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Identification of secondary aerosol precursors emitted by an

aircraft turbofan

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- 13 Abstract. Oxidative processing of aircraft turbine-engine exhaust was studied using a potential aerosol mass
- 14 (PAM) chamber at different engine loads corresponding to typical flight operations. Measurements were
- 15 conducted at an engine test cell. Organic gases (OGs) and particle emissions pre/post PAM were measured. A
- suite of instruments, including a proton-transfer-reaction mass spectrometer (PTR-MS) for OGs, a multi-gas analyzer for CO, CO, NO_x, and an aerosol mass spectrometer (AMS) for non-refractory particulate matter (NR-
- analyzer for CO, CO₂, NO_X, and an aerosol mass spectrometer (AMS) for non-refractory particulate matter (NR-PM₁) were used. Total aerosol mass was dominated by secondary aerosol formation, which was approximately
- 19 two orders of magnitude higher than the primary aerosol. The chemical composition of both gaseous and
- 20 particle emissions were also monitored at different engine loads and were thrust dependent. At idling load
- 21 (thrust 2.5-7%), more than 90% of the secondary particle mass was organic and could be explained by the
- 22 oxidation of gaseous aromatic species/ OGs; e.g. benzene, toluene, xylenes, tri-, tetra-, and pentamethyl-benzene
- and naphthalene. The oxygenated-aromatics, e.g. phenol, furans, were also included in this aromatic fraction and
- their oxidation could alone explain up to 25% of the secondary organic particle mass at idling loads. The organic
- 25 fraction decreased with thrust level, while the inorganic fraction increased. At an approximated cruise load
- sulfates comprised 85% of the total secondary particle mass.

27 1 Introduction

- 28 Airport activities emit both particulate and gaseous emissions (Unal et al., 2005; Hudda et al., 2014), and are a
- 29 significant source of local gas- and particle-phase pollutants (Westerdahl et al., 2008). These emissions affect
- public health (Lin et al., 2008) and local air quality by increasing pollutant concentrations, e.g. ultrafine
- 31 particulate matter (PM) number concentrations, at the surrounding residential areas (Hudda and Fruin, 2016;
- 32 Hudda et al., 2016).
- 33 The dominant source of airport aerosol is aircraft engine exhaust (Kim, 2009), and is classified as either directly
- emitted primary aerosol (PA) or secondary aerosol (SA). Due to the high combustion efficiency, PA from
- 35 aircraft engines contains mainly black carbon (BC) whereas SA is formed by the oxidation of emitted precursor
- 36 gases. PA and SA precursor emissions such as non-methane organic gases (NMOGs) strongly depend on aircraft
- engine operating conditions (Kinsey et al., 2010) e.g. the BC emission index (EI, g/kg fuel) of a gas-turbine
- 38 engine is usually higher at cruise climb-out and take-off loads (above 60% of the maximum thrust) than at lower
- 39 loads used at idle, taxi (7%) and approach (30%) (Liati et al., 2014; Brem et al., 2015). In contrast to BC,
- 40 NMOG emissions, including e.g. aromatic hydrocarbons, aliphatic hydrocarbons and carbonyls, are clearly
- 41 highest at low loads (Spicer et al., 1994; Slemr et al., 2001; Anderson et al., 2006; Herndon et al., 2006; Kilic et
- 42 al., 2017).
- 43 Aging of fossil fuel combustion exhaust leads to SA/PA ratios higher than 1. Single-ring aromatics are
- 44 traditionally thought to be the most important secondary organic aerosol (SOA) precursors from combustion
- emissions. While this has been shown to be the case for some emissions, *e.g.* from 2-stroke engines (Platt et al., 2014), in other cases non-traditional precursors were assessed to be responsible for the bulk of the SOA mass
- 46 2014), in other cases non-traditional precursors were assessed to be responsible for the bulk of the SOA mass formed, *e.g.* for biomass smoke (Bruns et al., 2016) or on-road vehicles (Platt et al., 2013; 2017; Pieber et al.,
- 48 2017). Similar to these emissions, aging of aircraft emissions studied by Miracolo et al. (2011; 2012) in a smog
- 49 chamber produced substantial amounts of secondary PM exceeding primary PM emissions several-fold. The
- authors showed the dominance of secondary organic aerosol (SOA) at low loads, while at high loads sulfate was the main SA produced. While single-ring aromatic compounds determined using gas-chromatography/mass

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- spectrometry seemed to be important precursors of the SOA formed, a greater part of SOA was believed to
- 53 originate from non-traditional precursors, whose nature remains to be identified (Miracolo et al., 2011; 2012).
- 54 In this study, we measured the SA production potential of aircraft jet engine exhaust as a function of engine load
- 55 and examined the bulk gas-phase organic emissions and their SOA formation potential. SOA was produced by
- 56 OH-initiated oxidation of aircraft NMOG emissions in a potential aerosol mass (PAM) flow reactor (Kang et al.,
- 57 2007). Primary and secondary PM mass was characterized for different engine loads, using an aerosol mass
- 58 spectrometer (AMS). SOA precursors were analyzed in real-time by a proton-transfer-reaction mass
- spectrometer (PTR-MS) and SOA closure was examined under different conditions. The impact of these
- 60 emissions and their SOA potential in typical urban atmospheres, at the proximity of airports is assessed and
- 61 compared to other mobile sources.

62 2 Methods

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absorption.

2.1 **Experimental setup**

64 Exhaust measurements were conducted to characterize NMOG and non-refractory submicron particulate mass 65 (NR-PM₁) emissions from an in-production CFM56 variant turbofan in the test cell of SR Technics at Zurich Airport. The test engine was fueled with standard JET A-1 fuel, and was operated at several engine loads, 66 67 selected to represent aircraft activities during a typical landing/take-off (LTO) cycle. Engine loads were set by 68 specifying the combustion chamber inlet temperature values which correlate with a specific thrust (lbf) at 69 standard atmospheric conditions. The selected loads included idle-taxi (3-7% of the maximum thrust), approach 70 (30% of the maximum thrust), and an approximated cruise load (50-65% of the maximum static thrust). After

71 starting the engine, a warm-up sequence of 25 minutes ran before each test, consisting of five minute-long steps

72 at thrusts of 5%, 15%, 7%, 65% and 85% in sequence.

A simplified scheme of the experimental setup is shown in Figure 1 and is discussed in detail elsewhere (Kilic et 73 74 al., 2017). Details about the sampling system for non-volatile particle emissions can be found in Durdina et al. 75 (2017) and Brem et al. (2015). The turbine engine exhaust was sampled by a single-point probe with an inner 76 diameter of 8 mm, located 0.7 m downstream of the engine exit plane. The exhaust drawn by the probe was 77 directed through a heated (160°C) transfer line to three different lines: (i) the raw gas line, (ii) diluted emissions 78 line and (iii) diluted aged emissions line. CO, CO₂, and NO_x were measured by a multi-gas analyzer (PG250, 79 Horiba Inc.) installed on the raw line. On the diluted line, primary gas and particle measurements were 80 performed. Two ejector dilutors (DEKATI DI-1000) were installed in sequence on this transfer line; after the 81 first dilution, sampling lines were heated to 120°C. The sample was diluted with synthetic air (99.999% purity) 82 either by a factor of 10 or 100, depending on the NMOG concentration. The NMOGs were quantified and 83 characterized by a proton-transfer-reaction time-of-flight mass spectrometer (PTR-ToF-MS) together with a flame ionization hydrocarbon detector (FID) (APHA 370 THC Monitor). The concentration of equivalent black 84 85 carbon (eBC) was determined by a 7-wavelength aethalometer (Drinovec et al., 2015) based on optical

87 Aging of the engine exhaust emissions was achieved by using a potential aerosol mass (PAM) chamber with a 88 continuous flow of 7.6 l/min and a volume of 13.3 liters. Two mercury lamps (emission lines at wavelengths 89 λ=182 nm - 254 nm, BHK Inc.), mounted inside the PAM, were used to irradiate HONO and O₂ required for 90 hydroxyl radical (OH) formation. Different time-integrated OH exposures (molecules cm⁻³ h) were achieved by modulating UV lamp intensity e.g. 80%, 90%, 100%. HONO to boost OH concentrations, and D9-butanol to 91 92 trace OH exposure (Barmet et al., 2012), were injected with flows of 1.8 and 0.4 l/min, respectively. Further, the 93 PAM was also humidified (~20% relative humidity) by injecting synthetic air with water vapor (with a flow of

94 1.6 l/min). All measurements were conducted at 295-298°K. Secondary aerosol formation was measured after

95 the PAM, while the primary emissions were measured from the bypass line.

- 96 Aging in a PAM is not completely analogous to that in a smog chamber, due to higher oxidant concentrations.
- 97 However, intercomparison studies suggest that the amount of SOA production and its bulk elemental
- 98 composition are comparable for both single precursors (e.g. α-pinene) (Lambe et al., 2015) and complex
- 99 emissions (e.g. wood combustion) (Bruns et al, 2015). In addition, in both the PAM and chambers, the dominant
- 100 oxidation pathways are similar to those in ambient air (Peng et al, 2015; 2016).

2.2 101 Instrumentation

102 PTR-ToF-MS 2.2.1

- 103 NMOGs having a higher proton affinity than water were quantified by a PTR-ToF-MS (PTR-TOF 8000,
- Ionicon Analytik G.m.b.H., Innsbruck, Austria) (Jordan et al., 2009). NMOG molecules were positively charged 104
- in the ionization unit (drift tube) of the instrument via hydronium ions (H₃O⁺), and the generated ions/fragments 105
- were measured by a time-of-flight mass spectrometer. The PTR-ToF-MS utilized a drift voltage (Udrift) of 550 106 107 V, a drift chamber temperature (Tdrift) of 60°C and a drift pressure (pdrift) of 2.2 mbar, maintaining a reduced
- 108 electric field (E/N) of ~120 Townsends (Td). Data were collected with one second time resolution.

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109 Tofware post-processing software (version 2.4.5, TOFWERK AG, Thun, Switzerland; PTR module as 110

distributed by Ionicon Analytik GmbH, Innsbruck, Austria), running in the Igor Pro 6.3 environment

111 (Wavemetrics Inc., Lake Oswego, OR, USA), was used for data analysis. The ion transmission function,

112 required to convert counts (cps) to volume mixing ratios (ppbv), was quantified using a gas standard containing

113 a mixture of 12 compounds (100 ppbv each) spanning mass-to-charge ratios (m/z) from m/z 33 to 181 (Carbagas

114 AG., Zurich, Switzerland). Volume mixing ratios (ppbv) were calculated according to De Gouw and Warneke,

115 2007, using H₃O⁺/NMOG reaction rate constants (k) from Cappellin et al., 2012, when available, and assuming

116 2x10⁻⁹ cm³ s⁻¹ otherwise.

117 During the exothermic proton-transfer reaction, some molecular fragments are formed in the drift chamber, with

118 the extent of fragmentation depending on the chamber conditions and functional groups in the molecules

119 (Gueneron et al., 2015). In particular, hydrocarbon fragments are obtained from aldehydes and dehydration of

120 some oxygenated ions. Assignment of these fragment ions to the corresponding parent ions is important for

121 quantification. The NMOG mixing ratios were corrected by accounting for this fragmentation. The compounds

122 were measured based on their parent ions, then their fragments were subtracted based on reference

123 fragmentation patterns. These subtractions combine a detailed fragmentation table for aldehydes using the

124 current drift chamber conditions from Klein et al. (2016) and fragmentation patterns for aromatic compounds

125 measured under similar chamber conditions reported (E/N ~120 Td) in other studies (Buhr et al., 2002; Brown et

al., 2010; Gueneron et al., 2015). The fragmentation of detected compounds containing other functional groups

(e.g. hydrocarbons and non-aldehyde oxygenated compounds) cannot be fully excluded but are not expected to

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128 cause significant error since the observed parent molecules were primarily low molecular weight alcohols and

129 acids (e.g. methanol, formic and acetic acid) that are less susceptible to fragmentation (de Gouw and Warneke, 130 2007). The NMOGs were then classified (acids, alcohols, aromatics, non-aromatics hydrocarbons and

131 unclassified hydrocarbon fragments, nitrogen and sulfur containing compounds, other oxygen containing

132 compounds, unidentified peaks) according to Kilic et al. (2017).

2.2.2 AMS

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134 The condensed phase was continuously monitored before and after the PAM using a high resolution time-of-

135 flight aerosol mass spectrometer (AMS) and a scanning mobility particle sizer (SMPS). The reader is referred to

136 DeCarlo et al. (2006) for a more detailed description of the AMS operating principles, calibrations protocols,

and analysis procedures. Briefly, a particle beam sampled through an aerodynamic lens is alternately blocked 137

138 and unblocked, yielding the bulk particle mass spectra (MS mode) of the non-refractory (NR) species, including

organic aerosols (OA), NO₃, SO₄², NH₄⁺, and Cl. The NR particles are flash vaporized by impaction on a 139

heated tungsten surface (heated to $\sim 600^{\circ}$ C) at $\sim 10^{-7}$ Torr. The resulting gases are ionized by electron 140

141 ionization (EI, 70 eV) and the mass-to-charge ratios (m/z) of the fragments are determined by the ToF mass 142 spectrometer. The AMS was operated in the V-mode, with a time resolution of 30 sec. The AMS data were

143 analyzed using the SQUIRREL (version 1.52L) and PIKA (1.11L) analysis software in Igor Pro 6.3

144 (WaveMetrics). Standard relative ionization efficiencies (RIE) were assumed for the organic aerosol and

145 chloride (RIE = 1.4, and 1.3, respectively) and experimentally determined for sulfate and ammonium (RIE =

146 ~1.1 and ~4, respectively). The collection efficiency due to the particle bounce was determined to be ~1 under

147 our conditions for organic rich aerosols by comparing the AMS mass to the SMPS volume (assuming an OA

148 density of 1.4).

149 2.3 Data analysis

150 Emissions from the aircraft turbofan were measured at different thrust levels referred to as "test points"

151 hereinafter. Test point durations were 18 minutes, except for one 60 minute-long run. Test points were

152 systematically interspersed with five minute-long periods to clean the PAM and the transfer lines by flushing the setup with synthetic air. The averaging of the primary emissions started from the third minute of a test point 153

154 when the engine operation was stable. After sampling primary emissions for five to eight minutes while

bypassing the PAM, secondary formation was measured after the PAM during the last five to eight minutes of 155

the test point. This allows SOA to reach a steady state in the PAM. During each test, the PA concentration was 156

157 measured by bypassing the PAM, while the SA concentration was calculated by subtracting PA from the OA

158 measured after aging (after the PAM). Both PA and SA concentrations were determined by AMS.

159 The expected SOA concentration from the sum of all NMOGs detected by the PTR-ToF-MS was also calculated

by multiplying the NMOGs oxidized in the PAM by its corresponding SOA yields, according to Eq. 1:

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161 $\sum_{i=1}^{n} SOA \ modelled = \sum_{i=1}^{n} \Delta NMOG_{i} \times Yield_{i}$ Eq. 1,

- where n is the number of NMOGs quantified and $\Delta NMOG$ is the difference between the primary NMOG
- 163 concentration and the NMOG concentration after aging. The same approach was applied by Bruns et al. (2016)
- and yields used can be found in Table 2. SOA yields available in the literature were used when possible.
- Otherwise, SOA yields of 0.2 were assumed as a lower limit estimate for aromatic and oxy-aromatics for which
- no SOA-yield values were reported (Presto et al., 2010; Tkacik et al., 2012), similar to Bruns et al. (2016). A
- yield of 0.15 was assumed for other NMOGs, including non-aromatic hydrocarbons and carbonyls. As NO is
- completely consumed in the PAM, we have chosen yields from low NO_X conditions for aromatic hydrocarbons (Ng et al., 2007; Chan et al., 2009; Hildebrandt et al., 2009; Nakao et al., 2011). The SOA contribution from
- 170 organic gases lighter than benzene (C_6H_6) was neglected. Predicted NMOG contributions to SOA are provided
- organic gases righter than belizene (C_6H_6) was neglected. Fredicted NMOG continuous in the Results section.
- Emission indices (*EI*, g/kg fuel) were calculated using a mass balance on fuel carbon:

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$$EI = [X] \times \left[\frac{MW_{CO_2}}{MW_{C} \times \Delta CO_2} + \frac{MW_{CO}}{MW_{C} \times \Delta CO} \right] \times C_f$$
 Eq. 1,

- where X denotes the pollutant concentration (μ g/m³) and MW (g/mole) is the molecular weight of the species
- denoted by the subscript. Background-subtracted CO and CO₂ concentrations (μ g/m³) are denoted as Δ CO and
- 176 ΔCO_2 , respectively. C_f is the carbon fraction of the JET-A1 fuel used during the campaign and was measured as
- 177 0.857 based on ASTM D 5291 method (ASTM, 1996).

3 Results and discussion

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179 3.1 SOA formation as a function of OH exposure

- The evolution of the chemical composition of the primary organic gases and NR-PM₁ components with increasing OH exposure is shown in Figure 2 for engine idling operation (thrust 3%). Measurements were
- increasing OH exposure is shown in Figure 2 for engine idling operation (thrust 3%). Measurements were conducted for primary emissions, as well as for OH exposures of 59x10⁶, 88x10⁶, and 113x10⁶ molecules cm⁻³
- h, which correspond to approximately 39, 58, and 75 hours of atmospheric aging under an average tropospheric
- 184 OH concentration of 1.5 x 10⁶ molecules cm⁻³ (Mao et al., 2009). The OH exposure, calculated using d9-
- butanol as a tracer, was varied by varying the light intensity.
- 186 Figure 2a shows the OG composition under these conditions with compounds classified as a function of their
- 187 molecular composition, as described in Kilic et al. (2017). A stepwise increase of the OH exposure reduced the
- NMOG mass detected in the chamber by 35%, 40% and 50%. Except for carboxylic acids, the concentrations of
- 189 all NMOGs decreased during aging, indicating that their loss rate exceed their production from other NMOGs.
- 190 For example, aromatic compounds and carbonyls were oxidized in the PAM by up to 90% and 50%,
- 190 For example, aromatic compounds and carbonlys were oxidized in the LAM by up to 90% and 30%
- respectively, while the acids doubled after 75 hours of daytime-equivalent aging.
- Figure 2b shows a time series of secondary NR-PM₁ composition, as well as the concentrations of two of the most abundant aromatic gases, $C_{10}H_{14}$ and $C_{11}H_{16}$, for the same experiment. Here stable oxidation conditions
- 193 most abundant aromatic gases, $C_{10}H_{14}$ and $C_{11}H_{16}$, for the same experiment. Here stable oxidation conditions 194 were alternated with sampling of primary emissions, with OH exposures indicated in the figure. Secondary
- aerosol, especially SOA, dominated the total NRPM₁. By increasing the OH exposure from 59x10⁶ to 88x10⁶,
- the generated SOA increased by approximately 14%. However, increasing the OH exposure further to 113x10⁶
- molecules cm⁻³ h yielded only an additional 3% increase in SOA mass. This suggests that at these OH
- 198 exposures, the bulk of SOA precursors have reacted and the additional SOA production did not significantly
- exceed its loss. Under these conditions, the formed SOA may be considered as a reasonable estimate for the
- 200 total SOA potential. The observed production rate of SOA against OH exposure is consistent with precursor
- reaction rates of 8×10^{-12} molecule⁻¹ cm³ s⁻¹. This estimate is based on the assumption of a constant SOA mass
- 202 yield with aging and instantaneous equilibrium partitioning of the condensable gases, and is therefore lower than
- the reaction rates of the main identified precursors (see below). SOA production rates are thus expected to be
- faster in the ambient atmosphere.

3.2 Particle and gaseous emissions as a function of engine load

- 206 Figure 3 shows both average primary and secondary emissions indices for varying engine loads (left) and EIs
- 207 from individual test points (right). The NMOG EI decreased from 30 to 0.8 g/kg fuel when the thrust level
- increased from 3-5% to 90%. At thrust 3-5%, the emissions of gaseous aromatic-hydrocarbons were highest
- 209 (with an EI of ~5g/kg fuel) and decreased with increasing thrust (with an EI of ~0.15 g/kg fuel at thrust 90%).
 210 Similar to aromatic gases, SOA were formed mostly at 3-5% thrust and had a declining trend with thrust. In
- 211 contrast, BC, POA and secondary SO₄ EIs were highest during the approximated cruise load (thrust 60%). At

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- 2.12 these conditions, secondary NR-PM₁ was mostly inorganic and SOA mass was comparable to that of primary
- 213 carbonaceous emissions (BC + POA). SOA was approximately 100 times higher than POA at idle and only 10
- 214 times higher at cruise (Figure 3). This dependence of the aged aerosol composition on the thrust level, obtained
- 215 using the PAM reactor, confirm quite readily the previous results obtained in a smog chamber (Miracolo et al.,
- 216 2011; 2012).

217 Precursor gases of SOA: Idling

- 218 Single-ring aromatics, such as xylenes, methylbenzenes, toluene, and benzene, were previously linked with
- 219 SOA formation (e.g. (Odum et al., 1997; Ng et al, 2007)). These aromatic gases are important contributors in the
- 220 emissions from combustion sources such as two-stroke scooters (Platt et al., 2013), or wood burning (Bruns et
- 221 al., 2016). Idling exhaust contained 20% (mass weighted) of aromatic HCs. Figure 4 presents the mass fractions
- 222 of aromatic hydrocarbons in primary exhaust for an idling turbine engine. More than half of the aromatic
- 223 hydrocarbons emitted were single-ring aromatics. 75 - 95% of these aromatics were oxidized with an OH
- 224 exposure of $\sim 90 \times 10^6$ molecules cm⁻³ h in the PAM.
- 225 By using previously reported SOA yields (Table 2) for NMOGs, SOA production was predicted from individual
- 226 precursors according to Eq. 1. Figure 5 shows a comparison of the predicted SOA with the SOA determined by
- 227 AMS measurements (top) and the predicted SOA contribution by the oxidation of NMOGs in the PAM
- 228 (bottom), for two idling thrusts, 2-5% (left) and 6-7% (right). The predicted SOA from the NMOGs reacted are
- 229 shown at the bottom panel of the figure and compound class-specific SOA fractions are separated for aromatic
- 230 HCs, oxygenated-aromatics, other HCs, N-containing OGs and other OGs.
- 231 Results in Figure 5 indicate that the most important SOA precursors emitted by turbine engines at idle are
- 232 aromatic hydrocarbons such as benzene derivatives but also oxygenated aromatics such as phenol. The predicted
- 233 SOA formed by aromatics alone, both by aromatic hydrocarbons (60-70%) and oxygenated-aromatics (15-25%),
- 234 explained all AMS-determined SOA at low loads (thrust 3-5%) and most of the SOA formed (by 80%) at idle 6-
- 235 7% (Figure 5). Predicted aromatic SOA from benzene (C₆H₆), C2-benzenes (C₈H₁₀), C3-benzenes (C₉H₁₂), C4-
- 236 benzenes (C₁₀H₁₄), dimethylstyrenes (C₁₀H₁₂), toluene (C₇H₈), methylbenzaldehydes (C₈H₈O) and phenol
- 237 (C₆H₆O) accounted for 60% of the AMS-determined SOA at 3-5% thrust (Figure 5). These results are consistent
- 238 with those previously obtained using a smog chamber, confirming that aromatic compounds are indeed
- 239 important SOA precursors in jet-engine emissions (Miracolo et al., 2011). Only a small fraction of these
- 240 compounds was determined in previous experiments using GC/MS measurements and therefore traditionally
- 241 considered as SOA precursors in models. Here, compared to previous experiments we show that non-traditional
- aromatic and oxy-aromatic compounds, including naphthalene and its alkyl derivatives, C>3 alkyl derivatives of 242
- 243 single ring aromatics, and phenols, can explain the gap between measured SOA and SOA predicted based on
- 244 traditional precursors.

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- 245 Exhaust-aging experiments were repeated 6 times at thrust 3-5% and the oxidation of NMOGs varied during 246 each of these aging experiments. Error bars shown in Figure 5 denote this variability in NMOG oxidation (in the
- 247 PAM) during aging experiments of the same thrust level. Indeed, errors related to yield values used may
- 248 significantly influence the results. These errors may be systematic and are complex to assess. They can be
- 249 affected by potential differences between the oxidation conditions in chambers and in the PAM (e.g. NOx, RH,
- 250 particle mass). Yields obtained with the PAM are consistent with those obtained from chambers (Bruns et al.,
- 251 2015), therefore we do not expect large systematic errors in the SOA predicted. However, based on the
- 252 variability of yields in previous chamber experiments we estimate the accuracy of our prediction to be within a
- 253 factor of 2, indicating that within our uncertainties a significant fraction of the precursors was identified.
- 254 NMOGs, including aromatic gases, were reduced with increasing thrust (from thrust 3-5% to thrust 6-7%) due
- 255 to more efficient operation of the turbine engine. This decrease amounted to 40% for the sum of aromatic HCs
- 256 and corresponded to a 30% decrease in SOA EI. Therefore, a more efficient engine operation implies less
- 257 NMOG emissions and reduced SOA formation potential at idle.

3.4 SOA formation at an approximated cruise load

- 259 A comparison of the predicted SOA with the SOA determined by the AMS is presented in Figure 6 at cruise
- loads (top panel). Figure 6 also shows the SOA contribution predicted by the oxidation of NMOGs in the PAM 260
- 261 (bottom panel) under the same engine conditions. The SOA EI was 0.07 g/kg fuel for cruise load. The predicted
- 262 SOA fraction accounted for only 30% of the AMS-determined SOA (green bar, Figure 6) during cruise load
- 263 experiments. Aromatic SOA (predicted) accounted for only 4% of the AMS-determined SOA during these
- 264 experiments. The major fraction of the remaining SOA mass that was assigned to the identified precursors was
- 265 predicted to be from oxygenated NMOG molecules (Figure 6). Another 6% of the determined SOA may 266 originate from non-aromatic HCs (aliphatics and HC fragments > C6).
- 267 Predicted SOA was significantly lower compared to the measured SOA. While SOA precursors remain
- 268 unidentified under these conditions, several hypotheses might explain the observation. First, we could not
- 269 determine the contribution of alkanes smaller than 9 carbon atoms to the formed SOA, because these

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compounds are not directly detected by the PTR-ToF-MS. Depending on the number of carbon atoms in their molecular structure, the SOA potential of many alkanes may be comparable to that of single-ring aromatic hydrocarbons (Tkacik et al., 2012) and therefore may play a role in the formation of the observed SOA. However, our data do not suggest that a great part of the observed SOA is from non-measured alkanes, as we do not observe any increase in the contribution of hydrocarbon fragments in the PTR-MS compared to idling emissions. Second, the oxidation of primary semi-volatile compounds may yield significant SOA, because of their elevated yields of near unity (Robinson et al., 2007). However, we note that these semi-volatile precursors would play an important role at low aerosol concentrations, when most of these precursors reside in the gasphase where they can be oxidized. Under our conditions, concentrations range between 10 and 50 μg m⁻³ and a substantial fraction of these products resides already in the particle phase. Therefore the oxidation of these products in the gas-phase by OH is unlikely to explain the observed entire 10-fold increase in the OA mass upon oxidation, but only part of the mass. Finally, the PTR-MS data suggest that a great part of the precursors measured are highly oxygenated gases, with O:C ratios ranging from 0.2 to 0.7, including, among others, anhydrides (e.g. phthalic, succinic and maleic) and quinone derivatives. Unlike aromatic compounds and alkanes present in the fuel, these compounds are likely formed at high temperature during combustion. The SOA yields of these compounds remain unknown and it is likely that the yield value of 0.15 used here is a lower estimate, which would result in an underestimation of the contribution of these compounds to the observed SOA. We also note that unlike precursors detected under idle conditions, the ionization efficiency and the fragmentation pattern of these compounds in the PTR-MS are highly uncertain, resulting in large uncertainties in our predicted SOA. Therefore, results in Figure 6 should be considered with care. Notwithstanding these uncertainties, we note that at cruise conditions the SOA contribution to the total secondary PM is minor compared to sulfate and therefore these uncertainties have little impact on the implications of our results.

4 Conclusions and implications for ambient air quality

Gas-phase primary emissions and SA formation from an in-production turbofan were investigated in a test cell. The engine loads (thrusts) during experiments were selected to simulate different aircraft operations. These operations are summarized as landing take-off (LTO) cycle under four modes taxi/idle, approach, climb and take-off with corresponding engine loads of 3-7%, 30%, 85% and 100%, respectively. In addition an approximated cruising load (60%) was selected.

At idle conditions, SOA formation was mostly attributed to the oxidative processing of aromatic gases. Benzene derivatives together with phenol were predicted as the major SOA precursors for an idling aircraft. Meanwhile, during cruise load the emission of aromatic compounds was much lower and only explained a minor fraction of SOA (4%). During these conditions, however, sulfate was found to dominate SA, contributing ~85% of the total mass of aged aerosols and therefore its fraction is more relevant aloft.

The oxidation of NMOGs in the PAM yielded a SOA EI 100 times greater than POA under idling conditions and 10 times greater at cruise load. According to our calculated production rates SOA from airport emissions (idling jet engines) exceeds POA by a factor of 10 after only 3 hours of atmospheric aging and therefore considerably impacts urban areas downwind of airport emissions. Compared to idling aircraft emissions, aging of vehicle exhaust emissions results in much lower enhancements, ranging between factors of 5-10 and 1.5-3, for gasoline and diesel vehicles, respectively (Gordon et al., 2014a; 2014b).

308 309 The NMOG emission factors and SOA potential can be used in conjunction with emission inventories and fuel 310 use data to assess the impact of aircraft emissions on air quality in comparison with other mobile sources. Here, 311 we have considered the Zurich international airport as an example (Switzerland, 23 million passengers in 2010). 312 Combining the recorded aircraft fuel use with the standard LTO cycle and the NMOG EIs measured, we 313 estimate aircraft NMOG emissions in Zurich for 2010 to be in the range of 90-190 tons/year (Kilic et al., 2017). 314 Based on the average SOA bulk yields (SOA/total NMOG) obtained herein (~5-8%), we estimate a total SOA 315 production potential from airport emissions for the area of Zurich to range from 5.4 to 13.2 tons/year. These 316 SOA production potential values can be directly compared to emissions from on-road vehicles derived from the 317 EDGARv4.2 emission inventory, which provides worldwide temporally and spatially resolved NMOG 318 emissions from road vehicles with a grid size of ~200 km². For the grid cell containing Zurich (47.25° North, 319 8.75° East) the NMOG emissions from on-road vehicles is estimated to be 631 tons/year. While SOA yields 320 from diesel vehicle emissions are expected to be more elevated than those from gasoline car emissions, due to 321 the presence of intermediate volatility species, recent reports suggest these yields to be comparably high, ~15% 322 (Gentner et al., 2017). Using this yield value for emissions from both types of vehicles (Platt et al., 2017), we 323 estimate the total SOA production potential from on road vehicles for the area of Zurich to be ~94 tons/year, 10 324 fold higher than SOA from aircraft emissions. However, the airport is a point source within this region and thus 325 the relative contribution of the airport emissions to a specific location downwind of this source is significantly 326 higher than implied by this calculation. Although this estimate applies to a specific airport, it does indicate that 327 aircraft NMOG emissions may constitute significant SOA precursors downwind of airports, while other fossil 328 fuel combustion sources dominate urban areas in general.

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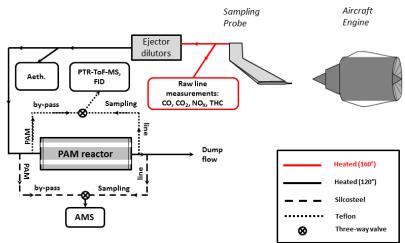


Figure 1: Simplified scheme of the experimental setup.

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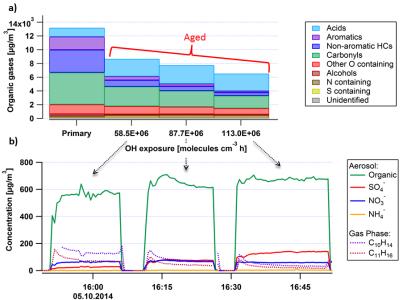


Figure 2: Sample experiment showing mean NMOG emissions (top) and representative time series for particle and NMOG components (bottom) for varying OH exposures. Hydrocarbon concentrations (non-aromatic HCs (dark blue), aromatic HCs (purple) and carbonyls (green) decrease in the PAM while the concentrations of acids (mostly formic and acetic ~90% of the total acids) increase. The bottom panel shows the aerosol (Organic, SO_4 , NO_3 , NH_4) formed and gaseous aromatics ($C_{10}H_{14}$, $C_{11}H_{16}$) for the different OH exposures in the PAM given in the top panel.

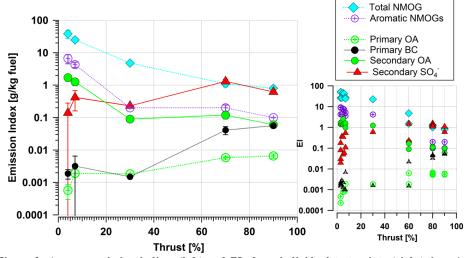


Figure 3: Average emission indices (left) and EIs from individual test points (right) for primary non-methane organic gases (NMOGs), aromatic gases, primary organic aerosol (POA), equivalent black carbon (BC), secondary organic aerosol (SOA), nitrate (NO $_3$) and sulfate (SO $_4$). Error bars (+/-) are the standard deviations of the means with a confidence interval of 95%. The OH exposure was in the range of 91-113 x $_3$ 106 molecule cm $_3$ 1 for the secondary aerosol cases.

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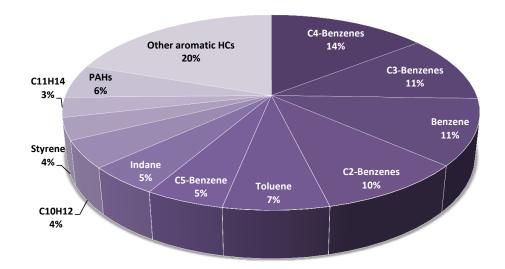


Figure 4: Mass fractions of aromatic compounds for primary emissions (directly emitted) at idle (thrust 3-7%). Benzene derivatives, xylenes, tri-, tetra-, pentamethylbenzene, benzene and toluene account for ~60% of all aromatics.

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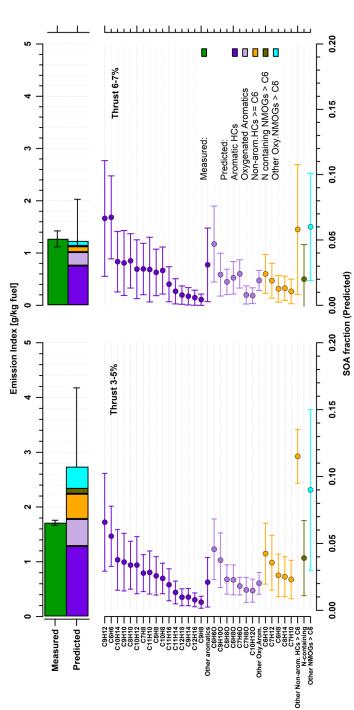


Figure 5: Comparison of the SOA measured by the AMS and the SOA predicted by the oxidation of NMOGs (top panel). The statistics are presented for low load idling (thrust 3-5%) on the left half and for idling 6-7% on the right. Aromatic hydrocarbons (purple) were the most abundant precursors of SOA at idle (thrust 3-7%) explaining all SOA formed (green, top panel) at thrust 3-5% and most (~90%) at thrust 6-7%. Aromatic SOA comprised the largest fraction followed by oxygenated aromatics (light purple - e.g. phenol, benzaldehydes), non-aromatic hydrocarbons (orange) with more than 6 carbon atoms in their molecular structure (non-arom. HCs ≥ C6), nitrogen containing compounds (brown), other oxygenated-NMOGs > C6 (cyan). Average fractions of individual NMOGs (bottom panel) were calculated by using SOA yields from literature (see Table 2) and the amount of NMOG reacted. Error bars show standard deviations of the means (CI: 95%).

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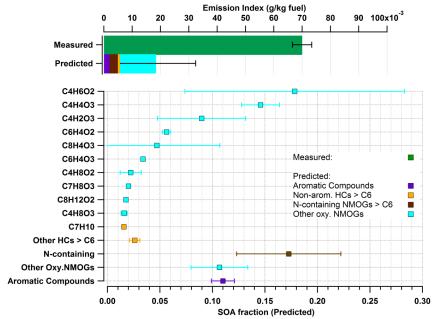


Figure 6: Measured and predicted SOA comparison at an approximated cruise load, using the same approach as in Fig. 5. In contrast to idle conditions, total NMOGs detected do not explain SOA formed.

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Table 1: Volume mixing ratios of gaseous emissions, engine parameters and emission indices (Els) for primary (directly emitted) and secondary (after aging) for all experiments.





SOA (g/kg fuel) 0.1 0.1 0.1 OH exposure (molec. cm⁻³ h) 8.80E+07 6.00E+07 9.00E+07 1.13E+08 1.00E+08 8.80E+07 8.80E+07 1.00E+08 1.00E+08 8.50E+07 8.50E+07 1.00E+08 8.50E+07 8.50E+07 8.80E+07 8.50E+07 SO₄ (g/kg fuel) 0.54 0.11 1.51 1.61 POA (g/kg fuel) 2.34E-04 4.74E-04 <2.0E-03 <2.0E-03 <2.0E-03 <2.0E-03 7.81E-04 8.13E-04 <2.0E-03 1.91E-03 <2.0E-03 6.21E-03 6.80E-03 5.55E-03 6.01E-03 5.24E-03 5.37E-03 5.89E-03 7.30E-03 1.84E-03 BC (g/kg fuel) 2.40E-06 2.00E-06 1.50E-06 2.80E-06 1.00E-06 1.60E-06 2.20E-05 5.00E-05 5.20E-05 1.30E-06 1.00E-06 7.00E-06 1.50E-06 2.30E-06 3.30E-05 4.60E-05 4.40E-05 5.50E-05 Gases (g/kg fuel) 7.1 4.2 0.2 0.2 0.2 0.1 0.2 (g/kg fuel) NMOG 26 26 39 44 42 28 23 515126 2 NO_x (ppmv) 14 114 114 117 117 21 23 62 195 195 131 131 THC (ppmvC) 114 222 222 86 45 94 CO (bbmv) 709 709 543 442 410 168 385 709 422 40 12 12 16 14 CO₂ (bpmv) 1978 3709 1560 1560 1884 1829 1934 1909 4291 4291 4657 4291 Consumption (kg/sec) 0.65 0.11 0.12 0.31 0.65 n/a 0.11 0.9 **Thrust** 8

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Table 2. Precursor OGs, their corresponding functional group and protonated m/z, SOA yield coefficients* from literature, and average SOA EI estimated for different thrusts.

				SOA Emission Index (g/kg fuel)			
VOC formula	m/z	Group	SOA yield*	Thrust 3-5%		Thrust 6-7%	
				Average	±	Average	±
$(C_9H_{12})H^+$	121.101	Aromatic	0.32	0.19	0.11	0.07	0.04
$(C_6H_6)H^+$	79.054	Aromatic	0.33	0.16	0.06	0.07	0.03
$(C_{10}H_{14})H^{+}$	135.117	Aromatic	0.2	0.11	0.07	0.03	0.02
$(C_9H_{10})H^+$	119.086	Aromatic	0.32	0.10	0.06	0.03	0.02
$(C_8H_{10})H^+$	107.086	Aromatic	0.2	0.10	0.05	0.04	0.02
$(C_{10}H_{12})H^{+}$	133.101	Aromatic	0.32	0.10	0.06	0.03	0.02
$(C_7H_8)H^+$	93.070	Aromatic	0.24	0.08	0.04	0.03	0.02
$(C_{11}H_{10})H^{+}$	143.086	Aromatic	0.52	0.08	0.05	0.03	0.02
$(C_8H_8)H^+$	105.070	Aromatic	0.32	0.07	0.04	0.03	0.02
$(C_{10}H_8)H^+$	129.070	Aromatic	0.52	0.07	0.03	0.03	0.02
$(C_{11}H_{16})H^{+}$	149.132	Aromatic	0.2	0.05	0.03	0.02	0.01
$(C_{11}H_{14})H^{+}$	147.117	Aromatic	0.2	0.04	0.02	0.01	0.01
$(C_{12}H_{18})H^{+}$	163.148	Aromatic	0.2	0.03	0.02	0.01	0.01
$(C_9H_{14})H^+$	123.117	Aromatic	0.2	0.03	0.02	0.01	0.01
$(C_{12}H_{16})H^{+}$	161.132	Aromatic	0.2	0.02	0.01	0.01	0.01
$(C_9H_8)H^+$	117.070	Aromatic	0.2	0.02	0.01	0.00	0.00
Other	-	Aromatic	0.2	0.06	0.05	0.00	0.00
$(C_6H_6O)H^+$	95.049	Oxy-arom	0.44	0.13	0.07	0.05	0.03
$(C_6H_8O)H^+$	97.065	Oxy-arom	0.32	0.07	0.03	0.02	0.01
$(C_7H_6O)H^+$	107.049	Oxy-arom	0.32	0.05	0.02	0.02	0.01
$(C_6H_6O_2)H^+$	111.044	Oxy-arom	0.39	0.03	0.01	0.01	0.00
$(C_{10}H_{12}O_2)H^+$	165.091	Oxy-arom	0.2	0.00	0.00	0.00	0.00
$(C_{10}H_{14}O_2)H^+$	167.107	Oxy-arom	0.2	0.00	0.00	0.00	0.00
Other NMOGs	> 79.054	Other NMOG	0.15	1.15	0.74	0.20	0.02

*SOA yields from (Ng et al., 2007; Alvarez et al., 2009; Chan et al., 2009; 2010; Hildebrandt et al., 2009; Shakya and Griffin, 2010; Chhabra et al., 2011; Nakao et al., 2011; Yee et al., 2013)