

Reply to the reviewers

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We thank the reviewers for their careful reading and constructive comments. We think that our implementation of the comments has improved the discussion paper and made it clearer for a wider audience.

Our responses are in italic, and our changes in the manuscript are straight. We have used a brown color for the part of the comments of reviewer 2 that we already incorporated in the original Discussion paper, and a blue response for the recent changes.

1 Reviewer 1

1.1 Decision

For this reason, I would like to suggest major revision including (i) a thorough discussion of the simulation results, (ii) a correction of the correlation estimations, and (iii) a proposition of a model that could be used in field experiments (or some other useful information for future field experiments), in order to improve the impact of the manuscript.

We improved our description of the model and added material to the discussion of the simulation results and correlation analysis.

1.2 Specific comments

1. The LES model: despite being a well-known technique and a largely used model, I think a little more information about the PALM-LES should be given. This is a simulation of free convection, in which no mean streamwise velocity is present. Have this type of simulation been performed with PALMLES before? If so, a citation and a brief summary of models performance should be given. Otherwise, some description of the velocity and temperature fields should be given, including an assessment of the level of reality being represented by the model.

We expanded the section on PALM, its simulation approach, and the boundary conditions and initial settings.

Reworked paragraphs in the manuscript (section 2.1):

For our simulations we have made use of the LES model PALM (Maronga et al 2015). More precisely, we ran our simulations with PALM version 3.9. PALM resolves the turbulence down to the scale of the grid spacing, all turbulence below is parameterized by implicit filtering. The closure model in PALM is a so-called 1.5-order closure scheme, where the equations for the resolved velocities and scalars are derived by implicit filtering over each grid box of the turbulent Navier-Stokes equations, and where an additional prognostic equation for the turbulent kinetic energy is solved. The turbulent kinetic energy in PALM (the sum of the variance of the subgrid-scale velocities) allows to model the energetic content of the subgrid-scale motions, and because it is related to spatial filtering it should not be confused with the typical turbulent kinetic energy in eddy-covariance measurements related to the averaging of a time series. Of course, the latter can be approximated by the resolved kinetic energy in PALM plus the subgrid-scale turbulent kinetic energy. Finally, the Reynolds fluxes that appear in PALM’s filtered equations (the spatial covariances of the subgrid-scale quantities) are parameterized by a flux-gradient approach involving the resolved gradient and a diffusivity coefficient that depends on the before-mentioned turbulent kinetic energy, the grid spacing and the height above the lower surface. However, at the first gridpoint above the surface, Monin-Obukhov similarity theory is applied and therefore the turbulence there is completely parameterized.

Relevant parameters of the simulation setup are summarized in Table 1, the grid spacing is 10 m in all three dimensions and the domain size is 6×6 square kilometers in the horizontal, and 2.4 km in the vertical. The boundary conditions of the simulations are periodic in the lateral dimensions. For the velocity we have Dirichlet conditions at the bottom (i.e. rigid no-slip conditions) with zero vertical and horizontal wind. At the top the horizontal velocity is commonly set to the geostrophic wind and the vertical velocity is zero. However, we have turned the geostrophic wind off (this is a homogeneous horizontal pressure gradient): $(u_g, v_g) = (0, 0)$. Of course, due to the differences in surface heating, local pressure gradients will still develop. For potential temperature and humidity we have Neumann conditions at the lower boundary (given by the surface fluxes) and also at the top boundary (where the flux is given by the lapse rate at initialization). The domain is initialized with constant profiles for the velocity (equal to the geostrophic wind for x and y and zero for the vertical velocity). The initial profiles are homogeneous in x and y and for potential temperature (θ) it reads

$$\theta(z) = 300 \text{ K} - 0.01 \text{ K/m} \times (z - 1 \text{ km}) \times H(z - 1 \text{ km}) \quad (1)$$

with $H(\cdot)$ the Heaviside function. The top of the domain is situated within a stable inversion layer, which prevents that the turbulence within the boundary-layer is influenced by the vertical domain size. In the lateral dimensions the domain is about 3 to 5 times the boundary-layer depth. For the vertical velocity we have added an a very small subsidence term (leading to a vertical pressure gradient in the equations) for heights above 1 km to counteract the destabilizing influence of the surface heat flux, with the subsidence velocity $w_s = -0.00003 \text{ s}^{-1} \times (z - 1 \text{ km})$ for all simula-

tions. The data are extracted for four hours after two hours of spin-up time. The data are extracted for four hours after two hours of spin-up time. For each hour a data point is collected by averaging over virtual measurements sampled at every second. As our focus lies on the influence of the surface characteristics, we concentrate in the present study on the wind circulations purely generated by the surface heat flux, without complicating the analysis with additional synoptic drivers such as a geostrophic wind.

2. The simulations: all the information needed to reproduce the simulations exactly should be given. For example, the exact values of initial and boundary conditions of all variables, the strength of the inversion and the subsidence, etc. I'm still confused about how many simulations were run. I'm assuming it was two, one for the kilometer and another for the hectometer case. If so, the information in Tables 2 and 3 are confusing. Does the word cases mean patches? What are the ranges in ABL height and Obukhov length, are they in time or space? Are these ranges reasonable?

We added the information about the initial and boundary conditions (see above). We clarified the distinction between patch and case in the methods section. In brief, the word "cases" means the different simulations within one suite with varying parameters. The word patches means the different surface types, the number of patches depends on the surface length scales of the particular simulation, which depends on the case. The total number of simulations was 288, one suite of 144 simulations for the kilometer scale heterogeneities and another suite of 144 simulations for the hectometer scale heterogeneities. We have stated this more clearly within the text. The ranges indicate the spread between these 144 simulations, as such neither in time or physical space, but a spread in the "parameter space" of the suite. The ranges are reasonable for free convection.

Excerpts from methods section:

In Fig. 1 we plot an example of a synthetic surface heat flux as in (1) creating eight patches on the surface with four different values for the surface sensible heat flux. The number of patches depends on the length scale of the heterogeneity.

The main aim of this parameter study is to find out the response of virtual towers when the surface parameters are varied, and for this reason we create a suite of simulations where each simulated case has another combination of the surface parameters.

3. p. 6, l. 2122: the Gauß-Ostrogradski theorem has been used to reformulate a divergence within the control volume as a surface term, please be explicit on what was done.

We added it as a footnote explaining this standard theorem in vector analysis and differential geometry. Further information can be found in e.g. Methods of Theoretical Physics by Morse and Feschbach. For more information upon the mathematical terminology, see e.g. Rudin's Principles of Mathematical Analysis.

In the manuscript:

Where possible, the Gauß -Ostrogradski theorem [1] has been used to reformulate a divergence within the control volume as a surface term. Due to the choice of a cuboid aligned with the coordinate system for the control volume, the control volume energy balance (4) simplifies further because only the velocity components perpendicular to the faces remain.

[1] The Gauß -Ostrogradski theorem or “divergence theorem” is a special case of the Stokes-Cartan theorem in differential geometry. For our purposes, we also restrict ourselves to three-dimensional space. We consider a compact volume V with a piecewise smooth boundary S . If \mathbf{F} is a continuously differentiable vector field defined on a neighborhood of V , then:

$$\int_V (\nabla \cdot \mathbf{F}) \, dV = \oint_S \mathbf{F} \cdot d\mathbf{S}. \quad (2)$$

The left side is a volume integral of the divergence of the vector field \mathbf{F} over the volume V , with dV the volume element, and the right side is the surface integral over the boundary of the volume V . $d\mathbf{S}$ is the outward pointing unit normal field of the boundary $S = \partial V$ multiplied by the surface element. For our purposes we take $\mathbf{F} = \mathbf{v} \theta$ and V is the control volume described in the text.

4. The PCA analysis: in the Methods section, a brief description of the PCA method and how to interpret its results should be given. Right now this is completely left to references, but I think I should be able to understand the technique and the plot overall without having to look in another paper. Also, a more exact description of what was done should be given, including how many and which variables were used, which equation or software, etc.

We expanded the paragraph on the PCA method and its interpretation.

In manuscript:

For investigating the response of the virtual tower measurements to the changes in the parameters, and for investigating the correlation between the measured variables, a principle component analysis (PCA) is applied. PCA relies on the singular value decomposition (SVD) of the data matrix, which consists of the data points for each of the data variables. Through SVD, the data matrix decomposes into the matrix of the left eigenvectors, a diagonal matrix with the singular values and a matrix with the right eigenvectors. The singular values are ordered by their magnitude, because the square of each singular value is the variance of the data explained by its corresponding eigenvectors. Hence the first eigenvectors with the largest singular values represent the principal components that explain the largest fractions of the data variability. We will present many of our results in correlation biplots introduced by Gabriel (1971, 1978). Correlation biplots offer a picture of the relationship between the interdependent variables that make up the data matrix through the PCA method. First of all,

for a correlation biplot, each variable is centered around its mean and normalized by its standard deviation. On the normalized data matrix PCA is applied. The data variables are projected into the subspace spanned by the first principal components and then the vectors of the projection within this subspace are plotted in a 2D (or a 3D) biplot, when the two (or three) largest principal components are chosen. In a correlation biplot, the inner product between the variable vectors (hence, the product of their length and the cosine of the angle) directly measures their correlation. The scree plots related to the biplots express how much variance is captured by the principal components by plotting the (relative) variance explained by the principal components. The variance explained is a measure for the goodness of the fit. The better the variable can be explained by the first two principal components, the longer the length of the vector of the variable in a two-dimensional correlation biplot, which is at most unity, indicated by the unit circle. For a pedagogical description of biplots see e.g. Greenacre (2010).

For producing the biplots we have made use of Python3, combining our own routines with standard packages. The correlation matrix contains exactly the same variables that are plotted in the biplot.

5. Simulation results: the simulation results should be presented and discussed before presenting the statistics. For example, how do the spatial fields of temperature and heat flux look like, and where do the towers rest in this field? Some time series at the tower place, to see what the towers are measuring and what are the scales of motion in it. How do they compare with the scales of heterogeneity? How much of the fluxes are resolved compared to the sub-grid scale? How realistic are these simulations? A thorough discussion of the simulation is definitely needed, as it would help to discuss the physics of the results presented later.

To the discussion we added an analysis of the simulation results: where the updrafts are concentrated, the dependence of the friction velocity on the heterogeneity amplitude, and a comparison with the homogeneous reference case. Our 10 m grid spacing is more than sufficient to capture the turbulence responsible for the motions in the boundary-layer (the heterogeneity is large compared to the grid spacing) and therefore our simulations are realistic. Of course the measurement height is higher than would be ideal and the control volume method is an approximation to the tower measurements, but these are approximations out of computational grounds. To speak of LES in the first place most of the flux has to be resolved at the subgrid-scale flux is only important at the lowest grid points, which is why we evaluate the energy balance closure at the fifth grid point (50 m).

Added in discussion: 3.1 Circulation patterns in heterogeneous terrain

6. Discussion: there are three distinct physical phenomenon that could be impacting the residual: transport of the mean field, transport of the fluctuating field, and storage. What are the physics involved in each process, how is the simulation capturing them,

and how do they look like in the simulation? Is it realistic to look into the advection effect, for example, in a simulation that has no mean streamwise advection? What happened to the vertical and horizontal dispersive fluxes?

The simulation captures all turbulent processes on scales larger than the gridsize and smaller than the boundary layer depth (when the horizontal extent is sufficiently large). Transport of the mean field is well captured, transport of the fluctuating field is captured up to the grid cutoff scale (in our simulations this would roughly correspond to resolution of the turbulent fields up to 1 Hz). The storage fluctuations are captured up to the tiny changes faster than 1 Hz but its average behaviour is well captured. Due to the boundary conditions (and the smaller eddy sizes there) at the lower surface in the first grid points the turbulence is not completely resolved. This is exactly the reason why we study the energy balance closure at the fifth grid point.

Even though the simulation has no mean streamwise advection, there is still locally advection. This is realistic, because in reality near thermal updrafts there is convergence near the lower surface and hence also net advection due to continuity of the air fluid (at least within the window that the thermal resides at that location, but Kanda et al (2004) showed that this leads to net effects for half hour windows). For our heterogeneous simulation the thermals are preferentially attached to the hotter patches, leading to advection effects on longer timescales. There is no contradiction here, neither does it make the simulation unrealistic. The vertical dispersive flux is the turbulent flux at the measurement height. The horizontal dispersive fluxes is taken into account by considering the flux-divergence.

In short, locally there is still advection even in free convection, as the convection cells create their own circulation. We focus on free convection for two reasons: one it disentangles the “purely heterogeneous” effect from the meteorology, second, in the literature it is found that meteorological conditions towards pure convection lead to stronger imbalances.

7. p. 7, l. 19: what is the available energy? It is the reference value in the results section, but there is no definition of it. It is only explained in the Fig. 2 caption, but it should be clear in the text too.

We have added it to the main text.

Changes in manuscript: for our model setup the available energy is equal to the surface flux

8. p. 7, l. 19: please make it clear if the advection term includes both horizontal and vertical advection.

It does. We added this explicitly in the text.

In manuscript: this means that our advection term is the sum of the horizontal and vertical advection by the mean flow

9. p. 7, l. 2931: We notice that most towers show the typical underestimation of the energy balance, except for the tower located at the warmest spot where there is an updraft. How do you know it is an updraft? Is it always an updraft? On average? It is mentioned in the abstract that updraft and downdraft positions were chosen for the towers, but this is not showed or discussed in the paper. Do constant regions of updraft/downdraft exist in the simulation or in reality?

With “updraft” we do not necessarily mean the central region of a thermal, but more generally the existence of $\bar{w} > 0$. In real complex terrain there are certainly areas that have preferential updrafts, e.g. above a mountain range during summer days next to the relatively flat foothills (this phenomenon is called “Alpine pumping”) or on a smaller scale, in mixed terrain consisting of darker forests and cooler lakes paragliders can make use of the updrafts above the forests in summer (pers. comm.). Therefore we are not surprized to see preferential updrafts above the hotter patches.

Added in the introduction: Persistent updrafts and downdrafts tied to the landscape heterogeneity have been found e.g. by Mauder et al (2008) during the 2008 Ottawa field campaign.

We added a spatial analysis of the updrafts in the results section 3.1

10. p. 7, l. 3031: please explain better physically the causes of a negative/positive residual, and why there is a negative residual where there is an updraft.

The negative residual (turbulent flux larger than the surface flux) appears because there is a net advection of sensible heat from the downdraft region towards the updraft region. A complete physical understanding of the coupling between the residual and the wind field is beyond our present capacities and this paper is one step to understanding the linking. We can however give a few arguments, which we added to the discussion.

We present some arguments why the regions with updrafts have better closure. Banerjee et al (2017) investigated the dependence of the aerodynamic resistance on the atmospheric stability for homogeneous terrain. As a consequence a surface with a higher surface heat flux is more efficient in transporting away this surface flux. Therefore, one hypothesis is that when a patch with higher surface flux is coupled to a patch with lower surface flux in heterogeneous terrain, the patch with the higher surface flux transports part of the surface flux of the patch with the lower surface flux, due to its higher efficiency, leading to a net advection of sensible heat from the downdraft region to the updraft region. Another hypothesis is that the shape of the cellular convection cells matters: the updrafts cover a smaller area than the downdrafts. Therefore, as the turbulence structures move across the towers, above a region with preferential updrafts, the likelihood of sampling both the updrafts and downdrafts is higher than above a region with preferential downdrafts.

11. p. 8, l. 1314: In the left panel of Fig. 4 we note that the normalized flux-divergence correlates rather well to the normalized turbulent flux, when we look at their average behavior at each tower. What does normalized mean? If it is the normalized by the

available energy at their respective location mentioned in the caption of Fig. 2, it should be mentioned in the text too.

This was only mentioned for Fig. 2 at the beginning of the section. We now repeat this in the paragraphs for Fig. 3.

In the manuscript: Let us however take a closer look in Fig. 3, where the flux-divergence and advection by the mean flow, resp. are plotted against the energy balance ratio. As in Fig. 2 flux-divergence and advection are normalized by the available energy (i.e. the surface flux in our settings).

12. p. 8, l. 2223: flux-divergence and advection separately correlate well with energy balance ratio and consequently also with each other. What does that mean physically? Does it makes sense that these two processes are correlated in the simulation? What is the implication of this for the imbalance observed in the real case?

It means, e.g. for the kilometer scale, that a larger advection (due to higher mean temperature or higher wind speed) is coupled to less correlation between the temperature and the velocity fluctuations. The precise mechanisms of this phenomenon are still unclear. We are confident that when the simulation shows such correlation, this should be there in reality too. For turbulence of scales larger than 10 m (the grid spacing) our LES is a good model for turbulence of the same order in reality. One of the implications would be that the EBR can be explained by the advection or flux-divergence only, because the latter two are also well correlated.

Added in the conclusions: Remarkably, flux-divergence and advection by the mean flow correlate separately very well with the energy balance ratio, which implies that the EBR can be explained by the advection or flux-divergence only, as the latter two are well correlated among themselves.

13. p. 8, l. 2426: “Finally, we want to remark that, due to computational constraints, the virtual measurement height in our simulations lies at 50 meters, which is an order of magnitude larger than the typical tower height over short vegetation with comparable surface roughness. This means that our findings for virtual EC towers cannot be directly transferred to real eddy-covariance towers.” Why not compare the residual observed in the simulation as a function of height, including the lower points? If I understood correctly, the residual term is estimated at a given height, so it does not need the control volume approach. If so, you can see if the results at 50m are similar at 10 m, and if the conclusions could be extrapolated. Without this extrapolation, I see little usefulness in the conclusions obtained here.

We need the control volume in order to be able to estimate advection and flux-divergence more accurately. We need a minimal number of grid points in the vertical because at the lowest grid level, the turbulence is parameterized by MOST. Extrapolation of the residual from 10 m height would only make sense if we resolve the simulation with $O(1\text{ m})$ resolution, and then we could study the height dependence. We’ve already done a separate study on the variation with height of the energy balance

closure for smaller grid sizes in homogeneous terrain, but these simulations were too computationally expensive to set up for the two suites of 288 simulations in total, especially because the presence of the heterogeneity calls for a larger domain in the horizontal. Finally, the residual is calculated as the difference between turbulent flux at the top and the surface flux (we're actually considering a local area average). On its own it does not need the control volume method but we need the control volume method to quantify advection and flux-divergence. However, the problem remains that the turbulence in the first grid points is not completely resolved, but this is a general issue of LES due to the lower boundary condition.

In the conclusions: By means of a control volume approach, we decomposed the modeled surface energy budget to highlight its partitioning, and we have shown that the modeled energy balance ratio exhibits values that are found in field experiments. In addition, this approach allows us to investigate the energy balance closure in two-dimensional complex terrain.

14. p. 8, l. 3233: “the towers in the center of the patches even behave in the opposite manner when the kilometer and hectometer scales are compared”. This needs to be better investigated and discussed physically. What can be causing this?

We refer to comment 16.

15. Discussion: I think it is important to discuss the differences when there is a small residual due to low values of all other fluxes, or due to their canceling effect. What is likely to be happening in field experiments?

For field experiments in general we expect that this will be something site-specific. We do notice here and also in Eder et al 2015 that the flux-divergence and the advection act oppositely, but for different sites with different type of heterogeneity or different synoptic or radiative conditions the residual could also be present because all fluxes are small. There is a multitude of factors that play a role and this paper only focuses on strongly convective conditions to free convection for chessboard shaped heterogeneity of 2 times kilometer scale and 2 times hectometer scale, which already required 288 simulations.

16. p. 9, l. 4–7: “The likely cause for the different behavior between the two scales of heterogeneity would be the blending of the hectometer landscape heterogeneity due to the virtual tower heights of 50 meter. For the surface heterogeneity of $O(10^2 \text{ m})$ the flux footprint of each of the towers can cover several of the surface patches, regardless of the type of tower.” I agree this is likely the cause of difference, but how does this make the relation between flux-divergence and EBR opposite, or the relation between the residual and the surface flux opposite?

One way to investigate this would be to simulate additional length scales interpolating between our current heterogeneity lengths and investigate at what point the behaviour switches. However, our periodic boundary condition in the horizontal places strong

constraints on the possible heterogeneity lengths (the heterogeneity length has to be a divisor of the domain size). Furthermore, it would have added a significant number of additional simulations.

17. PCA results: from the very little I know about PCA analysis, I think the results obtained here are not useful. I believe it is useful to look at correlation biplots when most of the variance are explained by the first two PCs (something around 90%), not the 60% found here. As explained by Greenacre (2010) (your own reference on the topic), PCA correlation biplots are useful when there is a clear separation in the scree plot between the first two PCs and the rest (called elbow), which is definitely not the case here. In your data, the third PC is almost as important as the second, and it is not taken into account. In addition, the EBR (the variable you want to explain) is the one with less representation by the first two PCs among the variables in the correlation biplot, being much less than 50% representation in the hectometer case. I dont know which analysis should be done instead, but I think PCA is not the one.

Yes, we know that biplots are more useful when the variance explained of the first two PC's is higher than 60% and the elbow is more pronounced. We do not claim otherwise in the text, but we made it clearer now. Nevertheless, even when the variance explained is lower than 60%, we can still make a biplot. The PCA is always done with all the principal components, the biplot is just the figure of the first two PC's. We chose for the correlation biplot precisely because the unit circle gives guidance as to how well the variance is captured by the first two components. The arrows which are close to the unit circle in the correlation biplot are still well explained by the first principal components. The residual variance from the latter PC's then explains the short arrows in the biplot. Alternatively, we could yield tables with the correlation coefficients, which is the same information as in the biplot, just not visual. The variance explained concerns all the variables, but we are mainly interested in the EBR. Anyway, we also think it's still meaningful to show that we do not see enough correlation from a linear analysis. We also think it is more instructive to give a graphical representation of the correlations. The PCA is only a linear analysis and therefore a higher order scheme might help, but it would introduce a lot of dimensional coefficients and it is sometimes said that "with a fifth order spline one can fit an elephant". We think it is necessary to a come to a deeper physical understanding in order to be able to fit a higher-dimensional model with a minimal number of parameters that could be used in field-experiments.

Added in the results: Despite the variance explained of around 60%, plotting the correlation biplot is still possible, it remains a graphical representation of the correlation between the variable vectors, even though it shows that the variance in those variables cannot be simply explained by the first two principal components. Furthermore, the linear correlation analysis in the biplots is still useful in a few other respects: for one, it shows that EBR does not linearly depend on easily measured

characteristics.

18. Conclusions: ignoring the results from the PCA, the only conclusion from this work is that this type of heterogeneity in the surface flux generates a difference between the turbulent flux measured at 50m and the surface flux itself. This is an interesting information, but given the potential of these simulations, I believe that much more can be obtained. I would like to see some results and conclusions that could help improve or understand the closure problem in field experiments. The idea of finding parameters measurable in the field that correlate well with the residual is a good approach. But another technique should be used to find the right parameters. After finding them, I suggest that a model for the residual should be developed and tested against the LES results. Naturally, in reality things are not equal to the LES, but this would give us a place to start. When combined with a thorough discussion of the simulation itself, it would be easier to extrapolate the results and conclusions to the real case. Without it, I don't see any significant contribution to the field.

In addition to a more extensive physical discussion of the simulation output (see below for additions) To find the right parameters that can be used in a model will require additional physical analysis because linear correlation analysis a la PCA has not provided us with clear insights. There is a simple model by Huang et al (2008) but it focuses on the mixed layer and its applicability near the surface is limited (its fit is based on the mixed layer and some of the fitting functions are undefined near the surface). We think that our paper with its investigation of the energy balance closure problem at a coarser resolution has its merits, by decomposing the imbalance as found by the LES simulations in a way that allows us to quantify the individual components, by showing it is in the right order of magnitude of field experiments (though the setting is simplified but we vary the parameter space that determines the surface heterogeneity) and from the simplified setting trying to find the parameters influencing the EBC over a range of the parameter space. With respect to "given the potential of the simulations", we think that we got most of the potential out of it, at least with respect to the goal of the paper. The high correlation between advection, flux divergence and the energy balance residual is also an important conclusion.

Added in PCA discussion: In addition, friction velocity and boundary-layer depth cluster together separately, as do the normalized flux-divergence and advection. Although we might have supposed that higher boundary-layer heights will arise if patches are present with vigorous surface heating, however we found that u^* decreased with stronger surface heterogeneity. Closer analysis reveals that the highest boundary layer heights are obtained when the heterogeneity amplitudes are smaller and the domain is more homogeneous. Hence the former clustering can be explained because in our scenario with varying heterogeneity amplitudes the highest boundary-layer height and larger u^* are both obtained for smaller heterogeneity amplitudes.

Added in PCA discussion: In the literature (e.g. Stoy et al 2013, Eder et al 2015a) a correlation between friction velocity and energy balance closure has been found: a

high friction velocity leads to a smaller residual. Typically, a higher friction velocity is correlated to smaller atmospheric instability, and hence roll-like convection instead of cellular convection. Maronga and Raasch (2013) found that boundary-layer rolls “smear out” the surface heterogeneity, leading to an effective surface that looks less heterogeneous, which has been related to a higher EBR (Mauder et al 2007, Stoy et al 2013). Therefore a possible cause for the present low correlation of u^* with the EBR, could be our range of the stability parameter. For the free convective cases considered here the stability parameter lies below the range where the friction velocity has a high correlation with EBR.

Added in conclusions: By means of a control volume approach, we have decomposed the modeled surface energy budget to highlight its partitioning, and we have shown that the modeled energy 20 balance ratio exhibits values that are found in field experiments. In addition, this approach allows us to investigate the energy balance closure in two-dimensional complex terrain.

1.3 Technical corrections

- Abstract: there is too much introduction information in this abstract. It is also clear from it that there is no significant contribution from this work. After improving the results and conclusion, the abstract should focus more on them.

We suppressed the introductory information in the abstract and focused on the conclusions of the article.

New abstract:The imbalance of the surface energy budget in eddy-covariance measurements is still an unsolved problem. A possible cause is the presence of land surface heterogeneity, which affects the boundary-layer turbulence. To investigate the impact of surface variables on the partitioning of the energy budget of flux measurements in the surface layer under convective conditions, we set up a systematic parameter study by means of large-eddy simulation. For the study we use a virtual control volume approach, which allows the determination of advection by the mean flow, flux-divergence and storage terms of the energy budget at the virtual measurement site, in addition to the standard turbulent flux. We focus on the heterogeneity of the surface fluxes and keep the topography flat. The surface fluxes vary locally in intensity and these patches have different length scales. Intensity and length scales can vary for the two horizontal dimensions but follow an idealized chessboard pattern. Our main focus lies on surface heterogeneity of the kilometer scale, and one order of magnitude smaller. For these two length scales, we investigate the average response of the fluxes at a number of virtual towers, when varying the heterogeneity length within the length scale and when varying the contrast between the different patches. For each simulation, virtual measurement towers were positioned at functionally different positions (e.g. downdraft region, updraft region, at border between domains, etc.). As the storage term is always small, the non-closure is given by the sum of the advection by the mean flow and the flux-divergence. Remarkably, the

missing flux can be described by either the advection by the mean flow or the flux-divergence separately, because the latter two have a high correlation with each other. For kilometer scale heterogeneity, we notice a clear dependence of the updrafts and downdrafts on the surface heterogeneity, and likewise, we also see a dependence of the energy partitioning on the tower location. For the hectometer scale we do not notice such a clear dependence. Finally, we seek correlators for the energy balance ratio and the energy residual in the simulations. Besides the expected correlation with measurable atmospheric quantities such as the friction velocity, boundary-layer depth and temperature and moisture gradients, we have also found an unexpected correlation with the temperature difference between sonic temperature and surface temperature. The correlation with the friction velocity is less pronounced than previously found, but this is likely due to our concentration on effectively strongly to freely convective conditions.

- p. 4, l. 17: “we have added a very small moisture flux” why? why not make it zero?
We did not choose to run dry simulations, as it is sometimes viewed as less realistic. Of course, a simulation with a very small moisture flux approximates the results of a dry simulation. In any case, we wanted to concentrate on the partitioning of the sensible heat flux before adding a significant latent heat flux.
- Figure 1: missing unit of color plot (surface heat flux)
It's in Kms^{-1} (added)
- Equation (3): a sketch of the fluxes and a figure showing where in the 50 by 50m box each term is being calculated would be useful.
To avoid copyright issues we prefer to refer to Eder et al (2015).
- p. 7, l. 30: include text: “most towers show the typical underestimation of the energy balance (i.e., positive energy balance residual)”
Done
- p. 8, l. 12: what is “resp.”?
Respectively.
- p. 8, l. 12, 13: it should be Fig. 3 instead of Fig. 4
Thanks, corrected.
- p. 8, l. 20: opposite slope? They look the same to me...
Yes, but the text is really correct because we have unfortunately made an error while editing the figures for the approved submission. On demand of reviewer 2 in the quick submission we had removed some plots, and in this action we accidentally plotted figure 5 on the location of figure 3 as well (with two times the caption of figure three, to make matters worse). We updated with the correct figure, where the slope

is opposite. In the original submission for the quick review we had the correct plot. The latest figure also has the different markers for each tower type, compared to the plots in the quick review submission.

- p. 8, l. 31: since you are comparing Fig. 2 with Fig. 4, why not make them one single plot? It makes it easier to compare.

It might be easier to compare, but we think that the details come out better in two separate plots.

- Fig. 3 and Fig. 5 are equal, one of them is wrong (I guess it is Fig. 3, based on the text)

Indeed, see above. In the quick review submission we had the correct figure, which we repeat for this revised submission (with individual tower markers).

- p. 9, l. 2: Fig. 4 should be Fig. 3

Thanks, corrected.

2 Reviewer 2

2.1 Major comments

1. Energy balance (Eq. 3)

First of all, we made a typo when typing the storage term (not in our data processing) but other than that the main misunderstanding seems to come from our application of the divergence theorem. Applying Gauss-Ostrogradski (or Stokes-Cartan if need be) is a common procedure in a mathematical treatment of fluid dynamics and is textbook material, see e.g. “Fundamentals of Momentum, Heat and Mass Transfer” by Welty et al.

I am struggling with this equation due to several reasons. First, the dimensions do not fit. A flux should be given in K m/s . The storage term, however, is the integral of d/dt over all three dimensions in space so that the resulting dimension is $\text{K / s} * \text{m}^3 = \text{K m/s} * \text{m}^2$, which is NOT a flux. The equation thus can't be correct (this applies to the original equation in Eder et al. 2015 as well).

Thanks for catching our typo in the equation, the dimensions of course work out as they should. We added the normalization factor for the volume averaging (so the integral turns into an average). The volume integral is normalized by the surface area, which is the same as taking the average line integral over z , the way it is presented now. We already corrected this in the discussion paper.

Second, the authors refer to the second right hand side term as the flux divergence. That is not correct. The divergence involves the derivation in space, but here only a sum (difference) is calculated. Using the divergence, the equation would start to

make sense, as the dimension of a flux divergence is K/s, which fits to a storage term (d/dt).

That term is the average flux-divergence over the volume, it's just reformulated into a difference. The flux divergence at a point indeed has a spatial derivative, but after integration over the control volume (and normalization) the derivative can be removed.

Third, to me it would make more sense to put storage on the left hand side and the rest on the right hand side.

Whether it's a plus sign on the right or a minus sign on the left it's a matter of taste. The surface flux is our constraint, we put all other terms on the right where they retain a plus sign.

Fourth, why is the storage term integrated over a volume? Which volume? Shouldn't ALL terms be integrated over the entire control volumes? Is it really an integral or an averaging?

Which volume: "the" volume of the control volume. All terms are integrated over the entire control volume, but the storage term is the only term that cannot be (analytically) reformulated into a surface term because it has no (spatial) divergence in front.

Moreover, you name the $\langle w \rangle \langle \theta \rangle$ terms "vertical advection" and so on. But a turbulent flux is also advective, so this is not correct language. You mean the advection by the mean flow, which the flux divergence represents the advection by the turbulent flow?!

We replaced the shorthand "advection" by "advection by the main flow". Flux-divergence is a standard term so we keep it.

Lastly, The summation over the lateral fluxes seems to work, but I expect the same summation over the vertical fluxes, i.e., $\overline{w'\theta'} + H$, but even in the equation it seems to be a difference and not a sum ($\overline{w'\theta'} - H$ if you put all terms on one side). In Summary, the equation is very difficult to understand, and reading the Eder et al. paper does not really contribute to the understanding.

It has to be a difference in order to close the energy balance over the control volume. The convention is that a positive H is directed upward. Imagine that there were no advection and no storage, then the turbulent flux should equal the surface flux. Hence $\overline{w'\theta'} - H = 0$.

Finally, I am also not sure that you can apply your averaging procedure for such a large control volume. Temperature, e.g. has a logarithmic profile near the surface, so you must be careful when integrating the storage term over all control volumes.

While it is in principle true that we have to be careful when integrating a logarithmic profile by adding the interpolated values, in our convective simulations the log profile is only in the first gridpoint (by applying MOST) and due to the smallness

of the roughness length compared to the half-height of the gridsize the argument of the logarithm is very large, where the behaviour of the log can be well approximated by a linear function, leading to a good approximation of the integral by the sum of the gridpoint values. Therefore the error is quite small. Anyway, the storage term is small on its own, so this is only a small correction on a small term.

In the manuscript:

Where possible, the Gauß-Ostrogradski theorem [1] has been used to reformulate a divergence within the control volume as a surface term. Due to the choice of a cuboid aligned with the coordinate system for the control volume, the control volume energy balance (4) simplifies further because only the velocity components perpendicular to the faces remain.

[1] The Gauß– Ostrogradski theorem or “divergence theorem” is a special case of the Stokes-Cartan theorem in differential geometry. For our purposes, we also restrict ourselves to three-dimensional space. We consider a compact volume V with a piecewise smooth boundary S . If \mathbf{F} is a continuously differentiable vector field defined on a neighborhood of V , then:

$$\int_V (\nabla \cdot \mathbf{F}) \, dV = \oint_S \mathbf{F} \cdot d\mathbf{S}. \quad (3)$$

The left side is a volume integral of the divergence of the vector field \mathbf{F} over the volume V , with dV the volume element, and the right side is the surface integral over the boundary of the volume V . $d\mathbf{S}$ is the outward pointing unit normal field of the boundary $S = \partial V$ multiplied by the surface element. For our purposes we take $\mathbf{F} = \mathbf{v} \theta$ and V is the control volume described in the text.

2. Homogeneous control run From Fig. 2 it becomes obvious that the EC flux cannot make up for the available energy. I think that is the main point of the paper. It is shown nicely, that advection (of the mean flow) plays an important role, and also flux divergence. You relate this to the heterogeneous surface, but you do not prove it. What you need to do is to add results from control runs with a homogeneous surface. What do you expect to happen? At least advection should go to zero, because all velocity components should go to zero when sufficiently averaged.

We do have homogeneous control runs, more precisely the cases when the amplitude of the surface flux is zero ($A_x = A_y = 0$): then the terrain is homogeneous because in our setup the heterogeneity can only appear in the spatial variation of the surface flux. We would like to stress that also in homogeneous terrain the energy balance is not necessarily closed, see e.g. Kanda et al (2004), because turbulence structures can exist for longer than e.g. half an hour. We agree that when “sufficient averaging” is applied in homogeneous terrain (assuming stationarity of the turbulence) the EBR should be one.

In manuscript: 3.1 Circulation patterns in heterogeneous terrain

3. Measurement height I do understand why you did your virtual measurements at an elevated height because of a relatively coarse grid spacing and you need 5 grid volumens. However, I could not find the grid spacing in the text, so I had to infer it from the table. The main point, however, is and you state that yourself that EC measurements are performed much closer to the surface (2 m) so that it is completely unknown whether your results are transferable to 2 m height. Maronga and Raasch (2003) showed, e.g., that the effect of secondary circulations (heterogeneity effect) tends to zero close to the surface and is most pronounced at upper levels. To me it remains unclear what the benefit of your study is to the research community.

We added the grid spacing and the other important dials of Table 1 in the main text (see also the first comment of reviewer 1).

In the methods: Relevant parameters of the simulation setup are summarized in Table 1, the grid spacing is 10 m in all three dimensions and the domain size is 6×6 square kilometers in the horizontal, and 2.4 km in the vertical. The boundary conditions of the simulations are periodic in the lateral dimensions.

While we strive towards simulating real EC measurements performed at 2 m height (which is extremely costly computationally because it requires less than 0.5 m resolution, without suitable model manipulations that we are working on) these simulations are a first step towards that goal, at the time we used the computing time available to us to produce the 288 runs. This article provides a method that can be repeated for higher grid resolution. Though the domain averaged energy balance of Maronga and Raasch (2013) tends to zero close to the surface, we do not think it means that it's absent (in fact, in reality the non-closure is there at 2 m) and we are still investigating this. There are some issues related to high-resolution LES near the surface, not only related to the computational demand, so we think this problem merits additional research. One of the major benefits of our approach is that we can study the energy balance closure locally in 2D complex terrain.

Added in the conclusions: By means of a control volume approach, we decomposed the modeled surface energy budget to highlight its partitioning, and we have shown that the modeled energy balance ratio exhibits values that are found in field experiments. In addition, this approach allows us to investigate the energy balance closure in two-dimensional complex terrain.

4. Figures and length I suggest to shorten the paper and stick to the main message. Not all figures are needed I think. Especially the special plots are difficult to read given the rather simple message you want to convey. By the way, figure 1 could be plotted nicer.

We combined plots 2 and 3 into plot 2 (new) and 5 and 6 into plot 4 (new). We inserted different markers for each tower in figure 1.

5. Language You should be more careful with language editing before submission. I understand that correct English is an issue for non-native speakers, but please avoid

wrong syntax and incorrect formatting. Examples: P1 L4: there is an extra “was”, at several points you use the phrase “in function of”, which to my knowledge simply does not exist, P7 L14: “Table table:2”, wrong formatting. Referees spend their rare time for reading your manuscript without having any benefit from it. Being confronted with such carelessness suggests that the authors did not read their own manuscript carefully and this does not really motivate to review your manuscript in-depth. See my detailed language corrections below.

We apologize for the typos that we didn't catch beforehand and thank you for your time and efforts. We already incorporated these corrections in the Discussion paper.

2.2 Minor comments

1. P2 L17: Why is there a correlation between the friction velocity and the energy balance closure? Also: there is nothing as a good correlation. It has a value, and can be possible regarded as high.

Corrected: good \rightarrow high

In the results: In the literature (e.g. Stoy et al., 2013; Eder et al., 2015b) a correlation between friction velocity and energy balance closure has been found: a high friction velocity leads to a smaller residual. Typically, a higher friction velocity is correlated to smaller atmospheric instability, and hence roll-like convection instead of cellular convection. Maronga and Raasch (2013) found that boundary-layer rolls “smear out” the surface heterogeneity, leading to an effective surface that looks less heterogeneous, which has been related to a higher EBR (Mauder et al., 2007; Stoy et al., 2013). Therefore a possible cause for the present low correlation of u^* with the EBR, could be our range of the stability parameter. For the free convective cases considered here the stability parameter lies below the range where the friction velocity has a high correlation with EBR.

2. P2 L19: You talk about secondary circulations by self-organization, but I am not sure this contradicts the definition of a secondary circulation. Imagine a self-organized flow (give an example!), then what is the difference between primary and secondary circulation? I consider the hexagonal patterns for instance as the typical case of self-organization in the CBL, but that is what we call the primary circulation.

We agree that the hexagonal patterns should be called primary circulation in the homogeneous case. The secondary circulation is the additional circulation due to the presence of the heterogeneity (insofar it is a small effects that can be superimposed upon the primary circulation, as the NS equations are nonlinear). However, in our case the hexagonal patterns arising from the convective conditions are preferentially tied to the landscape heterogeneity in the case of $O(km)$ heterogeneity, so the primary and secondary circulation become indistinguishable.

In the introduction: In the case of cellular convection in heterogeneous terrain

the distinction between the primary and the secondary circulation becomes blurred, when the convection cells are tied to the landscape heterogeneity.

3. P2 L29: Secondary circulations do not decay to zero at the surface! They are simply not there.

Rewritten: “they are not present at the ground level”.

4. P3 L5: Why is $w=0$ at first grid level?

The lowest level (I would prefer to call it level zero) is the level where the boundary condition is applied. By constructing in the LES, there is no vertical velocity at the ground level which is supposed to be a hard boundary, not a movable or permeable membrane. We summarize this as a “rigid no-slip boundary condition” (added in the text) which implies zero values for the horizontal and vertical wind components.

In manuscript: Firstly, from continuity we indeed expect no vertical meso-scale transport by advection with the mean flow at the lowest grid point representing the lower surface, since $w=0$ due to the rigid no-slip boundary, but horizontal flux-divergence plays a role, too.

5. P3 L19: The statement does not make sense. You can’t say that a different partitioning of sensible and latent heat fluxes led to a higher Bowen ratio, because that is simply the definition of the Bowen ratio!

We didn’t intend to say this. The first subclause states the finding (Bowen ratio depends on the scale of the heterogeneity), the second makes it more precise (Bowen ratio is largest for intermediate scales).

Rewritten: Brunsell et al. (2011) found that the partitioning between latent and sensible heat was affected by the scale of heterogeneity. More precisely, the intermediate scales yielded a higher Bowen ratio.

This is one of the results of their article, and we don’t want it to be understood as a definition.

6. P4 L19: What is “strong convection”? All your simulated cases are without mean wind, so you have free convective conditions in all your simulations.

We rephrased it as “strongly convective conditions”. Taking the Obukhov length as the criterion for the strength of the instability of the CBL we have cases that fit the tag “strongly unstable” of Patton et al (2016) for which they take $L \approx -10$ m. For purely free convection we should at least have $|L| < 1$ which is not satisfied for all cases. Even though we do not have a synoptic background wind, the circulation between the patches generates a nonzero u^ that increases L . When we determine the instability from surface variables (u^* and $\overline{w'T'}$) we cannot call all our cases free convection (in reality we would determine it from the EC tower, so we only have knowledge about the surface variables).*

In introduction: To disentangle the influence of the surface heterogeneity from that of the meteorology, we will focus on a set-up of free convection without a synoptic wind (which will effectively lead to strongly to freely convective conditions diagnosed by the virtual towers).

In the introduction: In addition, as both the lack of closure and the strength of the circulations are most pronounced for strongly convective conditions, we will likewise focus on (effectively) strongly unstable conditions to free convection, we will likewise focus on strongly unstable conditions to free convection, with the instability parameter $-z/L$ ranging from 1 to 5000. The $-z/L$ is different from ∞ because the convective conditions lead to cellular circulation patterns, which locally induce a friction velocity at the surface, and due to its positiveness, there will also be a horizontally averaged u^* different from zero. From the perspective of the tower measurement, by eddy-covariance measurements alone it cannot be distinguished if a measured u^* follows from the wind aloft or locally from the convection-driven circulation. In addition, the circulation locally leads to advective terms that can influence the energy balance closure: e.g. near an updraft there will be horizontal convergence in the flow field. Even in homogeneous terrain these advective terms can lead to a non-closure of the surface energy budget (e.g. Kanda et al 2004).

We have also added an analysis of the dependence of the (horizontally averaged) u^ on the amplitude of the surface heterogeneity. In homogeneous terrain a stronger surface heating leads to stronger circulation patterns and therefore the dependence could be complicated. However, it turns out that the domain-averaged u^* drops monotonically with stronger amplitudes of the surface heterogeneity.*

In the results: On the topic of circulations driven by a surface conditions that are by design freely convective, we investigate how the domain average of u^* is influenced by the surface heterogeneity. The ratio between the surface flux at the hottest patch and the surface flux at the coolest patch is given by:

$$r = (1 + A_x + A_y + A_x \cdot A_y) \times (1 - A_x - A_y + A_x \cdot A_y)^{-1}. \quad (4)$$

The horizontal mean of the friction velocity scales very well with the natural logarithm of this ratio,

$$u^* = -0.046 \ln(r) + 0.384, \quad R^2 = 0.85 \quad (5)$$

The remaining spread in u^* does not result from the time stamp or the heterogeneity length scale. The monotonous decrease of u^* in function of the heterogeneity ratio shows that for more homogeneous terrain we will obtain a slightly larger domain averaged u^* .

7. P5 L16-31: You state that Neumann conditions are used at the lower boundary, which means you are prescribing surface fluxes. Then, how to you prescribe the surface momentum fluxes? With what values? Somehow you need to take into

account the surface roughness, but for that you will need to use Monin- Obukhov Similarity Theory.

For the velocity components, Dirichlet conditions are applied. The Neumann conditions are for scalars like potential temperature. There is a roughness length (indicated in table 1) and the first gridpoint is parameterized with MOST. We added a clarification of the model, as demanded by reviewer 1, including a more thorough discussion of our boundary conditions.

8. P6 L4: How can a tower be homogeneous? The surface around its base can, though.

It was shorthand for a tower situated in locally homogeneous terrain. We rephrased this.

9. P7 L14: There is no dataset in the table.

The table summarizes the simulation parameters within that suite. We clarified this in the text and in the table captions.

10. P7 L31: “worst imbalance of only 69%”. I guess you mean closure, not imbalance.

Indeed, we meant lowest mean closure, corrected.

11. P8 L1: finally you mention that you are talking about the “mean advection”, but it should read “advection by the mean flow”.

We replaced “mean advection” everywhere by “advection by the mean flow.”

12. P8 L25: You start the second sentence nearly exactly as you have finished the preceding one. That sounds odd.

We removed that sentence.

13. P8: You discuss the difference between kilometer and hectometer scale heterogeneity; but from previous studies it is known that only those can trigger secondary circulations whose scale is in the order of magnitude of the boundary layer depth. Now I am wondering whether you took this into account or not. In the end, you do not show secondary circulations at all, so it remains a secret whether your findings are related to the scale of the heterogeneity of the ratio of the scale of the heterogeneity to the boundary layer depth. Or do you see local circulations that were not seen in previous studies? If yes, you should show them. You only provide very little evidence here.

The references show that also landscape heterogeneity of scale smaller than the boundary layer depth has a signature on the spectrum of the heat flux (e.g. Brunzell et al 2011) and can affect the EBR (Schmid et al 1990). We improved our choice of words and replaced “secondary circulations” by “secondary circulations at the landscape up to the boundary-layer scale”. We would expect a dimensionless parameter such as the scale of heterogeneity divided by either L or by z_i (these are the most obvious choices,

the former for local circulations, the latter for secondary circulations spanning the entire boundary-layer). Because our heterogeneity length is limited to four values (after all our domain has to be periodic) this is not enough to do the correlation analysis. Nevertheless it is an interesting idea to simulate different heterogeneity lengths (and a larger range of u^) to investigate correlation with L_{het}/L or L/z_i but this study focuses on 288 simulations of strongly to freely convective conditions. We added a subsection on the local circulations.*

Added in the discussion: We start our analysis with a discussion of the location of the updrafts and downdrafts in heterogeneous terrain. For this purpose, we concentrate on a few specific cases, more precisely $A_x = A_y = 0.3$ and all four heterogeneity lengths (with $L_x = L_y$). We will take the mean vertical velocity as the simplest proxy for circulation patterns in the boundary layer. In Fig. 2 we plot the time-averaged vertical velocity at the height of the control volumes (50 m). We stress that the structures at 50 m extend into the mixed layer above where the absolute velocities become larger (not shown). The reason for the additional time average (over the complete virtual measurement interval of 4 hours) of the already hourly mean data is to remove the drift of the turbulent structures. We notice that for the heterogeneity lengths of O(km), the motions within the mixed-layer clearly reflect the surface pattern, with updrafts concentrated above the hotter patches and downdrafts above the lower patches in the 3-km heterogeneity length, and a little offset in case of the 1.5-km heterogeneity length. However, the structure of the convective turbulence for both kilometer scale are clearly different from homogeneous control run, where typical cellular convection patterns arise (Schmidt and Schumann 1989), though the hectometer scales are qualitatively rather similar to the homogeneous run. The latter could be a consequence of the blending height. Investigating the heterogeneity lengths of O(hm) with more horizontal detail for the time-averaged w , we do not see clear updrafts or downdrafts tied to the surface heterogeneity. However, in this respect it could be interesting to note that some of the hourly mean vertical velocity (without additional time-average) for the O(hm) appear better related the surface structure. Similar results appear for weaker amplitudes and also when A_x is different from A_y , in which case the dominant pattern is visible along the direction with the larger amplitude (not shown). We can conclude that circulations are tied to the landscape heterogeneity when it is of O(km). For the O(hm) such a correspondence is unclear. However, the latter could be related to the “coarse” grid resolution and the distance from the ground. Indeed, Mauder et al (2010) found persistent updraft and downdraft regions during the 2008 Ottawa field campaign.

14. P9 L13: Strictly, the friction velocity is zero in free convection as the mean wind is zero, so how can it increase for stronger circulation patterns? You must describe that you treat u^* as a local quantity and that the primary circulation creates local wind shear near the surface (if that is what you mean).

Yes, we clarified our description. Nevertheless, the circulation pattern that arises

from the surface patches leads to a mean nonzero u^* as well, because u^* is always positive. (This does not contradict the mean zero mean wind because that has a direction so the average becomes zero. Hence, locally the flux-gradient assumption can still hold, but it doesn't hold for the area-average of the simulation domain.)

In the methods: In addition, as both the lack of closure and the strength of the circulations are most pronounced for strongly convective conditions, we will likewise focus on strongly unstable conditions to free convection, we will likewise focus on (effectively) strongly unstable conditions to free convection, with the instability parameter $-z/L$ ranging from 1 to 5000. The $-z/L$ is different from ∞ because the convective conditions lead to cellular circulation patterns, which locally induce a friction velocity at the surface, and due to its positiveness, there will also be a horizontally averaged u^* different from zero. From the perspective of the tower measurement, by eddy-covariance measurements alone it cannot be distinguished if a measured u^* follows from the wind aloft or locally from the convection-driven circulation. In addition, the circulation locally leads to advective terms that can influence the energy balance closure: e.g. near an updraft there will be horizontal convergence in the flow field. Even in homogeneous terrain these advective terms can lead to a non-closure of the surface energy budget (e.g. Kanda et al 2004).

2.3 Language

1. P1 L1: pending problem - language.

Corrected: unsolved problem

2. P1 L4: extra was, boundary-layer scale

Corrected

3. P1 L14: order of magnitude instead of decade

Corrected

4. P2 L1: Earth's

Corrected

5. P5 L3: influence on what?

On virtual flux measurements. Rewritten.

6. P5 L18: (and throughout the text): "in function of" \rightarrow "as a function of"?

We have removed all occurrences of "in function of".

7. P6 L6: what is the "?" for?

Missing latex reference. Corrected.

8. P6 L27,29: Decide: “Hz” or “Hertz”
We confused it with the writing of e.g. ”1-Hertz sampling” Corrected.
9. P7 L19: “time steps”
Corrected
10. P7 L24: “we now plot” — rewrite.
Rewritten, it’s in the same plot as well because we condensed the figures.
11. Fig. 2: what does “in casu” mean?
“In casu” means “in this case”. We removed it.
12. Tab. 2: What does “1.4 ? 2.2” mean?
Should have been a dash. Corrected.
13. Tab. 2: -36,1 should read 36.1,
Corrected.
14. Tab. 2: I’d more like a long-list with all simulations
This would yield two tables with 144 rows (6x6x2x2 cases) and 7 columns, which is basically the information in tables 2 and 3.
15. Tab. 2+3: What is the Boundary-layer height in “short” (1.4 – 2.2), while the Obukhov length is in “long” (From ... to ...)?
The Obukhov length is negative for unstable conditions and therefore the dash distracted. Both are now in the long format without a dash.