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Modelling the reversible uptake of chemical species in the gas phase by ice particles formed in a convective cloud

V. Marécal¹, M. Pirre¹, E. D. Rivière², N. Pouvesle³, J. N. Crowley³, S. R. Freitas⁴, and K. M. Longo⁴

¹Laboratoire de Physique et Chimie de l'Environnement et de l'Espace, CNRS-Université d'Orléans, Orléans, France

²Groupe de Spectrométrie Moléculaire et Atmosphérique, Université de Reims-CNRS, Reims, France

³Max-Planck-Institut für Chemie, Division of Atmospheric Chemistry, Mainz, Germany ⁴Center for Weather Forecasts and Climate Studies, INPE, Cachoeira Paulista, Brazil

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Correspondence to: V. Marécal (virginie.marecal@cnrs-orleans.fr)

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Abstract

The present paper is a preliminary study preparing the introduction of reversible trace gas uptake by ice particles into a 3-D cloud resolving model. For this a 3-D simulation of a tropical deep convection cloud was run with the BRAMS cloud resolving model using a two-moment bulk microphysical parameterization. Trajectories encountering the convective clouds were computed from these simulation outputs along which the variations of the pristine ice, snow and aggregate mixing ratios and size distributions were extracted. The reversible uptake of 11 trace gases by ice was examined assuming applicability of Langmuir isotherms using recently evaluated (IUPAC) laboratory data. The results show that ice uptake is only significant for HNO₃, HCl, CH₃COOH and HCOOH. For H₂O₂, using new results for the partition coefficient results in significant partitioning to the ice phase for this trace gas also. It was also shown that the uptake is largely dependent on the temperature for some species. The adsorption saturation at the ice surface for large gas concentrations is generally not a limiting factor

except for HNO₃ and HCl for gas concentration greater than 1 ppbv. For HNO₃, results were also obtained using a trapping theory, resulting in a similar order of magnitude of uptake, although the two approaches are based on different assumptions. The results were compared to those obtained using a BRAMS cloud simulation based on a single-moment microphysical scheme instead of the two moment scheme. We found similar results with a slightly more important uptake when using the single-moment scheme which is related to slightly higher ice mixing ratios in this simulation. The way to introduce these results in the 3-D cloud model is discussed.

1 Introduction

It is well known that deep convective clouds transport chemical species rapidly from the lower troposphere to the upper troposphere (e.g. Dickerson et al., 1987; Wang et al., 1995; Marécal et al., 2006; Rivière et al., 2006) and occasionally directly to the 9, 24361-24410, 2009

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lower stratosphere (e.g. Danielsen, 1993; Fischer et al., 2003). Convective transport is particularly important in the tropics since deep convection is frequent. Rain formed in the convective clouds also plays an important role in the perturbation of the chemical composition of the troposphere by washing out soluble species and also by reactions

- of the soluble species within the liquid phase (see review work by Warneck, 2000). Deep convective clouds also contain large amounts of ice crystals that can interact with the gas species in the air. The processes associated with the liquid phase mostly act up to altitude levels corresponding to about 235 K while the ice phase processes are dominant above.
- ¹⁰ Tropospheric chemistry models generally take into account the transport, the chemical transformation of the gas species and the interactions of these species with liquid droplets (e.g. Mari et al., 2000; Barth et al., 2000). The equilibrium between the gas phase and the liquid phase is given by the effective Henry's constant (Sander, 1999) and is not reached for all species on each model time step. For these species the evolution of the mixing ratio of the gas and the liquid species towards this equilibrium can be computed (Audiffren et al., 1998; Barth et al., 2001). Most models also take into account the chemical reactions in the liquid phase.

In contrast, the interaction of the gas species with ice particles is either not incorporated in models or, due to the complexity of the processes involved, is taken into

- account using simplified approaches. In nature some of the atmospheric ice crystals are dry, pure ice particles but others are mixed with liquid water or doped with gas species at their surface or even formed with composite crystals (Nitric Acid Trihydrate in polar stratospheric clouds for example). Their surface has a variety of geometric forms (e.g. needles, hexagonal plates, columns), some of them being complex (dendrites, ag-
- gregates). The different kinds and properties of real atmospheric ice particles are difficult to reproduce in laboratory studies. The interaction of the gas species with ice can be reactive or reversible or a mixture of both. Finally, the chemical species dissolved in the liquid droplets may be partially or totally retained when droplets freeze by riming or may be released to the gas phase. Because of this complexity, all these processes

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are generally not taken into account in tropospheric chemistry models, though a few have attempted to include a representation of some of these processes. Tabazadeh and Turco (1993) developed a surface chemistry model to describe the heterogeneous chemical processes on ice surfaces relevant to polar stratospheric clouds. In this model the non-reactive adsorption of HNO₃ and HCI was described by the Langmuir isotherm in terms of the equilibrium surface coverage for a non-dissociative adsorption. The reactive interaction stratospheric trace gases with ice surfaces was described by a first-order uptake coefficient. Using the same surface chemistry model, Tabazadeh et al. (1999) described the nonreactive adsorption of HNO₃ on cirrus clouds by the Langmuir isotherm assuming a dissociative adsorption. Meier and Hendricks (2002)

- ¹⁰ Langmuir isotherm assuming a dissociative adsorption. Meier and Hendricks (2002) performed sensitivity studies of the influence of uptake of HNO_3 by cirrus clouds on tropospheric chemistry. They used the formulation of Tabazadeh and Turco (1993) incorporating the laboratory data of Abbatt (1997) and Zondlo et al. (1997) for the non-reactive interaction of HNO_3 with ice surfaces. Nonreactive adsorption of H_2O_2 was
- optionally included. They also considered the uptake of adsorbed trace gases into the bulk of the ice crystal when the particle size distribution is changing due, for instance, to aggregation of ice crystals. They showed that these processes lead to a large decrease of NO_x and therefore to a reduction in ozone production. Using a three-dimensional cloud resolving model with interactive dynamics, aerosols, cloud microphysics, radia-
- tion and chemistry, Wang (2005) calculated the uptake of several key species based on first order uptake coefficients by ice particles formed in a tropical deep convective event. The simulations showed large concentrations of ozone and formaldehyde in the ice phase. HNO₃ in the ice phase is only located at the edge of the convective turrets. Nitric acid uptake by ice was also examined in the MATCH-MPIC Chemistry Transport
- ²⁵ Model (von Kuhlmann and Lawrence, 2006) in which different parameterisations of uptake were compared, including dissociative Langmuir uptake with different adsorption enthalpies and a description of the uptake analogous to the Henry's law allowing bulk uptake (Crutzen and Lawrence, 2000; von Kuhlmann et al., 2003). Several studies (Mari et al., 2000; Barth et al., 2001; Yin et al., 2002) also showed that when liquid

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droplets freeze during riming, the retention coefficient plays an important role for the transport of chemical species from the lower troposphere to the upper troposphere in convective clouds. Within the convective updraft, species of low solubility are transported by air and can interact with ice particles in the upper troposphere while soluble

species only reach the upper levels if degassed when droplets are freezing (retention coefficient close to 0) during riming. Yin et al. (2002) defined an additional parameter called the gas burial efficiency which is the amount of trace gases trapped within the ice particles. They showed that the transport of the gas species from the lower troposphere to the upper troposphere is not very sensitive to this burial efficiency because
 of the ice sedimentation.

In this context, the ultimate objective of this work is to include the removal of various chemical species from the gas phase by ice particles in a three-dimensional cloud resolving model for studying its impact on air composition in tropical deep convective environments. Here we present a preliminary study to assess the importance of the ice

¹⁵ uptake process for various trace gases in the cold part of a deep convective cloud (temperature lower than 235 K) in order to prepare its parameterisation in the 3-D model. This work is based on uptake calculations along air parcel trajectories encountering an idealized convective cloud simulated with the 3-D meso-scale model BRAMS.

In the cold part of a convective cloud, the trace gases which interact with the ice particles are:

- 1. low solubility species which are not efficiently scavenged by liquid droplets,
- 2. high solubility species which are degassed when liquid droplets freeze
- 3. any trace gas in air parcels of the environment entrained in the convective updraft at the ice formation level
- 4. trace gases initially in air parcels located at high altitude and experiencing ice formation because of the waves generated by the convective event.

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In the first stage, we limit our work to the simulation of reversible uptake of gas species by dry pure ice particles. Two different approaches have been proposed in the literature to describe this process. The first one is the Langmuir approach which assumes equilibrium between the gas phase concentration and the number (per $\rm cm^2$ of ice) of surface

- ⁵ adsorbed molecules. This equilibrium can be derived from the surface partition coefficient K_{linC} and the maximum number of sites available for adsorption N_{MAX}. A large number of laboratory studies (Abbatt, 1997; Chu et al., 2000; Bartels-Rausch et al., 2002; Dominé and Rey-Hanot, 2002; Hudson et al., 2002; Hynes et al., 2002; Sokolov and Abbatt, 2002; Winkler et al., 2002; Bartels-Rausch et al., 2004; Peybernès et al.,
- ¹⁰ 2004; Cox et al., 2005; Ullerstam and Abbatt, 2005; Kerbrat et al., 2007; von Hessberg et al., 2008) have been recently assessed by the IUPAC Subcommittee on Gas Kinetic Data Evaluation (http://www.iupac-kinetic.ch.cam.ac.uk) to derive the partition coefficients for several species of atmospheric interest. The second approach has been proposed by Diehl at al. (1995), Clegg and Abbatt (2001), Kärcher and Basko (2004),
- ¹⁵ Ullerstam and Abbatt (2005), Voigt et al. (2007) who suggest that the Langmuir approach is not valid in a real environment where the ice particles are generally not found in steady state conditions during cloud lifetime. Kärcher and Basko (2004) developed a theory of trapping of trace gases when ice particles grow by water deposition. Recently, Kärcher et al. (2009) extended this theory and applied it to HNO₃ using laboratory and
- field campaign data. In trapping theory the Langmuir approach is assumed to be valid only when the ice particle size remains constant. When ice is growing by water deposition, trace gases can be trapped into the bulk of the ice particles and are released to the gas phase only when the ice particles evaporate.

Here we present results on the ice uptake process based on both the Langmuir and the trapping approaches. For the Langmuir approach the uptake efficiency for 11 different species is treated. For the trapping approach, only HNO₃ is studied since the necessary parameters are only available for this species.

The descriptions of the BRAMS model, of the idealized simulation of a deep tropical convective cloud and the air parcel trajectory results are given in Sect. 2. Section 3 is

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devoted to the results of the Langmuir approach. The trapping results for HNO_3 are provided in Sect. 4. In Sect. 5 we compare the results of the two approaches and their implications for their use in a 3-D coupled meteorology-chemistry cloud resolving models.

5 2 Convective cloud simulation

2.1 Model description

The BRAMS model (Brazilian developments on the Regional Atmospheric Modeling System, http://www.cptec.inpe.br/brams) is used in the present study to simulate an idealized deep convective cloud developing in a tropical environment. BRAMS is a
version of the RAMS (Walko et al., 1995) tailored to the tropics, the main features of BRAMS are described in Freitas et al. (2009). The BRAMS/RAMS model is a multipurpose numerical prediction model designed to simulate atmospheric circulations spanning in scale from hemispheric scales down to large eddy simulations of the planetary boundary layer.

¹⁵ Two cloud microphysical schemes based on a bulk approach have been used. They both include rain, liquid cloud and five categories of ice: pristine ice, snow, aggregates, graupel and hail. They also assume a generalised gamma size distribution for each category of hydrometeors. Using this formalism leads for any category to :

$$n(D) = \frac{N_t}{\Gamma(\nu)} \left(\frac{D}{D_n}\right)^{\nu-1} \frac{1}{D_n} \exp\left(-\frac{D}{D_n}\right)$$

20 and

$$q = \frac{1}{\rho_a} \int_0^\infty n(D)m(D)dD = \frac{N_t}{\rho_a} \alpha_m D_n^{\beta_m} \frac{\Gamma(\nu + \beta_m)}{\Gamma(\nu)}$$

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(1)

(2)

where n(D) is the number density distribution (m⁻⁴), D is the diameter (m), N_t the total concentration (m⁻³). v is the shape parameter and D_n the characteristic diameter of the gamma function. q (kg/kg) is the mixing ratio, m(D) is the mass of an ice particle of diameter D, ρ_a is the air density (kg m⁻³) and α_m and β_m are the coefficients of the mass-diameter relationship for the considered hydrometeor category:

 $m(D) = \alpha_m D^{\beta_m}$

5

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with m(D) the mass in kg and α_m in kg m^{- β_m}.

The crystal shape assumed in the microphysical processes for the pristine ice and the snow is diagnosed at each grid point depending on temperature and relative humidity.

The first microphysical scheme used is the two-moment bulk scheme described in Meyers et al. (1997). It includes prognostic equations for both the mixing ratio and total concentration for total water, rain and the five categories of ice. In this case, only one of the three parameters of the gamma distribution needs to be set (either u, D, or N). The second microphysical scheme is the single moment bulk scheme

- v_{15} v, D_n or N_t). The second microphysical scheme is the single-moment bulk scheme described in Walko et al. (1995) which includes prognostic equations for the mixing ratios of total water, rain and all five ice categories, and a prognostic equation for the total concentration of pristine ice. This implies that, except for pristine ice, two parameters of the gamma distribution are set and do not vary during the simulation. In
- ²⁰ both microphysical schemes the water vapour and liquid cloud mixing ratios, and the total concentration of cloud droplets are diagnosed from the prognostic variables using criteria based on water vapour saturation.

In the model, pristine ice is formed by nucleation and can only grow by vapour deposition (Walko et al., 1995). The pristine ice category is restricted to relatively small crystals and large pristine ice crystals are categorized as snow. The snow category is defined as consisting of relatively large ice crystals which have grown by vapour deposition and riming. Aggregates are defined as ice particles that have formed by collision and coalescence of pristine ice, snow and/or other aggregates. Pristine ice, snow and

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(3)





aggregates are all low density and low fall-speed particles. Graupel is an intermediate density hydrometeor with an assumed spherical shape formed by moderate to heavy riming and/or partial melting of pristine ice, snow and aggregates. Hail is a high-density hydrometeor with an assumed spherical shape formed by freezing of raindrops or by riming or by partial melting of graupel.

2.2 Model setup

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Two simulations of an idealized tropical convection cloud based on the same general setup were run with the BRAMS model: a reference simulation (REF) using the two-moment bulk microphysical scheme and a sensitivity test (RUN1M) using the single-moment. By using two prognostic equations per hydrometeor category, the twomoment scheme provides a better description of the ice microphysics. But it requires more computing resources and is therefore generally not affordable when the chemistry module is coupled on-line to the BRAMS model. This is why a sensitivity simulation was run using the single-moment scheme to evaluate the impact of the microphysical scheme chosen on ice uptake. The shape parameter v is set to 2 for all hydrometeor categories in REF and RUN1M simulations. For RUN1M, the characteristic diameter D_{p} is set to 0.173 mm for rain, 0.064 mm for snow, 0.190 mm for aggregates, 0.346 mm for graupel and 0.520 mm for hail while the total concentration N_t is set to 7.5×10^7 particles m⁻³ for liquid cloud. These values were chosen because they correspond to approximately the mean values provided by the two-moment simulation 20 (REF).

In both simulations the parameterization used for longwave/shortwave radiation is from Harrington (1997). It is a two-stream scheme which interacts with liquid and ice hydrometeor size spectra. The turbulence parameterization is from the Mellor and Yamada (1982) level 2.5 scheme which employs a prognostic turbulent kinetic energy.

The domain is $120 \text{ km} \times 120 \text{ km}$ with a 1 km horizontal grid spacing. It extends vertically from the surface to 25 km altitude with a 200 m grid spacing up 18 km and coarser above. The time-step is 2 s. To simulate an idealized tropical convective cloud we

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used temperature, pressure, horizontal wind and humidity data from a radio-sounding launched from Bauru (Brazil, 22.4° S, 49.0° W) on 3 February 2004 at 18:00 UT in the frame of the TroCCiBras project (Tropical Convection and Cirrus experiment Brazil; Held et al., 2008). These meteorological quantities are assumed to be horizontally homogeneous at the beginning of the simulation. A warm and moist perturbation is applied during the first 750 s of the simulation below 1 km altitude and over a horizontal area having a 15 km diameter. This perturbation is located in the south west part of the domain. This leads to an unstable atmosphere and creates a convective cloud, which reaches the tropical upper troposphere and forms liquid and ice hydrometeors.

10 2.3 Results of the cloud simulations

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The results of the REF simulation for pristine ice, snow and aggregate mixing ratios are displayed in Fig. 1. Graupel and hail categories are not shown since they are assumed in the BRAMS model to carry liquid water on their surface. Therefore they are not considered for ice uptake calculations which only apply to dry ice. Hereafter dry ice will refer to the sum of pristine ice, snow and aggregates.

After about one hour into the simulation, convection starts to develop leading to significant ice contents up to about 16 km altitude (Fig. 1a–c). The top part of the convective cloud is mainly composed of pristine ice (up to $0.9 \, g \, kg^{-1}$ at 14 km) and the lower part by falling aggregates (up to $0.9 \, g \, kg^{-1}$ at 10 km). Snow mixing ratios have intermediate values (up to $0.7 \, g \, kg^{-1}$ at 14 km) because once large values are

- have intermediate values (up to 0.7 g kg⁻¹ at 14 km) because once large values are reached snow is converted in the model into aggregates. After two hours (Fig. 1d–f) the convective updraft is less intense leading to lower total ice contents. The cell has travelled North-eastwards thanks to advection and developed a stratiform part. At this stage, pristine ice mixing ratios are still large. Aggregates have had sufficient time to
- grow and to sediment leading to values up to 0.6 g kg⁻¹ around 9 km altitude. Later in the simulation (Figs. 1g–i) the convective cell is in a dissipating stage. The remaining dry ice is mainly in the 12–14 km altitude range and composed of slow falling pristine and snow crystals. The mixing ratios of both pristine ice and snow decrease as a



function of time with a maximum of $0.30-0.35 \,\mathrm{g \, kg^{-1}}$ after 2 h of simulation down to a maximum of $0.2 \,\mathrm{g \, kg^{-1}}$ after 3.5 h of simulation.

The results for the RUN1M simulations are displayed in Fig. 2. The general development of the ice in the convective cell is similar to the REF simulation. The RUN1M ⁵ gives mixing ratios for dry ice of the same order of magnitude but slightly larger (~20%) than the REF simulation during the whole simulation. It also provides less pristine ice and more snow and aggregates showing that pristine ice is more rapidly converted into snow and aggregates in the RUN1M simulation.

2.4 Air parcel trajectories

- ¹⁰ Trajectories are calculated from the simulation outputs using the trajectory model developed by Freitas et al. (2000). The seven trajectories selected illustrate all the different types of microphysical evolution that experience dry ice particles above the 235 K isotherm in the 3-D convective cloud simulation. Altitudes as a function of time for the seven trajectories of the REF run are displayed in Fig. 3a. Two of the trajectories (purple and light blue lines in Fig. 3a) come from the lower troposphere and are uplifted by the convective updraft. Liquid and then ice particles are formed in these air parcels. One trajectory (dark green line) intercepts the convective updraft in the midtroposphere. The other four start and stay in the upper troposphere (dark blue, light green, orange and red lines). Figure 3b shows the evolution of temperature along the
- seven trajectories. In the upper troposphere, temperatures range from 235 K to 203 K. Dry ice particles are first found on all trajectories between 1.07 and 1.20 h after the beginning of the simulation (Fig. 4a). Water vapour deposition occurs when saturation above ice is larger than 1. Figure 4a shows that dry ice is found initially in sub-saturated conditions for the 4 upper tropospheric trajectories (orange, red, light green and dark
- ²⁵ blue) and for the trajectory coming from the mid-troposphere (dark green). For these trajectories dry ice in the air parcels considered comes initially from the interception of the air parcel by the convective updraft. Figure 4b–d show pristine ice, snow and





aggregates as a function of time along the 7 trajectories. At the beginning of the trajectories, pristine ice, snow and aggregates mixing ratios are similar. At the end of the simulation pristine ice is the main ice category. The snow mixing ratio is smaller than the pristine mixing ratio but still significant. The mixing ratio of aggregates is very low and negligible with respect to snow and pristine ice.

The 7 trajectories in the RUN1M simulation, ending at the same location as in the REF simulation are displayed in Fig. 5. The RUN1M simulation shows a similar general behaviour as in REF for the altitude, the temperature and the dry ice mixing ratio as a function of time. Snow and aggregates mixing ratios are larger in the RUN1M simulation than in the REF simulation (Fig. 5c and d). On the contrary pristine ice mixing ratios are lower in the RUN1M simulation than in the REF simulation than in the REF simulation (Fig. 5c and d). This is consistent with the comparison between Figs. 1 and 2.

3 Description and results of the Langmuir approach

3.1 The Langmuir theory

¹⁵ The Langmuir theory establishes the equilibrium between the gas phase concentration of each species and the ice surface concentration for reversible adsorption of the species by ice particles. In this approach, it is assumed that the number of adsorbed molecules per ice surface unit cannot be higher than a maximum value N_{MAX}. This maximum number is measured in laboratory for each species. It does not usually ²⁰ depend on temperature. Assuming equilibrium between the adsorption flux and the desorption flux leads to the relation between the species concentration on the ice surface n_S (molecules cm³ of air) and the gas concentration n_G (molecules cm³ of air) if the interaction is non-dissociative:

 $n_S = A\theta N_{MAX}$

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(4)

where A is the surface area of the ice particles (cm² cm⁻³), N_{MAX} is in molecules cm⁻² and θ is the fractional coverage of the ice surface.

The fractional coverage is defined by:

$$\theta = \frac{\frac{K_{\text{linC}}}{N_{\text{MAX}}} n_G}{1 + \frac{K_{\text{linC}}}{N_{\text{MAX}}} n_G}$$

⁵ where K_{linC} (cm) is the partition coefficient. This coefficient is measured in laboratory studies and depends on trace gas. It usually increases when temperature decreases. For low gas concentrations, n_G, the denominator in relationship (Eq. 5) is close to 1 which leads to a linear dependence of n_S on n_G :

 $n_{S} = AK_{linC}n_{G}$

- ¹⁰ For higher gas concentrations, saturation occurs (θ close to 1) and leads to the decrease of the ratio $\frac{n_S}{n_G}$ when n_G increases. The limit between the low concentrations, for which the surface concentration is proportional to the gas phase concentration, and the high concentrations, for which saturation occurs, depends on K_{linC} and therefore on the trace gas considered.
- ¹⁵ In case of a competitive adsorption of two or more trace gases a modified form of the Langmuir isotherm must be used. For two trace gases i and j in competition the relation (Eq. 4) must be written:

$$n_{Si} = \frac{AK_{linC_i}n_{Gi}}{1 + \frac{K_{linC_j}}{N_{MAX_i}}n_{Gi} + \frac{K_{linC_j}}{N_{MAX_j}}n_{Gj}}$$

where index i refers to trace gas i and index j to trace gas j.

In this case, trace gases in contact with the surface are assumed to compete for similar adsorption sites (e.g. von Hessberg et al., 2008). Such competive adsorption has been applied to calculate the surface concentration of HCI (needed e-g- for

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(5)

(6)

(7)

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heterogeneous processing rates of CIONO₂) in the presence of HNO₃ (IUPAC, 2009, http://www.iupac-kinetic.ch.cam.ac.uk).

The temperature dependence of K_{linC} is given by K_{linC}=Aexp(B/T). Table 1 gives the parameters A and B for the 11 species HCl, HNO₃, PAN, H₂O₂, HCHO, CH₃OH,
C₂H₅OH, C₃H₇OH, HCOOH, CH₃COOH and CH₃COCH₃ taken into account in this paper as well as N_{MAX}. These species were chosen because partition coefficients have been evaluated by the IUPAC Subcommittee on Gas Kinetic Data Evaluation (http://www.iupac-kinetic.ch.cam.ac.uk). For H₂O₂, we also used preliminary results of the Max Planck Insitute fur Chemie in Mainz which will be reported in detail elsewhere (Pouvesle et al., in preparation, 2009).

Briefly, partition coefficients for H₂O₂ were obtained in the MPI laboratory at temperatures between 203 and 233 K in the same apparatus used to study the interaction of several oxidized organic trace gases with ice surfaces at upper tropospheric temperatures (Winkler et al., 2002; von Hessberg et al., 2008). Results were obtained using both single species adsorption of H₂O₂ and a competitive approach, whereby the displacement of HC(O)OH from the ice surface by adsorbed H₂O₂ was examined. Both methods yielded consistent results and values obtained in the more reliable single species adsorption experiments may be summarisd as K_{linC} (203–233 K)=2.1×10⁻⁵ exp(3800/T) cm. The value calculated at 228 K (K_{linC}≈360 cm) is thus more than 2 orders of magnitude larger than the value of 1.6 cm, reported by Clegg and Abbatt (2001) for the temperature range 228–240 K.

Figure 6 shows the partition coefficient K_{linC} for the 11 trace gases as a function of the temperature. Table 1 and Fig. 6 show that for various trace gases large differences exist between the absolute value of the partition coefficients at any one temperature ²⁵ and on their temperature dependence. In contrast, the maximum number of species N_{MAX} adsorbed on the ice surface is similar for all the trace gases as it is largely a characteristic of the ice surface (e.g. number of active adsorption sites) for the small molecules considered here.

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In the model, an instantaneous equilibrium was assumed between the ice surface concentration and the gas phase concentration at each time step of the calculations. This assumption will be justified in Sect. 3.3.

3.2 Surface area of the ice particles

⁵ The ice surface area is required to determine relation (Eq. 4). For the total number of ice particles in an air parcel, assuming that all particles of the same category in the same size class have the same surface, the ice surface area, A, is given by:

$$A = \sum_{i=1}^{m} \left(\int_{0}^{\infty} \sigma_{i}(D) n_{i}(D) dD \right)$$

where i refers to one of the model ice categories, m is the number of ice categories. As previously explained we only take into account pristine ice, snow and aggregate categories (m=3). σ_i is the surface of each individual ice particle, D is the diameter of an equivalent spherical particle having the same volume as the actual ice particle and

 $n_i(D)$ is the size distribution of each ice category given by relation (Eq. 1).

In the two microphysical schemes of the BRAMS model, the geometrical form of pris-¹⁵ tine ice and snow are diagnosed during the simulation at each grid point and timestep depending on air temperature and relative humidity. Results from the REF simulation have shown that the geometrical form for pristine ice and snow that is the most frequently predicted is the hexagonal column. Therefore this geometrical form was assumed for these two categories of ice in the Langmuir uptake approach. The as-²⁰ pect ratio which gives the relation between the diameter D and the length L of the columns is set to D=2.5 L^{0.6} as in Wyser and Yang (1998) who fitted the data given

- in Hobbs (1974). For aggregates the geometrical form is more complex. Here it is assumed that they are formed of n hexagonal columns and that the surface and the volume of each aggregate particle are n times the surface and the volume of an individ-
- $_{5}$ ual hexagonal column. Consistent with usage in the BRAMS model the coefficients $lpha_{m}$

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(8)



and β_m of the mass diameter relationship (Eq. 3) used are respectively 110.8 kg m^{-2.91} and 2.91 for pristine ice, 2.739×10⁻³ kg m^{-1.74} and 1.74 for snow and 0.496 kg m^{-2.4} and 2.4 for aggregates.

This leads to the following ice surface area for each ice category

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 $= A = N_t n [(0.01747/n^{6/11}) D_n^{1.636} \Gamma(3.636) / \Gamma(2) + (20.85/n^{8/11}) D_n^{2.182} \Gamma(4.182) / \Gamma(2)]$ (9)

where A is in $m^2 m^{-3}$, D_n (m) is the characteristic diameter of the distribution of the ice category, N_t (m⁻³) is the ice category concentration Γ is the gamma function and n is the number of hexagonal columns forming the ice particle; n is 1 for pristine ice and snow. It has been assumed to be 4 for aggregates in the REF and the RUN1M simulation.

 D_n and N_t are provided at each time step by the microphysical scheme of the BRAMS model. Note that in the RUN1M simulation D_n is set to a constant value for snow and aggregates while it is a prognostic variable in the REF simulation.

- The choice of the number, *n*, of hexagonal columns which compose the aggregates is arbitrary. Choosing n=8 or n=2 leads to a change in the surface area of only $\pm 23\%$ relatively to n=4. The reason for this relatively small change in the surface area is that σ_i in relation (Eq. 8) is a function of the diameter D of an equivalent spherical particle having the same volume as the actual ice particle: increasing or decreasing the number of hexagonal columns per aggregates is partially balanced by the decrease or the increase of the volume and of the surface of each hexagonal column. Sensitivity
- tests on the number n of hexagonal column per aggregates in the Langmuir approach are presented in Sect. 3.3.

On the 7 selected trajectories of the REF simulation the total surface area of dry ice particles has been computed. It gives values between $2 \times 10^3 \mu m^2 cm^{-3}$ and $2 \times 10^4 \mu m^2 cm^{-3}$ on the high altitude trajectories. These values are consistent with the measurements made during the CRYSTAL-FACE experiment in Florida (Popp et al., 2004) in which surface area between $2 \times 10^2 \mu m^2 cm^{-3}$ and $4 \times 10^4 \mu m^2 cm^{-3}$ have been measured. In the ascending part of the trajectories the surface area can reach

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 $1.5 \times 10^5 \mu m^2 \, cm^{-3}$ due to the large ice mixing ratios observed on this part of the trajectories.

As already discussed, the size distribution of the pristine ice category has a smaller characteristic diameter D_n than the snow category. For the same mixing ratio, the surface area of the pristine ice category is expected to be larger than the surface area of the snow category because of the larger number of pristine ice crystals. This is confirmed by the results of Fig. 7 which shows the ratio of the surface area of snow over the surface area of pristine ice as a function of the volume mixing ratio of snow over the volume mixing ratio of pristine ice. We observe in particular that if the snow

- volume mixing ratio is the same as the pristine ice mixing ratio (ratio of volume mixing ratio is 1) the surface area of snow is smaller than the surface area of pristine ice (ratio of surface area smaller than 1). This figure also shows that the aggregates category, which has a smaller number of crystals than the pristine ice and the snow categories, has nevertheless a larger surface area than these two categories. This is due to the
- ¹⁵ fact that the individual surface of each aggregate is larger than the individual surface of pristine ice and snow crystals for the same equivalent diameter D.

3.3 Results

Calculations of the uptake of trace gases by the ice surface using the Langmuir approach were performed using the ice mixing ratios for pristine ice, snow and aggregates

- along the seven trajectories. For each species the sum of the mixing ratio in the gas phase and of the mixing ratio on the ice surface is assumed to be conserved along the trajectories. In reality this is not generally observed due to exchanges in the gas phase with the environment and to sedimentation. Nevertheless, the aim of this paper is not to compute exactly the evolution of the mixing ratio of the species on the trajectories
- ²⁵ but to assess the importance of the ice uptake of the species. The important parameter is therefore the ratio of the gas phase mixing ratio on the total mixing ratio (gas phase + surface adsorbed gases) at each timestep of the simulation. In order to take

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into account the range of total mixing ratios possibly encountered in the atmosphere, the calculations were done with different total mixing ratio up to 10 ppbv.

In these calculations a timestep of 120 s was chosen. We checked that this timestep is sufficient to reach the equilibrium. For this we calculated the rate constant R (s^{-1}) to ⁵ reach the equilibrium:

$$R = k_{des} + \frac{\alpha u A(1 - \theta)}{4}$$

where k_{des} is the desorption rate, α is the accommodation coefficient, u is the thermal velocity of the gas species, A is the surface area of the ice particles and θ is the fractional coverage of the ice surface (0< θ <1). The time τ to reach the equilibrium is $\tau = 1/R$. It depends on the species, on the gas phase concentration and on the characteristics of the air parcels. In the range of the gas concentration assumed in the present paper (mixing ratio lower than 10 ppbv) and on average over all the trajectories τ varies between 3 s and 45 s depending on the species. Since the time step of the ice uptake calculations is 120 s, the assumption of an instantaneous equilibrium between the gas phase and the ice surface concentration is justified.

Table 2 gives the mean mixing ratio, the standard deviation and the minimum mixing ratio in the gas phase of the 11 species computed when dry ice is present in the 7 selected trajectories from REF simulation. A constant total mixing ratio of 100 pptv (gas phase + species adsorbed on the ice surface) has been used in these calculations.

- On average over the 7 trajectories the uptake of HNO₃ and HCl by ice particles is very large (≈85%±15% for HNO₃ and 50%±20% for HCl). It is lower but significant for CH₃COOH (≈18%±14%) and HCOOH (6%±6%). For these 2 species the maximum uptake can be large with 68% and 36%, respectively. For the other species (C₂H₅OH, HCOOH, PAN, HCHO, CH₃COCH₃ and CH₃OH) uptake is small or negligible because they have law participants (and Fig. 6). For the Q the uptake is called a significant for the participant.
- ²⁵ they have low partition coefficients (see Fig. 6). For H₂O₂ the uptake is significant (8%±7%) if the partition coefficient of Pouvesle et al. (2009) is used. It is negligible if the partition coefficient of Clegg and Abbatt (2001) is used.

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(10)





As the photolysis of H_2O_2 can be a significant source of HO_x (OH, HO_2) e.g. in the convectively influenced upper troposphere over the oceans (Prather and Jacob, 1997; Cohan et al., 1999; Collins et al., 1999). Assessment of the impact of H_2O_2 in regions impacted by convective inflow require correct values for the partition coefficient.

- Figure 8a shows the mixing ratio of HCl in the gas phase computed in the REF simulation. A constant total mixing ratio of 100 pptv is assumed as in Table 2. The gas concentration decreases rapidly for all trajectories around 1.2 h of simulation with minimum values ranging from 0.084 to 0.009 ppbv. This corresponds to the time when large dry ice mixing ratios are found on all trajectories (see Fig. 4a). Then it increases
- with time fairly steadily for all trajectories as dry ice mixing ratios decrease. The uptake efficiency is well correlated with the dry ice mixing ratio. It does not depend on the origin of the trajectory since the lower values of gas concentrations are found for trajectories coming from the lower troposphere (purple and light blue lines) as well as the mid-troposphere (dark green line) and upper troposphere (orange line).
- ¹⁵ Comparing Figs. 4d and 8a shows that the ice aggregates have a larger impact on the uptake of species than pristine ice or snow. This is illustrated by the purple, dark green, light blue and dark blue trajectories. For these trajectories the variations in time of the gas concentration is closely related with the variations of the aggregates mixing ratio when and where this mixing ratio is significant. This is not only due to their larger
- mixing ratio but also to their larger surface area compared with pristine ice and snow for the same mixing ratio. At the end of the simulation, the aggregates mixing ratio is very low on the selected trajectories. As a consequence the uptake of the species is mainly dependent on the pristine ice and on the snow mixing ratios.

The results for CH₃C(O)OH are shown in Fig. 8b. Comparing Figs. 3b, 4a and 8b show that uptake is not only a function of the dry ice mixing ratio. It is also a function of the temperature for trace gases having a partition coefficient strongly dependent on temperature such as CH₃C(O)OH (Table 1). In Fig. 8b the uptake is more important on the red trajectory for which the dry ice mixing ratio is small (Fig. 4a) and the temperature is low (Fig. 3b) than on the dark blue trajectory for which the dry ice mixing ratio is larger

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(Fig. 4a) and the temperature is higher (Fig. 3b). The influence of the temperature is emphasized in comparing the uptake of $CH_3C(O)OH$ (Fig. 8b) with the uptake of HCI (Fig. 8a) for which the partition coefficient is not strongly dependent on the temperature. Clearly uptake on the low temperature trajectories at high altitude (red and orange) is much more important for $CH_3C(O)OH$ than for HCI relatively to the other trajectories.

In the Langmuir approach the trace gas mixing ratios on the ice surface evolves linearly as a function of the gas mixing ratio for low values of this gas mixing ratio. Due to saturation effects at the ice surface it increases more slowly when the gas mixing ratio is larger. The saturation effect is clearly seen for HNO₃ by comparing Fig. 9a–c assuming respectively a total mixing ratio of 100 pptv, 1 ppbv and 10 ppbv. The gas mixing ratio relatively to the total mixing ratio is increasing when the total mixing ratio is increasing on each trajectory. Figure 10 shows the ratio of the mean mixing ratio on the 7 trajectories of 4 species HNO₃, HCI, CH₃COOH and H₂O₂ (MPIC) in the gas phase on the total mixing ratio as a function of the total mixing ratio. The total mixing

- ¹⁵ ratio varies in the range 100 pptv–10 ppbv. The saturation effect occurs above a total mixing ratio of \approx 1 ppbv for HNO₃ and HCl. It is small for CH₃COOH and H₂O₂. It has been checked that it is not occurring for the other species. Nevertheless if a saturation effect occurs for HNO₃ or HCl, this effect has an impact on the gas phase mixing ratio of all the other trace gases. According to relation (Eq. 7) the saturation effect of HNO₃
- or HCl leads to a decrease of the surface concentration of the other trace gases if they compete for the same adsorption sites. This impact will have to be taken into account in a 3-D model.

Table 3 shows the impact of the number of hexagonal columns assumed to compose an aggregate ice particle on the gas phase mixing ratios of HNO₃, HCl and CH₃COOH in the 7 selected trajectories from REF simulation. For these three species the impact on the mean mixing ratio is very small: 0.3% for CH₃COOH, 0.7% for HCl and 1.4% for HNO₃ when the number of hexagonal columns is assumed to be 8 instead of 4. This is explained by the smaller average mixing ratio of aggregates particles on all trajectories relatively to the mixing ratios of snow and pristine ice (Fig. 4). The minimum gas mixing

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ratios are observed on the purple trajectory for HNO_3 (Fig. 9a) and HCl (Fig. 8a) and on the orange trajectory for CH_3COOH (Fig. 8b). On these trajectories at the time of the minimum, the ratio of the surface area of aggregates relatively to the total ice surface area is large: 60% on the purple trajectory and 23% on the orange trajectory. This is the reason why the impact on the minimum gas mixing ratio is larger than on the mean

the reason why the impact on the minimum gas mixing ratio is larger than on the mean gas mixing ratio: 11.5% for HNO_3 and HCI and 3.4% for CH_3COOH . In general the gas phase mixing ratio is therefore not very sensitive to the exact number of hexagonal columns which compose an aggregate particle.

The results for RUN1M simulation are also given in Table 2. The mean and the minimum mixing ratios in the gas phase computed in RUN1M simulation (Table 2) are consistent but usually lower than in the REF simulation. This is mainly related to the fact that the RUN1M simulation provides larger dry ice mixing ratios along the trajectories than the REF simulation. It cannot be attributed to the temperature differences between the two simulations because they are small.

¹⁵ 4 Description and results of the trapping theory for HNO₃

4.1 The trapping theory

In this theory, it is assumed that when ice grows by water vapour deposition, a surfaceadsorbed trace can be trapped in the bulk of the ice particles. In contrast to reversible, surface-only adsorption, in which the adsorbed trace gas can rapidly desorb, trapped molecules are retained in the ice particles until it evaporates. From these assumptions a trapping theory was developed by Kärcher and Basko (2004). It has been recently improved by Kärcher et al. (2009) to take saturation of the uptake process on the ice surface layer into account. Following Kärcher et al. (2009) the number of gas phase particles trapped per ice particle per unit of time is defined by

 $\frac{dN}{dt} = 4\pi r^2 \frac{dr}{dt} n_v$



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where n_{ν} is the species concentration trapped in the bulk of the ice, r is the radius of the ice particle and $\frac{dr}{dt}$ is the increase of the radius of the particle per unit of time (Pruppacher and Klett, 1997)

- The bulk concentration n_v is linked to the concentration in the gas phase by imposing continuity of the species fluxes in the gas, in the bulk and at the surface boundary. The flux at the surface boundary is a balance between the adsorption flux, taking into account surface saturation, and the desorption flux in a reference frame moving with velocity $\frac{dr}{dt}$ in the direction of increasing particle radius. The desorbed flux depends on an effective escape velocity, v, a result of complex processes occurring in the surface layer of the ice particle. v is derived from results of laboratory studies and field measurements (Kärcher et al., 2009), the surface desorption lifetime, τ_{des} , playing an important role. Up to now the escape velocity has been estimated empirically
- only for HNO₃ using the Langmuir partition coefficient given in the IUPAC database (http://www.iupac-kinetic.ch.cam.ac.uk/). In the present paper the trapping theory is
 therefore only applied to HNO₃. In this context, we note that HNO₃ has an exceptionally long desorption time at low temperatures on ice surfaces. Based on partition coefficients and surface accomodation coefficients listed by IUPAC for HNO₃, a surface residence time of ≈2 min at 213 K can be calculated. Other traces gases, including the organic species and H₂O₂ studied here will have shorter residence times and are less
 likely to be susceptible to burial unless very large supersaturation exist. However, there are almost no laboratory data to test the trapping theory and this remains an urgent requirement to improve our understanding of trace-gas incorporation into ice particles

According to the detailed calculations given in Kärcher and Basko (2004) and ²⁵ Kärcher et al. (2009) the trapping rate per ice particle can be written:

under real conditions.

$$\frac{dN}{dt} = 2\pi DD_{iff} \varepsilon n_G$$
(12)

where D_{iff} is the diffusion coefficient of species in air and D is the equivalent diameter of the ice particle. n_G (molecules cm⁻³) is the gas species concentration far away 24382

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from the ice surface and ε is the trapping efficiency which depends on the radius of the ice particle, the increase of this radius per unit of time, the escape velocity, the accommodation coefficient α and the diffusion coefficient D_{iff} (see Kärcher et al., 2009). ε does not depend on the gas concentration n_G except in case of saturation of the ice surface.

In the calculations the accommodation coefficient is set to α =0.3 which is consistent with the evaluation α >0.2 of the IUPAC Subcommittee on Gas Kinetic Data Evaluation. Finally, combining (Eq. 12) and the size distribution of the three ice categories (Eq. 1), the number of molecules per cm³ removed from the gas phase per unit of time due to trapping may be written:

$$\frac{\mathrm{dn}_G}{\mathrm{dt}} = -2\pi D_{\mathrm{iff}} n_G \sum_{i=1}^m \left(\int_0^\infty \varepsilon_i(D) Dn_i(D) \mathrm{d}D \right)$$
(13)

10

To simplify this relation we assume that ε_i (D)= ε_i (D_{mean,*i*}) where D_{mean,*i*} is the mean diameter of each ice particle category. D_{mean,*i*} is related to the characteristic diameter D_{*n*,*i*} by D_{mean,*i*}=2 D_{*n*,*i*}. This leads to negligible errors on n_G(t) (lower than 1% at any time step of the calculations). Relation (Eq. 13) becomes:

$$\frac{\mathrm{dn}_{G}}{\mathrm{dt}} = -2\pi \mathrm{D}_{\mathrm{iff}} \mathrm{n}_{G} \sum_{i=1}^{m} (\mathrm{N}_{t,i} \varepsilon_{i} (\mathrm{D}_{\mathrm{mean},i}) \mathrm{D}_{n,i} \Gamma(3) / \Gamma(2))$$
(14)

From (Eq. 13), a trapping rate $k_G(s^{-1})$ such as $\frac{dn_G}{dt} = -k_G n_G$ can be derived. It is written:

$$k_{G} = 2\pi D_{iff} \sum_{i=1}^{m} (N_{t,i} \varepsilon_{i} (D_{mean,i}) D_{n,i} \Gamma(3) / \Gamma(2))$$
(15)

The trapping rate does not depend on the gas concentration except when saturation occurs via the ε_i parameter. In case of saturation it decreases when HNO₃ gas concentration increases.

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4.2 Release of species in the gas phase by ice evaporation

The release of species trapped in the bulk of the ice to the gas phase is not described by any theory at the present time. The number of molecules released by unit time depends on the location in the bulk of the trapped trace gas and an exact calculation would require a complete history of the growth and of the evaporation of each ice particle which is not available in any model. Here it is assumed that the concentration of the trace gas in the bulk of the ice particles is uniform. The number n_v of molecules per cm³ in the bulk of the ice particles released to the gas phase is then proportional to the evaporation of the ice particles per unit of time:

$$\frac{1}{n_{\nu}} \frac{dn_{\nu}}{dt} = \frac{1}{q} \frac{dq}{dt}$$

where q (see relations 1 and 2) is the mixing ratio of the ice particles

$$q = \frac{1}{\rho_a} \sum_{i=1}^{m} \int_{0}^{\infty} n_i(D) m_i(D) dD; \quad \frac{dq}{dt} = \frac{1}{\rho_a} \sum_{i=1}^{m} \int_{0}^{\infty} n_i(D) \frac{dm_i}{dt} dD$$
(17)

The evaporation rate k_v (s) can be defined such as $\frac{dn_v}{dt} = -k_v n_v$. It can be written:

$$k_{\nu} = \frac{1}{q} \frac{dq}{dt} = 2 \sum_{i=1}^{m} \left(\frac{\beta_{m,i} \frac{dr}{dt} (D_{n,i})}{D_{n,i}} \frac{\Gamma(\nu + \beta_{m,i} - 2)}{\Gamma(\nu + \beta_{m,i})} \right)$$
(18)

15 4.3 Results

As in Sect. 3.3, the calculations are made in assuming that the total mixing ratio of HNO_3 is conserved along the trajectories. In reality, this assumption is generally not true but is convenient to assess the importance of the ice uptake process. The important parameters are the trapping rate and the evaporation rate defined in Sects. 4.1

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and 4.2. These parameters give a quantitative evaluation of the importance of the trapping/evaporation at each timestep of the simulations.

In the trapping theory, trace gases are removed from the gas phase when the water vapour saturation coefficient above ice is larger than 1 and are released from the ice

- ⁵ particles to the gas phase when the saturation coefficient is lower than 1. Figure 11a shows the trapping rate k_G computed in the REF simulation as a function of time on the 7 trajectories. In this simulation the initial HNO₃ gas phase mixing ratio is 100 pptv and the bulk concentration is zero. During this simulation the saturation effect of gas adsorption on the ice surface is always negligible. We observe that the trapping rate is very large (between 10^{-2} s^{-1} and 10^{-3} s^{-1}) on the trajectories of the air parcels which are lifted rapidly by convection (purple, light blue and deep green lines) approximately
- between 1 and 1.4 h of simulation. On these trajectories HNO_3 is rapidly removed from the gas phase while the air parcels are lifted by convection. On the other trajectories the trapping rate is lower with most of the values between $1 \times 10^{-5} \text{ s}^{-1}$ and $7 \times 10^{-4} \text{ s}^{-1}$.
- In this case the removal of HNO₃ from the gas phase is nevertheless significant during the lifetime of the convective cloud (few hours). For larger gas phase concentrations of HNO₃, the saturation effect of the ice surface leads to a decrease of the trapping rate. Figure 11b shows the trapping rate computed with an initial gas mixing ratio of 10 ppbv. During this simulation the gas mixing ratio varies between 5 and 10 ppbv which cor-
- ²⁰ responds to saturation conditions. Decreases up to a factor of 10 are observed with respect to the case without saturation effects (Fig. 11a). Figure 11c shows the trapping rate computed in the RUN1M simulation in the same conditions as for those shown in Fig. 10b. The results are consistent with those of the REF simulation. Relatively large differences are nevertheless observed on particular trajectories and times. This
- ²⁵ is the case at the beginning of the high altitude trajectory (orange triangles). These differences are due to relatively small but significant differences of the variation of the temperature on this trajectory leading to changes in water vapour deposition.

The evaporation rate k_v computed in the REF simulation (Fig. 11d) is of the same order as the trapping rate. It is mainly a function of the water vapour saturation coefficient

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with respect to ice. It is also a function of the size of the ice particles. According to relation (Eq. 18) the evaporation rates are neither dependent on the gas HNO_3 concentration nor on the bulk HNO_3 concentration. The evaporation rates computed in the RUN1M simulation (Fig. 11e) are also consistent with those computed in the REF sim-⁵ ulation.

Figure 12a shows the evolution of the HNO₃ gas mixing ratio computed in the REF simulation on the 7 trajectories. The total mixing ratio (gas + bulk) is conserved. In Fig. 12a the total mixing ratio is 1 ppbv. The bulk concentration is assumed initially to be zero. Due to the large trapping rates at the beginning of the trajectories which are lifted by convection (purple, light blue and deep green) the removal of HNO₃ from the gas phase is very large. For the other trajectories, which stay at high altitude, it is also significant since 10% to 50% of the initial gas phase mixing ratio is removed from the gas phase at the end of the trajectories. The comparison between Figs. 9b and 12a shows that the removal of species from the gas phase computed by the Langmuir approach or by the trapping theory is on average roughly of the same order.

As discussed above the adsorption saturation effect of the ice surface can be large. This is confirmed in Fig. 12b which shows the evolutions of the HNO_3 gas phase mixing ratio assuming a total mixing ratio of 10 ppbv on the 7 trajectories. In this case the removal is <50% of the initial gas mixing ratio for all trajectories. It is negligible for three of the trajectories (light green, red and orange). This is because for these trajectories

²⁰ of the trajectories (light green, red and orange). This is because for these trajectories the water vapour deposition and evaporation is low and adsorption saturation effect is large.

Figure 12c shows the results for a total mixing ratio of 1 ppbv in the RUN1M simulation. The results are consistent with those of the REF simulation (Fig. 12a) except

²⁵ for the highest altitude trajectory (orange line). This is due to the higher trapping rate computed in the RUN1M simulation as already discussed above.

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5 Discussion and conclusion

The overall objective of this paper is to assess the importance of the reversible ice uptake process for various gas species in the cold part of deep convective clouds (T<235 K). This is done to prepare the incorporation of this process in a 3-D limited area cloud model. To this end an idealized convective cloud is simulated with the 3-D cloud resolving model BRAMS and ice uptake is studied on 7 air parcels trajectories representative of the different ice histories inside the cloud and within its environment. A reference simulation using a two-moment microphysical scheme (Meyers et al., 1997) and a sensitivity test using a lower computing time one-moment scheme (Walko and al., 1995) are done. The Langmuir approach and the trapping theory are both studied.

The Langmuir approach is used for 11 species for which the parameters are assessed by the IUPAC Subcommittee on Gas Kinetic Data Evaluation (http://www. iupac-kinetic.ch.cam.ac.uk). Due to the balance between the adsorption and desorp-

- tion processes, an instantaneous equilibrium is assumed between the gas phase concentration and the surface concentration of each species. This assumption is justified since the time step of the calculations (120 s) is larger than the time needed to reach the equilibrium on average on all the trajectories (3 s to 45 s). In both simulations the surface concentration is found to be negligible along all trajectories for PAN, HCHO,
- ²⁰ CH₃COCH₃ and CH₃OH, and small for C₂H₅OH and C₃H₇OH. On average over all the trajectories the surface concentration is significant compared with the total concentration for HCOOH (6%), CH₃COOH (17%), HCI (50%) and HNO₃ (80%). For these species the surface concentration can be very large in some particular cases 36%, 67%, 91% and 99% respectively. For H₂O₂ the surface concentration is negligible when using the published data of Clegg and Abbatt (2001), but is significant (8% on average with a maximum of 36%) if the partition coefficient derived from new labora-
- tory studies (Pouvesle et al., 2009) are used. The effect of saturation the ice surface is observed for mixing ratios of HNO_3 and HCl larger than 1 ppbv. This saturation effect

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leads to an increase of the gas phase concentration relatively to the total (gas + ice) concentration up to a factor 4 for a HNO₃ total mixing ratio of 10 ppby. The saturation effect is very low for the other trace gases. Nevertheless, if the saturation effect occurs for HNO₃ or HCl, an impact must be observed on the surface concentration of the other trace gases due to competitive adsorptions. This impact will have to be taken into ac-

5 count in a 3-D model. Gas phase mixing ratios in the RUN1M simulation have been found to be consistent with the results obtained in the REF simulation but are usually lower because the RUN1M simulation provides larger dry ice mixing ratio along the trajectories than the REF simulation The one-moment microphysical scheme can be therefore a good approximation in a 3-D cloud model to reduce the computation time. 10

The trapping theory developed by Karcher and Basko (2004) and by Karcher et al. (2009) for HNO₃ has been used. The trapping rate of HNO₃ has been shown to be very large $(10^{-3} \text{ to } 10^{-2} \text{ s}^{-1})$ on trajectories of air parcels which are rapidly uplifted by convection, leading to fast removal of HNO₃ from the gas phase. On the other trajectories the rate is lower $(10^{-5} \text{ to } 7 \times 10^{-4} \text{ s}^{-1})$ but still leads to significant HNO₃ removal

- 15 from the gas phase on the lifetime of the convective cloud. The saturation effect on the ice surface is observed on the trapping rate which is reduced by a factor 10 when HNO₃ mixing ratio in the gas phase increases from 100 pptv to 10 ppbv. An escape rate was also defined assuming a uniform concentration of the species in the bulk of the ice
- particles. It is of the same order as the trapping rate. The HNO₃ removal computed 20 by the trapping theory is of the same order as in the Langmuir approach for HNO₃. Trapping could therefore be important for the other species HCl, H_2O_2 , $CH_3C(O)OH$ and HC(O)OH for which the Langmuir approach removal is significant, though the lack of confirmatory data from either the laboratory or field experiments precludes a definite conclusion at this stage. 25

In a 3-D cloud model, the single-moment microphysical scheme will be used to reduce the time computation and all species for which the uptake is significant will be treated using the Langmuir theory, except HNO₃ for which the trapping theory exists. We will introduce ice surface concentration variables for HCl, H_2O_2 , $CH_3C(O)OH$ and

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HC(O)OH. Other species such as HONO and HO₂NO₂ could be added later once their partition coefficient is assessed by IUPAC. The time evolution of HCl, H₂O₂, CH₃C(O)OH and HC(O)OH species will be computed by the Langmuir approach assuming the equilibrium between adsorption and desorption. This will limit the time resolution of the calculations since the equilibrium is justified only if the time required to reach the equilibrium is lower than the timestep. In the cases studied in the present paper the time to reach the equilibrium was found for these species to be between 3 s and 20 s on average but it can be larger in some particular cases. For instance, a maximum time of 140 s for CH₃C(O)OH was computed.

- ¹⁰ For HNO₃ the Langmuir and the trapping approaches can be applied. On one hand, the Langmuir theory assumes that the ice surface is in a steady state and in principle only applies to this case. On the other hand, the trapping approach is valid when water deposition on ice is significant. At the present stage of the development of the trapping theory the location of the trapped species and in particular the number of species on
- the ice surface is not yet determined. Knowledge of not only the gas-to-ice partitioning but also the ice surface concentration of absorbed trace gases is needed because the reactive interaction of other species with the ice surface can depends on the surface composition. In the adsorption limit of the trapping theory, the surface concentration derived by the Langmuir approach can be nevertheless assumed. It seems reasonable
- ²⁰ to use this approach in the case when the trapping rate or the evaporation rate is low relatively to the rate constant to reach the Langmuir equilibrium. The trapping rate and the evaporation rate for HNO₃ are between 10^{-6} s^{-1} and 10^{-3} s^{-1} most of the time (Fig. 11a, b and d) while the rate constant to reach the Langmuir equilibrium is on average on all the trajectories between 10^{-1} s^{-1} and $2 \times 10^{-2} \text{ s}^{-1}$ with a minimum of $4 \times 10^{-3} \text{ s}^{-1}$. Therefore we will introduce in the 3-D cloud model a variable for the bulk concentration and also a variable for the ice surface concentration. In the cases of low trapping or low evaporation rates the evolution of the bulk concentration of HNO₃ will use the trapping and evaporation as proposed by Kärcher et al. (2009) and the evolution of the surface concentration will use the Langmuir equilibrium.

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5 TROCCIBRAS database. We acknowledge B. Kärcher for fruitful discussions on the trapping theory. We also acknowledge R. Joussot, M. Francis and J. B. Renard for their help.



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10 **References**

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Table 1. Parameters A and B used to compute the partition coefficient. K_{linC} and maximum number of molecules N_{MAX} adsorbed on the ice surface for the 11 species taken into account in the present paper.

Species	A (cm)	B (K ⁻¹)	N_{MAX} (cm ⁻²)
C₂H₅OH	5.8×10^{-14}	7500	2.8×10 ¹⁴
CH ₃ C(O)OH	1.0×10 ⁻¹⁰	6660	2.4×10 ¹⁴
CH ₃ COCH ₃	1.0×10 ⁻¹¹	5850	2.7×10 ¹⁴
НСНО	7.0×10 ⁻⁰¹	0	2.7×10 ¹⁴
HC(O)OH	5.8×10^{-11}	6500	2.2×10 ¹⁴
CH₃OH	6.2×10 ⁻¹²	6180	3.2×10 ¹⁴
H ₂ O ₂ IUPAC	1.6	0	2.7×10 ¹⁴ *
H ₂ O ₂ Mainz	2.1×10 ⁻⁰⁵	3800	2.7×10 ¹⁴ *
HNO3	7.5×10 ⁻⁰⁵	4585	2.7×10 ¹⁴
PAN	1.5×10 ⁻⁰⁹	3608	2.7×10 ¹⁴ *
C ₃ H ₇ OH	3.6×10^{-14}	7800	3.1×10 ¹⁴
HCI	2.2×10 ⁻⁰²	2858	3.0×10 ¹⁴

 * N_{MAX} is not available for this species in the IUPAC subcommittee assessment. In this case N_{MAX} is assumed to be 2.7×10¹⁴ cm⁻² which is the median value of the other species assessed by IUPAC.

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Table 2. Mean, standard deviation and minimum gas phase mixing ratio on the time interval when dry ice is present over the seven trajectories computed in the REF simulation. The total mixing ratio for all species is assumed to be 100 pptv. The results of the RUN1M simulation are given in parenthesis.

Species	Mean mixing ratio (pptv)	Standard deviation (pptv)	Minimum mixing ratio (pptv)
HNO ₃	14.8 (14.1)	15.6 (17.2)	1.3 (0.7)
C ₂ H ₅ OH	99.2 (99.1)	0.9 (0.9)	93.2 (92.7)
CH ₃ C(O)OH	82.3 (79.5)	13.7 (14.6)	31.7 (27.6)
CH ₃ COCH ₃	99.9 (99.9)	0.1 (0.1)	99.6 (99.4)
HCHO	>99.9 (>99.9)	0.1 (0.1)	99.9 (99.8)
HC(O)OH	93.7 (92.5)	6.0 (6.5)	63.3 (57.8)
CH ₃ OH	99.8 (99.8)	0.2 (0.2)	98.7 (98.2)
H ₂ O ₂ IUPAC	>99.9 (>99.9)	0.1 (0.1)	99.7 (99.5)
H_2O_2 Mainz	91.5 (89.6)	6.8 (8.8)	61.2 (47.8)
PĀN	>99.9 (>99.9)	0.1 (0.1)	>99.9 (>99.9)
C ₃ H ₇ OH	98.1 (97.8)	2.3 (2.3)	83.8 (82.7)
HCI	50.9 (47.2)	19.7 (22.4)	9.3 (6.1)

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Species	Number of hexagonal columns	Mean mixing ratio (pptv)	Minimum mixing ratio (pptv)
HNO ₃	2	14.96	1.43
HNO ₃	4	14.77	1.30
HNO ₃	8	14.57	1.15
CH ₃ C(O)OH	2	82.47	32.60
CH ₃ C(O)OH	4	82.26	31.67
CH ₃ C(O)OH	8	82.02	30.60
HCI	2	51.27	10.27
HCI	4	50.92	9.26
HCI	8	50.54	8.27

able 3. Impact of the number of hexagonal columns which compose an aggregate ice particle
n the mean and the minimum gas phase mixing ratios of HNO ₃ , CH ₃ COOH and HCI along the
trajectories of the REF simulation. The total mixing ratio (gas + surface) for the three species
100 pptv.

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Fig. 4. (a) Dry ice mixing ratio in $g kg^{-1}$ versus time, **(b)** Pristine ice mixing ratio in $g kg^{-1}$ versus time, **(c)**, snow mixing ratio in $g kg^{-1}$ versus time and **(d)** aggregates mixing ratio in $g kg^{-1}$ versus time along the selected trajectories from the REF simulation. The dry ice mixing ratio is defined as the sum of pristine ice, snow and aggregates mixing ratios. On each trajectory of Fig. 4a, the full square indicates the time at which ice begins to grow by water vapour deposition.







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Fig. 6. Partition coefficients (cm) used in the calculations as a function of the inverse of the temperature in the range 200 K–240 K.



Fig. 7. Ratio of the surface area of snow over the surface area of pristine as a function of the ratio of the mixing ratio of snow over the volume mixing ratio of pristine (blue diamonds); the same for aggregates and pristine ice (orange triangles) and for aggregates and snow (green diamonds). The pink line is the location of the points for which a ratio of the volume mixing ratio would lead to the same ratio of the surface area.

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Fig. 8. Results of the Langmuir approach. **(a)** HCl gas concentration versus time with an initial concentration of 0.1 ppbv, **(b)** $CH_3C(O)OH$ gas concentration versus time with an initial concentration of 0.1 ppbv, along the selected trajectories from the REF simulation.





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Fig. 9. Results of the Langmuir approach. HNO_3 gas concentration versus time along the selected trajectories from the REF simulation using an initial gas concentration of **(a)** 0.1 ppbv, **(b)** 1 ppbv and **(c)** 10 ppbv.



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Fig. 10. Ratio of the mean gas phase mixing ratio on the total mixing ratio as a function of the total mixing ratio of HNO_3 , $CH_3C(O)OH$, H_2O_2 and HCI. The total mixing ratio is defined as the sum of the gas phase mixing ratio and of the gas mixing ratio on the ice surface. For H_2O_2 the partition coefficient measured by MPIC is used.



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Fig. 11. Trapping and evaporation rates of HNO_3 computed in the trapping theory. (a) trapping rate computed for gas HNO_3 mixing ratios between 0 and 100 pptv, along trajectories of the REF simulation (b) trapping rates computed for gas HNO_3 mixing ratios between 5 and 10 ppbv, along trajectories of the REF simulation (c) same as (b) along trajectories of the RUN1M simulation, (d) evaporation rate computed along trajectories of the REF simulation, (e) same as (d) for the RUN1M simulation.



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Fig. 12. Time evolution of the HNO_3 gas phase mixing ratio computed in the trapping theory assuming a constant total (gas + bulk) mixing ratio. **(a)** Time evolution along the trajectories of the REF simulation for a total mixing ratio of 1 ppbv **(b)** Time evolution along the trajectories of the REF simulation for a total mixing ratio of 10 ppbv, **(c)** same as (a) along trajectories of the RUN1M simulation .



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