





1 throughout the atmospheric CBL, this capability being combined with the one to also measure daytime  
2 profiles of temperature fluctuations up to the fourth order.

3 For the considered case study, which represents a well-mixed and quasi-stationary CBL, the mean  
4 boundary layer height is found to be  $1290 \pm 77$  m a.g.l. Values of the integral scale for water vapour and  
5 temperature fluctuations at the top of the CBL are in the range of 70-125 s and 75-225 s, respectively;  
6 these values are much larger than the temporal resolution of the measurements (10 s), which testifies  
7 that the temporal resolution considered for the measurements is sufficiently high to resolve turbulence  
8 processes down to the inertial sub-range and consequently resolve the major part of the turbulent  
9 fluctuations. Peak values of all moments are found in the interfacial layer in the proximity of the top of  
10 the CBL. Specifically, water vapour and temperature second-order moment (variance) has a maximum  
11 value of  $0.29 \text{ g}^2\text{kg}^{-2}$  and  $0.26 \text{ K}^2$ , respectively, water vapour and temperature third-order moment has a  
12 peak value of  $0.156 \text{ g}^3\text{kg}^{-3}$  and  $-0.067 \text{ K}^3$ , respectively, while water vapour and temperature fourth-order  
13 moment has a maximum value of  $0.28 \text{ g}^4\text{kg}^{-4}$  and  $0.24 \text{ K}^4$ , respectively. Water vapour and temperature  
14 kurtosis have values of  $\sim 3$  in the entrainment zone, which indicate normally distributed humidity and  
15 temperature fluctuations. Reported values of the higher-order moments result to be in good agreement  
16 with previous measurements at different locations, thus providing confidence on the possibility to use  
17 them for turbulence parameterization in weather and climate models.

18 In the determination of the temperature profiles, particular care was dedicated to minimize potential  
19 effects associated with elastic signal leakage in the rotational Raman signals. For this purpose, a specific  
20 algorithm was defined and tested to identify and remove signal leakages and to assess the residual  
21 systematic uncertainty affecting temperature measurements after correction. The application of this  
22 approach confirms that for the present Raman lidar system the leakage factor keeps constant with time,  
23 and consequently an appropriate assessment of its constant value allows for a complete removal of the  
24 leaking elastic signal from the rotational Raman lidar signals at any time (with a residual error on  
25 temperature measurements after correction not exceeding 0.16 K).

26

## 27 **1 Introduction**

28 Water vapour and temperature are key meteorological variables playing a major role in the definition of  
29 the thermodynamic state of the atmosphere (Wulfmeyer *et al.* 2015). This is particularly true in the  
30 convective boundary layer, the unstably stratified boundary layer developing in the lower troposphere  
31 during the day, dominated by buoyant turbulence generation as a result of strong surface solar heating  
32 (Garratt, 1992). Entrainment processes at the top of the CBL are controlled by temperature (capping)



1 inversion in the interfacial layer, ultimately influencing the vertical transport of humidity in the free  
2 troposphere (Mahrt 1991; Sorbjan 1996; Sullivan *et al.* 1998, Wulfmeyer *et al.* 2016). Accurate  
3 measurements of water vapour and temperature from the surface to the entrainment zone at the top of  
4 the CBL are therefore essential for improving weather forecasting (Dierer *et al.*, 2009), reanalyses  
5 (Bengtsson *et al.*, 2004), and regional climate simulations (Milovac *et al.* 2016).

6 Measurements of higher-order moments of moisture and temperature fluctuations provide unique and  
7 essential information for the characterization of turbulent processes within the convective boundary  
8 layer (CBL). Water vapour and temperature variances are key variables in turbulence, convection, and  
9 cloud parameterizations considered in weather and climate models (e.g., Stull, 1988; Berg and Stull,  
10 2005; Gustafson and Berg, 2007). Within the CBL, water vapour variance increases with height,  
11 achieving a maximum at the top of the CBL due to the mixing of moist air in the updrafts with drier air  
12 from above the CBL (Wulfmeyer 1999a,b; Kiemle *et al.*, 2007). The water vapour variance profile can  
13 also be used to estimate the CBL height and characterize its internal structure by exploiting the tracing  
14 capabilities of atmospheric water vapour (among others, Wulfmeyer *et al.*, 2010; Turner *et al.*, 2014a,b).  
15 Furthermore, water vapour skewness and kurtosis are found to be characterized by an appreciable  
16 vertical variability within the CBL, which changes patterns during different phases of the CBL  
17 evolution (Couvreaux *et al.*, 2005, 2007).

18 Atmospheric turbulent processes within the CBL have been studied for decades based on the use of in-  
19 situ sensors (among others, Lenschow and Kristensen, 1985, Kalthoff *et al.*, 2011). However, lidar  
20 systems, on the basis of their capability to provide high space and time resolution and accurate  
21 measurements of atmospheric water vapour and temperature, have nowadays reached the level of  
22 maturity needed to investigate the relevant atmospheric processes and enable measurements of turbulent  
23 variables within the CBL (among others, Eberhard *et al.*, 1989; Frehlich and Cornman, 2002). The  
24 major advantage of the lidar techniques is represented by their capability to characterize turbulent  
25 variables from the proximity of the surface up to interfacial layer and above. Additionally, lidar systems  
26 can be operated from different platforms and, when applied from ground-based platforms, can provide  
27 excellent long-term statistics. This is also necessary for reducing sampling error which are usually  
28 larger for ground-based than for airborne measurements.

29 For the characterization of water vapour turbulent fluctuations, the DIAL and Raman lidar techniques  
30 have demonstrated to have the time and vertical resolution, as well as the accuracy, needed to  
31 characterize turbulent processes within the CBL (Wulfmeyer, 1999a,b; Kiemle *et al.*, 2007; Wulfmeyer  
32 *et al.*, 2010, Turner *et al.* 2014a; Muppa *et al.*, 2016). Profiles of second- to fourth-order moments of



1 turbulent temperature fluctuations in the convective boundary layer have been reported for the first time  
2 by Behrendt *et al.* (2015) based on the application of the rotational Raman lidar (RRL) technique  
3 (Behrendt and Reichardt, 2000; Behrendt *et al.*, 2002; Di Girolamo *et al.*, 2004, 2006; Behrendt, 2005;  
4 Radlach *et al.*, 2008; Hammann *et al.*, 2015a, Hammann and Behrendt, 2015). The present  
5 measurements have been carried out by the Raman lidar system *BASIL*, exploiting its capability to  
6 perform high-resolution and accurate measurements of atmospheric temperature and water vapour, both  
7 in daytime and night-time, based on the application of the rotational and vibrational Raman lidar  
8 techniques in the UV, respectively (Di Girolamo *et al.*, 2004, 2006, 2009a; 2016a, Bhawar *et al.*, 2011).  
9 These measurements allow for the determination of the vertical profiles of the turbulent fluctuation of  
10 these two atmospheric variables up to the fourth order throughout the atmospheric CBL in daytime with  
11 limited uncertainty. Results from this system are obtained based on the application of the approach  
12 introduced by Lenschow *et al.* (2000), which allows for estimating higher-order moments of turbulent  
13 variables in the presence of noisy data. Measurements of water vapour turbulent fluctuations by Raman  
14 lidar had been demonstrated by Wulfmeyer *et al.* (2010), based on the use of the data from the  
15 Atmospheric Radiation Measurement (ARM) Raman lidar. However, these authors came to the  
16 conclusion that the noise errors affecting the ARM Raman lidar water vapour mixing ratio  
17 measurements for the considered case study were too large to derive fourth-order moments with  
18 sufficient accuracy. Thus, to the best of our knowledge, *BASIL* is the first Raman lidar with a  
19 demonstrated capability to accurately retrieve simultaneous daytime profiles of water vapour and  
20 temperature turbulent fluctuations up to the fourth order throughout the atmospheric CBL. The main  
21 aim of this paper is to provide a detailed characterization of the performances of the Raman lidar *BASIL*  
22 and demonstrate that profiles of turbulent variables can be determined throughout the CBL with  
23 sufficient accuracy. For this purpose measurements from the High Definition Clouds and Precipitation  
24 for Climate Prediction (HD(CP)2) Observational Prototype Experiment (HOPE), held in Western  
25 Germany in spring 2013, are considered.

26 The paper outline is the following. Section 2 provides a description of the experimental setup, with  
27 details on the data processing and the error analyses; this section also describes the correction scheme  
28 considered for removing the elastic-signal leakage in the low-quantum number rotational Raman signal  
29 and the uncertainties associated with this approach. Section 3 provides a brief overview on the HOPE  
30 field campaign and illustrates the criteria considered for the selection of the case study; this section also  
31 illustrates the the time-height cross-sections of the water vapour mixing ratio and temperature data  
32 considered for the turbulence analysis, providing remarks on the meteorological conditions occurring  
33 during this period. Section 4 provides a brief description of the methodology considered for the



1 turbulence analysis and illustrates the results achieved in terms of vertical profiles of turbulent variables.  
2 Finally, section 5 summarizes all results and provides some indications for possible future work.

3

## 4 **2 Experimental setup**

### 5 **2.1 System Set up and derivation of mixing-ratio and temperature profiles**

6 Prior to HOPE, the University of BASILicata Raman lidar system (*BASIL*) underwent a substantial  
7 upgrade aimed to improve its overall performances in terms of measurement precision and vertical and  
8 temporal resolution. These setup modifications will be described in a separate forthcoming paper (Di  
9 Girolamo *et al.*, 2016b). *BASIL* is a ground-based Raman lidar hosted in a transportable sea-tainer. The  
10 major feature of *BASIL* is represented by its capability to perform high-resolution and accurate  
11 measurements of the vertical profiles of atmospheric temperature and water vapour, both in daytime and  
12 night-time, based on the application of the rotational and vibrational Raman lidar techniques in the UV  
13 (Di Girolamo *et al.*, 2004, 2006, 2009a; 2016a, Bhawar *et al.*, 2011). Besides temperature and water  
14 vapour, *BASIL* is also capable of providing measurements of the vertical profiles of particle backscatter  
15 at 354.7, 532 and 1064 nm, particle extinction at 354.7 and 532 nm and particle depolarization at 354.7  
16 and 532 nm (Griaznov *et al.*, 2007; Di Girolamo *et al.*, 2009b, 2012a, 2012b). *BASIL* is built around a  
17 Nd:YAG laser source, equipped with second and third harmonic generation crystals, capable of emitting  
18 pulses at 354.7 nm, 532 nm and 1064 nm, which are simultaneously transmitted in the atmosphere along  
19 the zenith. The receiver includes a large-aperture telescope in Newtonian configuration, with a 45 cm  
20 diameter primary mirror and a focal length of 2.1 m, and two small-aperture telescopes (50 mm  
21 diameter lenses). The radiation collected by the large-aperture telescope is split into eight portions by  
22 means of dichroic or partially reflecting mirrors: specifically, two portions are fed into the detection  
23 channels used for temperature measurements (at 354.3 and 352.9 nm for the low- and high-quantum  
24 number rotational Raman signals,  $P_{Low}(z)$  and  $P_{High}(z)$ , respectively), while two other portions are sent  
25 to the water vapour (at 407.5 nm) and molecular nitrogen Raman channels (at 386.7 nm); corresponding  
26 signals are  $P_{H_2O}(z)$  and  $P_{N_2}(z)$ , respectively, in what follows. Another two portions of the collected  
27 radiation are fed into the 354.7 and 532 nm elastic channels. A fraction of the signal entering the 354.7  
28 nm channel is split into two additional portions to allow the detection of the parallel and cross-polarized  
29 elastic signals, which are used for the determination particle depolarization. Signal selection is  
30 performed by means of narrowband interference filters, whose specifications were defined in Di  
31 Girolamo *et al.* (2004, 2009a).



1 The water vapour mixing ratio  $m$  can be obtained from the power ratio of water vapour to molecular  
2 nitrogen vibrational Raman signals ( $m(z) = K(z) \cdot (P_{H_2O}(z)/P_{N_2}(z))$ ), where  $K(z)$  is a calibration factor  
3 obtained by multiplying several height-dependent correction terms and a height-independent calibration  
4 term (e.g., Whiteman, 2003). The height-dependent correction terms included  $K(z)$  are a differential  
5 transmission term, accounting for the different atmospheric transmission by molecules and aerosols at  
6 the two wavelengths corresponding the water vapour and molecular nitrogen Raman signals, and a term  
7 associated with the use of narrowband interference filters and the consequent temperature dependence  
8 of  $H_2O$  and  $N_2$  Raman scattering signals selected by these filters. The height-independent calibration  
9 factor is finally obtained by the multiplication of the above mentioned signal ratio by the height-  
10 dependent correction terms included  $K(z)$  and the comparison of this quantity with simultaneous and co-  
11 located mixing ratio measurements from different sensors (e.g., from radiosondes, microwave  
12 radiometers, GPS tomography, etc.).

13 Based on the application of the pure rotational Raman lidar technique, atmospheric temperature is  
14 obtained from the power ratio of high-to-low quantum number rotational Raman signals  $Q(T)$  through  
15 the application of the analytical expression:

$$16 \quad Q(z) = P_{HiJ}(z)/P_{LoJ}(z) = \exp(\alpha/T(z) + \beta) \quad (1)$$

17 with  $\alpha$  and  $\beta$  being two calibration constants. Thus:

$$18 \quad T(z) = \frac{\alpha}{\ln[Q(z)] - \beta} \quad (2)$$

19 These two calibration constants can be determined through the comparison of the lidar signal ratio with  
20 simultaneous and co-located temperature measurements from different sensors (again, radiosondes,  
21 microwave radiometers, GPS tomography, etc.). The above considered analytical expression relating  
22  $Q(z)$  to  $T(z)$  is not the only possible expression, but it is probably the simplest and implies the smallest  
23 number of calibration constants. Other more complex analytical expression have been considered in  
24 literature (Behrendt and Reichardt, 2000; Di Girolamo *et al.*, 2004; Behrendt *et al.*, 2015). However, the  
25 systematic error associated with assuming the above calibration function to be valid for a large portion  
26 of the rotational Raman spectrum is found to have a typical amplitude of 0.2 K, which is not relevant for  
27 the purposes of the present study (see Wulfmeyer *et al.*, 2016 for an assessment of the effects of  
28 systematic errors on turbulence measurements).

29 During HOPE, water vapour mixing ratio and temperature measurements by *BASIL* were both  
30 calibrated based on the comparison with simultaneous radiosondes, which were launched from the



1 nearby supersite UHOH-KIT, located in Hambach, approx. 4 km E-SE. Mean calibration coefficients  
2 for both water vapour mixing ratio and temperature measurements were estimated by comparing *BASIL*  
3 and radiosonde profiles for all radiosondes launched at times when *BASIL* was operating (approximately  
4 60 comparisons). The comparisons were carried out in a vertical region with an extent of 1 km located  
5 above the boundary layer. This selection allows for minimizing the air mass differences related to the  
6 physical distance between the lidar and the radiosonde. The variability of the calibration coefficients  
7 was found to be very limited throughout the duration of the filed campaign, with single calibration  
8 values showing very small deviations from the mean values. For example, for what concerns water  
9 vapour measurements, the standard deviation of single calibration values from the mean calibration  
10 coefficient was found to not exceed 5 %.

11 As specified above, *BASIL* underwent an upgrade before HOPE which allowed for obtaining a  
12 substantial improvement of the overall performances in terms of both measurement precision and  
13 vertical and temporal resolution. The upgrade included a modification of the optical layout of the  
14 Nd:YAG laser source, which allowed to achieve a 65 % increase of its emitted power in the UV (from  
15 an original value of 6 W, single pulse energy of 300 mJ @ 20 Hz, to a final value of 10 W, with a single  
16 pulse energy of 500 mJ @ 20 Hz). The upgrade also included the implementation of a new sampling  
17 system (with double signal acquisition mode, i.e. both analog & digital) in some of the measurement  
18 channels allowing to acquire daytime and nighttime lidar signals with a maximum vertical and temporal  
19 resolution of 7.5 m and 1-10 sec, respectively. In signal pre-processing, four adjacent data points are  
20 binned together to reduce statistical fluctuations of the signals, this increasing the vertical step between  
21 adjacent data points to 30 m.

22

## 23 **2.2 Determination of noise errors**

24 In order to characterize the quality of water vapour mixing ratio and temperature measurements, an  
25 accurate assessment of noise error is necessary. Noise error is quantified as the root-square of the noise  
26 variance (i.e. the noise standard deviation). Profiles of noise error affecting water vapour mixing ratio  
27 and temperature measurements are illustrated in figure 1. Specifically, figure 1a illustrates the water  
28 vapour mixing ratio absolute error (expressed in  $\text{g kg}^{-1}$ ), figure 1b illustrates the water vapour mixing  
29 ratio relative error (expressed in %), while figure 1c illustrates the temperature absolute error (expressed  
30 in K). The figure shows the noise error profiles estimated based on the application of the auto-  
31 covariance method (described in detail in sub-section 4.1). More specifically, noise error assessments  
32 have been performed considering two options for temporal and vertical resolution: a higher resolution



1 configuration, with a time resolution of 10 s and a vertical resolution of 90 m and 30 m for water vapour  
2 mixing ratio and temperature, respectively (this is the selection considered for the turbulence  
3 measurements); and a lower resolution configuration, with a time resolution of 150 m and a vertical  
4 resolution of 5 min, which is the selection considered for the data set generated and uploaded to the  
5 HOPE archive (primarily used for verification purposes, process studies and data assimilation). For the  
6 first selection, the statistical error affecting water vapour mixing ratio measurements is smaller than 0.6  
7  $\text{g kg}^{-1}$  (or 50 %) up to 1.4 km, while the statistical error affecting temperature measurements is smaller  
8 than 1 K up to 1.8 km. For the second selection, the statistical error affecting water vapour mixing ratio  
9 measurements is smaller than 0.1  $\text{g kg}^{-1}$  (or 15 %) up to 1.8 km, while the statistical error  
10 affecting temperature measurements is smaller than 0,8 K up to 3 km. The above listed performances of  
11 *BASIL* in terms of water vapour mixing ratio measurements result to be comparable with those reported  
12 for the ARM Raman lidar (Wulfmeyer *et al.*, 2010, also 0.6  $\text{g kg}^{-1}$  at 1.4 km), considering the same time  
13 and vertical resolution. Same is true for the above listed performances of *BASIL* in terms of temperature  
14 measurements, which indicate statistical uncertainties with values similar to those reported for the ARM  
15 Raman lidar (Newsom *et al.*, 2013). The above quantified errors are used to derive - by means of error  
16 propagation - the noise error profiles of the higher-order moments. An overview of these equations is  
17 given in Wulfmeyer *et al.*, (2016).

18 In practice, water vapour mixing ratio and temperature profiles can be derived with different vertical  
19 and temporal resolutions depending on the considered application. Vertical and temporal resolutions can  
20 be traded-off with measurement precision, with random error affecting water vapour mixing ratio and  
21 temperature measurements being inversely proportional to the square root of both vertical and temporal  
22 resolution. Consequently, the consideration of the high temporal and vertical resolutions (10 sec, 30-90  
23 m, respectively) needed for the characterization of turbulence processes translates into a lower  
24 measurement precision (and consequently a larger statistical error). As a result of this, the  
25 corresponding statistical error affecting daytime water vapour mixing ratio and temperature  
26 measurements is smaller than 100 % and 1 K, respectively, up to 2 km (figure 1), these performances  
27 being well suited for lidar measurements finalized to the characterization of turbulent variables.

28 Figure 1 also includes the error profiles obtained with the application of Poisson statistics to signal  
29 photon counts. Signal photon counts are directly measured by the photon counting unit; “virtual” counts  
30 can also be obtained from the signals measured by the analog module (Newsom *et al.*, 2009). In order to  
31 get an estimate of the error affecting water vapour mixing ratio and temperature measurements through  
32 Poisson statistics, it is necessary to first apply Poisson statistics to the photon counts of the individual  
33 lidar signals contributing to the measurements and then, through error propagation, compute the overall





1 error affecting the measured atmospheric variables. The error propagation expression is different for  
 2 water vapour mixing ratio and temperature measurements as different are the analytical expressions  
 3 relating the individual signals to the two measured parameters. For water vapour mixing ratio  
 4 measurements the application of error propagation yields the expression (Di Girolamo *et al.*, 2009a):

$$5 \quad \frac{\Delta x_{H_2O}(z)}{x_{H_2O}(z)} = \sqrt{\frac{P_{H_2O}(z) + bk_{H_2O}}{P_{H_2O}^2(z)} + \frac{P_{N_2}(z) + bk_{N_2}}{P_{N_2}^2(z)}} \quad (3)$$

6 where the terms  $bk_{H_2O}$  and  $bk_{N_2}$  represent the sky background signal (primarily associated with solar  
 7 irradiance) collected in the water vapour and molecular nitrogen channels, respectively. Expression (3)  
 8 provides the relative statistical error (in percent if multiplied for 100), while the absolute statistical error  
 9 can be obtained by multiplying expression (3) for  $x_{H_2O}(z)$ . The mean photon number for the 10 sec  
 10 water vapour and molecular nitrogen vibrational Raman signals,  $P_{H_2O}(z)$  and  $P_{N_2}(z)$ , displayed in  
 11 figure 2, are found to vary featuring a maximum around 800 m of approx. 1500 and 12000 counts,  
 12 respectively, and progressively decreasing down to 0 and approx. 20 counts, respectively, around 10 km  
 13 (after background subtraction). Here the mean photon number is intended as the average of all 10 sec  
 14 signal profiles collected over the period 11:30-13:30 UT on 20 April 2013. Figure 2 also shows the  
 15 mean photon number for the 10 sec 354.7 nm elastic signal,  $P_{354.7}(z)$ , which has a maximum of approx.  
 16 2200 counts around 800 m and progressively decreases down to 2 counts around 10 km.

17 For temperature measurements the application of error propagation yields the expression (Behrendt *et*  
 18 *al.*, 2002, 2015, Di Girolamo *et al.*, 2006, 2009a):

$$19 \quad \Delta T(z) = \frac{\partial T(z)}{\partial R} R(z) \sqrt{\frac{P_{LoJ}(z) + bk_{LoJ}}{P_{LoJ}^2(z)} + \frac{P_{HiJ}(z) + bk_{HiJ}}{P_{HiJ}^2(z)}} \quad (4)$$

20 where the terms  $bk_{LoJ}$  and  $bk_{HiJ}$  represent the sky background signal collected in the low- and high-J  
 21 rotational Raman channels, respectively. The quantity  $\partial T(z)/\partial R$  can be estimated based on the  
 22 application of the calibration procedure mentioned above. The mean photon number for the 10 sec low  
 23 and high quantum number rotational Raman signals,  $P_{LoJ}(z)$  and  $P_{HiJ}(z)$ , also displayed in figure 2, is  
 24 found to vary featuring a maximum of approx. 4500 and 3500 counts, respectively, at 800 m, and  
 25 progressively decreasing down to 8 and 4 counts respectively, around 10 km. Figure 2 also shows the  
 26 temperature sensitivity of RRL measurement technique, i.e. the quantity  $\partial R(z)/\partial T$ , which is found to  
 27 vary between 0,06 K<sup>-1</sup> at surface level to approx. 0,03 K<sup>-1</sup> at 10 km, and the power ratio of high-to-low  
 28 quantum number rotational Raman signals,  $R(z)$ , which is found to vary between approx. 0,8 at surface



1 level to approx. 0,3 at 10 km. The large values of the measurement sensitivity ( $\partial R(z)/\partial T$ ) contribute to  
2 the small random errors affecting the reported temperature measurements.

3 The terms  $bk_{H_2O}$  and  $bk_{N_2}$  in expression (3) and the terms  $bk_{LoJ}$  and  $bk_{HiJ}$  in expression (4) can be  
4 determined considering the photon-counting signals at very high heights, this portion of the signals  
5 being characterized by negligible contribution from laser backscatter photons and being typically  
6 attributable to sky background radiation and intrinsic detector noise, the former being much larger than  
7 the latter, especially for daytime operation. For the reported measurements, values of  $bk_{H_2O}$  and  
8  $bk_{N_2}$  are found to be approx. 11000 and 8000 counts, respectively, while values of  $bk_{LoJ}$  and  $bk_{HiJ}$  are  
9 found to be approx. 200 and 1000 counts, respectively.

10 It is to be noticed that the auto-covariance analysis specifies the total statistical noise, while Poisson  
11 statistics accounts only for its shot noise contribution, i.e. the contribution associated with the discrete  
12 nature of the photons sampled by photon counting devices. Consequently, the application of Poisson  
13 statistics to signal photon counts leads to an underestimation of the total statistical noise (Wulfmeyer *et*  
14 *al.*, 2010, Behrendt *et al.*, 2015). Figure 1 reveals that noise error estimates obtained through the  
15 application of Poisson statistics are in good agreement with estimates obtained through the auto-  
16 covariance approach. Specifically, Poisson statistics accounts for approximately 75 % of the total  
17 statistical noise affecting the measurement of water vapour mixing ratio and temperature. In more detail,  
18 Poisson statistics accounts for 60 to 80 % of the total statistical noise affecting water vapour mixing  
19 measurements, with a mean value of 74.5 %, while it accounts for 60 to 90 % of the total statistical  
20 noise affecting temperature measurements, with a mean value of 78.0 %. This confirms that photon shot  
21 noise represents the main contribution to the total statistical noise, but other statistical error sources,  
22 usually very small, may also contribute.

23 As a result of the above described upgrades, *BASIL* performances in terms of the atmospheric variables  
24 of interest for the purposes of this paper, extrapolated at higher heights based on the application of  
25 Poisson statistics, are as follows. For water vapour mixing ratio measurements, the typical daytime  
26 statistical error (precision) is smaller than 20 % up 3 km and smaller than 100 % up 4.5 km, while the  
27 typical nighttime statistical error is smaller than 2 % up 3 km and smaller than 20 % up 9 km, based on  
28 an integration time of 5 min and a vertical resolution of 150 m. The statistical error  
29 affecting temperature measurements for daytime operation is typically smaller than 0.5 K up to 3 km  
30 (figure 1) and smaller than 1.5 K up to 4.5 km, while for night-time operation is typically smaller  
31 than 0.4 K up to 3 km (figure 1) and smaller than 1 K up to 6.5 km. These error values are consistent



1 with the performances of the ARM water vapour Raman lidar (Wulfmeyer *et al.*, 2010; Turner *et al.*,  
2 2014a).

3

## 4 **2.3 Systematic errors**

### 5 **2.3.1 Time independent systematic errors**

6 In addition to the statistical error, a small systematic error (bias) may affect both water vapour and  
7 temperature measurements. For example, for water vapour measurements, besides a bias (not exceed  
8 5 %) associated with the estimate of the calibration coefficient (resulting from radiosonde biases,  
9 different air masses being sensed by the radiosonde and the lidar), an additional very small bias  
10 (< 1 %) may be associated with the use of narrowband filters and, consequently, the accurate estimate of  
11 the height-dependent correction factor accounting for the temperature dependence of the H<sub>2</sub>O and N<sub>2</sub>  
12 Raman scattering signals selected by these filters, while a 1 % systematic uncertainty may be associated  
13 with the determination of the differential transmission term (Whiteman, 2003). For temperature  
14 measurements, besides a small bias associated with the estimate of the calibration coefficient, an  
15 additional small bias (< 0.2 K) is associated with the assumption of the calibration function (1) to be  
16 valid for the selected portions of the rotational Raman spectrum. It is to be pointed out that, as the above  
17 mentioned systematic error sources are time independent (see Whiteman, 2003, for water vapour  
18 measurements and section 4.2.2 of this paper for temperature measurements), biases can be  
19 substantially removed from water vapour and temperature time-series measurements based on the use of  
20 suitable spectral filters before calculating their fluctuations; consequently, time-independent systematic  
21 errors have a marginal influence on the accuracy of turbulence profiles, especially for a high accuracy  
22 system as ours (see equations A1-A8 in Wulfmeyer *et al.*, 2016).

23

### 24 **2.3.2 Elastic signal leakage in the rotational Raman signals and approach for its removal**

25 Specific check and sensitivity studies have been performed in order to verify the presence and  
26 amplitude of elastic signal leakages in the rotational Raman signals and their potential effect on  
27 temperature measurements. In this respect it is to be pointed out that in the present system set-up the  
28 low- and high-quantum number rotational Raman signals,  $P_{L\omega}(z)$  and  $P_{H\omega}(z)$ , are collected at 354.3  
29 and 352.9 nm, respectively, these wavelengths being very close to the laser emission at 354.7 nm.  
30 Consequently, particular care has to be paid in the definition of the spectral specifications of the  
31 interference filters used for the selection of  $P_{L\omega}(z)$  and  $P_{H\omega}(z)$ , especially for what concerns their



1 blocking at 354.7 nm. This is particularly true for the Lo-J filter, having a central wavelength just 0.4  
2 nm off the excitation wavelength, while it is less for the Hi-J filter, as its central wavelength is 1.8 nm  
3 off the excitation wavelength. The interference filters used in the present system set-up are  
4 characterized by a nominal blocking at 354.7 nm of  $10^{-6}$ - $10^{-7}$ . However, based on measurements carried  
5 out in the presence of clouds, we collected experimental evidence that the effective blocking of our Lo-J  
6 filter is not better than  $10^{-5}$ . For this motivation, in previous field deployments (among others, the  
7 Convective and Orographically-induced Precipitation Study - COPS, Wulfmeyer *et al.*, 2008; Behrendt  
8 *et al.*, 2011), a second narrow-band interference filter was put in cascade to the Lo-J filter, this second  
9 filter having the same center wavelength and pass-band of the Lo-J filter (this latter being 0.2 nm full  
10 width at half maximum), but having a nominal blocking at 354.7 nm of  $10^{-3}$ . The combination of two  
11 filters had been successfully applied before at 532 nm, obtaining undisturbed measurements even in  
12 clouds (Behrendt and Reichardt, 2000). Just recently, the possibility to achieve sufficient blocking at  
13 354.7 nm with only one filter could also be demonstrated based on recent advances achieved in multi-  
14 cavity interference filter technology (Hammann *et al.*, 2015b). The ultimate goal of using two cascading  
15 interference filters was to obtain an overall blocking at 354.7 nm of  $10^{-8}$  or better. However, because of  
16 the very narrow pass-band of the two cascading filters, a perfect superimposition of their transmission  
17 curves was found difficult to achieve. In this respect it is to be specified that a partial superimposition of  
18 the transmission curves of the two filters may determine an even narrower pass-band, ultimately  
19 compromising the filters' capability to select the rotational lines necessary for the temperature  
20 measurements. Additionally, also when a perfect superimposition of the two cascading filters'  
21 transmission curves is achieved, the overall center wavelength transmission is significantly reduced (not  
22 exceeding 15 %, with the transmission of the Lo-J filter being 30 % and the transmission of the second  
23 cascading filter being 50 %); thus, the introduction of the second cascading filter determines an overall  
24 reduction of  $P_{LoJ}(z)$  by 50 % and a consequent reduction in measurement precision.

25 In order to avoid these drawbacks, in recent field deployments the second cascading filter was remove  
26 from the Lo-J channel, fully aware that this would have determined an overall lower blocking at 354.7  
27 nm for the Lo-J interference filter and, consequently, a possible leakage of the 354.7 nm elastic lidar  
28 signal into the Lo-J rotational Raman signal, but also fully aware of the different research efforts, and  
29 corresponding literature papers, dedicated to the definition of approaches to identify and remove elastic  
30 signal leakages from the rotational Raman signals (Behrendt *et al.*, 2002; Su *et al.*, 2013). These authors  
31 demonstrated that elastic signal leakage into the Lo-J rotational Raman signals can be completely  
32 removed if simultaneous and co-located measurements of the elastic signal are available. Behrendt *et al.*  
33 (2002) tested their approach on a rotational Raman lidar operating at 532 nm, while Su *et al.* (2013)



1 applied their approach to a rotational Raman lidar operating at 354.7 nm. At 354.7 nm, the approach  
2 considers the expression:

$$3 \quad P_{LoJ}(z) = P_{LoJ}^{leak}(z) - k T_F P_{354.7}(z) \quad (5)$$

4 with  $P_{LoJ}^{leak}(z)$  being the leaked Lo-J rotational Raman lidar signal,  $P_{LoJ}(z)$  being the effective Lo-J  
5 rotational Raman lidar signal used for the derivation of temperature profiles,  $P_{354.7}(z)$  being the 354.7  
6 nm elastic lidar signal,  $T_F$  being the transmission of neutral density filters (used to attenuate the elastic  
7 signals and avoid signal induced noise effects associated with the low range echoes), and  $k$  being the  
8 leakage factor. Expression (5) specifies that, if the leakage factor is known, the effective Lo-J rotational  
9 Raman signal can be determined from leaked Lo-J rotational Raman signal by simply subtracting the  
10 354.7 nm elastic lidar signal from the latter.

11 In this respect, it is to be specified that the simultaneity and co-location of the measured Lo-J and 354.7  
12 lidar signals is in our case quite a strict requirement, as in fact the signals necessary for the present  
13 turbulence studies are acquired with high vertical and temporal resolution. In our system, the  
14 simultaneity is guaranteed by the use of two distinct acquisition channels, with a common triggering,  
15 included in a single sampling unit. The co-location of the measurements, i.e. the sounding of the same  
16 atmospheric air column, is guaranteed by the use of the same large-aperture telescope for the collection  
17 of the two signals and the proximity of the two detection channels within the optical layout of system.  
18 In this direction, it is also to be specified that the elastic and rotational Raman scattering are stimulated  
19 with the same laser wavelength (354.7 nm) and consequently the radiated air column is the same for the  
20 two measurement channels.

21 An accurate estimate of the leakage factor  $k$  is of paramount importance to remove, or at least minimize,  
22 potential systematic errors associated with any residual elastic signal leakage in the rotational Raman  
23 signals. For this purpose, a modified version of the approach defined by Behrendt *et al.* (2002) was  
24 applied. The approach is based on the selection of a measurement period with clouds, the calculation of  
25  $P_{LoJ}(z)$  for different values of  $k$  and the selection of the value of  $k$  leading to temperature values inside  
26 the cloud best fitting the temperature values from a near-by radiosonde.

27 For this purpose, we selected a 9 min time interval (13:38-13:46 UTC), shortly after the 2-h time period  
28 considered for the turbulence analysis (11:30-13:30 UTC); as a result of this selection, the value of  $k$   
29 determined for this time interval can be effectively used to correct the data in the time interval  
30 considered in the turbulence analysis. The 9 min time interval is characterized by the presence of high-  
31 level clouds (cirrus clouds) extending between 7.9 and 9.8 km, which are not optically thick, with all



1 measured lidar signals extending above the cloud top. This characteristic makes the selected time  
2 interval particularly suited for the estimate of  $k$ . A 9 min time interval was considered in order to  
3 achieve a sufficiently high signal statistics and, consequently, a lower uncertainty in the determination  
4 of the correct value of  $k$  based on the above mentioned best fit procedure. Figure 3 shows the vertical  
5 profiles of  $P_{Lol}^{leak}(z)$ ,  $P_{Hil}(z)$  and  $T_F P_{354.7}(z)$  averaged over the 9 min interval. To better illustrate the  
6 proposed approach, in figure 3 we focused our attention to the vertical interval 6-10 km. The elastic  
7 signal  $P_{354.7}(z)$  reveals the presence of several layers associated with cirrus clouds between 7.9 and 9.8  
8 km, with a peak at 9.3 km. The figure clearly highlights the elastic signal leakage into  $P_{Lol}^{leak}(z)$  in the  
9 height region inside the cloud, while no evidence of elastic signal leakage is present in  $P_{Hil}(z)$  in this  
10 same height region. To apply the best fit procedure the radiosonde launched at 13:00 UTC from the  
11 near-by launching station in Hambach (approx. 4 km E-SE) was considered. Considering an ascent  
12 speed of  $3.5 \text{ m s}^{-1}$ , which is the average speed experienced by the present radiosonde in the height  
13 interval from surface up to 10 km, the radiosonde is expected to cover the 8-10 km height region in the  
14 time interval 13:38-13:46 UTC, which is exactly the time interval considered for the application of our  
15 approach. The value of  $k$  leading to temperature values inside the cloud best fitting the radiosonde  
16 temperature values was found to be 0.91. The best fit procedure considers all data points (approx. 70  
17 points) within the height range where the cirrus cloud is located (7.9 and 9.8 km). This computation was  
18 repeated at different times during the cirrus clouds appearance period (12:22-18:52 UTC), also  
19 considering the data from the additional radiosondes available in this period (i.e. at 15:00 and 17:00  
20 UTC). Results reveal that  $k$  has a constant value of 0.91, with very limited dispersion (0.01) around this  
21 value, i.e.  $k \pm \Delta k = 0.91 \pm 0.01$  (Nocera, 2016). This result demonstrates that laser frequency or filter's  
22 position fluctuations, potentially generable by thermal drifts inside the laser cavity or the filter's housing,  
23 respectively, have negligible effects on  $k$ .

24 It is to be pointed out that leakage correction increases the statistical uncertainty affecting the  
25 temperature measurement as a result of the subtraction of  $P_{354.7}(z)$ , which is affected by statistical noise,  
26 from  $P_{Lol}^{leak}(z)$ , also affected by statistical noise, the two statistical noises being uncorrelated.  
27 Additionally, the correction factor  $k$  is determined with a certain degree of uncertainty (small, but not  
28 negligible), which may lead to a residual systematic error (bias) affecting temperature measurements  
29 after the application of the leakage correction approach. The systematic error associated with this  
30 residual leakage may be estimated through error propagation, considering the expression for  $T(z)$   
31 including leakage correction:



$$T(z) = \frac{\alpha}{\ln \left[ \frac{P_{Hil}(z)}{P_{Loj}^{leak}(z) - k T_F P_{354.7}(z)} \right] - \beta} \quad (6)$$

with  $T_F$  being the overall transmission ( $\sim 10^{-3}$ ) of the two neutral density filters located in front of the 354.7 nm interference filter. Consequently, the systematic error affecting each temperature profile associated with the uncertainty affecting  $k$  reads:

$$\Delta T_{leak}(z) = -\frac{T^2(z)}{\alpha} \frac{k T_F P_{354.7}(z)}{P_{Loj}^{leak}(z) - k T_F P_{354.7}(z)} \frac{\Delta k}{k} \cong -\frac{T^2(z)}{\alpha} \frac{k T_F P_{354.7}(z)}{P_{Loj}^{leak}(z)} \frac{\Delta k}{k} = -\frac{T^2(z)}{\alpha} \frac{T_F P_{354.7}(z)}{P_{Loj}^{leak}(z)} \Delta k \quad (7)$$

with  $\Delta k$  being the uncertainty affecting the estimate of  $k$ . The leakage signal is  $k T_F P_{354.7}(z)$ , which corresponds to about 22 % of  $P_{Loj}^{leak}(z)$  around the ABL top. Thus, the remaining error affecting temperature measurements becomes a fluctuating error, which is dependent on atmospheric properties, mainly on aerosol backscatter contribution to  $P_{354.7}(z)$ . This effect has to be properly taken into account in the determination of turbulence profiles, as in fact fluctuations in aerosol particle backscatter, especially in the upper portion of the CBL, may produce a time-dependent residual systematic error, which would propagate into the temperature fluctuations. Because of this, the quantity  $P_{Loj}(z) = P_{Loj}^{leak}(z) - k T_F P_{354.7}(z)$  has to be properly assessed in expression (6) for each 10 s temperature profile.

Considering an uncertainty of 0.01 on the estimate of  $k$ , a value of  $T=280$  K, a value of  $\alpha=1200$  K (which is the one resulting from the application of the calibration procedure), the systematic error  $\Delta T_{leak}(z)$  associated with residual leakage in the upper portion of the CBL results to be equal to 0.16 K.

An additional overall, spurious term  $\overline{(T'_{ov,leak}(z))^2}$  has to be considered in the temperature variance, which is associated with the residual systematic error affecting temperature measurements after the application of the leakage correction approach. This additional contribution is given by:

$$\overline{(T'_{ov,leak}(z))^2} \approx \overline{\Delta T_{leak}^2} + 2 \overline{T'_{ir}(t) \Delta T'_{leak}(t)} < \overline{\Delta T_{leak}^2} + 2 \sqrt{\overline{\Delta T_{leak}^2}} \sqrt{\overline{T'_{ir}^2}} \quad (8)$$

where the first term in the contribution to the “leakage variance” due to additional fluctuations caused by insufficient leakage correction and the second term is due to the correlation of the atmospheric temperature fluctuations within the not perfectly corrected leakage. We find that:



$$\begin{aligned}
 \overline{\Delta T_{leak}'^2} &\cong \left[ \frac{T^2}{\alpha} \right]^2 \frac{(k T_F)^2 (\overline{P_{354.7}(t) - \bar{P}_{354.7}})^2}{(\bar{P}_{LoJ}^{leak} - k T_F \bar{P}_{354.7})^2} \left( \frac{\Delta k}{k} \right)^2 = \left[ \frac{T^2}{\alpha} \right]^2 \frac{(k T_F \bar{P}_{354.7})^2}{(\bar{P}_{LoJ}^{leak} - k T_F \bar{P}_{354.7})^2} \left( \frac{\Delta k}{k} \right)^2 \frac{(\overline{P_{354.7}(t) - \bar{P}_{354.7}})^2}{\bar{P}_{354.7}^2} \\
 &= (\Delta T_{leak})^2 \frac{(\overline{P_{354.7}(t) - \bar{P}_{354.7}})^2}{\bar{P}_{354.7}^2} = (\Delta T_{leak})^2 \frac{\text{var}(\bar{P}_{354.7})}{\bar{P}_{354.7}^2} \approx (0.18\text{K})^2 \frac{1.7 \cdot 10^4}{500^2} = 2.2 \cdot 10^{-3} \text{K}^2 \quad (9)
 \end{aligned}$$

1  
 2 where we took the relative variance of the backscatter signal from our data at the ABL top. Here, the  
 3 variance is maximum so that we reach an upper limit of the spurious temperature variance of  
 4  $2.2 \cdot 10^{-3} \text{K}^2$  which can be neglected with respect to the atmospheric temperature variance (see section  
 5 4.3). For the correlation term, however, we get

$$\overline{2T_{lr}'(t) \Delta T_{leak}'(t)} < 2\sqrt{\overline{\Delta T_{leak}'^2}} \sqrt{T_{lr}'^2} \approx 2 \cdot 0.048\text{K} \cdot 0.64\text{K} = 0.06\text{K}^2 \quad (10)$$

7 where we took the maximum of the atmospheric temperature variance at the ABL top. This error is still  
 8 considerably smaller than our estimate of the atmospheric temperature variance at the peak in the  
 9 entrainment layer so that the structures in the higher-order moments are significant.

10 Based on the above considerations, we have to be aware that, besides a random error, represented in  
 11 figure 6b with the error bar, an additional systematic error (with a maximum amplitude of 0.16 K)  
 12 resulting from residual elastic signal leakage in the rotational Raman signals has to be considered. This  
 13 is also true when considering the noise error estimated in figure 1c. The missed inclusion of this  
 14 systematic error both in figure 6b and figure 1c is due to the very small amplitude of this contribution;  
 15 additionally, random and systematic error sources have always to be treated separately and cannot be  
 16 just summed up. Additionally, the spurious temperature variance, even if small with respect to the  
 17 atmospheric temperature variance, it is always positive. So an iteration with different values for  $k$  can  
 18 also be used to verify the correctness of the above determined value of  $k$ , as in fact the correct value  
 19 minimizes the overall variance.

20 Based on the above mentioned approach, before proceeding with the turbulence analysis, we corrected  
 21 all 10 sec Lo-J signals for the systematic effect associated with elastic signal leakage. However, in order  
 22 to overcome the residual systematic uncertainty associated with this correction, a future upgrade of  
 23 *BASIL* is planned with the introduction of a new Lo-J filter, with high blocking at 354.7 nm and high  
 24 center wavelength transmission, to be developed benefiting from the recent advances in multi-cavity  
 25 interference filter technology.

26

27





### 1 **3 Time-height cross-sections of water vapour mixing ratio and temperature**

#### 2 **3.1 Case study and weather conditions**

3 In this paper we illustrate measurements carried out in the framework of the HD(CP)2 Observational  
4 Prototype Experiment (HOPE). HOPE, embedded in the project High-Definition Clouds and  
5 Precipitation for advancing Climate Prediction (HD(CP)2) of the German Research Ministry, was  
6 specifically designed to provide a dataset for the evaluation of the German non-hydrostatic General  
7 Circulation Model ICON at the scale of the model simulations. It took place in Western Germany in the  
8 time period April-May 2013. For the purposes of HOPE, *BASIL* was deployed in the Supersite JOYCE,  
9 located within the Jülich Research Center (Central Germany, Lat.: 50°54' N; Long.: 6°24' E, Elev. 105  
10 m). The system operated between 25 March and 31 May 2013, collecting more than 430 hours of  
11 measurements distributed over 44 days and 18 IOPs. Quick-looks of these dataset are present on the  
12 HOPE Website (<https://code.zmaw.de/projects/hdcp2-obs/>), while water vapour and particle backscatter  
13 data can be downloaded from the HD(CP)2 database.

14 In the selection of the case study considered in this paper, attention was paid on identifying weather  
15 conditions characterized by the presence of a well-mixed and quasi-stationary CBL. Consequently, in  
16 those cases when measurements of the complete CBL cycle are available, i.e. from the onset to its  
17 progressive built up and final decay, attention has been focused only on those time segments  
18 characterized by a stable or almost stable CBL height, which corresponds to the period of its maximum  
19 development. Typically time segments with a duration of 1-2 hours are considered as in fact for longer  
20 periods the CBL can no longer be considered as being quasi-stationary, while the consideration of  
21 shorter periods would reduce the number of sampled thermals and thus increase the sampling errors.

22 The synoptic condition on 20 April 2013 was characterized by the presence of a high pressure system  
23 located over Great Britain, with effects extending over Central-Northern Germany, and a low pressure  
24 system located over Central Italy (see also Muppa *et al.*, 2016). The forecast for the HOPE region  
25 indicated some thin convective clouds from 8 to 10 UTC and clear sky starting from 10 UTC, with  
26 cirrus clouds startind from 15 UTC. This was considered as a day with suitable atmospheric conditions  
27 for an Intensive Observation Period (IOP), specifically IOP 5, dedicated to radiometer tomography.  
28 This IOP turned out to be also a good case study for the purpose of studying CBL development under  
29 clear-sky or almost-clear sky conditions. Indeed, the almost undisturbed solar irradiance resulted in the  
30 development of a well-mixed CBL which was not affected by clouds.

31

32



### 1 3.2 Water vapour mixing ratio, temperature, and backscatter fields

2 In order to select an appropriate time interval for the application of the turbulence analysis, we  
3 considered the measurements of the different energy balance components as provided by the surface  
4 energy balance station in Hambach (not illustrated here). The maximum net radiation was found to  
5 occur around 12:00 UTC ( $520 \text{ Wm}^{-2}$ ), with a very limited variability ( $<40 \text{ Wm}^{-2}$ ) within the time  
6 interval 11:30-13:30 UTC. This is the time interval that we selected for the turbulence analysis.

7 In order to achieve a sufficiently high signal-to-noise error (SNR) and consequently an acceptably low  
8 noise error level, a running average over 3 points was considered for the water vapour mixing ratio data,  
9 which translates into a reduced vertical resolution of 90 m, while no average was applied to the  
10 temperature data, keeping the original vertical resolution of 30 m.

11 Figure 4 illustrates the time-height plot of the particle backscatter coefficient at 1064 nm,  $\beta_{par}$ , between  
12 11:30 and 13:30 UTC on 20 April 2014. The figure reveals the presence of a significant aerosol loading  
13 within the boundary layer (with values of  $\beta_{par}$  in excess of  $1 \times 10^{-6} \text{ m}^{-1} \text{ sr}^{-1}$ ), tracing the presence of a  
14 well-mixed and quasi-stationary CBL at this time of the day, extending up to a height of approximately  
15 1300 m. The figure also reveals the presence of alternating updrafts and downdrafts.  $\beta_{par}$  was  
16 determined based on the application of a Klett-modified approach (Di Girolamo *et al.*, 1995, 1999). The  
17 identification of the CBL height and the monitoring of its variability is made possible by exploiting  
18 aerosols' property to act as atmospheric tracers. The mean CBL height,  $z_i$ , is an important scaling  
19 variable for turbulence profiles. The evolution of the instantaneous CBL height  $z'_i$  (black dots in figure  
20 4) was determined through the application of a conventional approach based on the detection of the  
21 strongest gradient of the aerosol backscatter signal (see, among others, Pal *et al.*, 2010; Summa *et al.*,  
22 2013). Within the considered time interval  $z'_i$  is found to be characterized by a limited variability, with a  
23 mean value  $z_i$  of 1290 m a.g.l and a standard deviation of 77 m. The minimum and maximum values of  
24  $z'_i$  during the observation period are 1140 and 1440 m a.g.l., respectively. This result is in very good  
25 agreement with the simultaneous measurements performed by the University of Hohenheim Differential  
26 Absorption Lidar (UHOH-DIAL) (Wagner *et al.*, 2013; Späth *et al.* 2016), deployed in Hambach,  
27 approx. 4 km E-SE, with a mean value of 1295 m and a standard deviation of 86 m (Muppa *et al.*,  
28 2016).  $z_i$  is used in the remaining part of the paper to determine the normalized height scale  $z/z_i$ . Particle  
29 backscatter coefficient data can also be used to identify the presence of aerosol layers and/or clouds  
30 within and above the CBL, with an effective demonstrated capability to detect cloud bases and tops (the  
31 latter in the case of cloud optical thickness typically smaller than 2, Di Girolamo *et al.*, 2009b).



1 Figure 5 illustrates the time-height cross section of water vapour mixing ratio (figure 5a) and  
2 temperature (figure 5b) for the same time interval considered in figure 4. Figures 5a and 5b clearly  
3 highlights the large variability of water vapour mixing ratio and temperature within the CBL associated  
4 with the presence of alternating updrafts and downdrafts. The largest variability of both water vapour  
5 mixing ratio and temperature is observed in the interfacial layer, as a result of the penetration of the  
6 warm humid air rising from the ground and the entrainment of cool dry air from the free troposphere.  
7 Figure 5b also reveals the presence of decreasing temperatures within the CBL up to a minimum around  
8 1200-1300 m and an appreciable temperature inversion (approx. 1 K) above.

9 Figure 6 illustrates the mean profile for water vapour mixing ratio (figure 6a) and temperature (figure  
10 6b) as measured by *BASIL* over the same time interval considered in figure 4 (11:30-13:30 UTC on 20  
11 April 2013), together with the corresponding profiles measured by the radiosonde launched at 13:00  
12 UTC from the nearby site of Hambach. The water vapour mixing ratio profiles from *BASIL* and the  
13 radiosonde are found to agree within  $0.2 \text{ g kg}^{-1}$  within the mixed layer. A larger deviation is found in the  
14 interfacial layer ( $0.5 \text{ g kg}^{-1}$ ). However, this is not surprising when considering that the Raman lidar data  
15 are averaged over a 2 h period (11:30-13:30 UTC), while the radiosonde reaches the CBL top few  
16 minutes after launch. Besides the different time interval considered for *BASIL* and the radiosonde, the  
17 two sensors are also sounding different air masses as a result of the 4 km distance between the lidar site  
18 and the radiosonde launching station and the horizontal drift of the sonde during its ascent caused by the  
19 wind and the consequent deviation of its atmospheric path from the vertical. In presence of intense  
20 convective activity, deviations from the sounding data are also possible for radiosondes launched from  
21 the lidar site: in this case humid air updrafts and dry air downdraft may have sizes of few kilometres and  
22 consequently the radiosonde data can capture different features during its ascent within the CBL with  
23 respect to the lidar. This property makes lidar systems much more suitable for studying turbulence  
24 statistics than in-situ sounding systems as in fact with lidars statistics is indeed measured in a vertical  
25 column. Similar considerations apply for the comparison between *BASIL* and the radiosonde in terms of  
26 temperature profile (figure 6b). In this case, the deviation between the two sensors is  $\approx 0.5 \text{ K}$  throughout  
27 the CBL, with *BASIL* being characterized by systematically smaller values than the radiosonde, while a  
28 better agreement (deviation not exceeding 0.3 K) is observed in the free troposphere above the CBL top.  
29 In this respect, it is to be noticed that the sequence of consecutive radiosondes launched during IOP 5  
30 (at 09:00, 11:00, 13:00 UTC, not shown here) reveals the occurrence of vertical profiles characterized  
31 by an almost constant potential temperature values within the mixed layer, as expected for a well-mixed  
32 CBL, with potential temperature constant value progressively increasing with time. Considering that  
33 Raman lidar data in figure 6 are averaged over a 2 h period (11:30-13:30 UTC) which is largely



1 anticipating the radiosonde launch time (at 13:00 UTC), the systematically smaller temperature values  
2 of *BASIL* with respect to the radiosonde within the CBL are easily justifiable.

3

#### 4 **4 Turbulence analysis methodology and results**

##### 5 **4.1 Methodology**

6 In CBL turbulence studies, the instantaneous value of a measured atmospheric variable,  $x(z,t)$ , at height  
7  $z$ , can be expressed as the sum of three terms: a slowly varying or even constant term,  $\overline{x(z)}$ , where the  
8 over-bar represents the time average over the considered temporal interval for the turbulence analysis, a  
9 fluctuation or perturbation term,  $x'(z,t)$  and a system noise term,  $\varepsilon(z,t)$ , following the expression:

$$10 \quad x(z,t) = \overline{x(z)} + x'(z,t) + \varepsilon(z,t) \quad (11)$$

11  $\overline{x(z)}$  can be derived from applying a linear fit to the data over the time period when the turbulent  
12 processes are studied (typically 60-120 min, 120 min in our case).

13 Here the fluctuation term  $x'(z,t)$  represents the de-trended fluctuation term with zero mean. To de-trend  
14 the data within a CBL in quasi-stationary state a linear fit is applied to the atmospheric variable time  
15 series.

16 For any measured atmospheric variable, as atmospheric variance and the noise variance are uncorrelated,  
17 total variance can be expressed as (Lenschow *et al.*, 2000):

$$18 \quad \overline{(x'_m(z))^2} = \overline{(x'_a(z))^2} + \overline{(x'_n(z))^2} \quad (12)$$

19 with  $\overline{(x'_m(z))^2}$  being the total measured variance,  $\overline{(x'_a(z))^2}$  being the atmospheric variance and  
20  $\overline{(x'_n(z))^2}$  being the noise variance.

21 Different procedures may be considered to separate atmospheric variance from noise variance in the  
22 total measured variance. The auto-covariance method is probably the most effective and straightforward  
23 among these procedures. This method is based on the consideration that atmospheric fluctuations are  
24 correlated in time, while instrumental noise fluctuations are uncorrelated (Lenschow *et al.*, 2000). This  
25 approach allows to determine atmospheric variance based on the computation of the auto-covariance  
26 function (ACF) for the considered atmospheric variable and then extrapolating this function to zero lag  
27 based on the application of a power-law fit. As specified in Lenschow *et al.* (2000), the auto-covariance



1 function at zero lag represents the total measured variance and, consequently, the noise variance can be  
2 determined as the difference between the auto-covariance function extrapolated to zero lag and its value  
3 at zero lag.

4 An alternative approach is represented by the spectral method. In this case, the power spectrum of the  
5 atmospheric variable fluctuations is computed and the constant white noise level close to the Nyquist  
6 frequency is evaluated. Both the spectral method, based on the assumption that the system noise is  
7 white, and the auto-covariance method allow to verify whether the major part of the turbulent  
8 fluctuations is resolved through the measurements either by comparing the high-frequency component  
9 of the spectrum with the theoretical decay in the inertial sub-range or by fitting the turbulent structure  
10 function to the auto-covariance function. Thus, there is no reason to transfer the data in the spectral  
11 domain for these applications and, because of that, the data analysis was kept in the time domain.  
12 Furthermore, while both approaches were considered and tested on the water vapour and temperature  
13 data considered in this paper, the auto-covariance technique (see figure 1) is to be preferred because of  
14 its capability to directly determine system noise variance by means of the Fourier transformation of the  
15 auto-covariance function, without introducing additional uncertainties (Wulfmeyer *et al.*, 2010).

16 Preliminary pre-processing steps have to be applied to the data before both techniques can be applied. In  
17 general, before any further processing, spikes must be detected and flagged, as they negatively affect  
18 the calculation of turbulent variables (Senff *et al.*, 1996). In fact, the presence of spikes in the time  
19 series may have a significant impact on the computations of higher moments of the turbulent statistics.  
20 Spikes in water vapour and temperature profiles are primarily resulting from non-linear effects  
21 associated with the application of retrieval algorithms, these being likely to happen especially at low  
22 signal-to-noise levels (Di Girolamo *et al.*, 2008). Low signal-to-noise levels are typically found in day-  
23 time Raman lidar water vapour and temperature measurements at heights above 3-5 km, this height  
24 varying depending on the considered variable (being lower for water vapour and higher for temperature),  
25 or in the presence of clouds as a result of the laser beam attenuation. For the application considered in  
26 this paper, i.e. the characterization of turbulent processes within the CBL, the vertical range of interest  
27 is up to 2000 m and within this range the signal-to-noise level of rotational and vibrational Raman  
28 signals is typically large enough to refrain from applying the spike removal algorithm to the data.  
29 Additionally, for the specific case study considered in this paper, clouds are completely missing within  
30 the CBL, and consequently the application of the spike removal algorithm to the lidar data returns a  
31 dataset with almost no data removed. However, there may be missing data or data gaps generated in the  
32 adaptation of the time resolution; because of this, a spike detection algorithm (McNicholas and Turner,



1 2014) is routinely applied to the data before either the auto-covariance method or the spectral method  
2 are applied.

3

#### 4 **4.2 Turbulent fluctuations, corresponding auto-covariance functions and assessment of the noise** 5 **error**

6 Figure 7 illustrates the time-height cross section of water vapour mixing ratio (figure 7a) and  
7 temperature fluctuations (figure 7b) in the same time interval considered in figure 4. Positive and  
8 negative humidity and temperature fluctuations are present within the CBL. In the interfacial layer, the  
9 fluctuations become larger than below. More specifically, instantaneous water vapour fluctuations are  
10 within  $\pm 0.5 \text{ g kg}^{-1}$  in the mixed layer and  $\pm 1 \text{ g kg}^{-1}$  in the interfacial layer, while instantaneous  
11 temperature fluctuations are within  $\pm 0.5 \text{ K}$  in the mixed layer and  $\pm 1 \text{ K}$  in the interfacial layer. In the  
12 free troposphere humidity and temperature fluctuations are almost completely missing and the observed  
13 variability is primarily driven by instrumental noise.

14 Figure 8 shows the auto-covariance functions obtained from water vapour (figure 8a) and temperature  
15 fluctuations (figure 8b) for the height levels between 400 and 1600 m a.g.l., i.e., 0.3 to 1.25  $z_i$ , and for  
16 lags from -200 to 200 s. As mentioned earlier, the difference between the peak at zero lag and the first  
17 lag provides an estimate of the system noise variance. This is also described in figures 8a and 8b, where  
18 the structure functions have been fitted to the auto-covariance functions for the height levels of 1230 m  
19 and 1410 m to verify the feasibility and reliability of this approach. In the figure, this difference is  
20 found to increase with height for both variables as a result of the increasing system statistical noise.  
21 Values of the ACFs close to the zero lag provide an estimate of the atmospheric variance: larger values  
22 for the ACFs found in the figure at 1230 and 1410 m indicate a larger atmospheric variance at these  
23 heights, as a result of the large atmospheric variability within the interfacial layer.

24

#### 25 **4.3 Measurements of higher-order moments**

26 Figure 9 illustrates the integral scale (IS) of water vapour mixing ratio (figure 9a) and temperature  
27 fluctuations (figure 9b) computed for the same time interval considered in figure 4. The integral time  
28 scale can be considered as an estimate of the mean size of the turbulent eddies involved in the boundary  
29 layer mixing processes. The integral time scale of both water vapour mixing ratio and temperature  
30 fluctuations is found to have large values (also exceeding 200 s) in the lower portion of the CBL up to  
31  $\cong 750 \text{ m}$  (i.e.  $z/z_i < 0.6$ ). Values of the integral scale for water vapour mixing ratio fluctuations in the



1 upper portion of the CBL (above 750 m) are in the range 70-125 s, with a peak value of 125 s at 1230 m  
2 (i.e.  $z/z_i=0.95$ ). These values are in agreement with those reported for water vapour by Wulfmeyer *et al.*  
3 (2010, 70-130 s) and by Turner *et al.*, 2014a (120-140), as well as with the simultaneous nearby  
4 measurements performed by the UHOH-DIAL, with values in the range 60-130 s (Muppa *et al.*, 2016).  
5 Values of the integral scale for temperature fluctuations in the upper portion of the CBL are in the range  
6 75-225 s, with a peak value of 225 s around the top of the CBL (at 1310 m). These values are in  
7 agreement with those reported by Behrendt *et al.* (2015, 40-120 s) for the nearby site of Hambach, but a  
8 different case study. Values of the integral scale throughout the CBL for both water vapour and  
9 temperature fluctuations are much larger than the temporal resolution used for the measurements (10 s),  
10 which demonstrates that the considered temporal resolution is high enough to characterize the major  
11 part of turbulence inertial sub-range and consequently resolve the major part of the CBL turbulent  
12 fluctuations.

13 Figure 10 shows the vertical profiles of atmospheric and total variance for water vapour mixing ratio  
14 (panel a) and temperature (panel b), including noise errors. Water vapour mixing ratio variance is  
15 almost zero up to  $\cong 750$  m (i.e.  $z/z_i=0.6$ ), it keeps small ( $<0.05 \text{ g}^2\text{kg}^{-2}$ ) in the middle and upper portion  
16 of the CBL ( $750 \text{ m} < z < 1100 \text{ m}$ , i.e.  $0.6 < z/z_i < 0.85$ ), and it sensitively increases in the interfacial layer  
17 due to the entrainment effects. The maximum of the variance profile in the interfacial layer is  $0.287$   
18  $\text{g}^2\text{kg}^{-2}$  at 1260 m (i.e.  $z/z_i=0.98$ ), with  $0.051 \text{ g}^2\text{kg}^{-2}$  and  $0.034 \text{ g}^2\text{kg}^{-2}$  being the sampling error and noise  
19 error, respectively. The near-zero values in the lower portion of the CBL are typical and indicate weak  
20 forcing from the surface. In the interfacial layer, the variance reaches a maximum as a result of the large  
21 water vapour mixing ratio variability which is generated by the vertical exchange associated with the  
22 strong updrafts and downdrafts (Wulfmeyer *et al.*, 2010; Turner *et al.* 2014a, Muppa *et al.*, 2016).  
23 Variance values at the top of the CBL are in good agreement with those reported by Wulfmeyer  
24 (1999a,b,  $0.1-0.2 \text{ g}^2\text{kg}^{-2}$ ), Lenschow *et al.* (2000,  $0.1-0.2 \text{ g}^2\text{kg}^{-2}$ ) and Kiemle *et al.* (1997,  $0.3-0.45$   
25  $\text{g}^2\text{kg}^{-2}$ ), as well as with the simultaneous nearby measurements by the UHOH-DIAL, with a peak value  
26 in the interfacial layer of  $0.39 \text{ g}^2\text{m}^{-6}$ , corresponding to  $0.19 \text{ g}^2\text{kg}^{-2}$ . The full width at half maximum of  
27 the largest variability in the entrainment zone is 240 m, i.e.  $0.19 z/z_i$ , in agreement with measurements  
28 reported by Wulfmeyer *et al.* (2010,  $0.16 z/z_i$ ) and by Turner *et al.* (2014a,  $0.15 z/z_i$ ). Values of water  
29 vapour mixing ratio variance decrease above the CBL top to approach zero around 1500 m.

30 For what concerns the temperature variance, this keeps smaller than  $0.1 \text{ K}^2$  in the middle and upper  
31 portion of the CBL up to 1150 (i.e.  $z/z_i < 0.9$ ). Larger values are observed in the interfacial layer, with a  
32 maximum of  $0.260 \text{ K}^2$  at 1310 m (i.e.  $z/z_i=1.02$ ), with  $0.051 \text{ K}^2$  and  $0.035 \text{ K}^2$  for the sampling error and  
33 noise error, respectively. Larger values of the temperature variance in the interfacial layer are the result



1 of the penetration of the warm humid air rising from the ground and the entrainment of cool dry air  
2 from the free troposphere (Stull, 1988; Behrendt *et al.*, 2015; Wulfmeyer *et al.*, 2016). Temperature  
3 variance decreases above the CBL top to approach zero around 1450 m. The full width at half  
4 maximum of the largest variability in the entrainment zone is 240 m, i.e.  $z/z_i=0.2$ . Similar peak variance  
5 values ( $0.40 \text{ K}^2$ ) at the top of the CBL were also observed by Behrendt *et al.* (2015) and Wulfmeyer *et*  
6 *al.* (2016). It is to be noticed that both water vapour mixing ratio and temperature variance are  
7 characterized by very small sampling and noise errors, which make the quality of the present turbulence  
8 measurements very high and demonstrates how well the structures present in these profile can be  
9 determined.

10 Figure 11 illustrates the vertical profiles of the third-order moment for water vapour mixing ratio (panel  
11 a) and temperature (panel b). The third-order moment of a variable quantifies the degree of asymmetry  
12 of its distribution, with positive values indicating a right-skewed distribution (with the mode smaller  
13 than the mean) and negative values indicating a left-skewed distribution (with the mode larger than the  
14 mean). Again, third-order moment estimates are characterized by very small errors, which testify the  
15 high quality of the present measurements of this turbulent variable. In figure 11 values of the third order  
16 moment of water vapour mixing ratio fluctuations are found to be close to zero between 400 and 900 m  
17 (i.e. for  $0.3 z_i < z < 0.7 z_i$ ) and are negative between 900 and 1290 m (i.e. for  $0.7 z_i < z < z_i$ ), with a  
18 negative peak value of  $-0.029 \pm 0.005 \text{ g}^3 \text{ kg}^{-3}$  at 1140 m. A large positive peak is observed just above  
19 CBL top, with a maximum of  $0.156 \pm 0.009 \text{ g}^3 \text{ kg}^{-3}$  at 1380 m ( $z=1.07 z_i$ ).

20 Negative values for the water vapour mixing ratio third-order moment in the upper portion of the CBL  
21 is the result of the sharp entrainment of dry air pockets into the boundary layer, which gradually mix  
22 with the environmental air (Couvreur *et al.*, 2005, 2007; Wulfmeyer *et al.*, 2010; Turner *et al.*, 2014a,  
23 Wulfmeyer *et al.*, 2016). Positive values for the water vapour mixing ratio third-order moment above  
24 the top of the CBL are associated with narrow, but strong, convective plumes that penetrate up to this  
25 height. The sign and shape of the third-order moment at the top of the boundary layer may also depend  
26 on the humidity gradient above the CBL (Couvreur *et al.*, 2007). The near-zero third-order moment  
27 values in the mixed layer ( $z/z_i < 0.7$ ) is to be attributed to a symmetric transport process of moisture  
28 (Mahrt, 1991; Wulfmeyer *et al.*, 2010).

29 For what concerns the temperature third-order moment, this shows values close to zero ( $<0.01 \text{ K}^3$ ) up to  
30 1100 m ( $z/z_i < 0.85$ ) and slightly positive values between 1100 and 1310 m ( $0.85 z_i < z < 1.02 z_i$ ), with  
31 a positive peak of  $0.055 \text{ K}^3$  at 1220 m. Above 1250 m it becomes negative, with a negative peak of -  
32  $0.067 \pm 0.01 \text{ K}^3$  at 1400 m ( $z/z_i=1.1$ ). The structure of this moment is basically inverted with respect to





1 water vapour (Behrendt *et al.*, 2015). This makes sense because the water vapour gradient is negative in  
2 the entrainment zone, whereas the temperature inversion gradient is positive. The positive peak in the  
3 interfacial layer is evidence of the predominant effect of narrow warm air downdrafts in the interfacial  
4 layer, while the negative peak above the CBL top is the result of narrow cooler updrafts above the CBL  
5 top associated with thermals from the surface. Figure 11b, besides temperature third-order moment, also  
6 includes the vertical profile of the water vapour mixing ratio third-order moment to better compare the  
7 shapes and locations of the peaks and zero crossing values for these two profiles. This allows to reveal  
8 that the negative peak in the temperature third-order moment appears at the same height (within 20 m)  
9 of the positive peak in the water vapour mixing ratio third-order moment, while the distance between  
10 the zero crossing values for the two profiles is approx. 100 m.

11 Figure 12 illustrates the vertical profiles of the fourth-order moment for water vapour mixing ratio  
12 (panel a) and temperature (panel b). The fourth-order moment of a variable gives an indication of the  
13 steepness of its distribution and the width of its peak. Water vapour mixing ratio fourth-order moment is  
14 almost zero up to  $\approx 750$  m (i.e.  $z/z_i=0.6$ ), keeps smaller than  $0.02 \text{ g}^4\text{kg}^{-4}$  in the middle and upper portion  
15 of the CBL ( $750 \text{ m} < z < 1100 \text{ m}$ , i.e.  $0.6 < z/z_i < 0.85$ ) and increases above 1100 m, reaching its maximum  
16 of  $0.28 \pm 0.13 \text{ g}^4\text{kg}^{-4}$  around the top of the CBL (at 1350 m). It gets again close to zero above 1530 m.  
17 Similarly, temperature fourth-order moment is almost zero ( $< 0.05 \text{ K}^4$ ) up to 1100 m (i.e.  $z/z_i=0.85$ ) and  
18 has positive values above, reaching a positive peak of  $0.24 \pm 0.10 \text{ K}^4$  around the top of the CBL (at 1370  
19 m, i.e.  $z/z_i=1.06$ ). It gets again smaller than  $0.05 \text{ K}^4$  above 1500 m (i.e.  $z/z_i=1.15$ ).

20 Besides the third- and fourth-order moments, also atmospheric skewness and kurtosis has been  
21 determined for both water vapour mixing ratio and temperature fluctuations. Figure 13 illustrates the  
22 vertical profiles of skewness (panel a) and kurtosis (panel b) for water vapour mixing ratio and  
23 temperature. Values of water vapour mixing ratio skewness are in very good agreement with those  
24 reported by Wulfmeyer *et al.*, 2010, with positive values (up to 1.5) in the lower portion of the CBL (up  
25 to 800 m, i.e.  $z/z_i=0.65$ ), with negative values (down to -1) in the middle and upper portion of the CBL  
26 ( $800 < z < 1290$  m, i.e.  $0.65 < z/z_i < 1.00$ ) and positive values just above the PBL top (with a maximum of  
27 approx. 5 at 1400 m, i.e.  $z/z_i=1.15$ ). Values and vertical structure of water vapour mixing ratio skewness  
28 are also in good agreement with the simultaneous and nearby measurements performed by the UHOH-  
29 DIAL (Muppa *et al.*, 2016), with negative values (down to -1.16) in the middle and upper portion of the  
30 CBL ( $0.35 < z/z_i < 1.00$ ) and positive values just above the PBL top (with a maximum of approx. 1 at  $z/z_i$   
31  $=1.05$ ), as well as with the measurements reported by Turner *et al.* (2014), with negative values (down  
32 to  $\sim -1$ ) up to the CBL top, zero values around  $z_i$  and positive values just above the CBL top (with a  
33 maximum of approx. 1 at  $z/z_i=1.1$ ).



1 Temperature skewness has a negative peak ( $\sim -4$ ) at 500 m, i.e.  $z/z_i=0.4$ , positive peaks ( $\sim 4$  and 8) at  
2 890 and 1100 m (i.e.  $z/z_i=0.7$  and  $z/z_i=0.85$ ), respectively, and a negative peak ( $\sim -7$ ) at 1460 m, i.e.  $z/z_i$   
3  $=1.13$ , in in good agreement with measurements reported by Behrendt *et al.* (2015, 40-120 s) for the  
4 nearby site of Hambach, but a different case study.

5 Values of kurtosis in the entrainment zone (in the height interval 1160-1340 m) are in the range 2.35-  
6 4.33, with a mean value of 3.15, for water vapour mixing ratio fluctuations, while they are in the range  
7 2.59-4.11, with a mean value of 3.22, for temperature fluctuations. These values indicate normally  
8 distributed (mesokurtic-Gaussian distribution) humidity and temperature fluctuations in the entrainment  
9 zone (Wulfmeyer *et al.*, 2010; Turner *et al.* 2014a, Behrendt *et al.*, 2015, Muppa *et al.*, 2016).

10

## 11 **5 Summary**

12 This paper illustrates measurements performed by the Raman lidar system *BASIL* during a recent field  
13 deployment which demonstrate the capability of this remote sensor to characterize turbulent processes  
14 within the CBL. For the first time simultaneous and co-located daytime measurements of the vertical  
15 profiles of higher-order moments of the turbulent fluctuations of water vapour and temperature carried  
16 out by a single instrument are reported. Thus, this paper demonstrates that state-of-art lidar systems,  
17 with both rotational and vibrational Raman measurement capability, allow for simultaneously  
18 determining higher-order moments (as well as skewness and kurtosis) of the fluctuations of these two  
19 fundamental turbulent variables. Results are based on the application of the auto-covariance analysis  
20 introduced by Lenschow *et al.* (2000) to high-resolution water vapour mixing ratio (10 s, 90 m) and  
21 temperature (10 s, 30 m) time series.

22 Measurements of water vapour turbulent fluctuations throughout the CBL by vibrational Raman lidar,  
23 with estimates of up to the fourth-order moment, had been demonstrated to be possible by Wulfmeyer *et*  
24 *al.* (2010) based on the use of the data from the Atmospheric Radiation Measurement (ARM) Raman  
25 lidar operated at the Southern Great Plains Climate Research Facility site in Oklahoma (U.S.A.). The  
26 same was demonstrated by Behrendt *et al.* (2015) for temperature turbulent fluctuations with rotational  
27 Raman lidar. To the best of our knowledge, *BASIL* is the first Raman lidar system demonstrating the  
28 capability to simultaneously measure profiles of water vapour and temperature turbulent fluctuations up  
29 to the fourth order during daytime throughout the atmospheric CBL.

30 In the present paper a comprehensive assessment of the performances of the Raman lidar system *BASIL*  
31 has been also carried out. Noise error profiles have been estimated based on the application of the auto-  
32 covariance method and compared with the noise profiles estimated through Poisson statistics. The



1 measurements of the higher-order moments of water vapour mixing ratio and temperature fluctuations  
2 are characterized by very small sampling and noise errors, which make the quality of the present  
3 turbulence measurements very high and demonstrates their capability to accurately observe the  
4 structures present in the turbulent variables' profiles. In the determination of the temperature profiles,  
5 particular care was dedicated in minimizing the potential systematic error associated with elastic signal  
6 leakage in the rotational Raman signals. For this purpose, a specific algorithm was illustrated and tested,  
7 which allowed to identify and remove signal leakages and to assess the residual systematic uncertainty  
8 affecting temperature measurements after correction. In order to overcome the systematic uncertainty  
9 associated with this correction, a future upgrade of *BASIL* is planned with the introduction of a new Lo-  
10 J filter with high blocking at 354.7 nm and high center wavelength transmission to be developed  
11 benefiting from the recent advances in multi-cavity interference filter technology.

12 Limited data is presently available in literature in terms of measurements or model simulations of  
13 higher-order moments for both water vapour mixing ratio and temperature fluctuations. Consequently, a  
14 deeper insight into possible interpretations of their vertical variability lacks of additional supporting  
15 data. The availability of state-of-art rotational and vibrational Raman lidar systems capable to provide  
16 high-resolution and accurate water vapour and temperature measurements will certainly help to fill this  
17 gap, at least on the measurement side.

18 Future evolutions of this research work include the possibility to (i) compare - for a large variety of  
19 clear sky cases collected during HOPE field campaign - the measurements of higher-order moments of  
20 moisture and temperature fluctuations performed by *BASIL* with those simultaneously measured by the  
21 University of Hohenheim water vapour DIAL and temperature rotational Raman lidar (located approx.  
22 4 km E-SE), (ii) extend the analysis to cloud-topped CBLs from different field deployments, as in fact  
23 important effect of clouds on turbulent exchange processes in the entrainment zone are expected to be  
24 relevant, (iii) compare the measurements of higher-order moments of moisture and temperature  
25 fluctuations from *BASIL* with estimates from large eddy simulation, and (iv) complement these studies  
26 with a dedicated evaluation of the correlation between temperature and moisture.

27

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3

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## 1 Figures captions

2 **Figure 1:** Profiles of noise error affecting water vapour mixing ratio (panels a and b) and temperature  
 3 (panel c) measurements The figure illustrates the estimates determined based on the application of the  
 4 auto-covariance method, obtained by extrapolating the structure function to lag zero, and the error  
 5 profiles obtained based on the application of Poisson statistics to signal photon counts.

6 Time-height cross-section of the particle backscatter coefficient,  $\beta_{par}$ , between 11:30 and 13:30 UTC on  
 7 20 April 2013. The black line in the figure identifies the CBL height  $z_i$ .

8 **Figure 2:** (panel a) The mean photon numbers (10 sec average) for the considered signals, i.e. the water  
 9 vapour and molecular nitrogen vibrational Raman signals,  $P_{H_2O}(z)$  and  $P_{N_2}(z)$ , the 355 nm elastic  
 10 signal,  $P_{355}(z)$ , and the pure-rotational Raman signals,  $P_{LoJ}(z)$  and  $P_{HiJ}(z)$ ; (panel b) temperature  
 11 sensitivity of RRL measurement technique.  $\partial R(z)/\partial T$ .

12 **Figure 3:** Vertical profiles of  $P_{LoJ}^{leak}(z)$ ,  $P_{HiJ}(z)$ ,  $T_F P_{354.7}(z)$  and  $P_{LoJ}^{sym}(z)$  for the time interval 13:38-13:46  
 13 UTC on 20 April 2013, revealing the presence of high cirrus clouds extending between 7.9 and 9.8 km.

14 **Figure 4:** Time-height cross-section of the particle backscatter coefficient,  $\beta_{par}$ , between 11:30 and  
 15 13:30 UTC on 20 April 2013. The black line in the figure identifies the CBL height  $z_i$ .

16 **Figure 5:** Time-height cross section of water vapour mixing ratio (panel a) and temperature (panel b) in  
 17 the same time interval considered in figure 4.

18 **Figure 6:** Mean water vapour mixing ratio (panel a) and temperature (panel b) profiles measured by  
 19 *BASIL* on 20 April 2013 between 11:30 and 13:30 UTC, together with the corresponding profiles as  
 20 measured by a radiosonde launched at 13:00 UTC from the nearby site of Hambach. Noise error bars  
 21 are also shown.

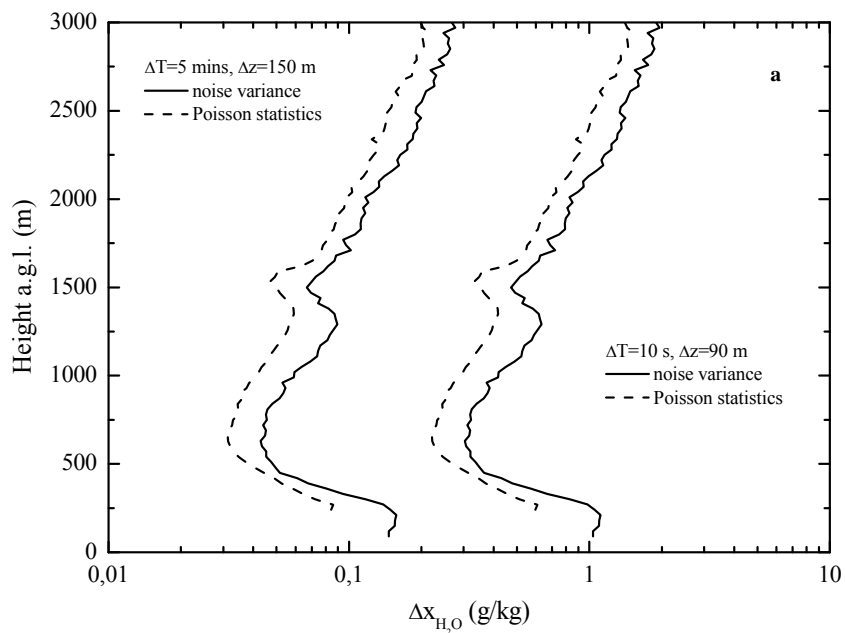
22 **Figure 7:** Time-height cross section of water vapour mixing ratio (panel a) and temperature fluctuations  
 23 (panel b) in the same time interval considered in figure 4.

24 **Figure 8:** Auto-covariance functions obtained from the measured water vapour mixing ratio (panel a)  
 25 and temperature (panel b) fluctuations in the same time interval considered in figure 4. Auto-covariance  
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 27 from -200 to 200 s.

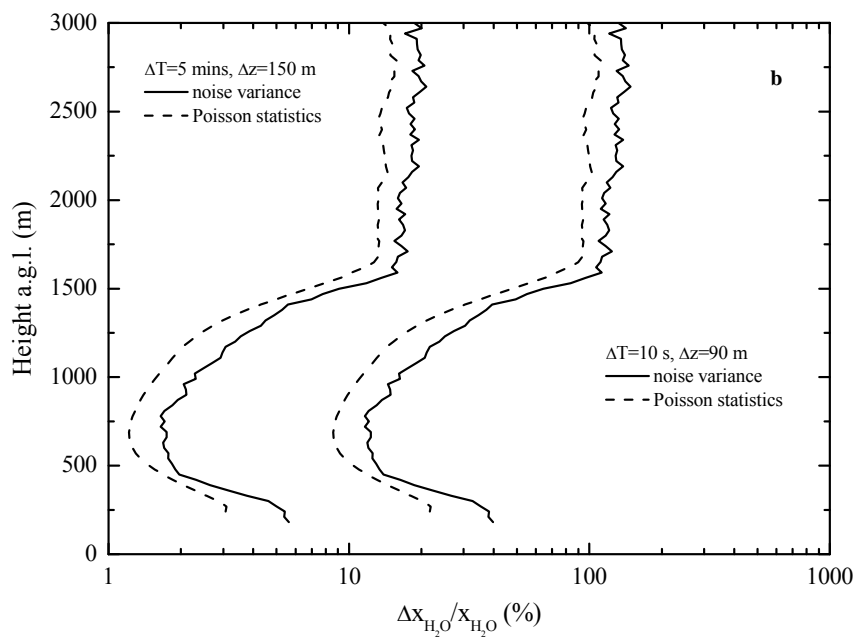
28 **Figure 9:** Integral scale of water vapour mixing ratio (panel a) and temperature fluctuations (panel b)  
 29 computed for the same time interval considered in figure 4.



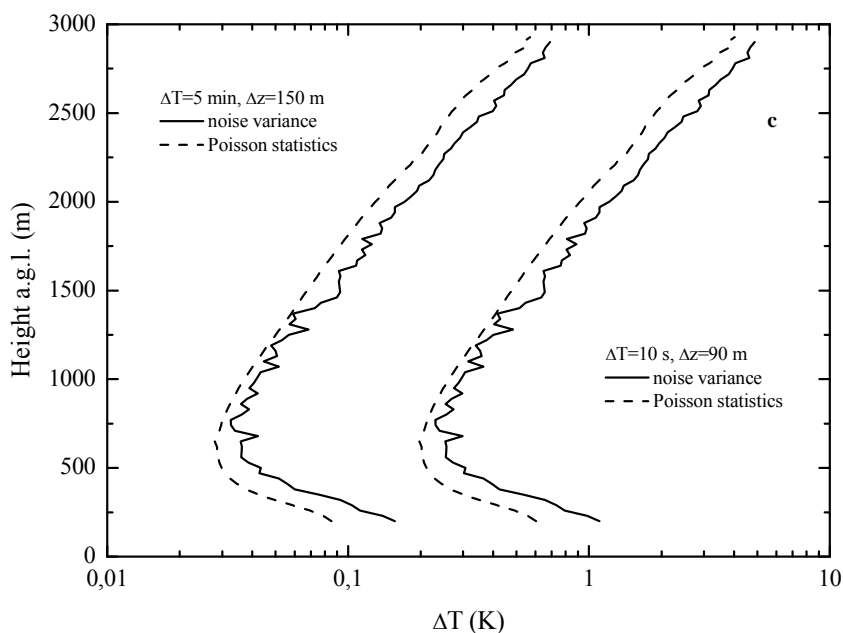
- 1 **Figure 10:** Vertical profiles of atmospheric and total variance for water vapour mixing ratio (panel a)  
2 and temperature (panel b) computed for the same time interval considered in figure 4. In the figure the  
3 error bars represent only the noise error.
- 4 **Figure 11:** Vertical profiles of the third-order moment for water vapour mixing ratio (panel a) and  
5 temperature (panel b) computed for the same time interval considered in figure 4. In the figure the error  
6 bars represent only the noise error.
- 7 **Figure 12:** Vertical profiles of the fourth-order moment for water vapour mixing ratio (panel a) and  
8 temperature (panel b) computed for the same time interval considered in figure 4. In the figure the error  
9 bars represent only the noise error.
- 10 **Figure 13:** Vertical profiles of skewness (panel a) and kurtosis (panel b) for water vapour mixing ratio  
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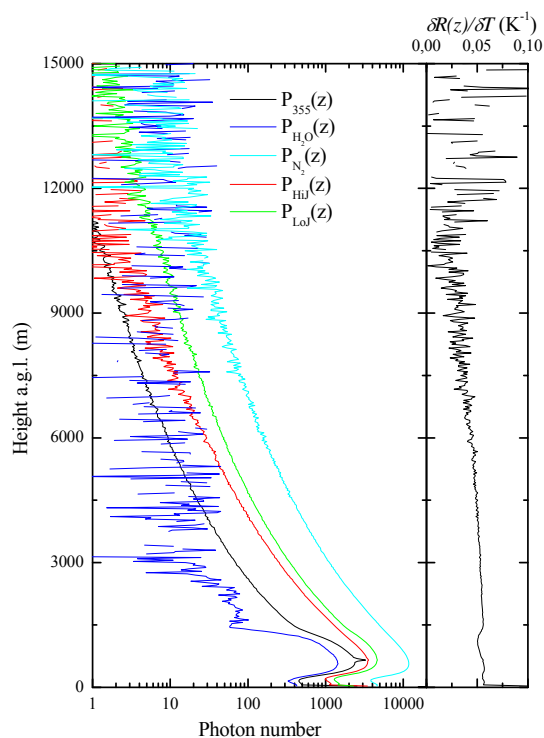
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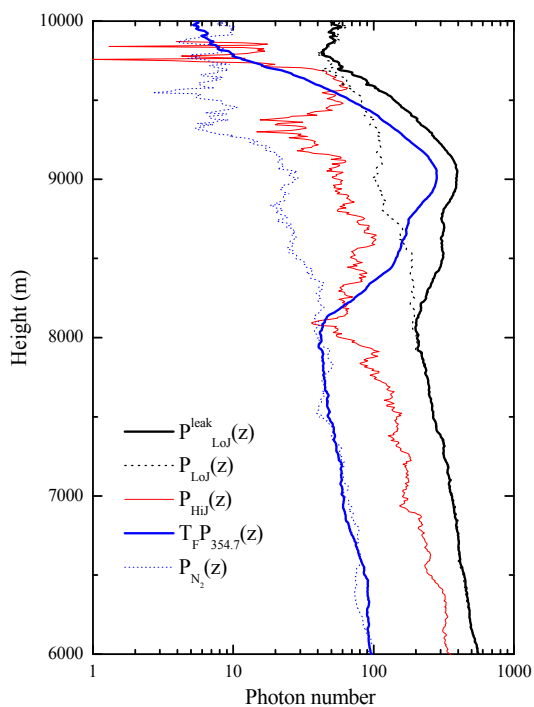
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2 **Figure 2:** (panel a) The mean photon numbers (10 sec average) for the considered signals, i.e. the water  
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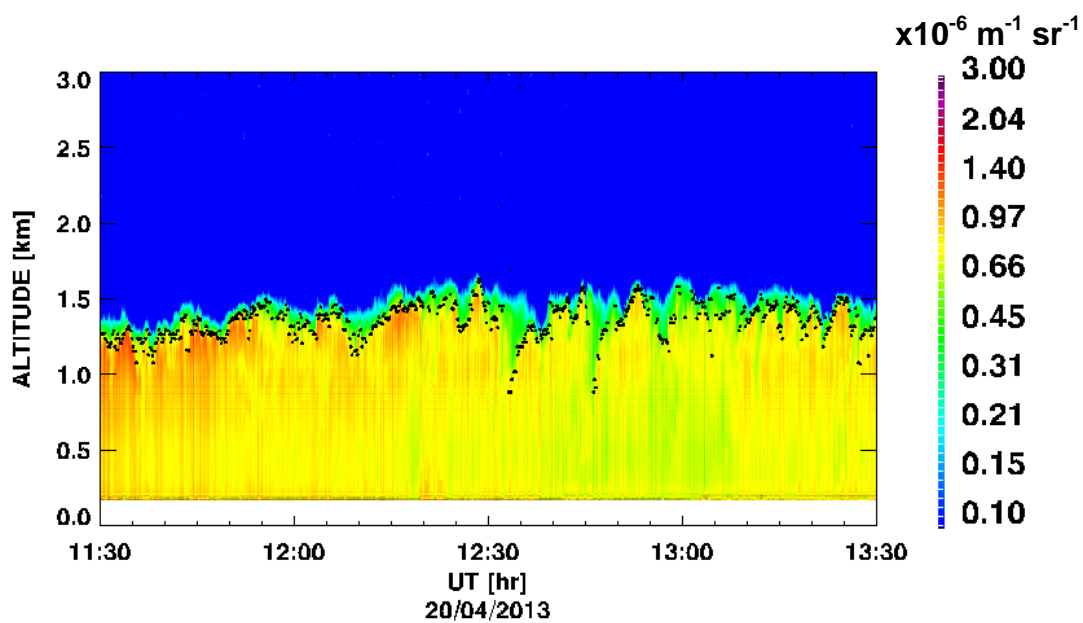
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**Figure 4:** Time-height cross-section of the particle backscatter coefficient,  $\beta_{par}$ , between 11:30 and

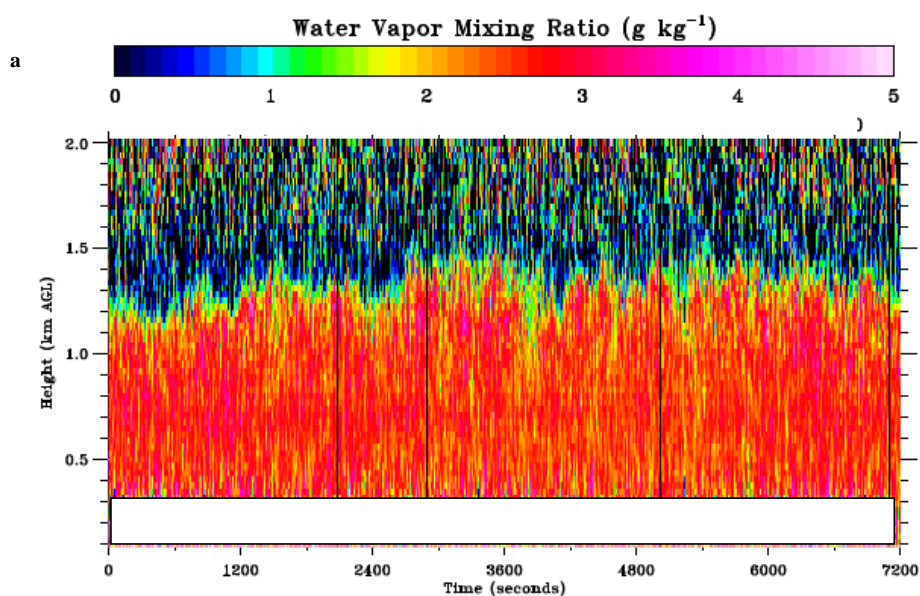
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13:30 UTC on 20 April 2013. The black line in the figure identifies the CBL height  $z_i$ .

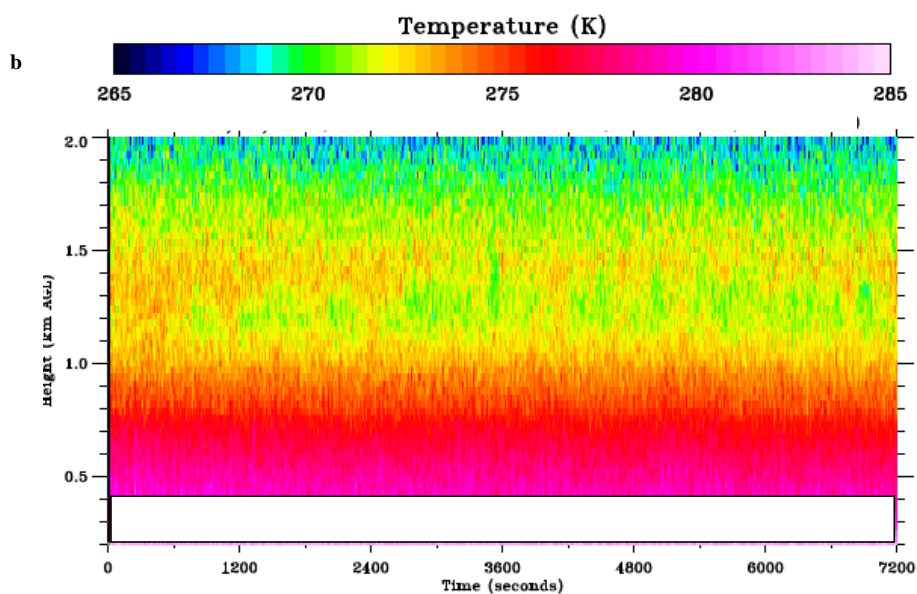
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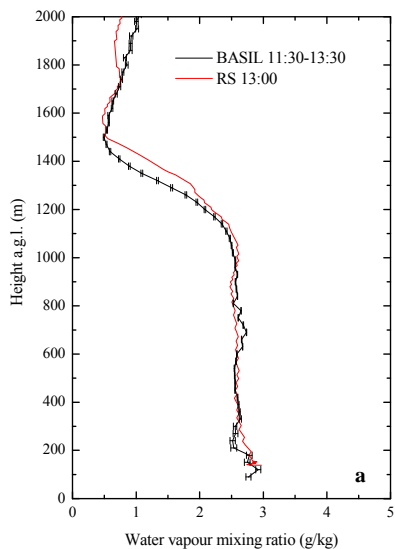
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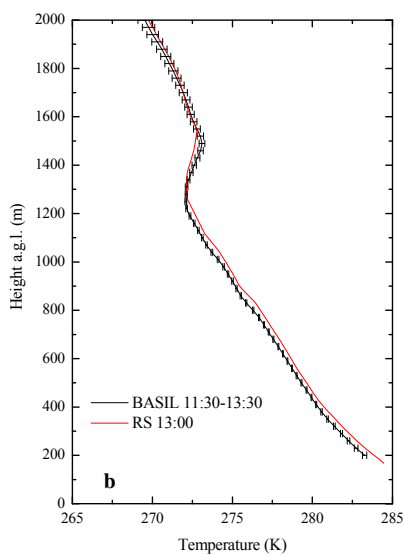


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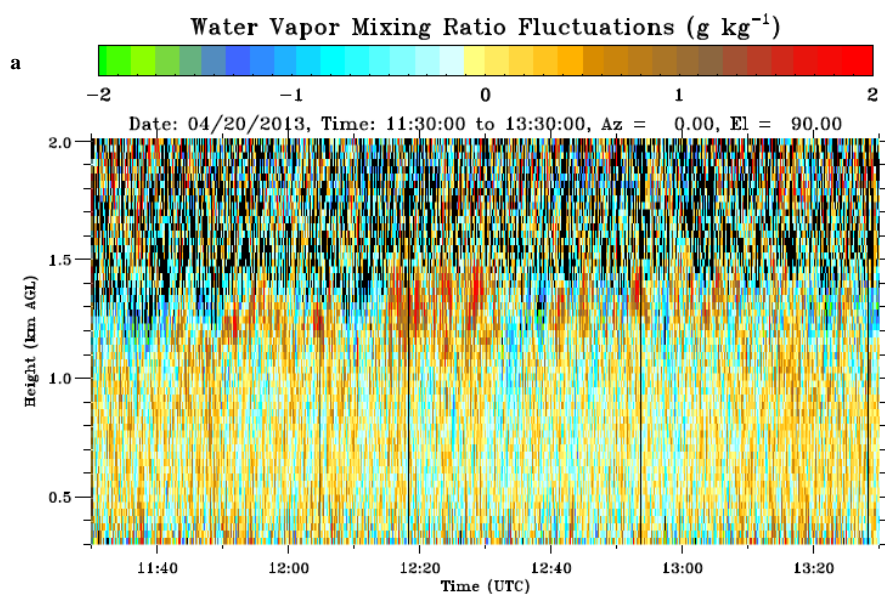
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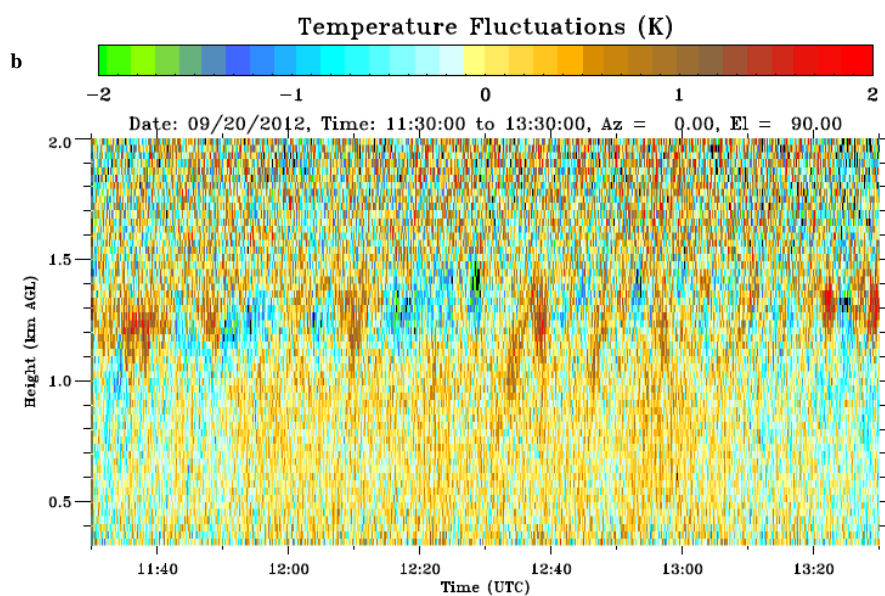
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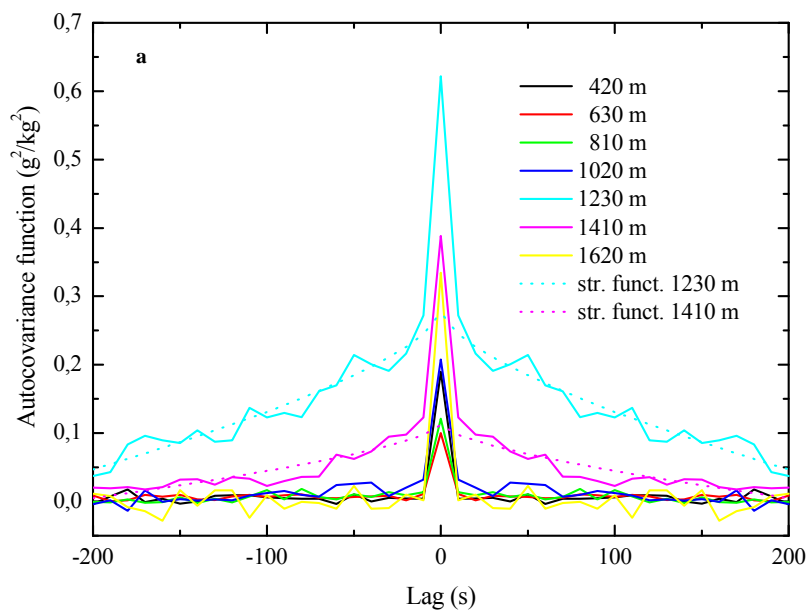
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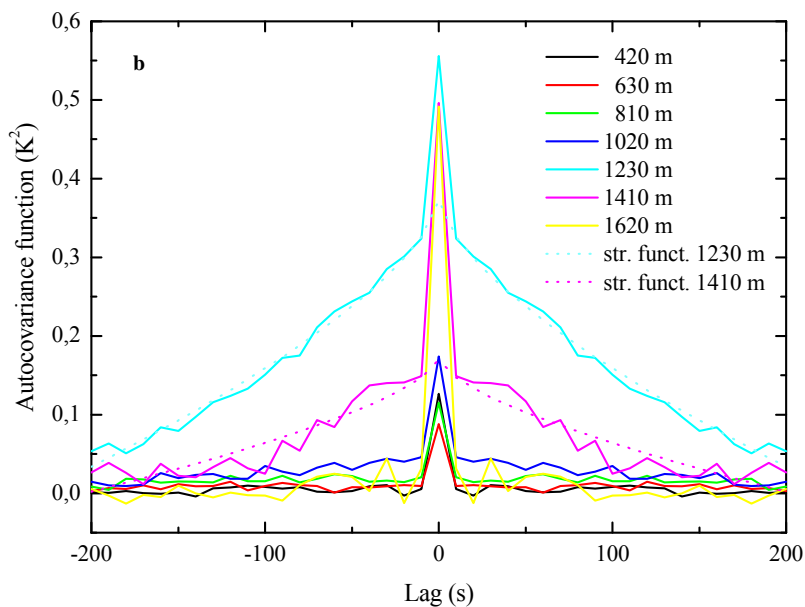
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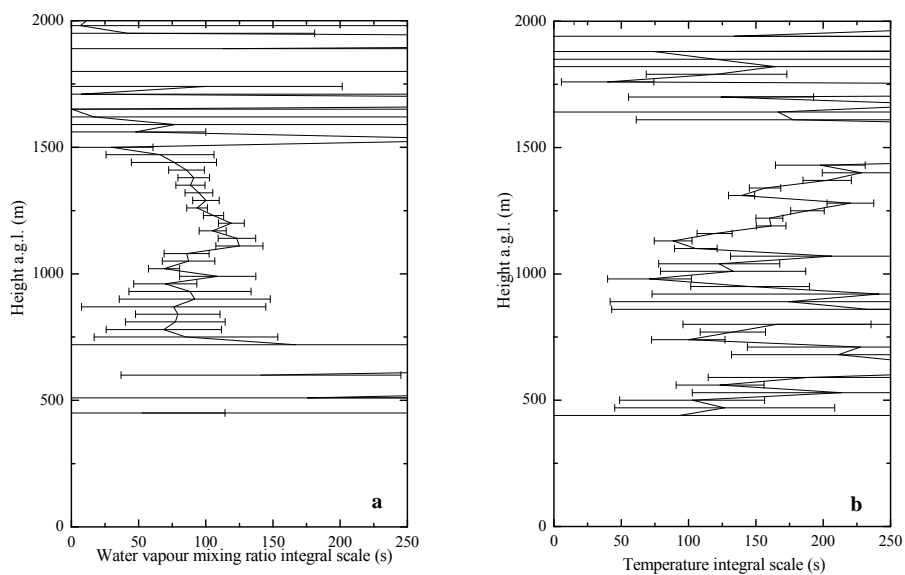
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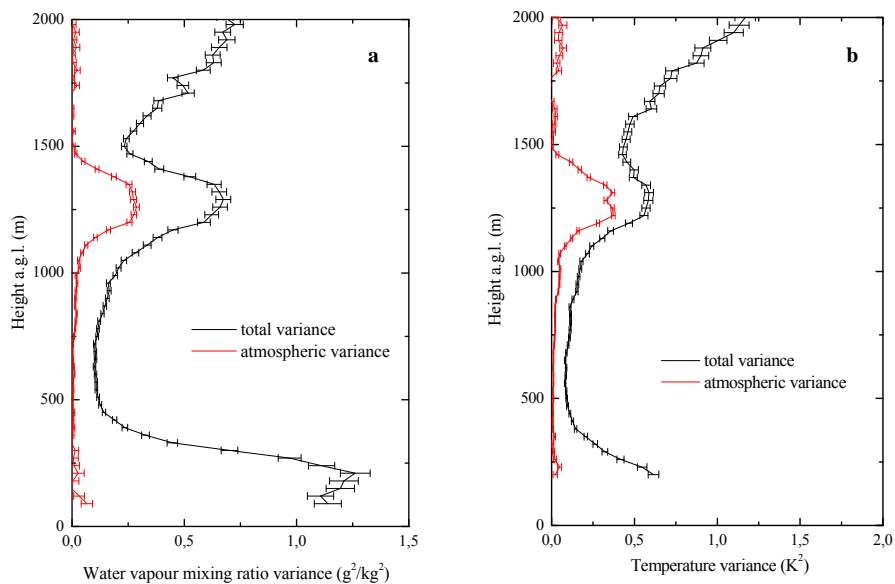
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2 **Figure 9:** Integral scale of water vapour mixing ratio (panel a) and temperature fluctuations (panel b)  
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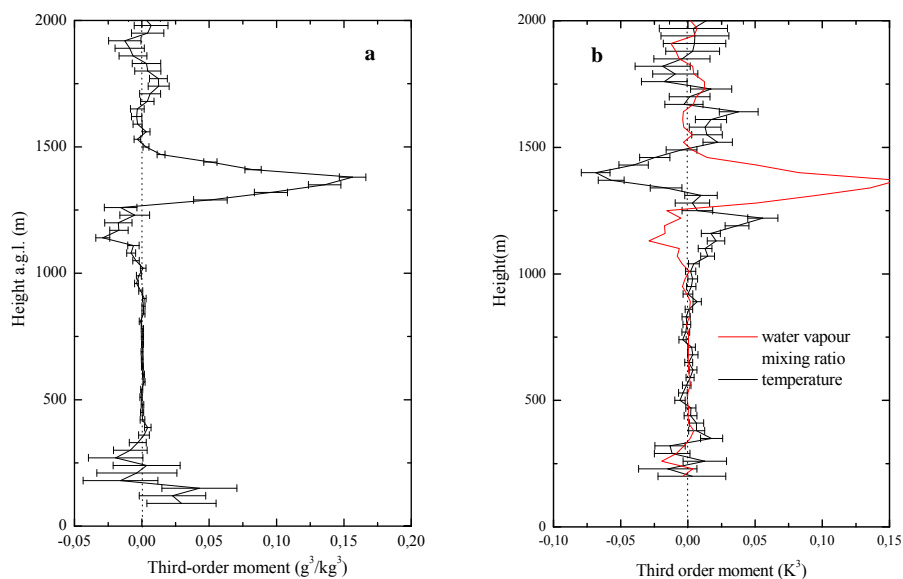


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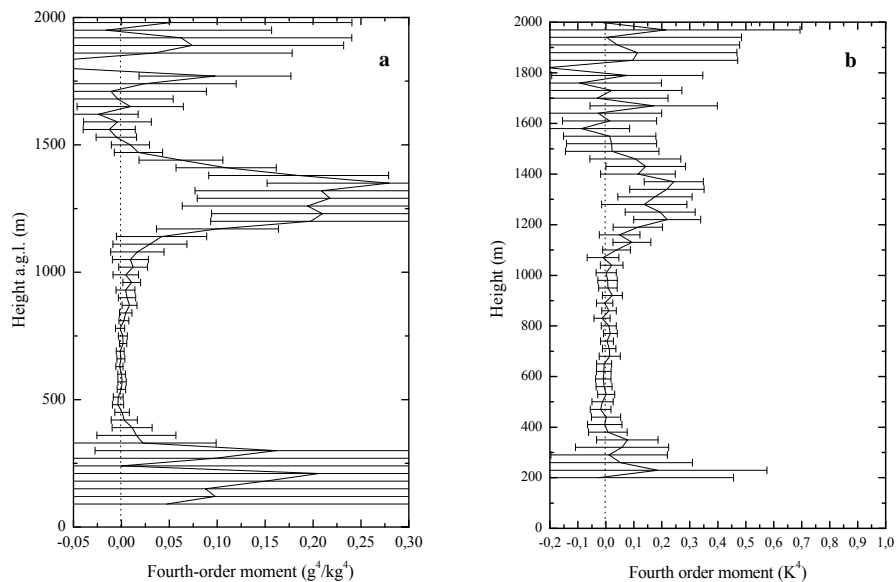
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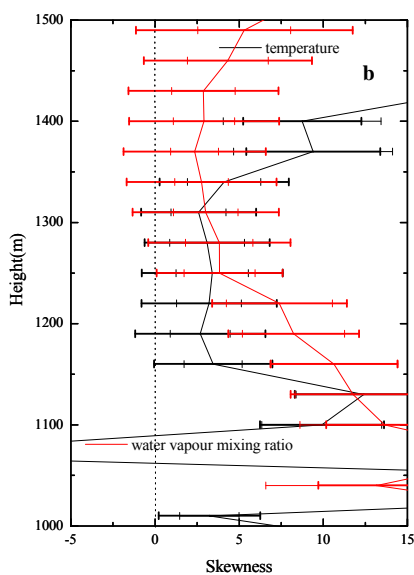
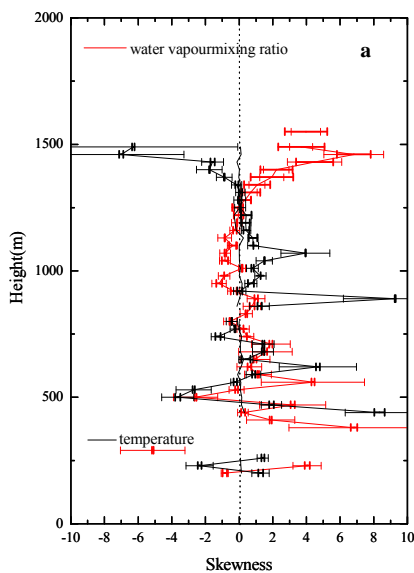
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