDV with DOC+DPF+SCR (Quiros et al., 2016) $12.7-85.6$ $0.2-66.4^{f}$ - $0.006-$ 14.9^{f} $<1.3^{f}$ HDV (May et al., 2014)driving driving cyclechassis dynamometer (hassis dynamometer $30-43$ HDV with SCR (May et al., 2014)cyclechassis dynamometer dynamometer $30-43$ HDV fleet average (Magen et al., 2018) 22.5 ± 0.9 remote sensing or cruise at 48 12.4 ± 0.6 8.9 5.9 ± 0.9 2.2 ± 0.4 HDT (model year 2004- 2006) (Preble et al., 2015)accelerating or cruise at 48roadside 5.1 ± 1.2 22.1 ± 8.4 HDT (model year 2001) (Burgard et al., 2006) $20-40$ roadside $ 9.1\pm0.5$ 26.0 ± 2.1 1.8 ± 0.6 HDT (model year 2000) (Burgard et al., 2006) $20-40$ roadside $2-5$ $ 17-24$ $1.9-2.3$ Fleet average in 2006 (Bishop and Stedman, 2008) $28-36$ roadside $2-5$ $ 17-24$ $1.9-2.3$ HDT (mean model year 2004) (Dalmann et al., 2012) 22.2 ± 0.4 remote sensing roadside 2.0 ± 1.6 9.7 8.2 ± 0.6^{d} 3.7 ± 0.1^{d}							
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	(Bishop et al. 2013)	22.2±0.4	remote sensing	20.6 ± 0.6^d	9.7	8.2 ± 0.6^{d}	3.7 ± 0.1 ^d

HDT (mean model year 2009)	7 8+0 1	remote sensing	10 0+0 3 d	9.0	$73+05^{d}$	$0.6+0.6^{d}$
(Bishop et al., 2013)	7.0±0.1	Temote sensing	19.9±0.5	9.0	7.5±0.5	0.0±0.0

- ^a Given errors are at 95% CI.
 ^b In NO₂ equivalents.
 ^c RSD data. For the RSD data sets of multiple individuals, negative values were replaced by zero when calculating the averages.
- ^d Standard deviation.
- ^e Median.
- ^f Average fuel consumption of 0.26 L km⁻¹ for HDV during long haul and regional delivery tests (Rexeis et al., 2018), the density of 0.815 kg dm⁻³ (Swedish Environmental Protection Agency, 2013) of diesel particles were assumed.





Figure 1. (a) Sampling site at the roadside in Gothenburg, Sweden, (b) schematic of the experimental set-up. HDT (Heavy-duty truck), RSD (Remote Sensing Device), CPC (Condensation Particle Counter), EEPS (Engine Exhaust Particle Sizer
Spectrometer), TD (Thermodenuder) and HR-ToF-CIMS* (High-Resolution Time-of-Flight Chemical Ionization Mass
Spectrometer) and examples of signals from three passing HDTs. Concentrations of CO₂, PN, non-volatile PN (black line),
PM, non-volatile PM (black line), and NO_x from (c) a typical Euro III HDT and (d) a typical Euro VI HDT and (e) a Euro VI
HDT with low PN emission. *The data from the HR-ToF-CIMS will be presented elsewhere.



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Figure 2. (a) EF_{PM} , (b) EF_{PN} , (c) EF_{BC} , (d) EF_{NO2} and EF_{NOx} for Euro III to Euro VI and non-Swedish HDTs. Non-detectable pollutant emission signals for captured plumes have been replaced by EF_{min} . For box-and-whisker plots, the top and the bottom line of the box are 75th and 25th percentiles of the data, the red line inside the box is the median, and the top and bottom whiskers are 90th and 10th percentiles. EF_{NOx} in (d) are in NO₂ equivalents. HDTs with either EF_{NO2} or EF_{NOx} lower than the detection limits of the instruments were removed in (d) for illustration purposes. Note that the comparison with the emission standard is only indicative as they are based on test cycle performance.



Figure 3. (a) EF_{PM} and EF_{PN} of individual HDTs in this study and previous studies and (b) the relationship between EF_{PM} and EF_{SPN} of Euro VI HDTs. Red dashed lines represent Euro emission standards (horizontal: PM emission standard; vertical: SPN emission standard). HDTs with either EF_{PM} or EF_{PN} lower than the detection limits of the instruments were removed in (a) for illustration purposes. Note that the comparison with the emission standard is only indicative as they are based on test cycle performance.



Figure 4. (a-e) Mean and median size-resolved EF_{PN} and $EF_{non-volatile PN}$ of different Euro class HDTs and (f) comparisons of mean size-resolved EF_{PN} of HDVs in this study and previous studies. Shaded regions in (a-e) represent the statistical 95% confidence interval. One HDT with extremely different EF in (d) was excluded and shown in blue.

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793 Figure 5. Cumulative emission factor distribution for (a) PM, (b) PN, (c) NO_x, and (d) NO₂ measured in HDT exhaust plumes

794 with HDTs ranked from the highest to lowest in terms of emission factors.



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Figure 6. Changes of average EFs of (a) PM, (b) PN, (c) BC and (d) NO_x with respect to the registration year of HDTs. Error bars represent the statistical 95% confidence interval. Black arrows mark the years that the particular type of HDT examined in this study was first registered.





Figure 7. Relative contributions of kilometers driven by (a) Swedish and Non-Swedish HDTs and (b) Swedish Euro 0, Euro
I, Euro II, Euro IV, Euro V and Euro VI HDTs on Swedish roads during 2018. Approximation of contributions of

pollutants emitted from Swedish HDTs in each Euro class to the total (c) PM, (d) PN, (e) BC and (f) NO_x emissions.