Supplement for

Role of black carbons mass size distribution in the direct aerosol radiative forcing

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1. Correcting the AE51

Fig. S1 showed the results of the loading effect corrections. At the beginning of the field experiment, parallel measurement of m_{BC} by AE51 and AE33 was conducted. Before corrections, the measured m_{BC} by AE51 and AE33 showed significant discrepancy with each other with slope and R^2 equaling 0.55 and 0.83. However, the m_{BC} measured by AE33 and by AE51 with loading effects corrections showed good consistency in trends and magnitudes with slope and R^2 of 0.98 and 0.94 respectively. These results demonstrated that the loading effects corrections of m_{BC} from AE51 were essential and the value of m_{BC} from AE33 can be used as a reference for the measured BCPMSD.

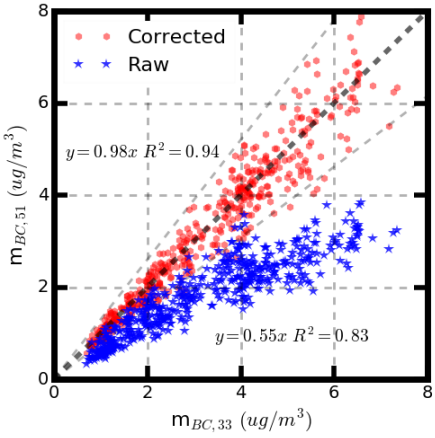

Figure S1. Comparison between the m_{BC} measured by AE51 and AE33. The blue stars and the red dots represents uncorrected and corrected m_{BC} of AE51 respectively.

2. Time correction

There were two reasons that can lead to this difference: firstly, the time of the AE51 system and

the computer that controls the CPC cannot be synchronized all the time; secondly, there existed a difference in the plumbing delay time, which was the time required for particles to flow through the tubing interconnecting the DMA and CPC or AE51, and arrive at the detector. To sum up, the synchronization of the time reported by CPC and AE51 was necessary.

Time synchronization was conducted by measuring the time lag of the signal pulses from the DMA to CPC and AE51. The signal pulses resulted from the sudden change of the aerosol diameter scanned by DMA. Details of the method were shown below. In fig. S2, the black solid line gave the time series of the measured m_{BC} by AE51. The dotted lines gave the time series of the aerosol number counted by CPC of (a) unsynchronized and (b) synchronized. In the beginning, the scan diameter of the DMA was set to be less than 13nm and the values measured by AE51 and CPC are nearly zero. The values get a step jump and a step drop when changing the scan diameter up to about 200nm and down back to less than 13nm. About 15s later, these procedures were conducted once again. From fig. S2(a) and fig. S2(b), the lag time of the AE51 and CPC were determined to be 20s by matching the pulse signals.

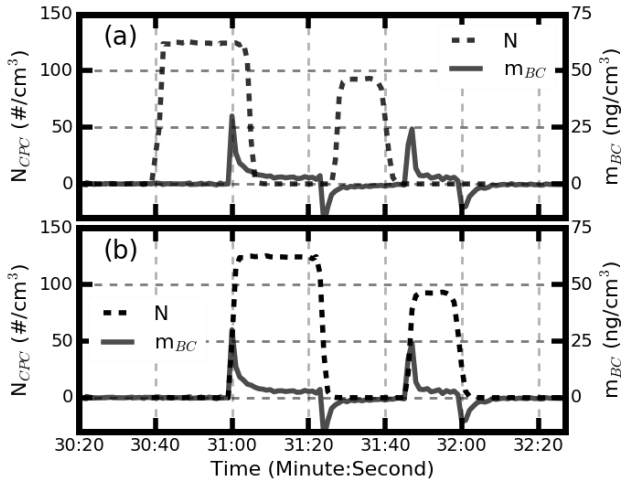

Figure S2. An example of time synchronization processing, (a) for unsynchronized and (b) for synchronized. The dotted line is the aerosol number concentration time series counted by CPC. The black solid line is the BC mass concentration measured by AE51.

3. Time series diagram of scanned aerosol diameters, measured m_{BC} and the aerosol number concentrations

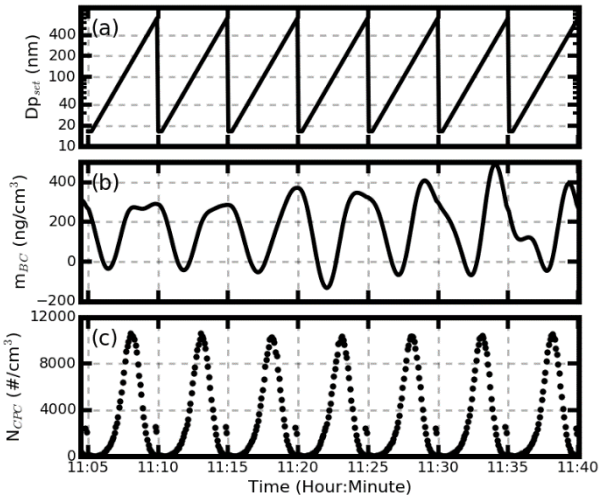

Figure S3 (a) the diameters of the aerosols that pass through the DMA (b) The m_{BC} values measured by AE51, (c) the aerosol number concentrations measured by CPC.

4 Validation of the multiple charging corrections

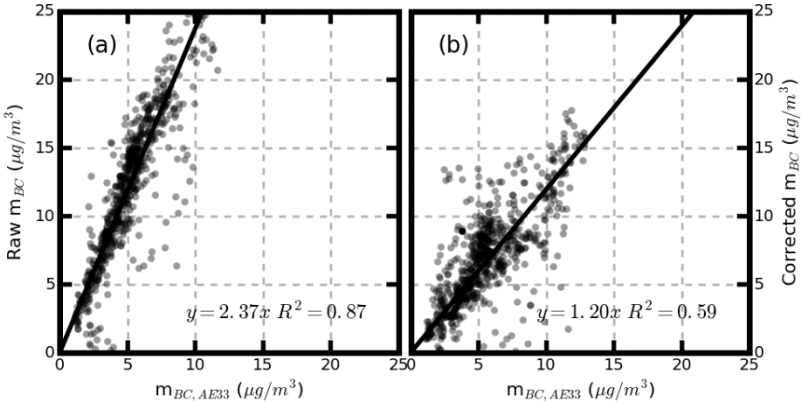

Figure S4. m_{BC} measured by AE33 versus m_{BC} integrated from AE51 of (a) uncorrected BCPMSD, (b) corrected BCPMSD.

5 Estimate the DARF

DARF is defined as the difference between radiative flux at the TOA under present aerosol conditions and aerosol-free conditions:

$$\mathrm{DARF} = (f_a \downarrow - f_a \uparrow) - (f_m \downarrow - f_m \uparrow) \ , \qquad (21)$$

Where $f_a \downarrow$ is the downward radiative irradiance and $f_a \uparrow$ is the outward radiative irradiance under given aerosol distributions; $(f_a \downarrow - f_a \uparrow)$ is the downward radiative irradiance flux with given aerosol distributions and $(f_m \downarrow - f_m \uparrow)$ is the radiative irradiance flux under aerosol free conditions. The wavelengths for irradiance range from 0.25 to 4 μm.

Input data for the SBDART are listed below. Vertical profiles of the aerosol optical properties, which include the aerosol extinction coefficient (σ_{ext}), aerosol single scattering albedo (SSA) and g with a height resolution of 50 m, come from the parameterization of aerosol vertical distributions (as shown in fig. S4 and the next paragraph) and the results of the Mie model.

Liu et al. (2009) studied vertical profiles of aerosol total number concentration (Na) with aircraft measurements, and derived a parameterized vertical distribution. In this scheme, Na is constant in the mixed layer, with a transition layer where it linearly decreases and an exponential decrease of Na above the transition layer. The same parameterized scheme proposed by Liu et al. (2009) is adopted by this study as shown in fig. S4 (b). Both the study of Liu et al. (2009) and Ferrero et al. (2010) manifest that the dry aerosol PNSD in the mixed layer varies little. The shape of the dry aerosol PNSD is assumed constant with height, which means that aerosol PNSD at different heights divided by Na give the same normalized PNSD.

As for the BC vertical distribution, Ferrero et al. (2011) and Ran et al. (2016) demonstrate that BC mass concentration in the mixed layer remains relatively constant and decreases sharply above the mixed layer. According to this, the parameterization scheme of BC vertical distribution is assumed to be the same as that of aerosol. The shape of the size-resolved BC mass concentration distribution is also assumed to be the same as that at the surface.

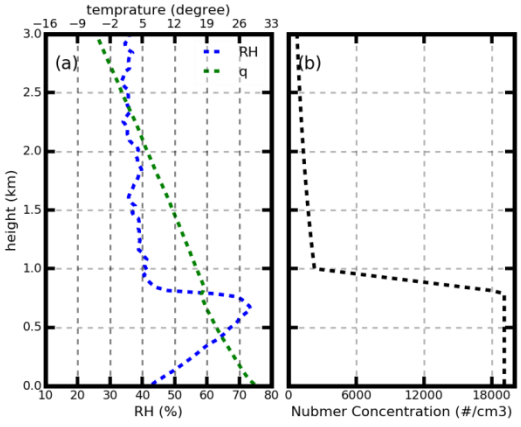

Figure S5. The mean RH, temperature, and aerosol number concentration profiles.

Atmospheric gas and meteorological parameter profiles come from the mean results of the radiosonde observations at the Meteorological Bureau of Beijing (39°48’ N, 116°28’ E), which include

profiles for water vapor, pressure and temperature during the summer (Supplementary S5). With the vertical distribution of aerosol PNSD and BCMSD, the aerosol optical properties at a given height can be calculated based on the method of S6. Surface albedo values are obtained from the Moderate Resolution Imaging Spectroradiometer (MODIS) V005 Climate Modeling Grid (CMG) Albedo Product (MCD43C3) during March, 2017 of Beijing, where the field campaign is conducted. The remaining input data for the SBDART are set to their default values.

6. Calculate the aerosol optical profiles under the given RH profile

The aerosol hygroscopic growth is taken into consideration when calculate the aerosol optical properties under the given RH. The κ-Köhler theory (Petters and Kreidenweis, 2007) is widely used to describe the hygroscopic growth of aerosol particles by using a single aerosol hygroscopic growth parameter (κ) and the κ-Köhler equation, which is shown as

$$\frac{RH}{100} = \frac{gf^3-1}{gf^3-(1-\kappa)} \cdot \exp\left(\frac{4\sigma_{s/a}M_{water}}{R\cdot T\cdot D_d\cdot gf\cdot \rho_w}\right) , \quad (1)$$

where D_d is the dry particle diameter; gf(RH) is the aerosol growth factor, which is defined as the ratio of the aerosol diameter at a given RH and the dry aerosol diameter (D_{RH}/D_d); T is the temperature; $\sigma_{s/a}$ is the surface tension of the solution; R is the universal gas constant and ρ_w is the density of water. The aerosol hygroscopic growth parameter κ can be further used to investigate the influence of aerosol hygroscopic growth on aerosol optical properties (Tao et al., 2014;Kuang et al., 2015;Zhao et al., 2017) and aerosol liquids water contents (Bian et al., 2014).

The κ-Köhler theory and the Mie scattering model are combined to calculate aerosol extinction coefficient, aerosol single scattering albedo and aerosol asymmetry factor under different RH conditions. The real time κ, which is derived from the measurement of f(RH), is used to account for aerosol hygroscopic growth. For each RH value, the gf can be calculated based on equation (1). The corresponding ambient aerosol PNSD at a given RH can be determined too. The refractive index ($\tilde{m}$), which accounts for water content in the particle, is derived as a volume mixture between the dry aerosol and water (Wex et al., 2002):

$$\tilde{m} = f_{V,dry}\,\tilde{m}_{aero,dry} + (1 - f_{V,dry})\,\tilde{m}_{water} \quad (2)$$

where $f_{v,dry}$ is the ratio of the dry aerosol volume to the total aerosol volume under a given RH condition; $\tilde{m}_{aero,dry}$ is the refractive index for dry ambient aerosols and $\tilde{m}_{water}$, the refractive index

of water, is $1.33+10^{-7}$i. Then, the corresponding aerosol optical properties under the given RH and PNSD can also be calculated. Finally, the aerosol optical profiles can be calculated. Fig. S5 shows one of the calculated aerosol optical profiles.

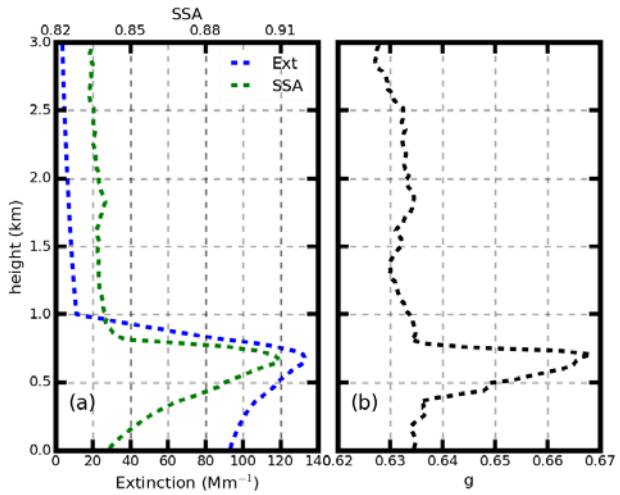

Figure S6. The calculated profiles of the aerosol extinction coefficient, aerosol single scattering albedo and the aerosol asymmetry factor.

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