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3 **SUPPLEMENTARY MATERIAL**

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5 **The influence of particle composition upon the evolution of  
6 urban ultrafine diesel particles on the neighbourhood scale**

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14 Here we present details of the input parameters used in the box model simulations (Section S1)  
15 and some results (Section S2). All figures and tables are given in the Appendix.

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17 **S1. Model input parameters** - size distribution, vapour pressures, modal composition mass  
18 fractions in the nucleation and Aitken modes, gas-phase ambient concentrations.

19

20 The initial size distribution is based on the measurements of Dall'Osto et al. (2011) and it is  
21 plotted in Figure 1-S. This ultrafine size resolved distribution represents the typical street canyon  
22 size distribution found next to a traffic site in Marylebone road in London (UK). The distribution  
23 has a well defined nucleation mode (particles with a diameter around or less than 30 nm) with a  
24 peak number concentration at ~ 23 - 24 nm. The Aitken mode (particles with diameter between  
25 30 and 100 nm) is seen as a shoulder attached to the nucleation mode with a centre between 50 -  
26 60 nm. Dall'Osto et al. (2011) show that the observed size distribution is subject to a major  
27 transformation caused by extensive evaporation of volatile material from the particles. The  
28 diameter of the nucleation mode particles decreased during the transport of the particles between  
29 the street canyon and the nearby city park over a distance of about 665m, as shown in Figure 1-S  
30 in the Appendix. The nucleation-mode peak diameter,  $D_{pg,nuc}$ , corresponding to the highest number  
31 concentration in the nucleation mode, was found at around 8 – 9 nm. In our study, we aim to put  
32 forward a realistic set of compositions and thermodynamic properties that could explain this  
33 diameter decrease as seen in the observations. Chemical analyses during the observations are  
34 missing; however, there are some laboratory data pointing to the nature of organics that  
35 participate in the composition from emitted particles collected from an engine testbed (Alam et  
36 al., 2016). Figure 2-S shows the normalised mass concentration per compound in the range  
37  $[C_{16}H_{34}:C_{32}H_{66}]$  for a given size class. Particles in the Nucleation and Aitken modes consist of  
38 about 10% and higher contribution from compounds in the range  $C_{25}H_{52}-C_{29}H_{60}$ .

39

40 In our modelling study the UFP size-resolved mass composition per mode (eq. 1) is initialised as  
41 follows. The mass of a particle,  $M_{ij}$ , per size bin  $i$  and compound  $j$  in the range [C<sub>16</sub>H<sub>34</sub>:C<sub>32</sub>H<sub>66</sub>] is  
42 expressed as

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$$M_{ij} = \sum_{k=1}^2 \frac{\pi}{6} Dp_i^3 \rho X_{jk} N_{ik} \quad (\text{eq. 1})$$

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47  $i = 1, \dots, 15$  – number of size bins

48  $j = 1, \dots, 18$  – indices [1-17] correspond to surrogate n-alkane compounds in the range C<sub>16</sub>H<sub>34</sub> –  
49 C<sub>32</sub>H<sub>66</sub>; index 18 refers to the involatile core

50  $k = 1, 2$  - particle mode, where 1 = Nucleation mode, 2 = Aitken mode

51  $Dp_i$  – particle diameter per size bin  $i$ , m

52  $M_{ij}$  – size resolved mass per size bin  $i$  and per compound  $j$ , kg m<sup>-3</sup>

53  $\rho = 1000$  kg m<sup>-3</sup>, particle density, held constant to avoid introducing highly uncertain parameters  
54 for density of involatile core.

55  $X_{jk}$  – fraction of mass in a particle in mode  $k$  per compound  $j$

56  $\pi = 3.14$

57 is the number of particles per bin width  $\Delta Dp$ , [ $\# \text{ m}^{-3}$ ]. The number log-normal size distribution  
58 (eq. 2) is given as follows:

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$$n(Dp)_{ik} = \frac{N_k}{\sqrt{2\pi} Dp_i \ln(\sigma_{gk})} \exp\left(-0.5 \left(\frac{\ln(Dp_i/Dp_{gk})}{\ln(\sigma_{gk})}\right)^2\right) \quad (\text{eq. 2})$$

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62

63  $N_k = 3.0 \times 10^{10}$  and  $1.8 \times 10^{10}$  ( $\# \text{ m}^{-3}$ ) are the total number concentrations in the Nucleation and  
64 Aitken mode, respectively

65  $D_{pk} = 23$  and  $65 \text{ nm}$  are the geometric mean diameter in the Nucleation and Aitken mode,  
66 respectively

67  $\sigma_{gk} = 1.6$  is the geometric standard deviation for both modes

68 The fraction of mass  $X_{jk}$  of each particle in a mode  $k$  per compound SVOC in the range  $C_{16}H_{34}-$   
69  $C_{32}H_{66}$  is calculated (eq. 3) as follows:

70

$$71 X_{jk} = \frac{f(m_j, \sigma_{modal})}{\sum_{j=1}^{17} f(m_j, \sigma_{modal})} (x_{jk} - sf_k) \quad (\text{eq. 3})$$

72

73 where  $f(m_j, \sigma_{modal})$  is the modal composition in the form of a Gaussian distribution (eq. 4),  $x_{jk}$  is  
74 SVOC composition given by the Gaussian parameterisation (eq. 5), and  $sf_k$  is the solid involatile  
75 fraction per mode  $k$ :

76

$$77 f(m_j, \sigma_{modal}) = \frac{1}{\sqrt{2\pi}\sigma_{modal}} \exp\left(-0.5\left(\frac{|x_j - m_j|}{\sigma_{modal}}\right)^2\right) \quad (\text{eq. 4})$$

78

$$79 x_{jk} = \sum_{j=1}^{17} \frac{f(m_j, \sigma_{modal})}{\sum_{j=1}^{17} f(m_j, \sigma_{modal})} = 1 \quad (\text{eq. 5})$$

80

81  $\sigma_{modal} = 1, \dots, 5$  – standard deviation of modal composition

82  $x_j = 1, \dots, 17$  – number assigned to the SVOC compound

83  $m_j = 1, \dots, 17$  – modal composition compound for each SVOC in the range  $C_{16}H_{34}-C_{32}H_{66}$

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85 In this study the role of an involatile core ( $sf_k$ ) is evaluated, too, by considering an involatile core  
86 to be 1%, 5% and 10% of the mass in a particle in the Nucleation mode ( $k = 1$ ). Input modal

87 composition mass fractions in the nucleation mode and composition standard deviation are  
88 presented in the Appendix in Table 1-S, 2-S and 3-S for involatile core of 1%, 5% and 10%,  
89 respectively. The involatile core in the Aitken mode is 90% and the input modal composition  
90 mass fractions are given in Table 4-S in the Appendix.

91

92 Input vapour pressure parameterisations are given in Table 5-S. A-a, B-c and Co are used in this  
93 study to represent the uncertainties in the vapour pressure and evaluate the overall effect on the  
94 evaporative shrinkage of the nucleation mode particle diameter. Figure 3-S shows the ratio of  
95 vapour pressure between 298 K and 273 K for A-a, B-c and Co vapour pressure parameterisations  
96 and n-alkane compounds in the range  $C_{16}H_{34}$ - $C_{32}H_{66}$ . The ratio for B-c and Co vapour pressure  
97 parameterisations is within an order of magnitude for compounds in the range  $C_{16}H_{34}$ - $C_{25}H_{52}$ ,  
98 however, it increases two to three orders of magnitude for higher molecular weight compounds.  
99 The ratio for A-a vapour pressure parameterisation is within an order of magnitude for  
100 compounds in the range  $C_{16}H_{34}$ - $C_{21}H_{44}$ , and increases substantially for the remaining compounds.  
101 This would imply that for the selected timescale of 100 s there will be a shift in the threshold  
102 modal compositions to lower carbon-number compounds in comparison with the threshold modal  
103 compositions discussed in this study. The temperature dependence on evaporation is not  
104 considered further in this study but should be borne in mind.

105

106 The initial gas-phase concentrations for the n-alkanes in the range  $C_{16}H_{34}$ - $C_{32}H_{66}$  (Table 6-S) are  
107 as for the study in Nikolova et al. (2016) and are based on the roadside atmospheric  
108 measurements of Harrad et al. (2003).

109

## 110 **S2. Results**

111 Figure 4-S and Figure 5-S show the nucleation mode peak diameter  $D_{pg,nuc}$  after 100 s using the  
112 vapour pressure parameterisations following Myrdal-Yalkowsky et al (1997, B-c) and Nannoolal

113 et al (2008, A-a), respectively. The nucleation mode particles consist of initial 1% non-volatile  
114 material. The threshold modal composition value changes from C<sub>27</sub>H<sub>56</sub> for the B-c  
115 parameterisation (Figure 4-S) to C<sub>22</sub>H<sub>46</sub> for A-a (Figure 5-S).

116

117 Figure 6-S shows the relative difference of the D<sub>pg,nuc</sub> between the highest (B-c) and lowest (A-a)  
118 vapour pressure parameterisations evaluated at 1 s, 10 s, 50 s and 100 s. Overall the largest  
119 difference is propagating to higher standard deviation sigma when simulation time increases as  
120 well as moving towards higher carbon-number modal compositions. In other words the relative  
121 differences become larger with time, pointing back to the huge differences in vapour pressure  
122 parameterisations between B-C and A-a. The choice of a particular vapour pressure dataset  
123 changes the range of carbon numbers by 2 in the first 10 seconds for which the highest relative  
124 difference is simulated. The 1-s relative difference is the highest for sigma 1 and modal  
125 compositions C<sub>19</sub>H<sub>40</sub>-C<sub>21</sub>H<sub>44</sub>. The 10-s highest relative difference has shifted to modal  
126 compositions C<sub>21</sub>H<sub>44</sub>-C<sub>23</sub>H<sub>48</sub> and sigma = 1, 2. Higher relative differences (50% and more) are also  
127 simulated at sigma = 3. The 100-s relative difference is the highest for modal compositions  
128 C<sub>22</sub>H<sub>46</sub>-C<sub>24</sub>H<sub>50</sub> and sigma = 1, 2, 3, but also relative differences of around 50% are simulated for  
129 sigma = 5.

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131 Figure 7-S shows the ‘100-s effective involatile core’ for the nucleation mode particles. Results  
132 are shown at 1%, 5% and 10% initial non-volatile material in the nucleation mode particles,  
133 modal compositions C<sub>24</sub>H<sub>34</sub> and C<sub>32</sub>H<sub>66</sub> and for various composition standard deviations, sigma.  
134 Vapour pressure parameterisations follow Myrdal and Yalkowski (1997; B-c in Table 1-S) and  
135 Nannoolal et al. (2008; A-a in Table 1-S). Figure 5-S presents the sensitivity to the non-volatile  
136 core in the nucleation mode for modal compositions C<sub>24</sub>H<sub>50</sub> and C<sub>32</sub>H<sub>66</sub> evaluated for B-c and A-a  
137 vapour pressure parameterisations. The 100-s effective involatile core for modal composition  
138 C<sub>24</sub>H<sub>50</sub> and B-c vapour pressure parameterisation increases when the non-volatile core increases.

139 This is simulated for an increasing  $\sigma$  too, due the increasing number of lower volatility  
140 components that are added into the particle composition. The 100-s effective involatile core for  
141 modal compositions C<sub>24</sub>H<sub>50</sub> (for A-a vapour pressure) and C<sub>32</sub>H<sub>66</sub> (for A-a and B-c vapour  
142 pressures) shows an opposite trend with respect to sigma, i.e., the 100-s effective involatile core  
143 decreases due to the increasing number of higher volatility components added into the particle  
144 composition.

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#### 146 **Acknowledgements**

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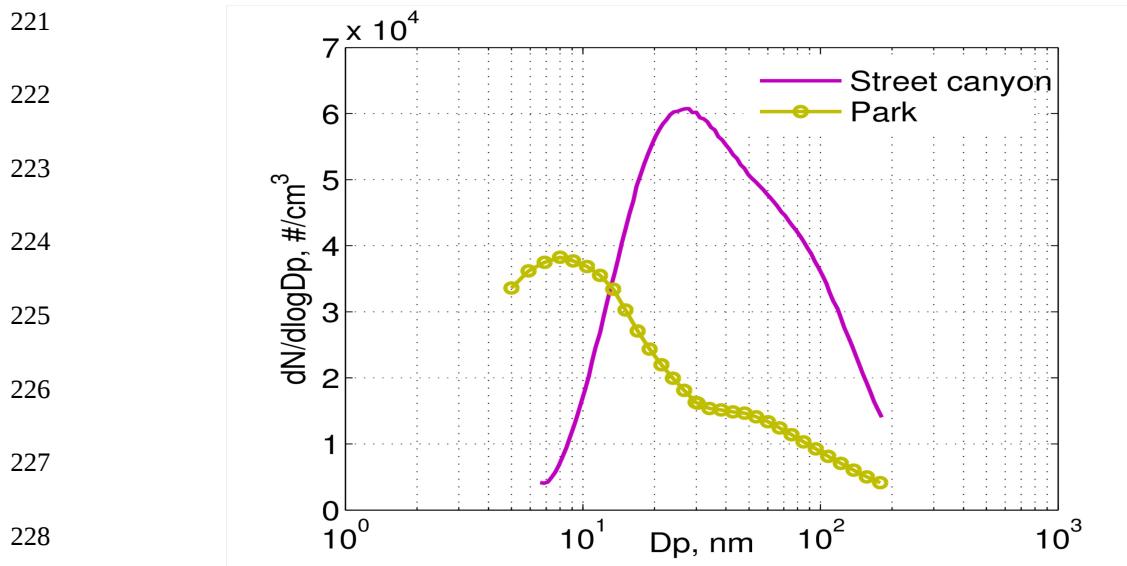
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217 **Appendix**

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257 **Figure 2-S.** Laboratory particulate mass fractions of  $n$ -alkanes  $C_nH_{(2n+2)}$ , where  $n=[16:32]$  for  
258 selected particulate diameter range [ $<10:100$  nm]. Figure plotted based on the data presented in  
259 *Alam et al. (2016)*.

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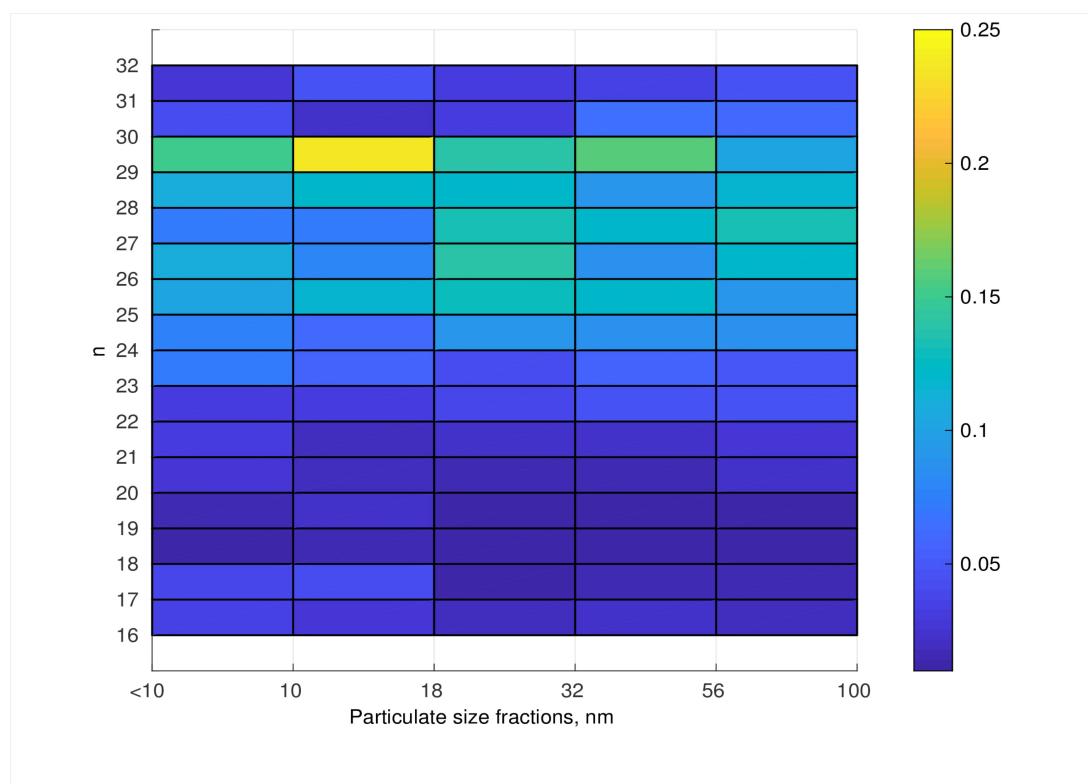
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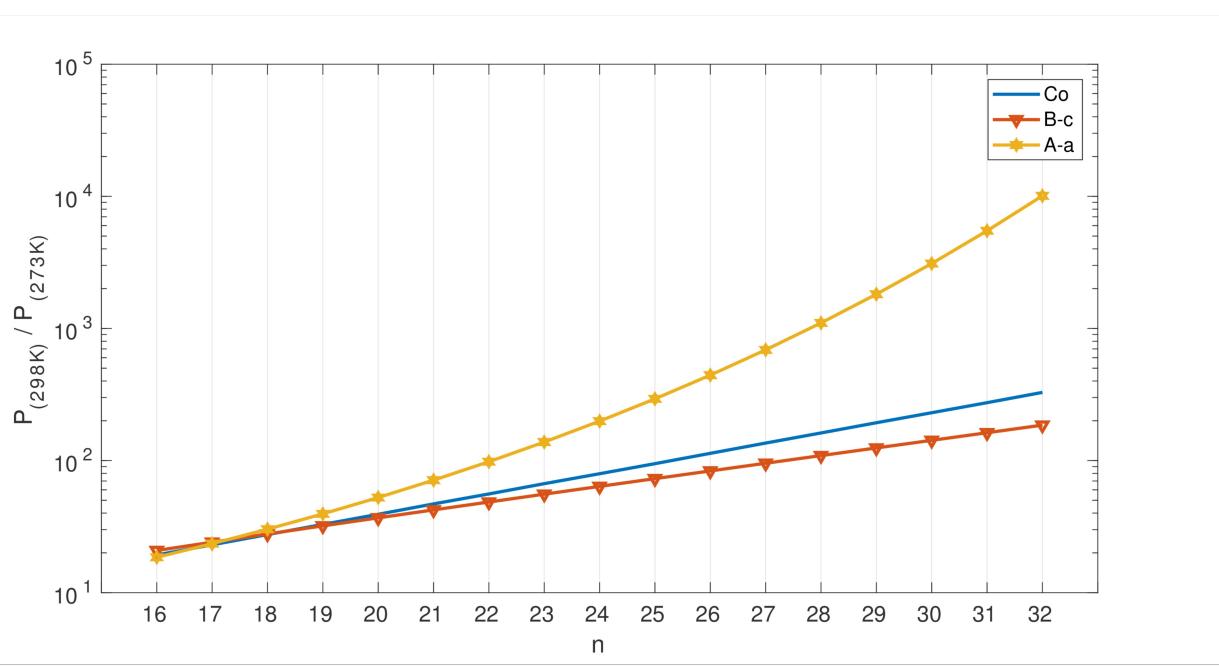
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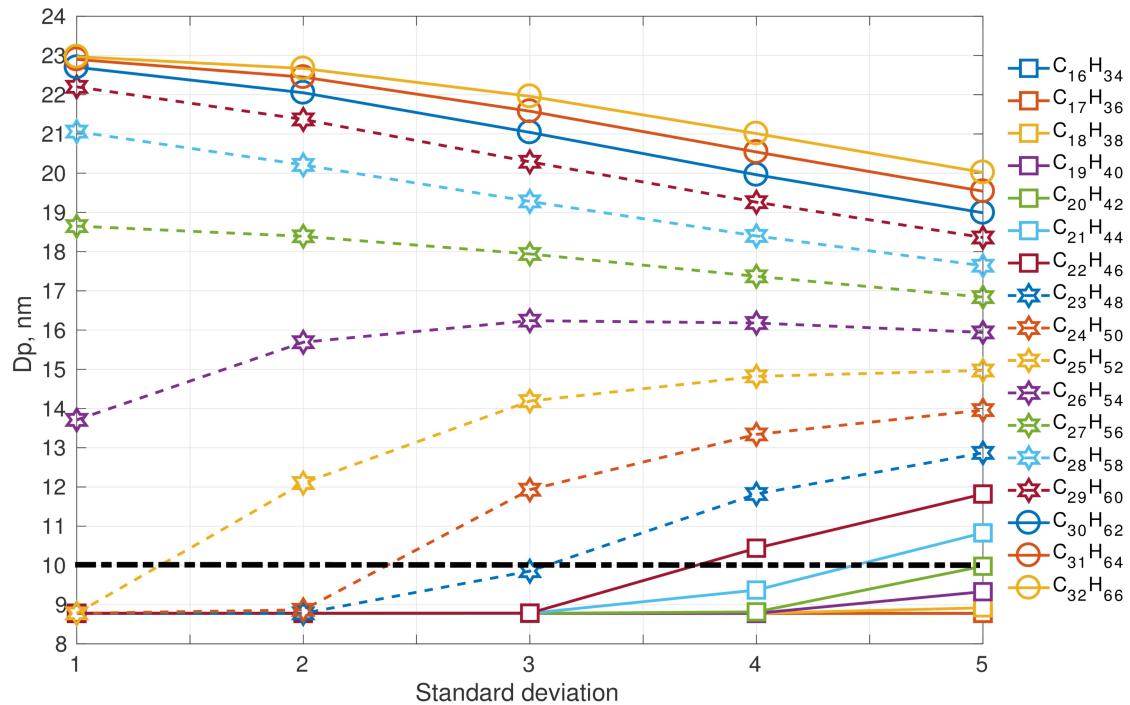
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308 **Figure 4-S.** Nucleation mode peak diameter  $D_p$  [nm] at 100 s of simulation depending on the  
 309 modal composition and the composition standard deviation. The initial nucleation mode peak  
 310 diameter is at 23 nm (not shown on the figure). Vapour pressure data follows Myrdal Yalkowsky  
 311 et al. (1997, B-c). Initial nucleation mode particle involatile core is 1%.

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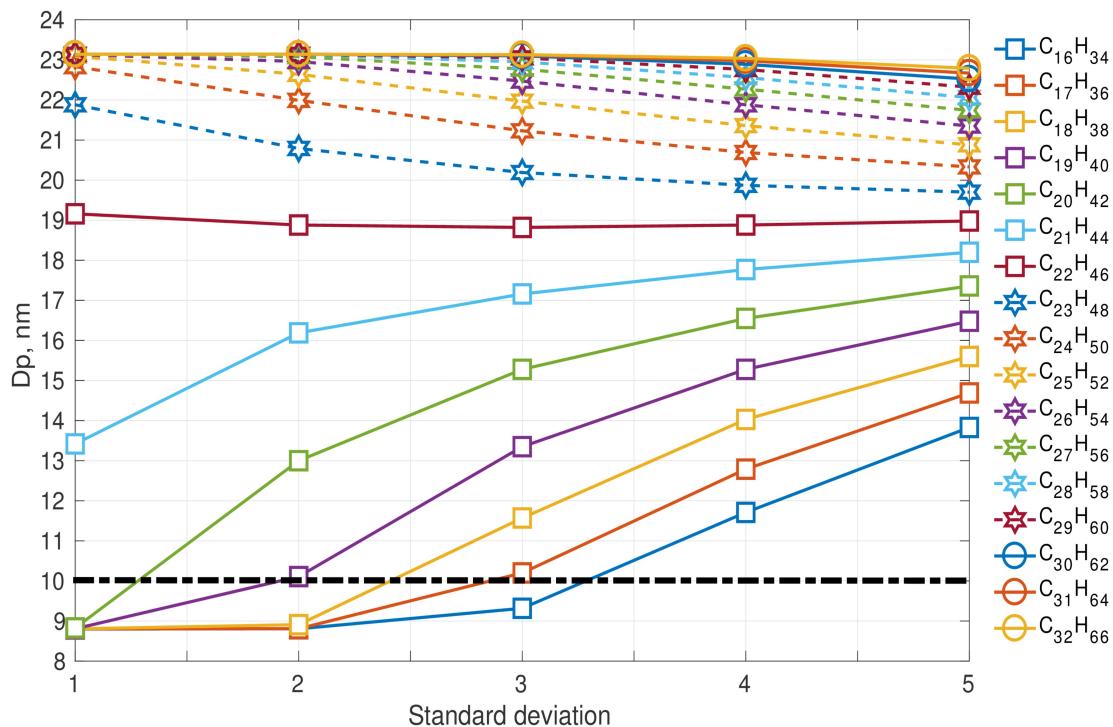
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334 **Figure 5-S.** Nucleation mode peak diameter  $D_p$  [nm] at 100 s of simulation depending on the  
 335 modal composition and the composition standard deviation. The initial nucleation mode peak  
 336 diameter is at 23 nm (not shown on the figure). Vapour pressure data follows Nannoolal et al.  
 337 (2008, A-a). Initial nucleation mode particle involatile core is 1%.

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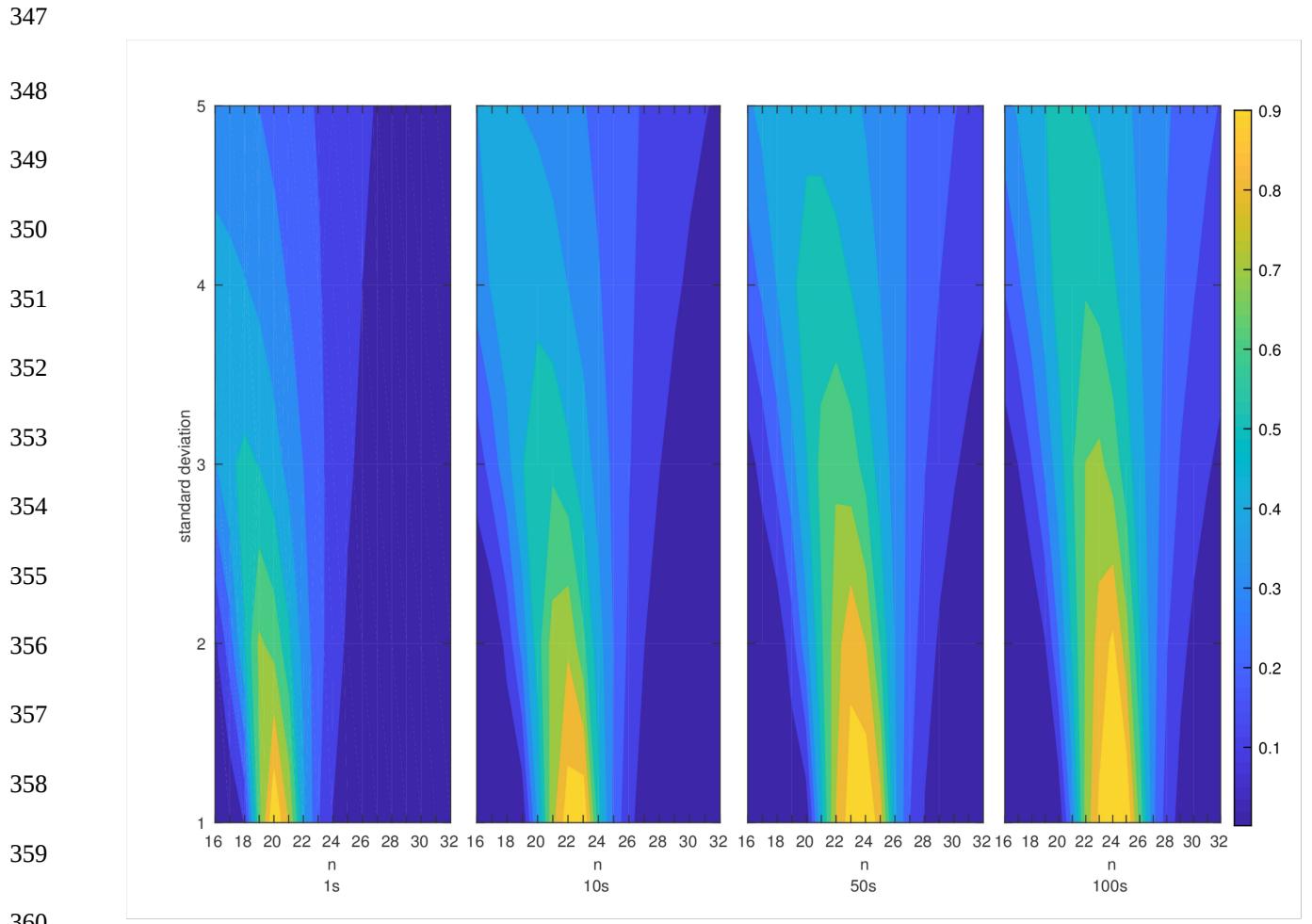
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362 **Figure 6-S.** Nucleation mode peak diameter relative difference (in %) between B-c and A-a

363 vapour pressure parameterisations for modal compositions  $C_nH_{(2n+2)}$  for  $n = 16:32$  and

364 composition standard deviation from 1 to 5.

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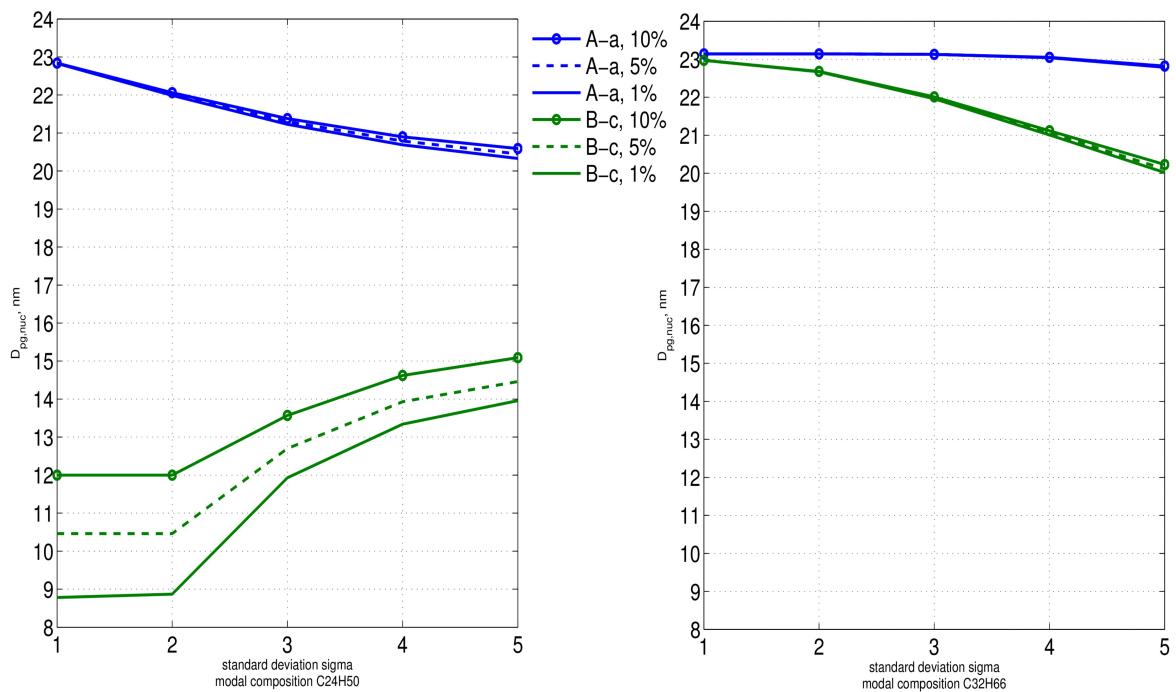
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383 **Figure 7-S.** Nucleation mode peak diameter  $D_p$  [nm] after 100s: the ‘100-s effective involatile  
 384 core’ for the nucleation mode. Results are shown at 1%, 5% and 10% initial non-volatile material  
 385 in the nucleation mode particles, modal compositions  $C_{24}H_{34}$  (left) and  $C_{32}H_{66}$  (right) and for  
 386 various composition standard deviations, sigma. Vapour pressure parameterisation follows  
 387 Myrdal and Yalkowski (1997; B-c in Table 1-S) and Nannoolal et al. (2008; A-a in Table 1-S).

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$\sigma$	modal composition																	
1	$C_{18}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
	5.65E-01	2.54E-01	5.37E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.00E-15	1.02E-18	7.62E-23	2.10E-27	2.12E-32	7.92E-38	1.09E-43	5.82E-50	1.45E-56	
	3.42E-01	4.20E-01	2.41E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.00E-15	1.02E-18	7.62E-23	2.10E-27	2.13E-32	7.96E-38	1.15E-43	7.83E-50	
	7.64E-02	2.54E-01	3.97E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.00E-15	1.02E-18	7.62E-23	2.10E-27	2.13E-32	8.41E-38	1.55E-43	
	6.27E-03	5.68E-02	2.41E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.00E-15	1.02E-18	7.62E-23	2.11E-27	2.26E-32	1.13E-37	
	1.89E-04	4.66E-03	5.37E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.00E-15	1.02E-18	7.65E-23	2.23E-27	3.04E-32	
	2.10E-06	1.41E-04	4.41E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.00E-15	1.02E-18	8.09E-23	3.00E-27	
	8.60E-09	1.56E-06	1.33E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.04E-12	5.02E-15	1.08E-18	1.09E-22	
	1.29E-11	6.39E-09	1.48E-06	1.33E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.02E-09	9.08E-12	5.31E-15	1.45E-18	
	7.15E-15	9.61E-12	6.04E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.47E-06	6.04E-09	9.61E-12	7.15E-15	
	1.45E-18	5.31E-15	9.08E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.32E-04	1.48E-06	6.39E-09	1.29E-11	
	1.09E-22	1.08E-18	5.02E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.39E-03	1.33E-04	1.56E-06	8.60E-09	
	3.00E-27	8.09E-23	1.02E-18	5.00E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.35E-02	4.41E-03	1.41E-04	2.10E-06	
	3.04E-32	2.23E-27	7.65E-23	1.02E-18	5.00E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.40E-01	5.37E-02	4.66E-03	1.89E-04	
	1.13E-37	2.26E-32	2.11E-27	7.62E-23	1.02E-18	5.00E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.95E-01	2.41E-01	5.68E-02	6.27E-03	
	1.55E-43	8.41E-38	2.13E-32	7.62E-23	1.02E-18	5.00E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.40E-01	3.97E-01	2.54E-01	7.64E-02		
	7.83E-50	1.15E-43	7.96E-38	2.13E-32	7.62E-23	1.02E-18	5.00E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.35E-02	2.41E-01	4.20E-01	3.42E-01		
	1.45E-56	5.82E-50	1.09E-43	7.92E-38	2.12E-32	7.62E-23	1.02E-18	5.00E-15	9.04E-12	6.02E-09	1.47E-06	1.32E-04	4.39E-03	5.37E-02	2.54E-01	5.65E-01		
	9.90E-001																	
2	$C_{18}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
	3.29E-01	2.25E-01	1.34E-01	6.67E-02	2.70E-02	8.70E-03	2.19E-03	4.32E-04	6.62E-05	7.91E-06	7.36E-07	5.35E-08	3.04E-09	1.37E-10	5.04E-12	1.55E-13	4.17E-15	
	2.91E-01	2.55E-01	1.94E-01	1.25E-01	6.49E-02	2.68E-02	8.68E-03	2.19E-03	4.32E-04	6.63E-05	7.92E-06	7.38E-07	5.39E-08	3.13E-09	1.47E-10	5.63E-12	2.01E-13	
	2.00E-01	2.25E-01	2.20E-01	1.81E-01	6.12E-02	6.43E-02	2.67E-02	8.68E-03	2.19E-03	4.32E-04	6.63E-05	7.93E-06	7.44E-07	5.54E-08	3.35E-09	1.70E-10	7.54E-12	
	1.07E-01	1.54E-01	1.94E-01	2.05E-01	1.76E-01	1.20E-01	6.41E-02	2.67E-02	8.68E-03	2.19E-03	4.32E-04	6.64E-05	8.00E-06	7.65E-07	5.94E-08	3.88E-09	2.20E-10	
	4.46E-02	8.26E-02	1.34E-01	1.81E-01	2.00E-01	1.75E-01	1.20E-01	6.41E-02	2.67E-02	8.68E-03	2.19E-03	4.33E-04	6.70E-05	8.23E-06	8.21E-07	6.87E-08	5.01E-09	
	1.45E-02	3.45E-02	7.15E-02	1.25E-01	1.76E-01	1.98E-01	1.74E-01	1.20E-01	6.41E-02	2.67E-02	8.68E-03	2.20E-03	4.37E-04	6.69E-05	8.82E-06	9.49E-07	8.89E-08	
	3.66E-03	1.12E-02	2.98E-02	6.67E-02	1.21E-01	1.75E-01	1.98E-01	1.74E-01	1.20E-01	6.41E-02	2.67E-02	8.70E-03	2.22E-03	4.49E-04	7.39E-05	1.02E-05	1.23E-06	
	7.20E-04	2.83E-03	9.68E-03	2.78E-02	6.49E-02	1.20E-01	1.74E-01	1.97E-01	1.74E-01	1.20E-01	6.41E-02	2.68E-02	8.78E-03	2.28E-03	4.82E-04	8.54E-05	1.32E-05	
	1.10E-04	5.57E-04	2.45E-03	9.02E-03	6.43E-02	1.20E-01	1.74E-01	1.97E-01	1.74E-01	1.20E-01	6.41E-02	2.68E-02	8.79E-03	2.29E-03	4.82E-04	8.55E-05	1.10E-04	
	1.32E-05	8.54E-05	4.82E-04	2.28E-03	8.78E-03	2.68E-02	6.41E-02	1.20E-01	1.74E-01	1.97E-01	1.74E-01	1.20E-01	6.49E-02	2.78E-02	9.68E-03	2.33E-03	7.20E-04	
	1.23E-06	1.02E-05	7.39E-05	4.49E-04	2.22E-03	8.70E-03	2.67E-02	6.41E-02	1.20E-01	1.74E-01	1.98E-01	1.75E-01	1.21E-01	6.67E-02	2.98E-02	1.12E-02	3.66E-03	
	8.89E-08	9.49E-07	8.82E-06	6.69E-05	4.37E-04	2.20E-03	8.68E-03	2.67E-02	6.41E-02	1.20E-01	1.74E-01	1.98E-01	1.76E-01	1.21E-01	6.75E-02	3.45E-02	1.45E-02	
	5.01E-09	6.87E-08	8.21E-07	8.23E-06	6.70E-05	4.33E-04	2.19E-03	8.68E-03	2.67E-02	6.41E-02	1.20E-01	1.75E-01	2.00E-01	1.81E-01	1.34E-01	8.26E-02	4.46E-02	
	2.20E-10	3.88E-09	5.94E-08	7.65E-07	8.00E-06	6.64E-05	4.32E-04	2.19E-03	8.68E-03	2.67E-02	6.41E-02	1.20E-01	1.76E-01	2.05E-01	1.94E-01	1.54E-01	1.07E-01	
	7.54E-12	1.70E-10	3.35E-09	5.54E-08	7.44E-07	7.93E-06	6.63E-05	4.32E-04	2.19E-03	8.68E-03	2.67E-02	6.43E-02	1.21E-01	1.81E-01	2.20E-01	2.25E-01	2.00E-01	
	2.01E-13	5.83E-12	1.47E-10	3.13E-09	5.39E-08	7.38E-07	7.92E-06	6.63E-05	4.32E-04	2.19E-03	8.68E-03	2.68E-02	6.49E-02	1.25E-01	1.94E-01	2.55E-01	2.91E-01	
	4.17E-15	1.55E-13	5.04E-12	3.04E-09	5.35E-08	7.36E-07	7.91E-06	6.62E-05	4.32E-04	2.19E-03	8.70E-03	2.70E-02	6.67E-02	1.34E-01	2.25E-01	3.29E-01		
3	$C_{18}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
	2.32E-01	1.80E-01	1.32E-01	9.08E-02	5.79E-02	3.39E-02	1.81E-02	8.71E-03	3.78E-03	1.47E-04	5.17E-04	1.64E-04	4.73E-05	1.25E-05	2.15E-06	3.08E-07	7.09E-07	1.55E-07
	2.20E-01	1.90E-01	1.56E-01	1.20E-01	5.60E-02	5.33E-02	1.86E-02	8.69E-03	3.79E-03	1.48E-04	5.26E-04	1.70E-04	5.02E-05	1.38E-05	2.35E-06	3.86E-07		
	1.86E-01	1.80E-01	1.65E-01	1.42E-01	1.13E-01	8.26E-02	5.49E-02	3.31E-02	1.79E-02	8.71E-03	3.82E-03	1.51E-03	5.45E-04	1.80E-04	5.53E-05	1.59E-05	4.34E-06	
	1.41E-01	1.52E-01	1.56E-01	1.50E-01	1.33E-01	8.11E-02	5.45E-02	3.30E-02	1.79E-02	8.78E-03	3.89E-03	1.57E-03	5.79E-04	1.98E-04	6.38E-05	1.94E-05		
	9.55E-02	1.15E-01	1.32E-01	1.42E-01	1.29E-01	8.07E-02	5.41E-02	3.30E-02	1.78E-02	8.74E-03	3.85E-03	1.60E-03	5.63E-04	1.63E-04	6.37E-04	2.29E-04	7.80E-05	
	5.79E-02	7.82E-02	1.00E-01	1.33E-01	1.26E-01	1.06E-01	8.02E-02	5.45E-02	3.33E-02	1.84E-02	9.26E-03	4.28E-03	1.83E-03	5.92E-04	1.75E-04	2.80E-04		
	3.15E-02	4.74E-02	8.57E-02	1.11E-01	1.26E-01	1.33E-01	1.25E-01	1.05E-01	9.06E-02	9.01E-02	7.75E-02	4.95E-02	2.03E-02	5.60E-02	2.03E-02	1.08E-02	2.58E-03	
	6.64E-03	1.25E-02	2.23E-02	3.73E-02	5.79E-02	8.26E-02	1.07E-01	1.25E-01	1.32E-01	1.25E-01	1.07E-01	8.26E-02	5.79E-02	3.73E-02	2.23E-02	1.25E-02	6.64E-03	
	2.59E-03	5.43E-03	1.08E-02	2.03E-02	3.51E-02	5.60E-02	8.11E-02	1.06E-01	1.25E-01	1.32E-01	1.26E-01	1.09E-01	8.55E-02	6				

401

402 **Table 1-S.** Input modal composition mass fractions (by columns) in the nucleation mode and  
403 composition standard deviation for involatile core of 1%.

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		modal composition																	
	$\sigma$	$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
1	1	5.42E-01	2.44E-01	5.15E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.80E-15	9.77E-19	7.31E-23	2.01E-27	2.04E-32	7.60E-38	1.05E-43	5.58E-50	1.39E-56	
2	1	3.29E-01	4.03E-01	2.31E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.80E-15	9.77E-19	7.31E-23	2.01E-27	2.04E-32	7.63E-38	1.11E-43	7.51E-50	
3	1	7.33E-02	2.44E-01	3.81E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.80E-15	9.77E-19	7.31E-23	2.01E-27	2.05E-32	8.07E-38	1.49E-43	
4	1	6.02E-03	5.45E-02	2.31E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.80E-15	9.77E-19	7.31E-23	2.02E-27	2.17E-32	1.09E-37	
5	1	1.82E-04	4.47E-03	5.15E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.80E-15	9.77E-19	7.34E-23	2.14E-27	2.92E-32	
6	1	2.02E-06	1.35E-04	4.23E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.80E-15	9.81E-19	7.76E-23	2.88E-27	
7	1	8.25E-09	1.50E-06	1.28E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.68E-12	4.82E-15	1.04E-18	1.05E-22	
8	1	1.24E-11	6.13E-09	1.42E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.77E-09	8.72E-12	5.10E-15	1.40E-18	
9	1	6.68E-16	9.22E-12	5.80E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.41E-06	5.80E-09	9.22E-16	6.86E-15	
10	1	1.40E-18	5.10E-15	8.72E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.27E-04	1.42E-06	6.13E-09	1.24E-11	
11	1	1.05E-22	1.04E-18	4.82E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.21E-03	1.28E-04	1.50E-06	8.25E-09	
12	1	2.88E-27	7.76E-23	9.81E-19	4.80E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.13E-02	4.23E-03	1.35E-04	2.02E-06	
13	1	2.92E-32	2.14E-27	7.34E-23	9.77E-19	4.80E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.30E-01	5.15E-02	4.47E-03	1.82E-04	
14	1	1.09E-37	2.17E-32	2.02E-27	7.31E-23	9.77E-19	4.80E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.79E-01	2.31E-01	5.45E-02	6.02E-03	
15	1	1.49E-43	8.07E-38	2.05E-32	2.01E-27	7.31E-23	9.77E-19	4.80E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.30E-01	3.81E-01	2.44E-01	7.33E-02	
16	1	7.51E-50	1.11E-43	7.63E-38	2.04E-32	2.01E-27	7.31E-23	9.77E-19	4.80E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.13E-02	2.31E-01	4.03E-01	3.29E-01	
17	1	1.39E-56	5.58E-50	1.05E-43	7.60E-38	2.04E-32	2.01E-27	7.31E-23	9.77E-19	4.80E-15	8.68E-12	5.77E-09	1.41E-06	1.27E-04	4.21E-03	5.15E-02	2.44E-01	5.42E-01	
18	2	9.50E-01	2.16E-01	1.28E-01	6.40E-02	2.59E-02	8.35E-03	2.11E-03	4.15E-04	6.36E-05	7.59E-06	7.07E-07	5.13E-08	2.92E-09	1.32E-10	4.84E-12	1.49E-13	4.00E-15	
19	2	3.16E-01	2.16E-01	1.28E-01	6.40E-02	2.59E-02	8.35E-03	2.11E-03	4.15E-04	6.36E-05	7.60E-06	7.08E-07	5.15E-08	2.93E-09	1.33E-10	4.85E-12	1.50E-13	4.01E-15	
20	2	2.79E-01	2.44E-01	1.86E-01	1.20E-01	6.22E-02	2.57E-02	8.33E-03	2.11E-03	4.15E-04	6.36E-05	7.60E-06	7.08E-07	5.15E-08	2.94E-09	1.34E-10	5.59E-12	1.93E-13	
21	2	1.92E-01	2.16E-01	2.11E-01	1.74E-01	1.61E-01	6.17E-02	2.57E-02	8.33E-03	2.11E-03	4.15E-04	6.36E-05	7.61E-06	7.14E-07	5.32E-08	3.22E-09	1.63E-10	7.23E-12	
22	2	1.03E-01	1.48E-01	1.86E-01	1.97E-01	1.69E-01	1.15E-01	6.16E-02	2.56E-02	8.33E-03	2.11E-03	4.15E-04	6.37E-05	7.68E-06	7.34E-07	5.70E-08	3.72E-09	2.11E-10	
23	2	4.28E-02	7.93E-02	1.28E-01	1.74E-01	1.92E-01	1.68E-01	1.15E-01	6.15E-02	2.56E-02	8.33E-03	2.11E-03	4.16E-04	6.43E-05	7.90E-06	7.87E-07	6.59E-08	4.81E-08	
24	2	1.39E-02	3.31E-02	6.66E-02	1.20E-01	1.69E-01	1.90E-01	1.67E-01	1.15E-01	6.15E-02	2.56E-02	8.33E-03	2.11E-03	4.19E-04	6.61E-05	8.47E-06	9.10E-07	8.53E-08	
25	3	3.51E-03	1.07E-02	2.86E-02	6.40E-02	1.61E-01	1.68E-01	1.90E-01	1.67E-01	1.15E-01	6.15E-02	2.57E-02	8.35E-03	2.13E-03	4.31E-04	7.09E-05	9.79E-06	1.18E-06	
26	3	6.91E-04	2.71E-03	9.28E-03	2.67E-02	1.62E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.16E-02	2.57E-02	8.42E-03	2.19E-03	4.62E-04	8.19E-05	1.27E-05	
27	3	1.06E-04	5.34E-04	2.35E-03	8.66E-03	2.59E-02	6.17E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.17E-02	2.59E-02	8.66E-03	2.35E-03	5.34E-04	1.06E-04	
28	3	1.27E-05	8.19E-05	4.62E-04	2.19E-03	8.42E-03	2.57E-02	6.16E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.22E-02	2.67E-02	9.28E-03	2.71E-03	6.91E-04	
29	3	1.18E-06	9.79E-06	7.09E-05	4.31E-04	2.13E-03	8.35E-03	2.57E-02	6.15E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.22E-02	2.67E-02	9.28E-03	2.71E-03	
30	3	8.53E-08	9.10E-07	8.47E-06	6.61E-05	4.19E-04	2.11E-03	8.33E-03	2.56E-02	6.15E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.22E-02	2.66E-02	9.31E-02	
31	3	4.81E-09	6.59E-08	7.87E-07	7.90E-07	6.43E-05	4.16E-04	2.11E-03	8.33E-03	2.56E-02	6.15E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.22E-02	2.66E-02	
32	3	2.11E-10	3.72E-09	5.70E-08	7.34E-07	6.78E-06	6.37E-05	4.15E-04	2.11E-03	8.33E-03	2.56E-02	6.15E-02	1.15E-01	1.67E-01	1.90E-01	1.67E-01	1.15E-01	6.21E-02	
33	3	7.23E-12	1.63E-10	3.22E-09	5.32E-08	7.14E-07	7.61E-06	6.36E-05	4.15E-04	2.11E-03	8.33E-03	2.57E-02	6.17E-02	1.16E-01	1.74E-01	2.11E-01	1.26E-01	1.92E-01	
34	3	1.93E-13	5.59E-12	1.41E-10	3.00E-09	5.18E-08	7.08E-07	7.60E-06	6.36E-05	4.15E-04	2.11E-03	8.33E-03	2.57E-02	6.22E-02	1.20E-01	1.86E-01	2.44E-01	2.79E-01	
35	3	4.00E-15	1.49E-13	4.84E-12	2.92E-10	5.13E-09	7.07E-08	7.59E-07	6.36E-06	4.15E-05	2.11E-04	8.35E-03	2.59E-02	6.40E-02	1.28E-01	2.18E-01	2.16E-01	3.16E-01	
36	3	2.23E-01	1.73E-01	1.27E-01	8.71E-02	5.10E-02	5.56E-02	3.26E-02	1.74E-02	8.36E-03	3.62E-03	1.41E-03	4.96E-04	1.57E-04	4.54E-05	1.20E-05	2.95E-06	6.80E-07	
37	3	2.11E-01	1.82E-01	1.50E-01	1.15E-01	8.20E-02	5.37E-02	3.20E-02	1.72E-02	8.34E-03	3.63E-03	1.42E-03	5.05E-04	1.63E-04	4.82E-05	1.32E-05	3.41E-06	8.31E-07	
38	3	1.79E-01	1.73E-01	1.51E-01	1.36E-01	8.08E-02	5.72E-02	3.27E-02	1.71E-02	8.33E-03	3.68E-03	1.43E-03	5.10E-04	1.73E-04	5.32E-05	1.53E-05	3.51E-06	8.41E-07	
39	3	1.30E-01	1.46E-01	1.															

453 **Table 2-S.** Input modal composition mass fractions (by columns) in the nucleation mode and  
454 composition standard deviation for involatile core of 5%.

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		modal composition																	
$\sigma$		$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
479	1	5.13E-01	2.31E-01	4.88E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.55E-15	9.25E-19	6.93E-23	1.91E-27	1.93E-32	7.20E-38	9.91E-44	5.29E-50	1.32E-56	
480		3.11E-01	3.81E-01	2.19E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.55E-15	9.25E-19	6.93E-23	1.91E-27	1.93E-32	7.23E-38	1.05E-43	7.12E-50	
481		6.95E-02	2.31E-01	3.61E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.55E-15	9.25E-19	6.93E-23	1.92E-27	1.94E-32	7.65E-38	1.41E-43	
482		5.70E-03	5.16E-02	2.19E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.55E-15	9.25E-19	6.93E-23	1.92E-27	2.05E-32	1.03E-37	
483		1.72E-04	4.24E-03	4.88E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.55E-15	9.25E-19	6.96E-23	2.03E-27	2.76E-32	
484		1.91E-06	1.28E-04	4.01E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.55E-15	9.29E-19	7.36E-23	2.73E-27	
485		7.82E-09	1.42E-06	1.21E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.57E-15	9.83E-19	9.90E-23	
486		1.18E-11	5.81E-09	1.34E-04	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.47E-09	8.22E-12	4.83E-15	1.32E-18	
487		6.50E-15	8.73E-12	5.49E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.81E-09	8.73E-12	6.50E-15	
488		1.32E-18	4.83E-15	8.26E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.20E-04	1.34E-06	5.81E-09	1.18E-11	
489		9.90E-23	9.83E-19	4.57E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	3.99E-03	1.21E-04	1.42E-06	7.82E-09	
490		2.73E-27	7.36E-23	9.29E-19	4.55E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.86E-02	4.01E-03	1.28E-04	1.91E-06	
491		2.76E-32	2.03E-27	6.96E-23	9.25E-19	4.55E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.18E-01	4.88E-02	4.24E-03	1.72E-04	
492		1.03E-37	2.05E-32	1.92E-27	6.93E-23	9.25E-19	4.55E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.59E-01	2.19E-01	5.16E-02	5.70E-03	
493		1.41E-43	7.65E-38	1.94E-32	1.91E-27	6.93E-23	9.25E-19	4.55E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.18E-01	3.61E-01	2.31E-01	6.95E-02	
494		7.12E-50	1.05E-43	7.23E-38	1.93E-32	1.91E-27	6.93E-23	9.25E-19	4.55E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.86E-02	2.19E-01	3.81E-01	3.11E-01	
495		1.32E-56	5.29E-50	9.91E-44	7.20E-38	1.93E-32	1.91E-27	6.93E-23	9.25E-19	4.55E-15	8.22E-12	5.47E-09	1.34E-06	2.10E-04	3.99E-03	4.88E-02	2.31E-01	5.13E-01	
496	3	$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
497		2.11E-01	1.64E-01	1.20E-01	8.25E-02	5.27E-02	3.09E-02	1.64E-02	7.92E-03	3.43E-03	1.34E-03	4.70E-04	1.49E-04	4.30E-05	1.14E-05	2.80E-06	6.44E-07	1.41E-07	
498		2.00E-01	1.73E-01	1.42E-01	1.09E-01	7.77E-02	5.09E-02	3.03E-02	1.63E-02	7.90E-03	3.44E-03	1.35E-03	4.78E-04	1.54E-04	4.57E-05	1.25E-05	3.23E-06	7.87E-07	
499		1.69E-01	1.64E-01	1.50E-01	1.29E-01	1.03E-01	7.51E-02	5.00E-02	3.00E-02	1.63E-02	7.92E-03	3.47E-03	1.37E-03	4.95E-04	1.64E-04	5.03E-05	1.45E-05	3.94E-06	
500		1.28E-01	1.38E-01	1.42E-01	1.36E-01	1.21E-01	9.91E-02	7.37E-02	4.95E-02	1.02E-02	1.63E-02	7.99E-03	3.53E-03	1.42E-03	5.26E-04	1.80E-04	5.80E-05	1.77E-05	
501		8.69E-02	1.05E-01	1.20E-01	1.29E-01	1.28E-01	1.17E-01	9.73E-02	7.31E-02	4.94E-02	1.00E-02	1.64E-02	8.13E-03	3.66E-03	1.51E-03	5.79E-04	2.08E-04	7.09E-05	
502		5.27E-02	7.11E-02	9.09E-02	1.09E-01	1.21E-01	1.24E-01	1.15E-01	9.65E-02	7.29E-02	4.95E-02	1.24E-02	8.20E-03	3.70E-03	1.52E-03	6.05E-02	3.13E-02	1.32E-02	
503		8.08E-08	8.62E-07	8.02E-06	6.26E-05	3.97E-04	2.00E-03	7.89E-03	2.43E-02	5.83E-02	1.09E-01	1.59E-01	1.80E-01	1.60E-01	1.13E-01	6.50E-02	3.04E-02	1.32E-02	
504		4.56E-09	6.25E-08	7.46E-07	7.48E-06	6.09E-05	3.94E-04	2.00E-03	7.89E-03	2.43E-02	5.83E-02	1.09E-01	1.59E-01	1.82E-01	1.65E-01	1.21E-01	7.51E-02	4.05E-02	
505		2.00E-10	3.52E-09	5.40E-08	6.96E-07	7.28E-06	6.04E-05	3.93E-04	1.99E-03	7.89E-03	2.43E-02	5.83E-02	1.09E-01	1.59E-01	1.87E-01	1.77E-01	1.40E-01	9.72E-02	
506		6.85E-12	1.55E-10	3.05E-09	5.04E-08	6.77E-07	7.21E-06	6.03E-05	3.93E-04	1.99E-03	7.89E-03	2.43E-02	5.84E-02	1.10E-01	1.65E-01	2.00E-01	2.04E-01	1.82E-01	
507		1.83E-13	5.30E-12	1.34E-10	2.84E-09	4.90E-08	6.71E-07	7.20E-06	6.02E-05	3.93E-04	1.99E-03	7.89E-03	2.44E-02	5.90E-02	1.13E-01	1.77E-01	2.31E-01	2.64E-01	
508		3.79E-15	1.41E-13	4.58E-12	1.25E-10	2.77E-09	4.86E-08	6.69E-07	7.19E-06	6.02E-05	3.93E-04	2.00E-03	7.91E-03	2.46E-02	6.06E-02	1.21E-01	2.04E-01	2.99E-01	
509	3	$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$	
510		2.11E-01	1.64E-01	1.20E-01	8.25E-02	5.27E-02	3.09E-02	1.64E-02	7.92E-03	3.43E-03	1.34E-03	4.70E-04	1.49E-04	4.30E-05	1.14E-05	2.80E-06	6.44E-07	1.41E-07	
511		2.06E-02	4.31E-02	6.16E-02	8.25E-02	5.03E-02	3.09E-02	1.64E-02	7.92E-03	3.43E-03	1.34E-03	4.70E-04	1.49E-04	4.57E-05	1.25E-05	3.23E-06	7.87E-07		
512		1.28E-02	2.34E-02	3.74E-02	5.59E-02	7.77E-02	9.91E-02	1.15E-01	1.20E-02	1.14E-01	9.65E-02	7.37E-02	5.09E-02	3.19E-02	1.84E-02	9.85E-03	4.24E-03	1.92E-03	
513		6.04E-03	1.14E-02	2.03E-02	3.39E-02	5.27E-02	7.51E-02	9.73E-02	1.14E-01	1.20E-02	1.14E-01	9.73E-02	7.51E-02	5.27E-02	3.39E-02	2.03E-02	1.14E-02	6.04E-03	
514		2.35E-03	4.94E-03	9.85E-03	1.87E-02	3.19E-02	5.09E-02	7.37E-02	9.63E-02	1.14E-01	1.20E-02	1.14E-01	9.73E-02	7.51E-02	5.27E-02	3.39E-02	2.34E-02	1.39E-02	
515		8.17E-04	1.92E-03	2.48E-03	4.89E-03	1.73E-02	3.09E-02	5.00E-02	7.31E-02	9.63E-02	1.14E-01	1.22E-02	1.17E-01	1.03E-01	8.25E-02	6.16E-02	4.31E-02	2.86E-02	
516		2.54E-04	6.68E-04	1.66E-03	3.89E-03	8.42E-03	1.67E-02	3.03E-02	4.95E-02	7.29E-02	9.65E-02	1.15E-01	1.24E-02	1.16E-01	1.21E-01	1.09E-01	9.09E-02	7.11E-02	
517		7.09E-05	2.08E-04	5.79E-04	1.51E-03	3.66E-03	8.13E-03	1.64E-02	3.00E-02	4.94E-02	7.31E-02	9.73E-02	1.17E-01	1.28E-01	1.29E-01	1.20E-01	1.05E-01	8.69E-02	
518		1.77E-05	5.80E-05	1.80E-04	5.26E-04	1.42E-03	3.53E-03	7.99E-03	1.63E-02	3.00E-02	4.95E-02	7.37E-02	9.73E-02	1.21E-01	1.36E-01	1.42E-01	1.38E-01	1.28E-01	
519		3.94E-06	1.45E-05	5.03E-05	1.64E-04	4.95E-04	1.37E-03	2.47E-03	7.92E-03	1.63E-02	3.00E-02	4.96E-02	7.18E-02	9.73E-02	1.21E-01	1.36E-01	1.46E-01	1.39E-01	
520		7.87E-07	2.32E-06	1.25E-05	4.57E-05	1.54E-04	4.78E-04	1.35E-03	2.44E-03	7.93E-03	1.63E-02	3.02E-02	4.96E-02	7.18E-02	9.77E-02	1.22E-01	1.37E-01	2.00E-01	
521		1.41E-07	6.44E-07																

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506 **Table 3-S.** Input modal composition mass fractions (by columns) in the nucleation mode and  
507 composition standard deviation for involatile core of 10%.

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$\sigma$	modal composition																
1	$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$
532	5.70E-02	2.57E-02	5.42E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.13E-13	5.05E-16	1.03E-19	7.69E-24	2.12E-28	2.15E-33	8.00E-39	1.10E-44	5.87E-51	1.47E-57
3.46E-02	4.24E-02	2.43E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.13E-13	5.05E-16	1.03E-19	7.69E-24	2.12E-28	2.15E-33	8.04E-39	1.16E-44	7.91E-51	
7.72E-03	2.57E-02	4.01E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.13E-13	5.05E-16	1.03E-19	7.69E-24	2.12E-28	2.16E-33	8.50E-39	1.57E-44	
6.34E-04	5.73E-03	2.43E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.13E-13	5.05E-16	1.03E-19	7.70E-24	2.13E-28	2.28E-33	1.14E-38	
1.91E-05	4.71E-04	5.42E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.13E-13	5.05E-16	1.03E-19	7.73E-24	2.25E-28	3.07E-33	
2.13E-07	1.42E-05	4.45E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.13E-13	5.05E-16	1.03E-19	8.17E-24	3.03E-28	
8.69E-10	1.58E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.14E-13	5.08E-16	1.09E-19	1.10E-23	
1.31E-12	6.45E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.08E-10	9.18E-13	5.37E-16	1.47E-19	
7.22E-16	9.70E-13	6.10E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.10E-10	9.70E-13	7.22E-16	
1.47E-19	5.37E-16	9.18E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.49E-07	6.45E-10	1.31E-12	
1.10E-23	1.09E-19	5.08E-16	9.14E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.43E-04	1.34E-05	1.58E-07	8.69E-10	
3.03E-28	8.17E-24	1.03E-19	5.05E-16	9.13E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.40E-03	4.45E-04	1.42E-05	2.13E-07	
3.07E-33	2.25E-28	7.73E-24	1.03E-19	5.05E-16	9.13E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.42E-02	5.42E-03	4.71E-04	1.91E-05	
1.14E-38	2.28E-33	2.13E-28	7.70E-24	1.03E-19	5.05E-16	9.13E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	3.99E-02	2.43E-02	5.73E-03	6.34E-04	
1.57E-44	8.50E-39	2.16E-33	2.12E-28	7.69E-24	1.03E-19	5.05E-16	9.13E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.42E-02	4.01E-02	2.57E-02	7.72E-03	
7.91E-51	1.16E-44	8.04E-39	2.15E-33	2.12E-28	7.69E-24	1.03E-19	5.05E-16	9.13E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.40E-03	2.43E-02	4.24E-02	3.46E-02	
1.47E-57	5.87E-51	1.10E-44	8.00E-39	2.15E-33	2.12E-28	7.69E-24	1.03E-19	5.05E-16	9.13E-13	6.08E-10	1.49E-07	1.34E-05	4.43E-04	5.42E-03	2.57E-02	5.70E-02	
2	$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$
537	3.33E-02	2.27E-02	1.35E-02	6.74E-03	2.73E-03	8.79E-04	2.22E-04	4.36E-05	6.69E-06	7.99E-07	7.44E-08	5.40E-09	3.07E-10	1.39E-11	5.09E-13	1.57E-14	4.21E-16
2.94E-02	2.57E-02	1.96E-02	1.26E-02	6.55E-03	2.71E-03	8.77E-04	2.22E-04	4.36E-05	6.69E-06	8.00E-07	7.45E-08	5.45E-09	3.16E-10	1.49E-11	5.89E-13	2.03E-14	
2.02E-02	2.27E-02	2.22E-02	1.83E-02	1.22E-02	6.49E-03	2.70E-03	8.76E-04	2.22E-04	4.36E-05	6.69E-06	8.01E-07	7.52E-08	5.60E-09	3.39E-10	1.72E-11	7.62E-13	
1.08E-02	1.56E-02	1.96E-02	2.07E-02	1.78E-02	1.21E-02	6.48E-03	2.70E-03	8.76E-04	2.22E-04	4.37E-05	6.71E-06	8.08E-07	7.73E-08	6.00E-09	3.92E-10	2.23E-11	
4.50E-03	8.35E-03	1.35E-02	1.83E-02	2.02E-02	1.77E-02	1.21E-02	6.48E-03	2.70E-03	8.76E-04	2.22E-04	4.38E-05	6.77E-06	8.31E-07	8.29E-08	6.94E-09	5.07E-10	
1.46E-03	3.49E-03	7.22E-03	1.26E-02	1.78E-02	2.00E-02	1.76E-02	1.21E-02	6.48E-03	2.70E-03	8.76E-04	2.22E-04	4.41E-05	6.96E-06	8.91E-07	9.58E-08	8.98E-09	
3.69E-04	1.13E-03	3.01E-03	6.74E-03	1.22E-02	1.77E-02	2.00E-02	1.76E-02	1.21E-02	6.48E-03	2.70E-03	8.79E-04	2.24E-04	4.54E-05	7.46E-06	1.03E-06	1.24E-07	
7.28E-05	2.86E-04	9.77E-04	2.81E-03	6.55E-03	1.21E-02	1.76E-02	1.99E-02	1.21E-02	6.48E-03	2.71E-03	8.87E-04	2.30E-04	4.87E-05	8.63E-06	1.33E-06		
1.12E-05	5.62E-05	2.47E-04	9.11E-04	2.73E-03	6.49E-03	1.21E-02	1.76E-02	1.99E-02	1.21E-02	6.49E-03	2.73E-03	9.11E-04	2.47E-04	5.62E-05	1.12E-05		
1.33E-06	8.63E-06	4.87E-05	2.30E-04	8.87E-04	2.71E-03	6.48E-03	1.21E-02	1.76E-02	1.99E-02	1.21E-02	6.55E-03	2.81E-03	9.77E-04	2.86E-04	7.28E-05		
1.24E-07	1.03E-07	7.46E-06	4.54E-05	2.24E-04	8.79E-04	2.70E-03	6.48E-03	1.21E-02	1.76E-02	2.00E-02	1.77E-02	1.22E-02	6.74E-03	3.01E-03	1.13E-03	3.69E-04	
8.98E-09	9.58E-09	8.91E-07	6.96E-06	4.41E-05	2.22E-04	8.77E-04	2.70E-03	6.48E-03	1.21E-02	1.76E-02	2.00E-02	1.78E-02	1.26E-02	7.22E-03	3.48E-03	1.46E-03	
5.07E-10	6.94E-09	8.29E-08	8.31E-07	6.77E-06	4.38E-05	2.22E-04	8.76E-04	2.70E-03	6.48E-03	1.21E-02	1.77E-02	2.02E-02	1.83E-02	1.35E-02	8.35E-03	4.50E-03	
2.23E-11	3.92E-11	10.60E-10	6.00E-09	7.73E-08	8.08E-07	6.71E-06	4.37E-05	2.22E-04	8.76E-04	2.70E-03	6.48E-03	1.21E-02	1.78E-02	2.07E-02	1.96E-02	1.56E-02	
7.62E-13	1.72E-11	3.39E-10	5.60E-09	7.52E-08	8.01E-07	6.69E-06	4.36E-05	2.22E-04	8.76E-04	2.70E-03	6.49E-03	1.22E-02	1.82E-02	2.22E-02	2.02E-02		
2.03E-14	5.89E-13	1.49E-11	3.16E-10	5.45E-09	7.45E-08	8.00E-07	6.69E-06	4.36E-05	2.22E-04	8.77E-04	2.71E-03	6.55E-03	1.26E-02	1.96E-02	2.57E-02	2.94E-02	
4.21E-16	1.57E-14	5.09E-13	1.39E-11	3.07E-10	5.40E-09	7.44E-08	7.99E-07	6.69E-06	4.36E-05	2.22E-04	8.79E-04	2.73E-03	6.74E-03	1.35E-02	2.27E-02	3.33E-02	
3	$C_{16}H_{34}$	$C_{17}H_{36}$	$C_{18}H_{38}$	$C_{19}H_{40}$	$C_{20}H_{42}$	$C_{21}H_{44}$	$C_{22}H_{46}$	$C_{23}H_{48}$	$C_{24}H_{50}$	$C_{25}H_{52}$	$C_{26}H_{54}$	$C_{27}H_{56}$	$C_{28}H_{58}$	$C_{29}H_{60}$	$C_{30}H_{62}$	$C_{31}H_{64}$	$C_{32}H_{66}$
542	2.35E-02	1.82E-02	1.33E-02	9.17E-03	5.85E-03	3.43E-03	1.83E-03	8.80E-04	3.82E-04	1.49E-04	5.22E-05	1.66E-05	4.78E-06	1.26E-06	3.11E-07	7.16E-08	1.56E-08
2.22E-02	1.92E-02	1.57E-02	1.21E-02	8.63E-03	5.65E-03	3.37E-03	1.81E-03	8.78E-04	3.82E-04	1.50E-04	5.32E-05	1.71E-05	5.07E-06	1.39E-06	3.59E-07	8.75E-08	
1.88E-02	1.82E-02	1.66E-02	1.43E-02	1.14E-02	8.34E-03	5.55E-03	3.34E-03	1.81E-03	8.80E-04	3.86E-04	1.53E-04	5.50E-05	1.82E-05	5.58E-06	1.61E-06	4.38E-07	
1.42E-02	1.54E-02	1.57E-02	1.51E-02	1.35E-02	8.19E-03	5.50E-03	3.33E-03	1.81E-03	8.87E-04	3.93E-04	1.58E-04	5.85E-05	2.00E-05	6.44E-06	1.96E-06		
9.65E-03	1.17E-02	1.33E-02	1.43E-02	1.42E-02	1.30E-02	1.08E-02	8.12E-03	5.49E-03	3.34E-03	1.83E-03	9.04E-04	4.07E-04	1.68E-04	6.44E-05	2.31E-05	7.87E-06	
5.85E-03	7.90E-03	1.01E-02	1.21E-02	1.35E-02	1.37E-02	1.20E-02	8.12E-03	5.40E-03	3.37E-03	1.86E-03	9.36E-04	4.32E-04	1.85E-04	7.43E-05	2.83E-05		
3.18E-03	4.79E-03	6.84E-03	9.17E-03	1.14E-02	1.30E-02	1.27E-02	1.07E-02	8.10E-03	5.50E-03	3.37E-03	1.86E-03	9.36E-04	4.32E-04	1.85E-04	7.43E-05	2.83E-05	
1.54E-03	2.60E-03	4.15E-03	6.22E-03	8.63E-03	1.01E-02	1.28E-02	1.34E-02	1.26E-02	1.07E-02	8.12E-03	5.55E-03	3.43E-03	1.93E-03	9.94E-04	4.76E-04	2.13E-04	
6.71E-04	2.16E-03	2.25E-03	3.77E-03	5.85E-03	8.34E-03	1.08E-02	1.27E-02	1.34E-02	1.27E-02	8.24E-03	5.85E-03	3.77E-03	2.25E-03	6.71E-04			
2.61E-04	5.49E-04	1.09E-03	2.05E-03	3.55E-03	5.65E-03	8.19E-03	1.07E-02	1.26E-02	1.34E-02	1.28E-02	8.63E-03	6.22E-03	4.15E-03	2.60E-03	1.54E-03		

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558 **Table 4-S.** Input modal composition mass fractions (by columns) in the Aitken mode and

559 composition standard deviation for involatile core of 90%.

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584	n-alkanes	Chickos&Lipkind $C_nH_{(2n+2)}$	EPI Suite 2008	A) Nannoolal et al 2008 boiling point a      b      c	B) Myrdal and Yalkowsky 1997 boiling point a      b      c	Co) Compernolle et al 2011 for all boiling points
585	n					
	16		9.29E-001	2.87E-001 6.63E-001 5.38E-001	1.39E-001 3.46E-001 2.75E-001	3.05E-001
586	17		4.32E-001	6.85E-002 2.45E-001 2.06E-001	3.14E-002 1.24E-001 1.03E-001	9.98E-002
	18		1.95E-001	1.54E-002 9.22E-002 7.91E-002	6.74E-003 4.55E-002 3.86E-002	3.27E-002
587	19		8.97E-002	3.23E-003 3.54E-002 3.04E-002	1.38E-003 1.73E-002 1.47E-002	1.07E-002
	20		4.13E-002	6.33E-004 1.39E-002 1.17E-002	2.70E-004 6.76E-003 5.61E-003	3.50E-003
	21	6.93E-004	1.89E-002	1.16E-004 5.60E-003 4.47E-003	5.03E-005 2.73E-003 2.16E-003	1.15E-003
588	22	2.09E-004	9.23E-003	1.97E-005 2.26E-003 1.71E-003	8.94E-006 1.11E-003 8.35E-004	3.75E-004
	23	6.95E-005	4.73E-003	3.10E-006 8.86E-004 6.52E-004	1.52E-006 4.45E-004 3.25E-004	1.23E-004
589	24	2.31E-005	2.26E-003	4.50E-007 3.39E-004 2.48E-004	2.46E-007 1.75E-004 1.27E-004	4.01E-005
	25	8.51E-006	1.28E-002	6.01E-008 1.26E-004 9.38E-005	3.81E-008 6.71E-005 4.97E-005	1.31E-005
	26	2.83E-006	7.02E-004	7.37E-009 4.58E-005 3.53E-005	5.64E-009 2.53E-005 1.95E-005	4.30E-006
590	27	1.15E-006	1.31E-004	8.25E-010 1.61E-005 1.32E-005	7.97E-010 9.36E-006 7.68E-006	1.41E-006
	28	3.14E-007	2.06E-004	8.40E-011 5.53E-006 4.94E-006	1.08E-010 3.39E-006 3.03E-006	4.61E-007
591	29	1.05E-007	1.27E-004	7.74E-012 1.84E-006 1.83E-006	1.39E-011 1.20E-006 1.20E-006	1.51E-007
	30	3.48E-008	7.49E-005	6.44E-013 5.96E-007 6.75E-007	1.72E-012 4.20E-007 4.74E-007	4.93E-008
	31	1.16E-008	4.54E-005	4.81E-014 1.87E-007 2.47E-007	2.03E-013 1.43E-007 1.88E-007	1.61E-008
592	32	3.49E-009	2.66E-005	3.20E-015 5.70E-008 9.01E-008	2.29E-014 4.80E-008 7.43E-008	5.28E-009

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595 **Table 5-S.** Vapour pressure data at 298 K from different sources corresponding to Figure 2 in the  
 596 main manuscript. a, b, and c refer to the boiling point of Joback and Reid (1987), Stein and  
 597 Brown (1994) and Nannoolal et al. (2004), respectively. A-a, B-c and Co are used in this study.

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609	compound	vapour
610	C <sub>16</sub> H <sub>34</sub>	6.42 (3.62)
611	C <sub>17</sub> H <sub>36</sub>	9.32 (4.31)
612	C <sub>18</sub> H <sub>38</sub>	9.36 (4.41)
613	C <sub>19</sub> H <sub>40</sub>	9.74 (4.09)
614	C <sub>20</sub> H <sub>42</sub>	8.35 (3.59)
615	C <sub>21</sub> H <sub>44</sub>	6.20 (3.06)
616	C <sub>22</sub> H <sub>46</sub>	3.97 (1.98)
617	C <sub>23</sub> H <sub>48</sub>	2.32 (1.25)
618	C <sub>24</sub> H <sub>50</sub>	1.59 (1.79)
619	C <sub>25</sub> H <sub>52</sub>	1.20 (0.52)
620	C <sub>26</sub> H <sub>54</sub>	1.00 (0.50)
621	C <sub>27</sub> H <sub>56</sub>	1.28 (0.53)
622	C <sub>28</sub> H <sub>58</sub>	1.03 (0.53)
623	C <sub>29</sub> H <sub>60</sub>	1.24 (0.53)
624	C <sub>30</sub> H <sub>62</sub>	0.80 (0.38)
625	C <sub>31</sub> H <sub>64</sub>	0.77 (0.30)
626	C <sub>32</sub> H <sub>66</sub>	0.42 (0.18)

627     **Table 6-S.** Gas-phase concentrations used in the model. Numbers in parenthesis show the  
 628     standard deviation of the measurements. Unit, ng m<sup>-3</sup>.

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