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The evaluating study of the momentum and heat exchange process of two surface layer schemes during the severe haze pollution in east China

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17 Abstract. The turbulent flux parameterization schemes in surface layer are crucial for air pollution modeling. The pollutants 18 prediction by atmosphere chemical model exist obvious deficiencies, which may be closely related to the uncertainties of the 19 momentum and sensible heat fluxes calculation in the surface layer. In this study, a new surface layer scheme (Li) and a 20 classic scheme (MM5) were compared and evaluated based on the observed momentum and sensible heat fluxes in east 21 China during a severe haze episode in winter. The results showed that it is necessary to distinguish the thermal roughness 22 length z_{0h} from the aerodynamic roughness length z_{0m} , and ignoring the difference between the two led to large errors of 23 the momentum and sensible heat fluxes in MM5. The error of calculated sensible heat flux was reduced by 54% after 24 discriminating z_{0h} from z_{0m} in MM5. Besides, the algorithm itself of Li scheme performed generally better than MM5 in 25 winter in east China and the momentum flux bias of the Li scheme was lower about 12%, sensible heat flux bias about 5% 26 than those of MM5 scheme. Most of all, the Li scheme showed a significant advantage over MM5 for the transition stage 27 from unstable to stable atmosphere corresponding to the PM2.5 accumulation. The momentum flux bias of Li was lower 28 about 38%, sensible heat flux bias about 43% than those of MM5 during the PM_{2.5} increasing stage. This study result 29 indicates the ability of Li scheme for more accurate describing the regional atmosphere stratification, and suggests the 30 potential improving possibilities of severe haze prediction in east China by online coupling it into the atmosphere chemical 31 model

32 Key words: surface layer; turbulent flux parameterization; roughness length; numerical modeling; air pollution





33 1 Introduction

34 Adequate air quality modeling relies on accurate simulations of meteorological conditions, especially in planetary 35 boundary layer (PBL) (Hu et al., 2010; Cheng et al., 2012; Xie et al., 2012). The PBL is closely coupled to the earth's surface 36 by turbulent exchange processes. The surface layer (SL) close to the earth's surface reflects the surface state by calculating 37 momentum, heat, water vapor and other fluxes, and influences the atmospheric structure by turbulent transport process. The 38 SL provides important bottom boundary conditions, as the bottom layer of the PBL. In addition, atmospheric conditions in 39 both the PBL and upper layers are strongly dependent on the turbulent fluxes which are computed in the SL (Ban et al., 40 2010). Flux parameterization in the SL plays an important role in studies of the hydrological cycle and weather prediction 41 (Yang et al., 2001; Li et al., 2014).

In many numerical models, surface momentum, heat and moisture fluxes calculated by a SL scheme are coupled to a Land Surface Module, which in turn provides input to the PBL module. Therefore, an adequate SL scheme is crucial for the model performance (Jim énez et al., 2012). It was reported that the difference of 2-m temperature modeling in three PBL schemes is due to different calculation of sensible heat fluxes in the SL (Hu et al., 2010). Tymvios et al.(2017) evaluated the perfomence of Weather Research and Forecasting (WRF) model with a combination of several PBL and compatible SL schemes and emphasized the importance of SL schemes.

48 Most SL schemes used in numerical models are bulk algorithms which are based on Monin-Obukhov similarity theory 49 (hereinafter MOST, Monin and Obukhov, 1954). In a bulk algorithm, vertical fluxes in the SL can be considered constant. 50 The effects of shear stress and buoyancy on turbulent transport are discussed with the method of similarity theory and 51 dimensional analysis. Turbulent fluxes in models are parameterized by wind, temperature, moisture in the lowest layer, 52 surface skin temperature and humidity. Many international scholars verified the MOST using of field experiments and then 53 proposed the universal functions, the commonly used of which is Businger-Dyer (BD) equation (Businger, 1966; Dyer, 54 1967). With the development of observation technology, the coefficients in the BD equation have been further modified (e.g., 55 Paulson, 1970; Webb, 1970; Businger et al., 1971; Dyer, 1974; Högström, 1996). In addition to the BD equation, some 56 other schemes have been put forward and they may perform better especially for the strongly stable stratification (e.g., 57 Holtslag and De Bruin, 1988, Beljaars and Holtslag, 1991, Chenge and Brutsaert, 2005). The schemes can be divided into 58 two types according to the computing characteristics. One type is called as iterative algorithm (e.g., Paulson, 1970; Businger 59 et al., 1971; Dyer, 1974; Högström, 1996; Beljaars and Holtslag, 1991), and it keep the MOST completely with less 60 approximation so that the results can be more precise. However, it needs to take much more steps to converge and hence the 61 CPU time is consuming which affects the ability and efficiency of modeling (Louis, 1979; Li et al., 2014); The other one is 62 called as non-iterative algorithm (e.g., Louis et al., 1982; Launiainen, 1995; Wang et al., 2002; Wouters et al., 2012). Due to 63 the approximate treatment, there is no need for loop iteration in calculation. It is much simpler and less CPU time-consuming,





64 but it may lead to a lower accuracy of the results.

65 Although many researches above focused on the effects of the SL schemes on PBL and meteorological elements, few 66 studies discussed it based on a pollution episode corresponding various atmospheric states. The turbulent exchange of 67 momentum, heat, and moisture at the ground surface is more important than large-scale transport for the accumulation and 68 transport of pollutants when atmosphere is stable. In this paper, two kinds of surface flux calculation schemes were 69 compared and evaluated during a haze episode using observational flux data. One is a new scheme proposed by Li et al. 70 (2014; 2015, Li hereinafter), the other is MM5 similarity scheme (Zhang and Anthes, 1982, MM5 hereinafter) which is 71 widely applied in modeling investigation (e.g., Hu et al., 2010; Wang et al., 2015a, b; Tymvios et al., 2017). As a new one, 72 the Li scheme is not yet applied to the atmosphere chemical models, and few relevant articles evaluate this scheme using the 73 observational data especially in a haze episode. In this scheme, the aerodynamic roughness length z_{0m} and thermal 74 roughness length z_{0h} are distinguished each other and the effect of the roughness sublayer (RSL) is taken into account. In addition, this scheme can be applied to the full range of roughness status $10 \le \frac{z}{z_{om}} \le 10^5$ and $-0.5 \le \ln \frac{z_{om}}{z_{ob}} \le 30$ under 75 76 whole conditions $-5 \le Ri_B \le 2.5$. Here z is the reference height and Ri_B is the bulk Richardson number. Compared with Li, 77 the MM5 scheme does not consider the effect of both z_{0h} and the RSL. Further, in order to keep the stability of modeling, 78 some limits have been used in MM5 such as a limit of -10 is used for both the stability parameter ζ and universal functions.

79 2 Theory

80 The definition of the momentum and sensible heat flux are introduced, and the detailed algorithms of the Li and MM581 schemes are explained.

- 82 2.1 Introduction of the momentum and sensible heat flux
- 83 The turbulent fluxes from ground surface are defined as follows:

84
$$au = \rho u_*^2$$
 and (1a)

$$H = -\rho c_p u_* \theta_*. \tag{1b}$$

86 Where τ is the momentum flux, H is the sensible heat flux, ρ is the air density, c_p is the specific heat capacity at 87 constant pressure. u_* and θ_* are the friction velocity and the temperature scale, respectively, and they represent the 88 intensity of the vertical turbulent flux transport and they are approximately independent on height in the SL.

- 89 Both the Li and MM5 schemes are calculated with bulk flux parameterization. As an important dimensionless parameter
- 90 related with the stability, the bulk Richardson number $Ri_{\rm B}$ is defined as

91
$$Ri_{\rm B} = \frac{gz(\theta - \theta_{\rm g})}{\theta u^2}.$$
 (2)

92 Where g is the acceleration of gravity, z is the reference height which is the lowest level in the model, θ is the mean





- 93 potential temperature at height z, θ_g is the surface radiometric potential temperature, u is the mean wind speed at height z.
- 94 Thus, $Ri_{\rm B}$ can be computed through meteorological data at least two levels.
- 95 2.2 The Li scheme

96 The basic idea of Li is to parameterize ζ directly with Ri_B , z_{0m} and z_{0h} , and then calculate turbulence fluxes. In the

scheme, bulk transfer coefficients of the momentum and sensible heat fluxes (C_M , C_H) are expressed as

98
$$C_M = \frac{u_i^2}{u^2} = \frac{\tau}{\rho u^2} \quad \text{and} \tag{3a}$$

99
$$C_H = \frac{u_* \theta_*}{u(\theta - \theta_g)} = -\frac{H}{\rho c_p u(\theta - \theta_g)}.$$
 (3b)

Based on MOST and considering the RSL effect, the relationship between the bulk transfer coefficients and the profile
 functions corresponding to wind and potential temperature are usually expressed as

102
$$C_{M} = \frac{k^{2}}{\left[\ln \frac{z}{z_{0m}} - \psi_{M}\left(\frac{z}{L}\right) + \psi_{M}\left(\frac{z}{L}, \frac{z}{z_{*}}\right)\right]^{2}} \text{ and } (4a)$$

103
$$C_{H} = \frac{k^{2}}{R\left[\ln\frac{z}{z_{0m}} - \psi_{M}\left(\frac{z}{L}\right) + \psi_{M}\left(\frac{z_{0m}}{L}\right) + \psi_{M}^{*}\left(\frac{z}{L}, \frac{z}{z_{*}}\right)\right] \left[\ln\frac{z}{z_{0h}} - \psi_{H}\left(\frac{z}{L}\right) + \psi_{H}^{*}\left(\frac{z}{L}, \frac{z}{z_{*}}\right)\right]}.$$
 (4b)

104 Where k is the von K \acute{a} m \acute{a} n constant which is 0.4 in both two schemes, R is the Prandtl number which is 1.0 in two 105 schemes, ψ_M and ψ_H are the integrated stability functions for momentum and sensible heat, respectively, which are also 106 called universe functions. L is the Obukhov length ($\zeta = \frac{z}{L}$), ψ_M^* and ψ_H^* are the correction functions accounting for RSL 107 effect, z_* is the height of RSL. From above equations we can see that the calculation of the momentum and sensible heat 108 flux requires C_M and C_H (or u_* and θ_*), and there are 3 key points to get them:

109 1. z_{0m} and z_{0h} . z_{0m} and z_{0h} are two key parameters in the bulk transfer equations and their definitions and 110 influence will be given in Sect. 4.1.

111 2. ζ . In the Li scheme, the determination of ζ is the most crucial problem for calculation of turbulent fluxes. Li is a new 112 scheme based on the results of Yang et al. (2001), Wouters et al. (2012), Sharan and Srivastava (2014), and which is 113 proposed to approach the classic iterative computation results using multiple regressions. In particular, under stable 114 conditions, the calculation procedure for a given group of Ri_B , z_{0m} and z_{0h} is the following: (1) find the region 115 according to z_{0m} and z_{0h} with Table 1 (see Li et al., 2014); (2) find the section according to the region and Ri_B with 116 Eq. (5) and coefficients in Table 2 (see Li et al., 2014); (3) calculate ζ using Eq. (6) and Tables 3-10 (see Li et al., 117 2014).

118
$$Ri_{\rm Bcp} = \sum C_{mn} (\log L_{0M})^m (L_{0H} - L_{0M})^n, \tag{5}$$

119
$$\zeta = Ri_{\rm B} \sum C_{ijk} Ri_{\rm B}^{i} L_{0M}^{j} (L_{0H} - L_{0M})^{k}.$$
(6)

120 Where C_{mn} and C_{ijk} are the coefficients in Tables 3-10. $L_{0M} = \ln \frac{z}{z_{0m}}$, $L_{0H} = \ln \frac{z}{z_{0h}}$. m, n = 0, 1, 2, and m + 121 $n \le 3$; i, j, k = 0, 1, 2, 3, and i + j + k \le 4. Similarly, under unstable conditions, eight regions are divided according to





122	the method from Li et al. (2015). For each of the regions, ζ is carried out by following:
123	$\zeta = R i_{\rm B} \frac{L_{0M}^2}{L_{0H}} \sum C_{ijk} \left(\frac{-R i_{\rm B}}{1 - R i_{\rm B}} \right)^i L_{0M}^{-j} L_{0H}^{-k}.$ (7)
124	Where C_{ijk} is seen in Table 2 (Li et al., 2016), and $i = 0, 1$; $j, k = 0, 1, 2, 3$; $i + j + k \le 4$.
125	3. Universal function. It is also a key factor in flux calculation. The form of universal function is adopted from CB05
126	(Chenge and Brutsaert, 2005) under the stable condition (Eqs. (8a), (8b)) and Paulson70 (Paulson, 1970) under the
127	unstable condition (Eqs. (9a), (9b)):
128	$\psi_M(\zeta) = -a \ln \left[\zeta + (1+\zeta^b)^{\frac{1}{b}}\right], \zeta > 0 \text{(stable)}, \tag{8a}$
129	$\psi_H(\zeta) = -c \ln \left[\zeta + (1+\zeta^d)^{\frac{1}{d}}\right], \zeta > 0 \text{(stable)}, \tag{8b}$
130	$\psi_M(\zeta) = 2\ln\frac{1+x}{2} + \ln\frac{1+x^2}{2} - 2\arctan(x) + \frac{\pi}{2}, \zeta < 0 \text{ (unstable)},$ (9a)
131	$\psi_H(\zeta) = 2\ln\frac{1+y}{2}, \zeta < 0 \text{(unstable)}. \tag{9b}$
132	Where $a = 6.1$, $b = 2.5$, $c = 5.3$, $d = 1.1$, $x = (1 - 16\zeta)^{1/4}$, $y = (1 - 16\zeta)^{1/2}$.
133	In addition, the RSL effect is taken into account in the Li scheme. In the RSL, turbulence is strongly affected by
134	individual roughness elements, and the standard MOST is no longer valid (Simpson et al., 1998). Therefore, it is
135	necessary to consider the RSL effect in the calculation of turbulent fluxes, especially for the rough terrain such as forest
136	or large cities. Ridder (2010) proposed the expression of ψ_M^* and ψ_H^* :
137	$\psi_M^*\left(\zeta, \frac{z}{z_*}\right) = \phi_M\left[\left(1 + \frac{v}{\mu_M z/z_*}\right)\zeta\right]\frac{1}{\lambda}\ln\left(1 + \frac{\lambda}{\mu_M z/z_*}\right)e^{-\mu_M z/z_*} \text{ and } (10a)$
138	$\psi_H^*\left(\zeta, \frac{z}{z_*}\right) = \phi_H\left[\left(1 + \frac{v}{\mu_H z/z_*}\right)\zeta\right]\frac{1}{\lambda}\ln\left(1 + \frac{\lambda}{\mu_H z/z_*}\right)e^{-\mu_H z/z_*}.$ (10b)
139	Where $v = 0.5$, $\mu_M = 2.59$, $\mu_H = 0.95$, $z_* = 16.7z_{0m}$, $\lambda = 1.5$. ϕ_M and ϕ_H are universal functions before
140	integration. Here, set $\chi_M = 1 + \frac{v}{\mu_M z/z_*}$, $\chi_H = 1 + \frac{v}{\mu_H z/z_*}$:
141	$\phi_M(\chi_M\zeta) = 1 + a \frac{\chi_M\zeta + (\chi_M\zeta)^b [1 + (\chi_M\zeta)^b]^{\frac{1-b}{b}}}{\chi_M\zeta + [1 + (\chi_M\zeta)^b]^{\frac{1}{b}}}, \zeta > 0 (\text{stable}), (11a)$
142	$\phi_H(\chi_H\zeta) = 1 + c \frac{\chi_H\zeta + (\chi_H\zeta)^d [1 + (\chi_H\zeta)^d]^{\frac{1-d}{d}}}{\chi_H\zeta + [1 + (\chi_H\zeta)^d]^{\frac{1}{d}}}, \zeta > 0 \text{(stable)}, (11b)$

- 143 $\phi_M(\chi_M\zeta) = (1 16\chi_M\zeta)^{-1/4}, \quad \zeta < 0 \text{ (unstable)},$ (12a)
- 144 $\phi_H(\chi_H\zeta) = (1 16\chi_H\zeta)^{-1/2}, \quad \zeta < 0 \text{ (unstable)}.$ (12b)

145 The Li scheme is summarized as: firstly determine $Ri_{B^{n}} z_{0m}$ and z_{0h} according to the observation data, and then 146 calculate ζ with $Ri_{B^{n}} z_{0m}$ and z_{0h} . Finally carry out the momentum and sensible heat fluxes under different stratification 147 conditions.





148 2.3 The MM5 scheme

149 In this scheme, no distinction is made between z_{0m} and z_{0h} , thus we express the roughness length with z_0 . Under the 150 unstable condition, take Paulson70 with Eqs. (16a) and (16b), and under the stable condition, the atmospheric stratification 151 conditions are subdivided into three cases according to Zhang and Anthes (1982). In addition, this scheme does not consider 152 the RSL effect. 153 (1) Strongly stable condition ($Ri_B \ge 0.2$): $\psi_M = \psi_H = -10 \ln \frac{z}{z_0}.$ 154 (13)155 (2) Weakly stable condition ($0 < Ri_B < 0.2$): $\psi_M = \psi_H = -5 \left(\frac{Ri_{\rm B}}{1.1 - 5Ri_{\rm B}}\right) \ln \frac{z}{z_0}.$ 156 (14)(3) Neutral condition ($Ri_{\rm B} = 0$): 157 $\psi_M=\psi_H=0.$ 158 (15)(4) Unstable condition ($Ri_{\rm B} < 0$): 159

160
$$\psi_M = 2 \ln \frac{1+x}{2} + \ln \frac{1+x^2}{2} - 2 \arctan(x) + \frac{\pi}{2},$$
 (16a)

161
$$\psi_H = 2\ln\frac{1+y}{2},$$
 (16b)

162 where
$$x = (1 - 16\zeta)^{1/4}$$
, $y = (1 - 16\zeta)^{1/2}$.

This scheme calculates turbulent fluxes of the momentum and sensible heat with u_* and θ_* . In order to avoid the difference of u_* before and after is too large, u_* is arithmetically averaged with its previous value with Eq. (17), and a lower limit of $u_* = 0.1$ m/s is imposed in order to prevent the heat flux from being zero under very stable conditions. According to the profile functions of wind and temperature near the ground, θ_* then is deduced by Eq. (18).

167
$$u_* = \frac{1}{2} \left(u_* + \frac{ku}{\ln \frac{z}{z_{0m}} - \psi_M} \right), \tag{17}$$

168
$$\theta_* = \frac{k(\theta - \theta_g)}{R[\ln \frac{z}{z_{0h}} - \psi_H]}.$$
 (18)

169 Overall, the universal functions in different conditions are determined by $Ri_{\rm B}$ and z_0 . Then u_* and θ_* will be 170 calculated with meteorological data and flux data. At last, the turbulent fluxes are derived by Eqs. (1a) and (1b).

171 3 Observational data and methods

The observational data was from Gucheng station (GC), which is in China Atmosphere Watch Network (CAWNET) and located in the southwest of Beijing about 110km, at 115.40 £, 39.08 N. In winter, the station surface was covered with wheat and the surrounding areas were mainly farmland and scattered villages (Fig. 1). The eddy correlation flux measurement system is mainly composed of a three-dimensional (3D) Temperature measurement with a sonic anemometer





(CSAT3) and a fast response infrared gas analyzer (LI-7500) at 4m height. The data was collected from December 1, 2016 to January 9, 2017 including momentum fluxes, heat fluxes, wind speed and wind direction, air temperature, density of air and vapor, pressure with 30 minutes interval. Besides, there were radiation data provided by the net radiation sensor (CNR1) including the surface upward long wave radiation and the long wave radiation incident to the ground surface and PM_{2.5} data provided by the Environmental Protection Station of China's Ministry of Environmental Protection (EPS/CMEP).

181 3.1 Data processing

182 In order to obtain accurate flux data, it needs quality control of the observational data, including eliminated the outliers and the data in rainy days, as well as correcting momentum by using a double axis rotation for the sonic anemometer tilt 183 correction and correcting sensible heat fluxes by modifying sonic virtual temperature. In addition, we considered the effect 184 185 of wind field on the roughness length. Fig. 2 shows distribution frequency of wind speed and wind direction at GC during 186 observations (December 1, 2016 ~ January 9, 2017). The wind speed is stable during this period and the maximum is no more than 5m and most of them are about $1 \sim 2m/s$. The wind direction is relatively uniform except for the southeast wind 187 188 (135 degrees). Therefore, to avoid the measurement error of the instrument, the wind speed data less than 0.5m/s are 189 eliminated.

190 **3.2 Determination of surface skin temperature**

191 The surface skin temperature error caused by the CSAT3 is too large to be taken to calculate the flux as input. Therefore,192 the surface skin temperature is calculated from the radiation data detected by the CNR1 as:

193 $R_{lw}^{\dagger} = (1 - \varepsilon_s) R_{lw}^{\downarrow} + \varepsilon_s \sigma T_q^4, \tag{19}$

where R_{lw}^{\dagger} and R_{lw}^{\downarrow} are the surface upward longwave radiation and long wave radiation incident on the surface, 194 respectively. σ is the Stephen Boltzmann constant, $\sigma = 5.67 \times 10^{-8} \text{Wm}^{-2} \text{K}^{-4}$. T_g is the surface skin temperature, ε_s is 195 196 the surface emissivity which is the basis for calculating T_q . Many researches estimated ε_s and the range of the values is 197 always 0.9 ~ 1 (Stewart et al., 1994; Verhoef et al., 1997). According to the semi-empirical method in Yang et al. (2008), ε_s 198 is estimated when the RMSE is minimal. In this paper, the Li and MM5 schemes were used to estimate the ε_s value (as 199 shown in Fig. 3). It is clear that the ε_s value corresponding the minimum RMSE is not very sensitive to the choice of two 200 schemes. When ε_s is 1, the RMSE has the minimum value. Thus, we take 1 as the optimal value of ε_s to calculate T_g 201 value.

202 4 Results and discussion

The concept of roughness and its influence on the calculation of turbulent flux are going to be described in detail, and then the value of z_{0m} and z_{0h} will be determined by theories above. Using z_{0m} , z_{0h} and related observational data, we





will have offline tests on Li and MM5. Finally, the behavior of two schemes will be compared in a severe haze pollution atGC.

207 4.1 The influence of roughness length on the calculation of turbulent flux

208 z_{0m} is defined as a height at which the extrapolated wind speed following the similarity theory vanishes. It is mainly 209 determined by land-cover type and canopy height after excluding large obstructions. In models, z_{0m} is always based on a 210 look-up table which is related to land-cover type. In this paper, z_{0m} is simply classified based on the research of Stull (1988) 211 and is listed in Table 1. It can be seen that the more rough land surface is, the higher value of z_{0m} is. Thus, different 212 land-cover types have different effects on flux calculation. z_{0h} is a height at which the extrapolated air temperature is 213 identical to the surface skin temperature, and it is also a scalar quantity. Some early researches assumed that z_{0m} was equal 214 to z_{0h} (Louis, 1979; Louis et al., 1982). However, the assumption is not applicable in reality because z_{0m} and z_{0h} have 215 different physical meanings. Thus, many following studies modified this assumption and made it more reliable in the 216 situation that z_{0m} was not equal to z_{0h} or the difference between two values was much large (e.g., Song, 1998; Wouters et 217 al., 2012; Li et al., 2014; Li et al., 2015).

218 With the Li scheme, we test the effect of the roughness length on flux calculation. In the process, take z = 10m as the 219 reference height and set the range of Ri_B according to Louis82 (Louis et al., 1982) from -2 to 1. Firstly, discuss the effect of z_{0m} on flux calculation. Set $\frac{z_{0m}}{z_{0h}} = 1$, corresponding to four cases: $z_{0m} = 1$, 0.5, 0.05, 0.001m. These cases correspond to 220 221 large cities, forests, agricultural fields and wide water surface, respectively. Fig. 4 gives the relationship between $C_M(C_H)$ 222 and Ri_B for different z_{0m} values. The effects of different land-cover types on C_M and C_H are significant under both the 223 stable atmosphere ($Ri_B > 0$) and the unstable atmosphere ($Ri_B < 0$). The rougher the surface is (corresponding the larger 224 z_{0m} value), the larger the calculated momentum or sensible heat flux is. In addition, there is a corresponding relationship 225 between $C_M(C_H)$ and stability. The more unstable the atmosphere is, the larger difference the value of $C_M(C_H)$ is 226 and vice versa. Once the value of Ri_B exceeds the critical value (generally 0.2~0.25), the transfer coefficients decline 227 sharply but above 0.

Secondly, discuss the effect of difference between z_{0m} and z_{0h} on flux calculation. The relationship between z_{0m} and z_{0h} can be expressed as $kB^{-1} = \ln \frac{z_{0m}}{z_{0h}}$. Over the sea, z_{0m} is comparable to z_{0h} ; over the uniform vegetation surface (e.g., grassland, farmland, woodland), kB^{-1} is about 2 ($z_{0m}/z_{0h} \approx 10$) (Garratt and Hicks, 1973; Garratt, 1978; Garratt and Francey, 1978); over the surface with bluff roughness elements, the $\frac{z_{0m}}{z_{0h}}$ value may be very large. For example, in some large cities, kB^{-1} can reach 30 ($z_{0m}/z_{0h} \approx 10^{13}$) (Sugawara and Narita, 2009). Therefore, the $\frac{z_{0m}}{z_{0h}}$ value can varies over a wide range. Fig. 5 shows the relationship between $C_M(C_H)$ and Ri_B for different $\frac{z_{0m}}{z_{0h}}$ values. Set $z_{0m} = 1$, $z_{0h} = 1$, 0.01,





10⁻⁴, 10⁻⁶m, and The large difference derived from the different ratios in Fig. 5. The larger the ratio is, the slower $C_M(C_H)$ fails with a rising stability. These results show that distinguishing between z_{0m} and z_{0h} has great impact on flux calculation which is closely related to severe haze pollution. Ignoring the difference between the two may lead to large errors in flux calculation and finally in air quality modeling.

238 4.2 The determination of roughness length z_{0m} (z_{0h})

Based on above description and discussion, it can be seen that the determination of the appropriate value of z_{0m} (z_{0h}) is a key and basis for calculation of surface turbulent fluxes. Using observational flux data with quality control, z_{0m} and z_{0h} are derived by Eq. (20a) and (20b) following Yang et al. (2003) and Sicart et al. (2014).

$$\frac{u_*}{u} = \frac{k}{\ln \frac{z}{z_{0m}} - \psi_M},\tag{20a}$$

243
$$\frac{\theta_*}{(\theta - \theta_g)} = \frac{k}{R[\ln \frac{Z}{Z_{Dh}} - \psi_H]}.$$
 (20b)

During the observation period, the crops stopped growing and the height did not exceed 0.1 m, so the zero-plane displacement height can be ignored. The observation time is too short (about 1 month) to consider the effect of seasonal variations on roughness. Thus, assume z_{0m} and z_{0h} are two fixed values. Given the observational data, a dataset of z_{0m} (z_{0h}) then is generated. Finally take median of the dataset as typical values of z_{0m} and z_{0h} for GC site: $z_{0m} = 0.0419$ m, $z_{0h} = 0.0042$ m. These results are comparable to the typical values for agricultural fields ($z_{0m} = 0.05$, $z_{0m}/z_{0h} = 10$) discussed above. Therefore, the results are considered credible.

250 4.3 Comparison of two schemes for calculating momentum and sensible heat flux

251 Using the calculated roughness length and the relative observations, the Li and MM5 schemes are going to be tested 252 offline to compare their calculations of the momentum and sensible heat flux (Fig. 6). Firstly, take $z_{0m} = 0.0419$ and $z_{0h} = 0.0042$ in the Li scheme, $z_0 = z_{0m} = 0.0419$ in the MM5 scheme to calculate the momentum and sensible heat 253 254 fluxes and the comparison results are shown in Figs. 6a and 6b. Compared with MM5, Li performs better with higher 255 regression coefficient and determination coefficient. For momentum fluxes, the regression coefficient in Li is 0.6795 and that 256 in MM5 is 0.5598, indicating that the error of Li is 12% lower than that of MM5. For sensible heat fluxes, the regression 257 coefficient in Li is 0.7967 and that in MM5 is 1.7994. The latter is much larger than 1 which says the MM5 scheme 258 overestimate a lot. That is due to no distinction of roughness length in the MM5 scheme. In order to compare the difference of two schemes without considering the effect of roughness length, take $z_0 = z_{0h} = 0.0042$ in the MM5 scheme to 259 260 calculate the sensible heat fluxes as Fig. 6c. Compared with Fig. 6b, there is a great improvement after modifying z_0 value 261 that the regression coefficient in MM5 becomes 0.7363, which is indicated that the error of calculated sensible heat flux by 262 MM5 was reduced by 54% after discriminating z_{0h} from z_{0m} . However, the error in Li is still 5% lower than that in MM5.





This illustrates that in addition to the effect of roughness length, the Li scheme itself (including the selection of universal functions and the consideration of the RSL effect) is more reasonable than the MM5 scheme.

265 4.4 The specific performance of the two scheme in severe haze pollution

266 There were two obvious pollution processes during this observation period and one occurred during December 13 to 23, 267 2016. Fig. 7 shows the time series of PM2.5 as well as the momentum fluxes and sensible heat fluxes both for calculation and 268 observation in this pollution episode. For the research purpose significance, only the variation of above variables in the 269 daytime (set from 8:00 a.m. to 20:00 p.m.) is taken into account. All analysis data are processed as hourly average. It needs 270 to note that in MM5, take 0.0419 of z_0 when calculate momentum fluxes and take 0.0042 of z_0 when calculate sensible 271 heat fluxes. As shown in Fig. 7, on the whole, the calculated results of momentum and sensible heat fluxes for the two 272 schemes are consistent with the trend of the observed data. Specifically, for the momentum fluxes (Fig. 7a), when the 273 observed momentum fluxes are large, the calculated results of the two schemes have little difference. When the observed 274 momentum fluxes are small, the Li scheme results are close to or less than the observations, while the MM5 scheme results 275 are always higher than observations because of the limit of $u_* = 0.1$. For the sensible heat fluxes (Fig. 7b), MM5 results are 276 always lower than observations while Li results are closer to observations especially when the observed values are small.

277 Fig. 7 also shows the diurnal variation of PM2.5 during this process. According to the evolution characteristics of fluxes 278 and PM_{2.5} concentration, the process is then divided into three stages: the no pollution stage (stage 1: 13~14), the 279 accumulation stage (stage 2: 16~18) and the maintenance stage (stage 3: 21~22) to discuss and evaluate the two schemes. As 280 shown in Fig. 7, before the pollution occurs (stage 1), the atmospheric stratification is unstable, PM_{2.5} concentration is low 281 and there is a strong flux transport in the SL, the corresponding observations of the momentum and sensible heat flux are 282 relatively high and the daily change of them is also great. In the accumulation stage (stage 2), the atmosphere is changing 283 from unstable to stable corresponding with hazes formation, the momentum and sensible heat fluxes gradually decreases and 284 the daily variation also decreases. In the maintenance stage, the atmospheric stratification is very stable, and flux transport in 285 the SL is weak, both the momentum and sensible heat fluxes are at a low level.

286 Fig. 8 shows the probability distribution functions (PDF) of the difference of momentum (Figs. 8a, 8c, 8e, 8g) and 287 sensible heat fluxes (Figs. 8b, 8d, 8f, 8h) calculated by using Li and MM5 schemes from the observations in different stages. 288 In the whole pollution process, for momentum fluxes (Fig. 8a), compared with MM5, the distribution of bias from the Li 289 scheme tends to cluster in a narrower range centered by 0, and the probability of Li bias within ± 0.005 N m⁻² is 46.82%. The probability of MM5 bias within this range fall to 23.02%. For sensible heat fluxes (Fig. 8b), the distribution of bias from Li 290 291 is still more concentrated around 0 than it is from MM5. The probabilities of Li and MM5 bias within ± 2.5 W m⁻² are 32.54% and 13.49%, respectively. In stage 1, for momentum fluxes (Fig. 8c), the probability of Li bias within ±0.005N m⁻² is 38.09%. 292 293 The probability distribution of MM5 bias focus on area larger than 0, and its probability within ±0.005N m⁻² is 14.29%. For





294 sensible heat fluxes (Fig. 8d), the probability of Li bias within ±2.5W m⁻² is 38.09%, the same as momentum fluxes. The 295 probability distribution of MM5 bias focus on area less than 0, and its probability within ±2.5W m⁻² is 9.52%. In stage 2, the 296 difference between the schemes is more obvious. The momentum and sensible heat fluxes bias from Li is the most 297 concentrated around 0 in all cases, while the distribution of MM5 bias is similar to that in stage 1. Specifically, for 298 momentum fluxes (Fig. 8e), the probabilities of Li bias and MM5 bias within ±0.005N m⁻² are 56.25% and 25.00%. For 299 sensible heat fluxes (Fig. 8f), the probabilities of Li bias and MM5 bias within ±2.5W m⁻² are 40.62% and 6.25%. In stage 3, 300 the difference between two schemes is small. For momentum fluxes (Fig. 8g), the probabilities of Li bias and MM5 bias 301 within ±0.005N m⁻² are 22.73% and 27.27%. For sensible heat fluxes (Fig. 8h), the probabilities of Li bias and MM5 bias 302 within ± 2.5 W m⁻² are both 36.36%.

303 Four common evaluation metrics were used to further test the abilities of the Li and MM5 schemes in calculating fluxes 304 (Table 2). They are the mean bias (MB), normalized mean bias (NMB), normalized mean error (NME) and root mean square 305 error (RMES). Table 2 shows that the Li scheme generally gives a better estimate than the MM5 scheme. In whole process, 306 the momentum fluxes calculated by Li is underestimated by 3.63% relative to the observations, while the results calculated 307 by MM5 is overestimated by 34.03%. The sensible heat fluxes calculated by Li and MM5 are both underestimated and the 308 underestimations are 15.69% and 50.22%. In three selected stages, the Li scheme performs better than the MM5 scheme in 309 first two stages. Especially in stage 2, that is, the atmosphere transforming from unstable to stable stratification, the 310 difference between the Li and MM5 schemes are particularly significant. Both the Li and MM5 schemes have overestimates 311 for momentum fluxes and the values are 7.68% and 45.56, respectively. Two schemes have underestimates for sensible heat 312 fluxes and the values are 33.84% and 76.88%. It can be seen the Li scheme calculation error is much smaller than the MM5 313 scheme error. This stage plays an important role in the generation and accumulation of pollutants. How to simulate the atmospheric state in a more reasonable way is also a critical issue for air pollution modeling. Therefore, the superiority of the 314 315 Li scheme in the air pollution process, especially in this stage is of great reference value for improving the forecast of 316 pollutant concentration in the current air quality model. In stage 3, the difference between the two schemes is not obvious.

317 5 Conclusions

The applicability in describing the atmospheric stratification related with severe haze in east China of the Li and MM5 schemes are evaluated and discussed. The observed momentum and sensible heat fluxes, together with conventional meteorological data from December 1, 2016 to January 9, 2017, including a severe pollution episode from December 13 to 23, are used to do that. The transitional stage of atmospheric stratification from unstable to stable, corresponding to accumulation of $PM_{2.5}$, is mainly discussed in this paper. The contributions of roughness lengths (z_{0m} and z_{0h}) as well as the algorithms of the momentum and sensible heat flux calculation are discussed. The results are summarized as follows:





1) z_{0m} and z_{0h} have important effects on turbulent flux calculation. z_{0m} and $\frac{z_{0m}}{z_{0h}}$ both reflect the condition of 324 325 underlying surface and impact flux calculation greatly. Under the same condition, the larger z_{0m} (indicating rougher surface) is, the larger the calculated fluxes are. The fluxes over large cities ($z_{0m} = 1$) is quite different from those over 326 agricultural fields ($z_{0m} = 0.05$, similar to the value at GC). When z_{0m} is larger, the value of $\frac{z_{0m}}{z_{0h}}$ should be larger, and 327 the larger the value of $\frac{z_{0m}}{z_{0h}}$ is, the greater the differences of calculated fluxes are. Especially, for a super city like 328 Beijing, the value of $\frac{z_{0m}}{z_{0h}}$ may be much larger than 10⁶ and ignoring the difference between z0m and z0h may lead to 329 330 much uncertainties in flux calculation. It is very necessary to distinguish between z_{0m} and z_{0h} in SL scheme, which 331 is probably beneficial to improve simulation of regional atmosphere stratification over urban agglomeration with rough 332 surface and then PM2.5 during hazes. 333 2) It could be seen from the regression coefficients and determination coefficients between calculated fluxes by the two 334 schemes and observed fluxes of 40 days that the Li scheme was better than the MM5 scheme in general. For the 335 momentum fluxes, the determination coefficients of Li and MM5 was about 0.41 and 0.40. Both schemes passed the 336 significance level of 99.9%. The regression coefficient of Li was 0.68, and it generally reduced the error by 12% 337 compared with MM5. When z_{0m} and z_{0h} took the same value ($z_0 = z_{0m} = 0.0419$) in MM5, the sensible heat fluxes 338 were obvious overestimated. When z_{0h} was taken into account ($z_0 = z_{0h} = 0.0042$) in MM5, the calculated fluxes were significant improved and the error was reduced by 54%. However, this error was still higher about 5% compared 339

with the Li scheme, illustrating that apart from the impact of roughness length, the different algorithms of the twoschemes also achieves obvious differences in calculated fluxes.

3) During the heavy pollution process, the calculated momentum and sensible heat fluxes by the Li scheme were better
than those by the MM5 scheme generally. Especially in the PM2.5 accumulated stage, the advantages of Li were more
prominent. Compared with MM5, the probability distributions of both the momentum and sensible heat flux bias of Li
tended to cluster in a narrower range centered by 0. The calculated momentum fluxes by Li were overestimated by 7.68%
and this overestimation by MM5 was up to 45.56%. The calculated sensible heat fluxes by Li were underestimated by
33.84% while this underestimation by MM5 was even up to 76.88%.

The offline study in this paper showed that Li scheme was superior to the MM5 scheme in general. This superiority was even more remarkable during the atmosphere transforming stage from unstable to stable stratification. However, the comparison of the two schemes focusing on more underlying surfaces (e.g., super cities and agricultural fields) could not be conducted at present due to the shortage of observed fluxes data, which should be discussed in detail in next paper when the sufficient data is available. The offline results of this paper only offer a basic and a possible way to improve PBL diffusion simulation and then PM_{2.5} prediction, which will be achieved in the follow-up work of online integrating of the Li scheme





into the atmosphere chemical model.

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449	Table 1. Typical values of	Z_{0m}	corresponding to various land-cover types	
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<i>z_{0m}/</i> m	Land-cover types			
5~50	Mountain (above 100m)			
1~5	The center of large cities, hills or mountain area			
0.1~1	Forests, the center of large towns			
0.01~0.1	Flat grasslands, agricultural fields			
10-4~10-3	The snow surface, wide water surface, flat deserts			
10-5	The ice surface			

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453 Table 2. Statistics between the Li and MM5 schemes calculated turbulent flux.

		Li				MM5			
		MB	NMB	NME	RMSE	MB	NMB	NME	RMSE
Whole	τ	-0.0006	-3.63%	54.29%	0.0142	0.0058	34.03%	63.59%	0.0143
process	Н	-2.2723	-15.69%	52.73%	10.9649	-7.2735	-50.22%	69.68%	12.7946
Staga 1	τ	0.0021	9.98%	55.90%	0.0172	0.0091	43.45%	66.66%	0.0169
Stage 1	Н	1.1775	5.79%	37.87%	10.5734	-7.1891	-35.34%	55.70%	13.1324
Stage 2	τ	0.0013	7.68%	44.50%	0.0111	0.0079	45.56%	56.81%	0.0121
Stage 2	Н	-4.5752	-33.84%	50.28%	9.3995	-10.3924	-76.88%	81.40%	13.2553
Stage 3	τ	-0.0024	-13.25%	59.13%	0.0144	0.0030	16.72%	56.34%	0.0138
Stage 5	Н	1.2818	11.39%	66.31%	11.4778	-1.7479	-15.52%	65.90%	10.4219

454 * τ: momentum flux; H: sensible heat flux; MB: mean bias; NMB: normalized mean bias; NME: normalized mean error;

455 RMSE: root mean square error. The units of MB and RMSE: $\mu g \cdot m^{-3}$.







458 Figure 1. Location (a) and geographical environment (b) at GC. The map is from Bing Maps.

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Figure 2. Wind Rose map at GC from December 1, 2016 to January 9, 2017.

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Figure 3. The surface emissivity ε_s dependence of RMSE between observed near-neutral heat fluxes and parameterized heat fluxes (red for Li and blue for MM5) at GC.

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Figure 4. The relationship between $C_M(C_H)$ and Ri_B for different z_{0m} values. 475







Figure 6. Comparison of calculated and observed fluxes. (a) Momentum fluxes (MM5: $z_0 = 0.0419$); (b) sensible heat fluxes (MM5: $z_0 = 0.0419$); (c) sensible heat fluxes (MM5: $z_0 = 0.0042$). Red dots: the Li scheme; green plus signs: the

484 MM5 scheme.







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Figure 7. Variations of hourly turbulent fluxes and $PM_{2.5}$ at GC station in daytime. (a) Momentum fluxes τ (blue line: observations; red line: the Li scheme; green line: the MM5 scheme) and $PM_{2.5}$ concentration (black line); (b) sensible heat fluxes H (the same as τ) and $PM_{2.5}$ concentration (black line). Yellow box: stage 1; blue box: stage 2; purple box: stage 3.

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Figure 8. Probability distribution functions (PDF) of the difference between calculated fluxes (momentum fluxes: left;
sensible heat fluxes: right) by using two schemes (the Li scheme: red bars; the MM5 scheme: green bars) and observations in
different stages (a-b: whole process; c-d: stage 1; e-f: stage 2; g-h: stage 3).