

**Real-time  
measurements of  
inorganic gases and  
aerosol species**

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# Real-time measurements of ammonia, acidic trace gases and water-soluble inorganic aerosol species at a rural site in the Amazon Basin

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## Abstract

We measured the mixing ratios of ammonia ( $\text{NH}_3$ ), nitric acid ( $\text{HNO}_3$ ), nitrous acid ( $\text{HONO}$ ), hydrochloric acid ( $\text{HCl}$ ), sulfur dioxide ( $\text{SO}_2$ ) and the corresponding water-soluble inorganic aerosol species, ammonium ( $\text{NH}_4^+$ ), nitrate ( $\text{NO}_3^-$ ), nitrite ( $\text{NO}_2^-$ ), chloride ( $\text{Cl}^-$ ) and sulfate ( $\text{SO}_4^{2-}$ ), and their diel and seasonal variations at a pasture site in the Amazon Basin (Rondônia, Brazil). This study was conducted within the framework of LBA-SMOCC (Large Scale Biosphere Atmosphere Experiment in Amazonia Smoke Aerosols, Clouds, Rainfall and Climate). Sampling was performed from 12 September to 14 November 2002, extending from the dry season (extensive biomass burning activity), through the transition period to the wet season (background conditions). Measurements were made continuously using a wet-annular denuder in combination with a Steam-Jet Aerosol Collector (SJAC) followed by suitable on-line analysis. A detailed description and verification of the inlet system for simultaneous sampling of soluble gases and aerosol compounds is presented. Overall measurement uncertainties of the ambient mixing ratios usually remained below 15%. The limit of detection (LOD) was determined for each single data point measured during the field experiment. Median LOD values ( $3\sigma$ -definition) were  $\leq 0.015$  ppb for acidic trace gases and aerosol anions and  $\leq 0.118$  ppb for  $\text{NH}_3$  and aerosol  $\text{NH}_4^+$ . Mixing ratios of acidic trace gases remained below 1 ppb throughout the measurement period, while  $\text{NH}_3$  levels were an order of magnitude higher. Accordingly, mixing ratios of  $\text{NH}_4^+$  exceeded those of other inorganic aerosol contributors by a factor of 4 to 10. During the wet season, mixing ratios decreased by nearly a factor of 3 for all compounds compared to those observed when intensive biomass burning took place. Additionally, N-containing gas and aerosol species featured pronounced diel variations. This is attributed to strong relative humidity and temperature variations between day and night as well as to changing photochemistry and stability conditions of the planetary boundary layer.  $\text{HONO}$  exhibited a characteristic diel cycle with high mixing ratios at nighttime and was not completely depleted by photolysis during daylight hours.

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## 1. Introduction

Every year, large emissions of aerosols and trace gases occur during the dry season (May through September) in the Amazon Basin from widespread biomass burning activity. Smoke from biomass burning leads to a significant increase in cloud condensation nuclei (CCN) concentration causing alteration of cloud properties. This is likely to have considerable impact on the large-scale dynamics of the atmosphere (Andreae et al., 2002; Roberts et al., 2001). During the wet season, however, background conditions resemble CCN concentrations more typical of marine locations than most continental sites (Roberts et al., 2001). Both, water-soluble inorganic aerosol species and soluble gases are expected to play a major role in the nucleation and growth of cloud droplets under polluted as well as under clean conditions.

Ammonia ( $\text{NH}_3$ ), in the tropics mostly emitted by combustion processes, volatilization from manure and fertilizer application, plays a key role in neutralizing acidic atmospheric compounds (Asman et al., 1998). Due to heterogeneous reactions involving gaseous  $\text{NH}_3$  as well as sulfur dioxide ( $\text{SO}_2$ ), non-volatile aerosol constituents like  $(\text{NH}_4)_2\text{SO}_4$  and  $\text{NH}_4\text{HSO}_4$  can be formed.

Moreover, the abundance of semi-volatile aerosol species such as  $\text{NH}_4\text{NO}_3$  and  $\text{NH}_4\text{Cl}$  is strongly dependent on the gas phase precursors,  $\text{NH}_3$ ,  $\text{HNO}_3$  and  $\text{HCl}$ .  $\text{HNO}_3$  and  $\text{NH}_3$  exist in equilibrium with solid ammonium nitrate ( $\text{NH}_4\text{NO}_3$ ) at relative humidities below its deliquescence (61.8% at 25°C) (Stelson and Seinfeld, 1982) while at relative humidities above deliquescence,  $\text{NH}_4\text{NO}_3$  will be found in the aqueous state (Seinfeld and Pandis, 1998). Comparably, gaseous  $\text{NH}_3$  and  $\text{HCl}$  are precursors for the reversible formation of  $\text{NH}_4\text{Cl}$  (Pio and Harrison, 1987). These thermodynamic equilibria are strongly dependent on relative humidity and temperature, such that low temperature and high relative humidity will shift the equilibrium to the aerosol phase.

Nitrous acid ( $\text{HONO}$ ) is of atmospheric importance due to its expected significant contribution to the production of OH radicals. Rapid  $\text{HONO}$  photolysis can lead to an integrated OH· yield of up to 34% at daytime (Kleffmann et al., 2003 and references

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therein). The observation of persistent daytime HONO (up to 150 ppt) was found by several investigators and it is expected to be formed due to heterogeneous reaction of  $\text{NO}_2$  with surface water (Harrison and Kitto, 1994; Zhou et al., 2002; Alicke et al., 2003; Aumont et al., 2003; Genfa et al., 2003; Kleffmann et al., 2003).

Since the 1970's, adequate sampling of gaseous compounds and related semi-volatile aerosol species was recognized as a significant problem, especially with respect to the collection of  $\text{HNO}_3$ , nitrate ( $\text{NO}_3^-$ ), but also  $\text{NH}_3$ , ammonium ( $\text{NH}_4^+$ ), chloride ( $\text{Cl}^-$ ) and sulfate ( $\text{SO}_4^{2-}$ ) (Appel and Tokiwa, 1981; Appel et al., 1984; Slanina et al., 1992; Appel, 1993; Cheng and Tsai, 1997). In particular,  $\text{HNO}_3$  measurements without interferences are very difficult, since this molecule can readily absorb on surfaces of inlets (Appel et al., 1988; Neuman et al., 1999) and sampling substrates (e.g. filter materials) (Appel et al., 1984). Furthermore, desorption and re-evaporation of  $\text{HNO}_3$  from inlet surfaces or sampling substrates may considerably bias sampling results. The collection of aerosol species on filter materials without pre or after-stages to trap gaseous compounds leads to significant artifacts (Slanina et al., 2001). Long sampling times (hours to days) to collect sufficient aerosol on the filter material may result either in evaporation of semi-volatile aerosol species (negative artifact) or to collection of gaseous compounds (such as  $\text{NH}_3$ ,  $\text{HNO}_3$ ,  $\text{HCl}$  and  $\text{SO}_2$ ) which may be retained by filter media (positive artifact).

To date there are no reliable measurements of  $\text{NH}_3$  and acidic trace gases ( $\text{HNO}_3$ , HONO,  $\text{HCl}$ , and  $\text{SO}_2$ ) from the Amazon Basin, and in the past inorganic aerosol species were usually sampled by filter methods without accounting for possible artifacts. High temperatures and relative humidities (close to 100% at nighttime) are typical for this tropical region, which may significantly influence gas-aerosol partitioning processes. During the wet season, conditions usually remain very clean (low aerosol and trace gas concentrations are present) in contrast to the dry season when biomass burning takes place. For these reasons a method which provides continuous measurements with (a) high selectivity, (b) high time resolution (determination of diel variations for gas and aerosol compounds simultaneously), and (c) low detection limits is needed.

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Therefore, we applied the combination of a wet-annular denuder (WAD) and a Steam-Jet aerosol collector (SJAC) (Wyers et al., 1993; Slanina et al., 2001) followed by on-line analysis using ion chromatography (IC) and ammonium flow injection analysis (FIA). Here, we report the application of a sophisticated inlet system for simultaneous sampling of gas and aerosol species verified for potential sampling losses (particularly  $\text{HNO}_3$ ). Furthermore, an evaluation of the measurement performance of the instrument (with particular emphasis on measurement uncertainty and limit of detection) and first results of seasonal and diel variations of the measured species are presented.

## 2. Available measurement methods

Table 1 gives an overview of the most common sampling methods for the collection of inorganic gas and aerosol species with selected references.

The filter-pack method, usually with Teflon, Nylon or impregnated filters in series, is the least accurate, but simplest and most commonly used sampling procedure (Appel, 1993). This technique is laborious, and suffers from long sampling times as well as possible interference due to oxidation of nitrites collected on nylon filters, which may positively bias  $\text{HNO}_3$  collection (Perrino et al., 1988). Also, evaporation of aerosol  $\text{NO}_3^-$  from Teflon filters has been reported (Appel et al., 1981).

The most substantial approach for sampling a gas in the presence of corresponding aerosol particles is the denuder technique. Dry-coated diffusion denuders are reliable, but laborious and provide only long time-average concentration measurements (Dasgupta, 1993). These drawbacks were overcome by various other developments. Simon et al. (1991) have proposed four different designs for wet effluent diffusion denuders coupled to ion chromatography systems with continuously renewed collection surfaces. Efficient retention of trace gases and a higher time resolution may be achieved by parallel-plate denuders coupled to on-line analysis. Keuken et al. (1989) developed an automated thermodenuder system for the determination of  $\text{NH}_3$  in ambient air. A device that is becoming increasingly popular is the so called WAD which has the ability

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to maintain near-quantitative collection efficiencies at high sampling rates within a compact design (Dasgupta, 1993). The first WAD operating in batch mode was reported by Keuken et al. (1988) and a continuously rotating annular denuder was first described by Wyers et al. (1993). Diffusion scrubber and mist chamber techniques also provide measurements with higher time resolution and are little sensitive to artifacts.

Although the replacement of filter-based methods by continuous denuder devices and optical measurement techniques (also listed in Table 1) was a positive development in the last decade, usually these methods are only capable of measuring either one single compound or species of the same physical state (i.e. either gas or aerosol). The combination of new aqueous phase aerosol collectors with the denuder technique is up to date the only approach for the simultaneous collection of gas and aerosol species. Usually, these methods are continuous, followed by on-line analysis of the resulting aqueous solution. On-line IC has become the major analytical tool for these sampling systems, being able to measure ambient concentrations continuously in the low two-digit ppt range.

### 3. Experimental

#### 3.1. Site description

Sampling was performed at a pasture site in the state of Rondônia, Brazil (Fazenda Nossa Senhora Aparecida, FNS, 10°45'44" S, 62°21'27" W, 315 m asl). Clearing of rain forest by fire in Rondônia has taken place since 1968, creating a typical "fishbone"-like pattern of plantations, pastures, degraded land and forest patches (see Andreae et al., 2002). The vegetation at FNS is dominated by grass (*Brachiaria brizantha*) with small patches of *Brachiaria humidicola* and very few isolated palms and bushes, and the site is used as a cattle ranch (~200 "Blanco" cattle, *Bos indicus hybrid*). Nearby the site, flat hills (300 to 440 m) are located in distances of 3 to 4 km. The pasture is a rural, non-pristine site, with a highway (BR 364) in 10 km distance to the northeast. The

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towns Ouro Preto d'Oeste (~40 800 inhabitants) and Ji-Paraná (~110 000 inhabitants) are situated approximately 13 km and 40 km to the WSW of the site, respectively.

5 The site is characterized by small seasonal temperature variations, ranging from 23–24°C at the end of the wet season (June/July) to 25–26°C during the dry season (September/October). Annual relative humidity values are high, with averages of about 70% in the dry season and 80% during the wet season. Prevailing wind speeds are relatively low (daily average  $\sim 1.5 \text{ m s}^{-1}$ ) with a minimum during nighttime. Precipitation in this region shows a seasonal cycle with lowest values in July and is highest from November to April (up to  $\sim 300 \text{ mm}$  per month) (Andreae et al., 2002). A detailed  
10 description of the history of the site can be found in Kirkman et al. (2002).

Instrumentation for sampling and on-line analysis was arranged in a wooden house with several air conditioned laboratories. The house was surrounded by a fence (distance to the house  $\sim 10 \text{ m}$ ) to prevent cattle from approaching the sampling and measurement location.

## 15 3.2. Inlet system

### 3.2.1. Design

The sampling performance of the wet-annular denuder/steam-jet aerosol collector (WAD/SJAC) and the quality of the on-line analysis are strongly dependent on environmental parameters (i.e. air temperature and relative humidity). In order to provide  
20 controlled conditions for sampling and particularly for IC and FIA (i.e. minimal fluctuations of temperature and relative humidity), it was necessary to place the instrumentation in an air conditioned laboratory. An inlet system mounted to the wall outside of the air conditioned laboratory was used to bring sample air to the instruments (Fig. 1). For the design of this inlet system, three major requirements had to be considered: (a) Minimizing gas phase wall losses (particularly  $\text{HNO}_3$ ), (b) Minimizing aerosol losses due to non-isokinetic sampling, and (c) providing a reasonable sampling fetch. To meet these  
25 requirements, air was sampled from 530 cm above ground (150 cm above the roof of

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the house) through a vertical polyethylene conduit with an inner diameter of 7 cm. The conduit was wrapped on the outside with aluminum tape to reduce daytime heating of the material. The air flow in the conduit was generated by a suction fan assembled in the conduit bottom. A sub-sample of the air was aspirated from the center of the conduit's cross section area at a flow rate of  $\sim 17 \text{ l min}^{-1}$  (STP: 298.15 K and 1000 hPa) through a steel elbow (90° angle of steel tubing,  $d = 0.8 \text{ cm}$ , inner surface PFA Teflon coated) mounted inside the conduit (Fig. 1). The sampled air was then drawn through a PFA Teflon tubing connection ( $d = 0.8 \text{ cm}$ ,  $l = 70 \text{ cm}$ ) to the sampling system in the air conditioned laboratory. The PFA Teflon tubing inside the laboratory had a length of only 5 cm before entering the instrument and was insulated thoroughly to prevent condensation. During the field experiment, the steel elbow was replaced periodically with a pre-impactor (PM 2.5 size cut; type 413, University Research Glassware, aluminum cyclone, PFA Teflon coated). Velocity, relative humidity and temperature of the air stream in the polyethylene conduit were continuously monitored (time resolution 1 min) using a thermo-anemometer sensor (Velocicalc Plus 8386, TSI Instruments).

Neuman et al. (1999) tested different inlet materials for sampling  $\text{HNO}_3$  and found highest transmission efficiencies ( $\geq 95\%$ ) for plastic materials at  $22^\circ\text{C}$  (e.g. PFA, TFE, FEP and PVDF), whereas  $\text{HNO}_3$  loss on aluminum, steel or nylon materials was  $\sim 85\%$ . On the basis of these results, the polyethylene inlet conduit was considered to be appropriate for sampling of  $\text{HNO}_3$  and other soluble gases. A similar inlet construction for sampling  $\text{HNO}_3$  and HONO was used during the EPA Atlanta Supersite Experiment (1999) and proved to be satisfactory (Genfa et al., 2003). Also, using Teflon coated aluminum cyclones as inlet under atmospheric conditions, Appel et al. (1988) observed transmission efficiencies for  $\text{HNO}_3$  not significantly different from 100%. Nevertheless, to ensure the quality of our measurements, we present a theoretical verification of the applied inlet system in the following section.

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### 3.2.2. Sampling efficiency of the inlet system

To minimize gas phase losses (particularly  $\text{HNO}_3$ ), laminar conditions in the conduit are necessary to avoid turbulence and to minimize the contact of the sampled air with the inlet walls. However, since simultaneous sampling of gases and aerosol species was intended, it was crucial to account for possible inlet losses of both, gases and aerosols. The required flow rate for the pre-impactor ( $d = 0.8 \text{ cm}$ ) was  $\sim 17 \text{ l min}^{-1}$  (STP). The mean air velocity in the polyethylene conduit generated by the suction fan was adjusted to  $\sim 1 \text{ m s}^{-1}$  (Reynolds number  $\text{Re}_{\text{mean}} \sim 4500$ ) indicating the transition between laminar conditions and turbulence. This, in turn, led to slightly superisokinetic sampling at the entrance of the steel elbow and/or pre-impactor, since the mean air velocity at its entrance was around  $8 \text{ m s}^{-1}$ . Aerosol losses due to non-isokinetic sampling were calculated using the equation of Belyaev and Levin (1974) (Hinds, 1999):

$$\frac{\Delta c}{c_0} = 1 - \left( 1 + \left( \frac{v_0}{v} - 1 \right) \times \left( 1 - \frac{1}{1 + \left( 2 + 0.62 \times \frac{v}{v_0} \right) \times Stk} \right) \right) \quad (1)$$

where  $\Delta c/c_0$  is the relative aerosol loss between conduit and steel elbow and/or pre-impactor,  $v_0$  is the air velocity in the conduit ( $\text{m s}^{-1}$ ) (STP),  $v$  is the air velocity in the steel elbow and/or pre-impactor ( $\text{m s}^{-1}$ ) (STP) and  $Stk$  is the corresponding Stokes number. Aerosol losses ( $D_p \leq 2.5 \mu\text{m}$ ) were  $\leq 3\%$  for during the entire experiment, and are subsequently neglected.

To verify the performance of the inlet regarding the transmission of gaseous compounds, “worst case” wall losses were calculated for  $\text{HNO}_3$ . Therefore, a hypothetical complete coating of the inner conduit surface with water droplets and aerosols, and a  $\text{HNO}_3$  uptake coefficient of  $\gamma_{\text{HNO}_3} = 1$  (any molecule diffusing to the wall surface would be absorbed = “worst case scenario”) was assumed. The conduit was considered as a circular denuder tube with laminar flow conditions and hypothetical wall losses of  $\text{HNO}_3$  were calculated by application of the following equation (Gormley and Kennedy, 1949;

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equation modified):

$$\frac{\Delta c}{c_0} = 1 - \left( 0.8191 \times e^{-3.6568 \times \Delta} + 0.0975 \times e^{-22.3 \times \Delta} + 0.0325 \times e^{-57 \times \Delta} + \dots \right) \quad (2)$$

with

$$\Delta = \frac{\pi \times D_G \times L_C}{Q_C}, \quad (3)$$

5 where  $\Delta c/c_0$  denotes the relative gas phase loss,  $D_G$  the  $\text{HNO}_3$  diffusion coefficient ( $\text{cm}^2 \text{s}^{-1}$ ),  $L_C$  the length of the conduit (cm) and  $Q_C$  the air flow in the conduit ( $\text{cm}^3 \text{s}^{-1}$ ) (STP). The  $\text{HNO}_3$  diffusion coefficient in air was experimentally determined by several investigators ranging from  $0.04 \text{ cm}^2 \text{s}^{-1}$  to  $0.121 \text{ cm}^2 \text{s}^{-1}$  (STP) (Braman et al., 1982; Eatough et al., 1985; Durham and Stockburger, 1986 and Deandrade et al.,  
10 1992). In this study, we used the highest value ( $0.121 \text{ cm}^2 \text{s}^{-1}$ ). Mean hypothetical “worst case” gas phase losses ( $\gamma_{\text{HNO}_3} = 1$ ) of  $\leq 30\%$  were derived for the conditions observed during the entire measurement period. However, Kirchner et al. (1990), van Doren et al. (1990) and Ponche et al. (1993) reported from laboratory studies  $\gamma_{\text{HNO}_3} \ll 1$  for the heterogeneous uptake of  $\text{HNO}_3$  by pure aqueous droplets (typically  $\gamma_{\text{HNO}_3}$  was  
15  $< 0.2$  for  $T > 260 \text{ K}$ ). Taking into account atmospheric conditions and possible coating of the inner conduit walls with strong electrolytic aerosol mixtures, we consider a  $\text{HNO}_3$  uptake coefficient of  $\gamma_{\text{HNO}_3} = 0.5$  as a conservative estimate, appropriate for our study. Hence, replacing the “worst case scenario” by rather realistic conditions, theoretical mean gas phase  $\text{HNO}_3$  losses for the entire experiment were estimated to  $\leq 15\%$ .

20 To verify the performance of the inlet system from a practical point of view, we removed the complete inlet system (conduit and steel elbow and/or pre-impactor), resulting in sampling straight through the 70 cm long PFA Teflon tubing. During this procedure, we observed no significant differences to the typical  $\text{HNO}_3$  diel variation (see Fig. 6, Sect. 4.4.1), hence confirming our estimates calculated above.

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### 3.3. Sampling and analysis

A detailed description of the WAD/SJAC and the analytical procedures is given elsewhere (Slanina et al., 2001; Wyers et al., 1993). A simplified sketch of the sampling system is shown in Fig. 2. The air flow through the instrument ( $\sim 17 \text{ l min}^{-1}$ , STP) was generated by a scroll pump outside the wooden house and could be adjusted with a needle valve. The flow was measured continuously (1 min time resolution) with a mass flow meter (Bronkhorst, F-112AC-HA-55-V). After the sample air passed the steel elbow and/or pre-impactor and the PFA Teflon tubing, it entered a horizontally aligned WAD that scavenges soluble gaseous species. Trace gases (such as  $\text{NH}_3$ ,  $\text{HNO}_3$ ,  $\text{HNO}_2$ ,  $\text{HCl}$  and  $\text{SO}_2$ ) were collected in a  $10^{-4} \text{ M NaHCO}_3$  absorption solution. The liquid input was controlled automatically by an infrared sensor and a switching valve and the liquid was continuously pumped out of the denuder at a flow rate of  $0.5\text{--}0.6 \text{ ml min}^{-1}$  by a peristaltic pump. The liquid effluent was collected in a sample reservoir ("gas sample", see Fig. 2).

After the WAD, the air entered a reservoir where it was mixed with steam of highly purified water. The supersaturation causes aerosol particles to grow rapidly (within  $0.1 \text{ s}$ ) into droplets of at least  $2 \mu\text{m}$  diameter. These droplets, containing the dissolved aerosol species were then collected in a cyclone (Khlystov et al., 1995). The cyclone effluent ("aerosol sample") was transferred into the sample reservoir by a peristaltic pump at a flow rate of  $0.5\text{--}0.6 \text{ ml min}^{-1}$ .

Collection of liquid samples in the sample reservoir and the following analytical cycles were performed successively for gas and aerosol sample. On-line analyses were carried out using a mobile IC with suppressed conductivity detection. The system was operated with an HPLC separation column (Dionex, IonPac AS12A,  $4 \text{ mm}$ ) preceded by a guard column (Dionex, IonPac AG12A,  $4 \times 50 \text{ mm}$ ). Samples were injected via a  $199 \mu\text{l}$  loop into  $2.7 \text{ mM Na}_2\text{CO}_3\text{--}0.3 \text{ mM NaHCO}_3$  eluent. Internal  $\text{Br}^-$  standard addition using a peristaltic pump was performed continuously to calibrate the IC. The conductivity cell of the IC was temperature-stabilized at  $30^\circ\text{C}$  and therefore conductivity

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measurements were independent from room temperature.

Ammonium ( $\text{NH}_4^+$ ) was determined by FIA (Wyers et al., 1993). The general principle is the addition of  $\text{OH}^-$  ions, converting  $\text{NH}_4^+$  to  $\text{NH}_3$ , which will then pass through a Teflon membrane and is taken up by highly purified water. Subsequent  $\text{NH}_4^+$ -detection is based on conductometry. The conductivity cell of the FIA was not temperature controlled; therefore, conductivity measurements were dependent on temperature. Despite operating an air conditioner, diel temperature variations from 22°C at night to 30°C at daytime were observed in the laboratory. Fluctuations of the conductivity due to temperature changes in the air conditioned laboratory were corrected using:

$$\text{Condcorr} = \text{Cond} \times e^{(0.024 \times (20 - T))} \quad (4)$$

where *Condcorr* denotes the corrected conductivity value (mV), *Cond* is the original measured conductivity (mV) and *T* is the observed temperature (°C) in the laboratory. The FIA was calibrated once every week using standard solutions of 50 ppb and 250 ppb  $\text{NH}_4^+$ .

IC and FIA analyses were performed simultaneously for each sample. The analytical sample cycle was purged with ambient air after every run to avoid memory effects of the previous sample solution. The sampling system is fully automated and its software controls the sequence of sample injections and integrates detected peak areas. Cycle times for the successive analysis of “aerosol and gas sample” were set to 20 min (biomass burning season), 40 min (transition period) and 60 min (wet season).

Ambient mixing ratios for gas and aerosol species after IC analyses were determined using the following equation:

$$m = \frac{m_{\text{liq}} \times m_{\text{Br(std)}} \times Q_{\text{Br}} \times Q_{\text{Br}} \times M_{\text{air}}}{m_{\text{Br}} \times Q_{\text{air}} \times M_i}, \quad (5)$$

where *m* is the ambient mixing ratio (ppb),  $m_{\text{liq}}$  is the mixing ratio of the compounds found in “aerosol or gas sample” (ppb),  $m_{\text{Br(std)}}$  is the mixing ratio of the  $\text{Br}^-$  standard solution (ppb),  $Q_{\text{Br}}$  is the flow of the  $\text{Br}^-$  standard solution which is mixed into the

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liquid sample ( $\text{kg s}^{-1}$ ),  $G$  is the factor to convert the molar weight of ionic compounds analyzed into the molecular weight of the corresponding trace gas (the factor is 1 for aerosol species).  $M_{\text{air}}$  is the molar mass of air at 298.15 K and 1000 hPa ( $24.774 \text{ kg kmol}^{-1}$ ),  $m_{\text{Br}}$  is the analyzed  $\text{Br}^-$  mixing ratio (ppb),  $Q_{\text{air}}$  is the air mass flow through the system ( $\text{kg s}^{-1}$ ) and  $M_i$  is the molar weight of compound  $i$  ( $\text{kg kmol}^{-1}$ ). This equation is also valid for calculating ambient mixing ratios of  $\text{NH}_3$  and aerosol  $\text{NH}_4^+$ , except for parameters related to the  $\text{Br}^-$  standard addition and replacing  $Q_{\text{Br}}$  by  $Q_{\text{S}}$ , which is the liquid flow of “gas sample” ( $\text{NH}_3$ ) or “aerosol sample” ( $\text{NH}_4^+$ ) ( $\text{kg s}^{-1}$ ).

## 4. Results and discussion

The sampling period was chosen from 12 September to 14 November 2002, covering extensive biomass burning activity during the dry season (12 to 23 September), an intermediate phase (transition period, 7 to 31 October) and clean conditions during the wet season (1 to 14 November). Due to an instrument failure no samples were collected from 24 September to 7 October.

All results of our measurements of gas and aerosol species are presented as mixing ratios (ppb or  $\text{nmol mol}^{-1}$ ). All quantities were calculated for standard conditions of 298.15 K, 1000 hPa and dry air, following the recommendations from Schwartz and Warneck (1995) and Mills et al. (1993).

### 4.1. Estimation of measurement uncertainty

The uncertainty of the measurements was estimated applying “Gaussian Error Propagation” to the relationship (5) which resulted in the following equation:

$$\sigma_m = m \times \sqrt{\left(\frac{\sigma_{m_{\text{liq}}}}{m_{\text{liq}}}\right)^2 + \left(\frac{\sigma_{m_{\text{Br}(\text{std})}}}{m_{\text{Br}(\text{std})}}\right)^2 + \left(\frac{\sigma_{Q_{\text{Br}}}}{Q_{\text{Br}}}\right)^2 + \left(\frac{\sigma_{m_{\text{Br}}}}{m_{\text{Br}}}\right)^2 + \left(\frac{\sigma_{Q_{\text{air}}}}{Q_{\text{air}}}\right)^2}, \quad (6)$$

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where  $\sigma_m$  is the estimated relative uncertainty of the ambient mixing ratio (ppb) and  $\sigma_x$  are the standard deviations of the corresponding parameters (see Eq. 5). Equation (6) was also used to estimate uncertainties for ambient mixing ratios of  $\text{NH}_3$  and aerosol  $\text{NH}_4^+$ , omitting the factors regarding  $\text{Br}^-$  standard addition and replacing  $Q_{\text{Br}}$  by  $Q_{\text{S}}$  and  $\sigma_{Q_{\text{Br}}}$  by  $\sigma_{Q_{\text{S}}}$ .

Calculated total uncertainties  $\sigma_m$  for all measurements and compounds usually ranged from 10–15%, indicating a reliable and stable performance of the instrument. The standard deviations  $\sigma_x$  contributing to the total measurement uncertainty  $\sigma_m$  including their sources are listed in Table 2. For IC analyses, the contribution of  $\sigma_{Q_{\text{Br}}}$  was highest (57% of the total error, see Table 2) indicating that  $\text{Br}^-$  addition to the sample by the peristaltic pump is the largest source of measurement error. For FIA analyses, the value of  $\sigma_{m_{\text{liq}}}$  had the highest contribution to  $\sigma_m$  (84% and 57% for  $\text{NH}_3$  and  $\text{NH}_4^+$  analyses, respectively). Reasons for that may be an incomplete removal of the temperature dependence by Eq. (6), and also the temperature influence on the equilibrium constant of  $\text{NH}_4\text{OH}$  and the permeation of  $\text{NH}_3$  through the membrane.

#### 4.2. Limit of detection (LOD)

The accurate characterization and determination of the limit of detection is crucial for measurements in regions like the Amazon Basin since concentration levels can be extremely low during the wet season. The limit of detection ( $\text{LOD} = 3\sigma$ ;  $\sigma$  = standard deviation of the background signal) was determined for actual field conditions for every individual data point and each compound. For anionic species analyzed with IC, the background noise ( $3\sigma$ ) was calculated from the variation of the baseline at the beginning and the end of each chromatogram comprising 11% ( $n = 542$ ) of the total chromatogram data points. The limit of detection ( $\text{LOD} = 3\sigma$ ) for the FIA analyses was determined analogously by background noise calculation before and after the  $\text{NH}_4^+$ -peak, also comprising 11% ( $n = 111$ ) of the total measurements for each run. Frequency distributions of the LOD for each compound during the entire field experiment

are shown in histograms (Fig. 3). The determined median LOD values were 0.102 ppb for  $\text{NH}_3$ , 0.011 ppb for  $\text{HNO}_3$ , 0.012 ppb for  $\text{HONO}$ , 0.008 ppb for  $\text{HCl}$ , 0.004 ppb for  $\text{SO}_2$ , 0.118 ppb for aerosol  $\text{NH}_4^+$ , 0.015 ppb for  $\text{NO}_3^-$ , 0.009 ppb for  $\text{NO}_2^-$ , 0.008 ppb for  $\text{Cl}^-$  and 0.004 ppb for  $\text{SO}_4^{2-}$ . Higher LOD values (see Fig. 3), were a result of unstable and noisy baselines caused by insufficient purity of the water, which was used as matrix for the solutions applied during analyses. The LOD values obtained for FIA were about an order of magnitude higher than for IC, because of the influence of temperature on detection procedures.

#### 4.3. Seasonal variation of mixing ratios

Measurements of 10 different compounds were performed during the field experiment which resulted in ~7000 data points of ambient mixing ratios. The proportion of rejected data points below the LOD was  $\leq 20\%$  for all compounds, except for  $\text{NH}_3$  and  $\text{HNO}_3$  (25%) and for aerosol  $\text{NO}_2^-$  (40%).

Statistical illustrations of the seasonal pattern of mixing ratios are shown in Fig. 4 for gaseous compounds and in Fig. 5 for aerosol species. A substantial decline of mixing ratio levels from dry season, through transition period to wet season was observed for all measured compounds. Gaseous  $\text{NH}_3$  was abundant at mixing ratios an order of magnitude higher than acidic trace gases, and maxima reached 8 ppb under burning conditions. Correspondingly, aerosol  $\text{NH}_4^+$  was also found to be at least 4 to 10 times higher than anionic aerosol species. Values of  $\text{NH}_3$  and aerosol  $\text{NH}_4^+$  declined by a factor of 2–3 from dry to wet season, suggesting that biomass burning is a strong source of these species. Also,  $\text{NH}_3$  emissions from cattle waste contributed to the observed levels. The amount of  $\text{NH}_3$  present during the wet season (~0.5 ppb, see Fig. 4), when biomass burning activity was nearly zero, is expected to be entirely attributed to emissions from cattle manure.

All acidic trace gases showed mixing ratios within the same order of magnitude (0.01–0.9 ppb) and decreased by more than a factor of 2 to the wet season.  $\text{SO}_2$

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showed the lowest values (median  $<0.1$  ppb) and the least seasonal variation, suggesting that biomass burning is not a major source of this compound in this region. Mixing ratios of aerosol anions were highest during the biomass burning season. Unexpectedly, aerosol  $\text{NO}_3^-$  (max  $\sim 1.25$  ppb) was most abundant, followed by aerosol  $\text{SO}_4^{2-}$  (max  $\sim 0.6$  ppb). Aerosol  $\text{NO}_3^-$  dominated over  $\text{SO}_4^{2-}$  under biomass burning conditions and showed the strongest decrease to the wet season (factor  $\sim 4$ ).  $\text{Cl}^-$  and  $\text{NO}_2^-$  contributed only very little to the aerosol inorganic composition and seasonal variations were smaller.

When widespread biomass burning occurred,  $\text{NH}_3$  mixing ratios at this Brazilian rural pasture site were similar to values observed with the WAD/SJAC at an urban location (EPA Atlanta Supersite, 1999; Zhang et al., 2002 and references therein). Nevertheless,  $\text{HNO}_3$  and  $\text{HONO}$  mixing ratios under burning conditions in the Amazon Basin were about five times lower than measured at the Atlanta Supersite (see Genfa et al., 2003). Aerosol  $\text{NO}_3^-$  measured with the SJAC system in Atlanta compared relatively well to the values observed in our study (see Weber et al., 2003). However,  $\text{NH}_4^+$  was about five times and  $\text{SO}_4^{2-}$  an order of magnitude larger at the urban site (Solomon et al., 2003; Weber et al., 2003). These results show that pollution in urban areas can be more severe than during biomass burning in the Amazon Basin.

#### 4.4. Diel variations of trace gases

##### 4.4.1. $\text{NH}_3$ and $\text{HNO}_3$

Figure 6 shows diel cycles for  $\text{NH}_3$  and  $\text{HNO}_3$  from 17 to 20 September 2002 (burning season), exhibiting a pronounced diel variation.  $\text{NH}_3$  was relatively low from 14:00 to 05:00 (1 to 3 ppb), with one exception in the night from the 18 to 19 September. Usually, between 05:00 and 13:00 sharp peaks occurred with distinctive maxima between 08:00 and 09:00. This is most likely due to the evaporation of  $\text{NH}_3$  from wet surfaces (grass leaves) after sunrise.

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The diel variation observed for  $\text{HNO}_3$  usually featured low values during the night from 18:00 to 06:00 (<0.2 ppb) and high values at daytime reaching maxima around midday (0.4 to 0.6 ppb). Such diel cycles are typical for this compound and resemble those found in several other studies (e.g. Tanner et al., 1989; Meixner, 1994; Mehlmann and Warneck, 1995; ; Fehsenfeld et al., 1998; Lefer et al., 1999; Furutani and Akimoto, 2002; Huang et al., 2002; Genfa et al., 2003). The main reasons for this behavior are: (a) intensive turbulent mixing from the free troposphere into the boundary layer during daytime, (b) deposition processes at night promoted by a stable thermal stratification of the nocturnal surface layer (limiting  $\text{HNO}_3$  supply from residual layer), (c) higher temperature and lower relative humidity during daytime which enables evaporation of  $\text{HNO}_3$  from the aerosol phase, and (d) daytime photochemistry (reaction of  $\text{NO}_2$  with OH radical). A detailed investigation of the diel behavior of  $\text{NH}_3$  and  $\text{HNO}_3$  will be presented in a following paper.

#### 4.4.2. HONO

Figure 7 shows diel patterns of HONO measured from 17 to 20 September 2002 (biomass burning season) and from 17 to 20 October 2002 (transition period). In the burning season, HONO featured a pronounced diel cycle with higher values at night, reaching maxima just after 00:00 (0.4 to 0.6 ppb). Heterogeneous reaction of  $\text{NO}_2$  with surface water as reported recently by Kleffmann et al. (2003) may be regarded as a HONO source, especially for nighttime HONO accumulation at high relative humidities at the site. During the day, HONO levels were low, varying between 0.05 and 0.1 ppb. Similar HONO diel characteristics were observed in other studies (e.g. Perner and Platt, 1979; Appel et al., 1990; Harrison et al., 1996; Huang et al., 2002; Stutz et al., 2002; Alicke et al., 2003). Rapid photolysis during sunshine leads to a decline in HONO mixing ratios (Harrison et al., 1996). Moreover, our measurements in the Amazon Basin may be additional evidence for a continuous HONO source since a complete depletion at daytime did not occur.

Diel patterns observed one month later (transition period, see Fig. 7) show distinct

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tive differences to those observed during the biomass burning season. HONO levels were identical in daylight and during nighttime resembling those measured in daylight under biomass burning conditions. Since  $\text{NO}_2$  is considered as the main reactant for heterogeneous HONO formation, obviously a declining  $\text{NO}_2$  abundance under cleaner conditions will diminish HONO accumulation at night (for details see following paper).

#### 4.4.3. HCl and $\text{SO}_2$

Nighttime values of HCl and  $\text{SO}_2$  (Fig. 8) were very low in the burning season ( $\sim 0.05$  to  $0.1$  ppb) while during daytime higher mixing ratios were found, with HCl exceeding  $\text{SO}_2$  levels by a factor of two or three. The marked diel pattern of HCl has a maximum in the early to mid afternoon, which is generally coincident with the period of maximum concentration of  $\text{HNO}_3$ , in agreement with several previous investigations (Graedel and Keene, 1995 and references therein). HCl is known to be emitted directly by biomass fires, accounting for a large fraction of the total emitted chlorine (Andreae et al., 1996). Apparently, turbulent mixing during daytime and a stable thermal stratification at night (deposition of acidic gases on wet surfaces) have caused diel fluctuations as shown in Fig. 8. Discussion of this matter will also be presented in the following paper.

#### 4.5. Diel variations of aerosol species

##### 4.5.1. Aerosol $\text{NH}_4^+$ , $\text{NO}_3^-$ and $\text{SO}_4^{2-}$

Observed diel variations for aerosol  $\text{NH}_4^+$ ,  $\text{NO}_3^-$  and  $\text{SO}_4^{2-}$  (fine fraction,  $< 2.5 \mu\text{m}$ ) from 17 to 20 September 2002 are plotted in Fig. 9a. As for corresponding gaseous species, pronounced diel patterns were found for  $\text{NH}_4^+$  and  $\text{NO}_3^-$ . Obviously,  $\text{NH}_4^+$  was strongly influenced by its gas phase precursor  $\text{NH}_3$ , peaking between 08:00 and 09:00 in the morning and revealing much higher mixing ratios than the anionic aerosol species. Possible evaporation of  $\text{NH}_3$  from wet surfaces at sunrise, when relative humidities were still high (see Fig. 9b and Sect. 4.4.1) might have caused a significant fraction

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of gaseous  $\text{NH}_3$  to dissolve in still deliquescent aerosols, therefore enhancing aerosol  $\text{NH}_4^+$ . Generally,  $\text{NH}_4^+$  and  $\text{NO}_3^-$  began to increase at  $\sim 22:00$  and remained high during the night, while values found during daytime were usually two or three times lower (see Fig. 9a). Consequently, aerosol  $\text{NO}_3^-$  showed a strong anti-correlation to  $\text{HNO}_3$ .

5 The equilibrium assumption between  $\text{NH}_4\text{NO}_3$  and its gas phase precursors, strongly affected by relative humidity and temperature, is expected to influence the measured gas and aerosol mixing ratios. High relative humidities and lower temperatures at night (Fig. 9b) should shift the equilibrium to the aerosol phase, causing the  $\text{NH}_4\text{NO}_3$  content to increase and resulting in a simultaneous decrease of atmospheric gas phase  
10 constituents. At daytime, semi-volatile species can evaporate from the aerosol phase, induced by lower relative humidities and higher temperatures (Fig. 9b), consequently raising the gas phase mixing ratios.

Time series of  $\text{SO}_4^{2-}$  did not show the same behavior. Mixing ratios were relatively stable throughout day and night, resembling those found for  $\text{NO}_3^-$  during daytime. Con-  
15 sidering the non-volatility of  $\text{SO}_4^{2-}$ , relative humidity and temperature should not influence the amount of  $\text{SO}_4^{2-}$  present in aerosols.

#### 4.5.2. Aerosol $\text{Cl}^-$ and $\text{NO}_2^-$

The diel cycles for aerosol  $\text{Cl}^-$  and  $\text{NO}_2^-$  (Fig. 10, fine fraction,  $<2.5\ \mu\text{m}$ ) during the burning season were less pronounced than for the other aerosol species.  $\text{NO}_2^-$  is  
20 higher at night, which may be an indication of heterogeneous HONO formation on aerosol surfaces. This matter will also be discussed in a following paper.  $\text{Cl}^-$  mixing ratios showed less distinctive differences between day and night, suggesting that it may be attached also to involatile cations such as  $\text{K}^+$ ,  $\text{Ca}^{2+}$  and  $\text{Na}^+$ .

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## 5. Conclusions

We employed a WAD/SJAC coupled with IC and ammonium FIA for the continuous measurement of  $\text{NH}_3$ , acidic trace gases ( $\text{HNO}_3$ , HONO, HCl and  $\text{SO}_2$ ) and corresponding aerosol species ( $\text{NH}_4^+$ ,  $\text{NO}_3^-$ ,  $\text{NO}_2^-$ ,  $\text{Cl}^-$  and  $\text{SO}_4^{2-}$ ) at a rural site in the Amazon Basin. A specially designed inlet system was applied for simultaneous sampling of gases and aerosols. Calculated inlet losses of aerosol species due to non-isokinetic sampling were below 3% ( $D_p \leq 2.5 \mu\text{m}$ ).  $\text{HNO}_3$  is known as a problematic compound regarding absorption on inlet surfaces. Theoretical wall losses for  $\text{HNO}_3$  were calculated to be  $\leq 15\%$ , assuming an uptake coefficient of  $\gamma_{\text{HNO}_3} = 0.5$  for the inlet surface.

Total measurement uncertainties of the mixing ratios in ambient air were usually below 15%. The use of a peristaltic pump for the  $\text{Br}^-$  standard addition to calibrate the IC was found to have the greatest contribution (57%) to the total measurement error. In order to reduce the influence of this factor, peristaltic pumps should be replaced by other devices (e.g. syringe pumps), which are capable to supply more constant flows on a long-term scale.

The limit of detection ( $\text{LOD} = 3\sigma$ ) was determined for each individual data point under actual field conditions. LOD median values remained below 0.015 ppb for all acidic trace gases and aerosol anions (IC analyses) but were higher ( $\leq 0.118$  ppb) for  $\text{NH}_3$  and aerosol  $\text{NH}_4^+$  (FIA analyses). Higher background noises during  $\text{NH}_3$  and aerosol  $\text{NH}_4^+$  detection procedures were apparently caused by the temperature dependence of the FIA analyses, which should therefore be carried out under temperature controlled conditions in the future.

Widespread biomass burning in the Amazon Basin was found to be a strong source of  $\text{NH}_3$ , present at mixing ratios about 3 times higher (max  $\sim 8$  ppb) than under clean conditions during the wet season. Also, levels of  $\text{HNO}_3$ , HONO and HCl were considerably higher than during the wet season (at least two times) but were an order of magnitude lower ( $< 1$  ppb) than the  $\text{NH}_3$  mixing ratios. The enhancement of gaseous compounds during the burning season significantly increased the amount of water-

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soluble inorganic aerosol constituents.  $\text{NO}_3^-$  and  $\text{SO}_4^{2-}$  were most abundant reaching maxima of 1.25 ppb and 0.6 ppb, respectively. Aerosol  $\text{NO}_3^-$  was the dominating inorganic anion during the biomass burning season and showed the strongest decrease to the wet season ( $\sim 70\%$ ). Additionally, N-containing gas and aerosol species exhibited pronounced diel variations, and both HCl and  $\text{SO}_2$  varied distinctively with maxima at daytime and minima during the night. Turbulent mixing at daytime is considered to have a major influence on the observed diel patterns, contributing to an increase of gaseous compounds at ground level. Deposition processes at night combined with a stable thermal stratification of the nocturnal surface layer may cause a decline of gaseous compounds ( $\text{NH}_3$ ,  $\text{HNO}_3$ , HCl and  $\text{SO}_2$ ) at nighttime. Moreover, our measurements indicate that the interaction between N-containing gas and corresponding aerosol constituents was dependent on relative humidity and air temperature, resulting in an enhancement of aerosol  $\text{NO}_3^-$  and  $\text{NH}_4^+$  at nighttime. Non-volatile aerosol  $\text{SO}_4^{2-}$  did not show strong diel fluctuations and remained stable throughout day and night. HONO showed a typical diel pattern when biomass burning occurred, exhibiting higher mixing ratios at night and lower values during daylight. Besides heterogeneous formation from  $\text{NO}_2$  and surface water, our observations suggest a continuous HONO source since a complete depletion at daytime did not occur.

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**Table 1.** Overview of sampling methods for NH<sub>3</sub>, acidic trace gases and inorganic aerosol species.

Method	Example	Measured species	References
Filter	Impregnated filters, Teflon and nylon filters in series	NH <sub>3</sub> , HNO <sub>3</sub> , aerosol NH <sub>4</sub> <sup>+</sup> , NO <sub>3</sub> <sup>-</sup> , Cl <sup>-</sup> and SO <sub>4</sub> <sup>2-</sup>	Appel et al., 1980; Appel et al., 1981; Cadle et al., 1982; Parrish et al., 1986; Galasyn et al., 1987; Solomon et al., 1988; Appel et al., 1991
Denuder & filter	Denuder-filter pack (DFP)	NH <sub>3</sub> , HNO <sub>3</sub> , HONO, HCl, SO <sub>2</sub> , aerosol NH <sub>4</sub> <sup>+</sup> , NO <sub>3</sub> <sup>-</sup> , Cl <sup>-</sup> and SO <sub>4</sub> <sup>2-</sup>	Kitto and Harrison, 1992; Harrison et al., 1996; Danalatos and Glavas, 1999; Possanzini et al., 1999
Diffusion denuder	Dry-coated diffusion denuder	NH <sub>3</sub> , HNO <sub>3</sub> , HONO, HCl and SO <sub>2</sub>	Eatough et al., 1985; Durham et al., 1987; Marshall and Dimmock, 1992
	Wet-effluent diffusion denuder	NH <sub>3</sub> , HNO <sub>3</sub> , HONO, HCl and SO <sub>2</sub>	Simon et al., 1991; Vecera and Dasgupta, 1991; Taira and Kanda, 1993; Buhr et al., 1995; Zellweger et al., 1999
	Parallel-plate denuder	NH <sub>3</sub> , HNO <sub>3</sub> , HONO, HCl and SO <sub>2</sub>	Simon and Dasgupta, 1993; Boring et al., 1999; Genfa et al., 2003
	Thermodenuder Wet-annular denuder	NH <sub>3</sub> , HNO <sub>3</sub> NH <sub>3</sub> , HNO <sub>3</sub> , HONO, HCl and SO <sub>2</sub>	Keuken et al., 1989; Klockow et al., 1989 Keuken et al., 1988; Wyers et al., 1993; Allegrini et al., 1994; Slanina and Wyers, 1994; Oms et al., 1996; Jongejan et al., 1997
Diffusion scrubber	Diffusion scrubber and mist chamber	NH <sub>3</sub> , HNO <sub>3</sub> , HONO, HCl and SO <sub>2</sub>	Matusca et al., 1984; Cofer et al., 1985; Phillips and Dasgupta, 1987; Lindgren, 1992; Lefer et al., 1999; Sanhueza and Garaboto, 2002
Fluorescence	Laser-photolysis fragment-fluorescence (LPFF) and laser-Fluorescence derivatization	HONO, HNO <sub>3</sub> NH <sub>3</sub> , aerosol NH <sub>4</sub> <sup>+</sup>	Rodgers and Davis, 1989; Papenbrock and Stuhl, 1990; Papenbrock and Stuhl, 1991 Abbas and Tanner, 1981; Rapsomanikis et al., 1988

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Table 1. Continued.

Method	Example	Measured species	References
Spectroscopy	Differential optical absorption spectroscopy (DOAS)	HNO <sub>3</sub> , HONO	Perner and Platt, 1979; Plane and Nien, 1992; Winer and Biermann, 1994; Febo et al., 1996; Stutz et al., 2002
	Chemical ionization mass spectrometer (CIMS)	HNO <sub>3</sub> , SO <sub>2</sub>	Huey et al., 1998; Mauldin et al., 1998; Furutani and Akimoto, 2002; Hanke et al., 2003
	FT-IR spectrometer	NH <sub>3</sub> , HNO <sub>3</sub>	Doyle et al., 1979
	Cavity ring-down spectroscopy	HONO	Wang and Zhang, 2000
	Long path absorption photometer (LOPAP)	HONO	Heland et al., 2001; Kleffmann et al., 2003
Aqueous-phase aerosol collection	Particle mass spectrometer	aerosol NH <sub>4</sub> <sup>+</sup> , NO <sub>3</sub> <sup>-</sup> , Cl <sup>-</sup> and SO <sub>4</sub> <sup>2-</sup> and others	Gard et al., 1997; Jayne et al., 2000; Mallina et al., 2000; Lee et al., 2002; Jimenez et al., 2003
	Particle-into-liquid sampler (PILS)	aerosol NH <sub>4</sub> <sup>+</sup> , NO <sub>3</sub> <sup>-</sup> , NO <sub>2</sub> <sup>-</sup> , Cl <sup>-</sup> and SO <sub>4</sub> <sup>2-</sup>	Weber et al., 2001; Orsini et al., 2003
	Particle collection system (PCS)	aerosol NO <sub>3</sub> <sup>-</sup> , NO <sub>2</sub> <sup>-</sup>	Simon and Dasgupta, 1995; Simon and Dasgupta, 1995
	Vapor condensation aerosol collector system (VCACS)	aerosol NO <sub>3</sub> <sup>-</sup> , NO <sub>2</sub> <sup>-</sup>	Zellweger et al., 1999
	Wet effluent frit (WEF) and integrated collection and vaporization cell (ICVC)	aerosol NO <sub>3</sub> <sup>-</sup>	Buhr et al., 1995; Stolzenburg and Hering, 2000
	Steam jet aerosol collector (SJAC)	aerosol NH <sub>4</sub> <sup>+</sup> , NO <sub>3</sub> <sup>-</sup> , NO <sub>2</sub> <sup>-</sup> , Cl <sup>-</sup> and SO <sub>4</sub> <sup>2-</sup>	Khlystov et al., 1995; Slanina et al., 2001

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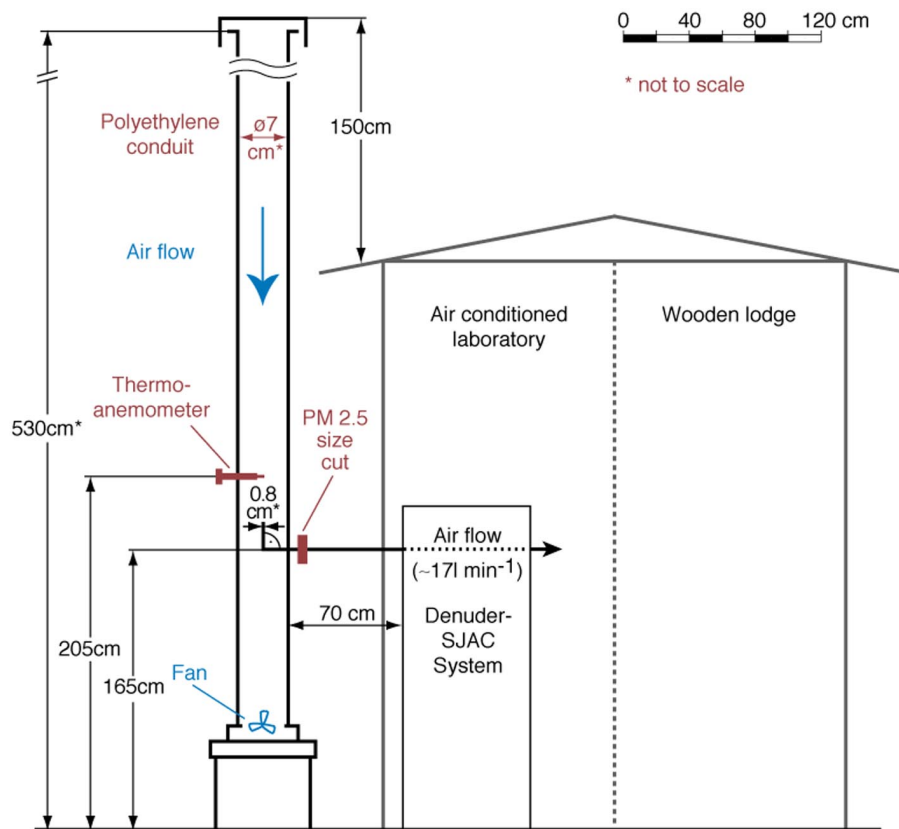
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**Table 2.** Standard deviations  $\sigma_x$  contributing to the total measurement uncertainty  $\sigma_m$ . (index  $x$  is the mixing ratio of the compounds found in “aerosol or gas sample” ( $m_{\text{liq}}$ ), the mixing ratio of the  $\text{Br}^-$  standard solution ( $m_{\text{Br}(\text{std})}$ ), the flow of the  $\text{Br}^-$  standard solution ( $Q_{\text{Br}}$ ), the analyzed  $\text{Br}^-$  mixing ratio ( $m_{\text{Br}}$ ) or the air mass flow through the system ( $Q_{\text{air}}$ ), and index  $m$  is the ambient mixing ratio).

Standard deviations $\sigma_x$	Value/range	Source/determination	Mean contribution to $\sigma_m$
<u>IC analyses</u>			
$\sigma_{m_{\text{liq}}}$	0.002–6.8 ppb	5% of $m_{\text{liq}}$ , analysis of standard solutions	18%
$\sigma_{m_{\text{Br}(\text{std})}}$	20 ppb	2% of $m_{\text{Br}(\text{std})}$ , estimated uncertainty of weighting procedures for creating $\text{Br}^-$ standard solutions	2%
$\sigma_{Q_{\text{Br}}}$	0.007 ml min <sup>-1</sup>	10% of $Q_{\text{Br}}$ , standard deviation of mean $Q_{\text{Br}}$ for the entire experiment	57%
$\sigma_{m_{\text{Br}}}$	2.9–12.0 ppb	5% of $m_{\text{Br}}$ , analysis of standard solutions	17%
<u>FIA</u>			
$\sigma_{m_{\text{liq}}}(\text{gas})$	0.07–25.0 ppb	10% of $m_{\text{liq}}$ , analysis of standard solutions	84%
$\sigma_{Q_s}(\text{gas})$	0.017 ml min <sup>-1</sup>	3% of $Q_s$ , standard deviation of mean $Q_s$ for the entire experiment	10%
$\sigma_{m_{\text{liq}}}(\text{aerosol})$	0.15–7.9 ppb	10% of $m_{\text{liq}}$ , analysis of standard solutions	57%
$\sigma_{Q_s}(\text{aerosol})$	0.041 ml min <sup>-1</sup>	8% of $Q_s$ , standard deviation of mean $Q_s$ for the entire experiment	37%
$\sigma_{Q_{\text{air}}}$	0.02–10.6 l min <sup>-1</sup>	Standard deviation of mean $Q_{\text{air}}$ for each sampling interval	6%

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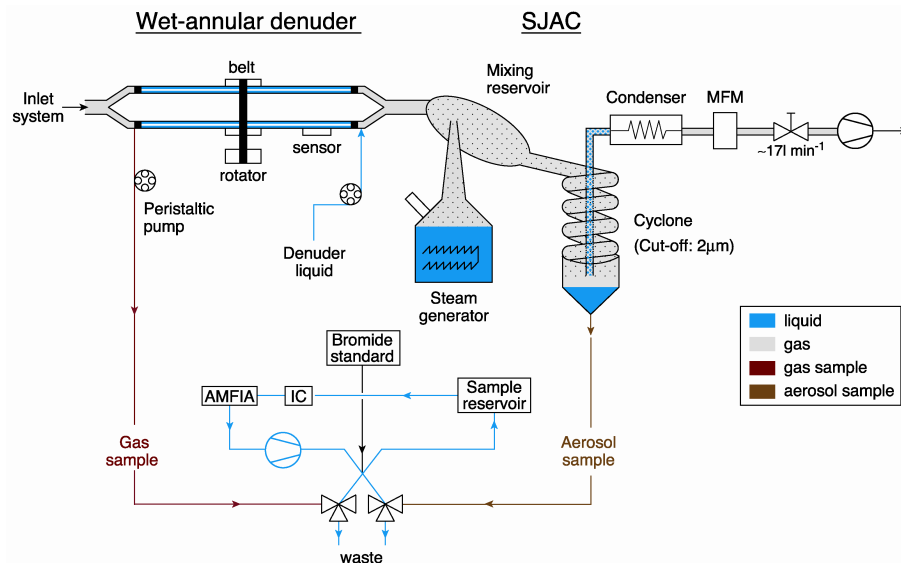


**Fig. 1.** Design and setup of the inlet system for simultaneous sampling of soluble gases and inorganic aerosol species.

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**Fig. 2.** Simplified sketch of the WAD/SJAC system including analytical part.

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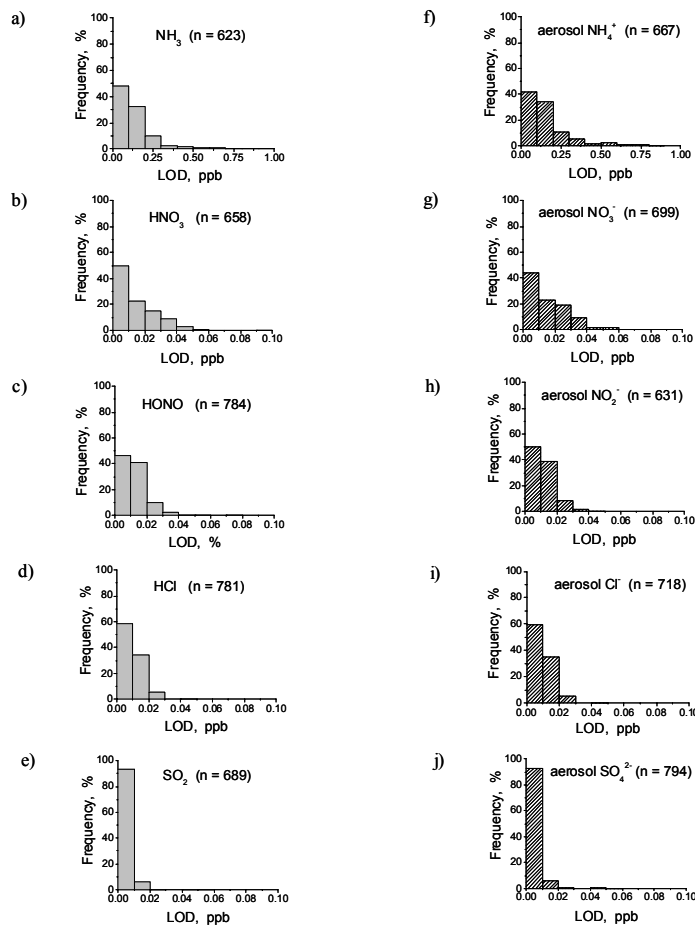
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**Fig. 3. (a)–(j).** Limit of detection (LOD) frequency distributions of gaseous **(a)–(e)** and aerosol **(f)–(j)** species measured during the LBA-SMOCC campaign (n = total number of values).

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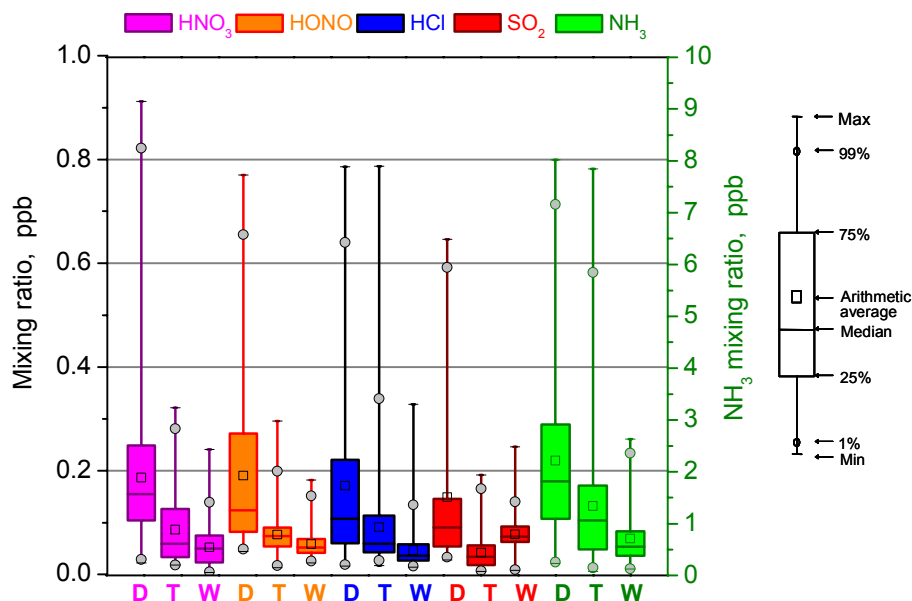
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**Fig. 4.** Box-and-whisker plots showing seasonal mixing ratio variations of gaseous compounds during dry season (D), transition period (T) and wet season (W) at FNS.

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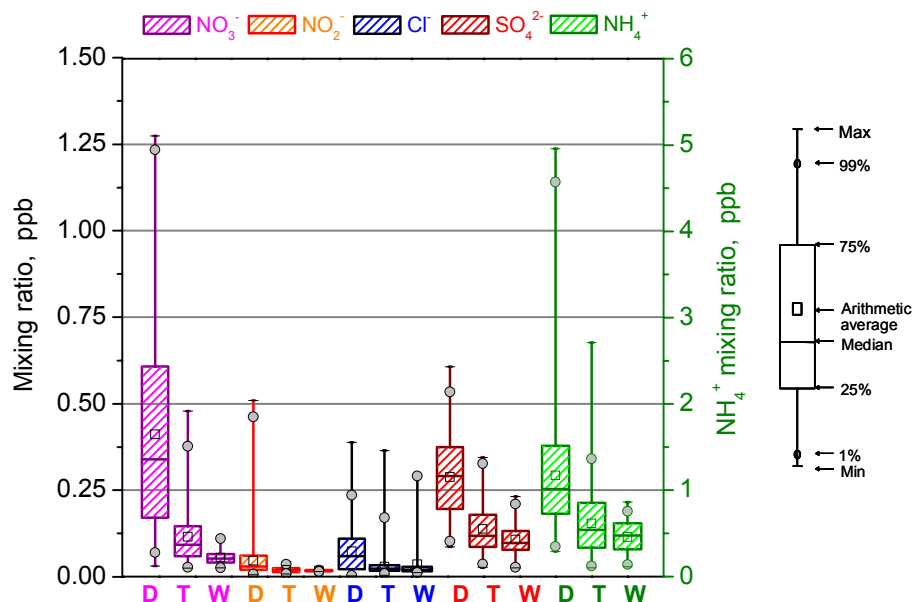
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**Fig. 5.** Box-and-whisker plots showing seasonal mixing ratio variations of aerosol species during dry season (D), transition period (T) and wet season (W) at FNS.

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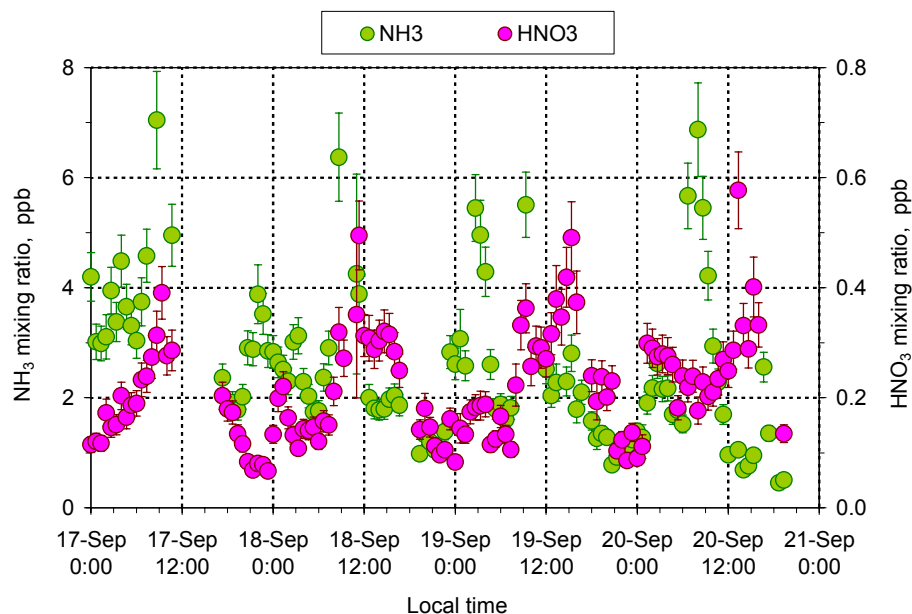
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**Fig. 6.** Diel variations of  $\text{NH}_3$  and  $\text{HNO}_3$  during 17 to 20 September 2002 (biomass burning season) at FNS. Error bars indicate measurement uncertainty for each data point.

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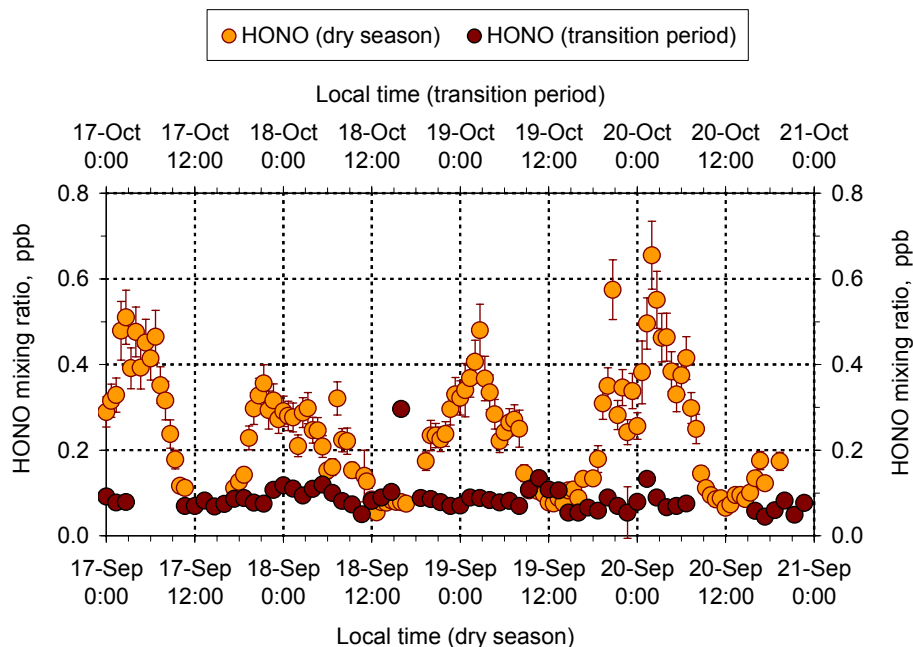
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**Fig. 7.** Diel variations of HONO during 17 to 20 September 2002 (biomass burning season) and during 17 to 20 October 2002 (transition period) at FNS. Error bars indicate measurement uncertainty for each data point.

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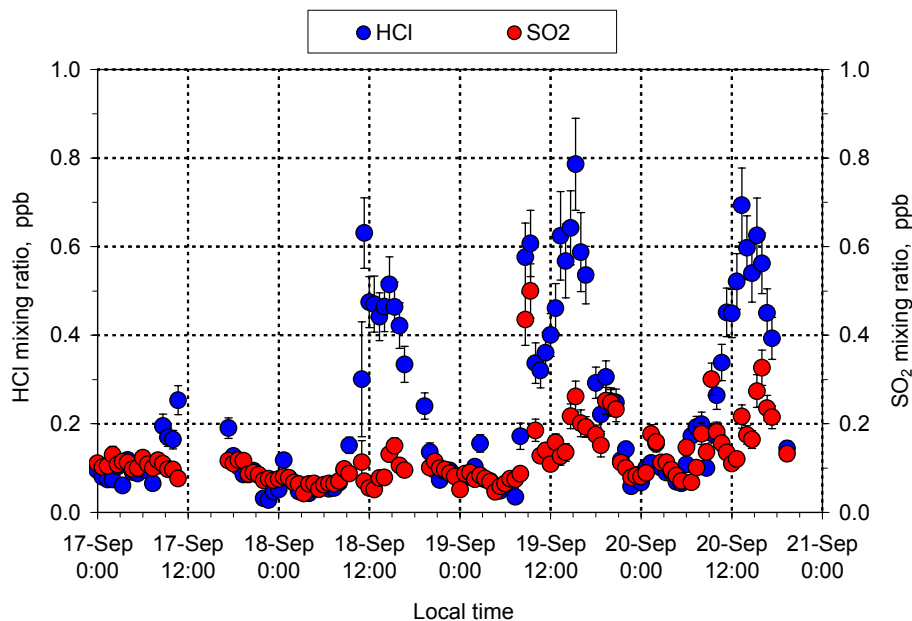
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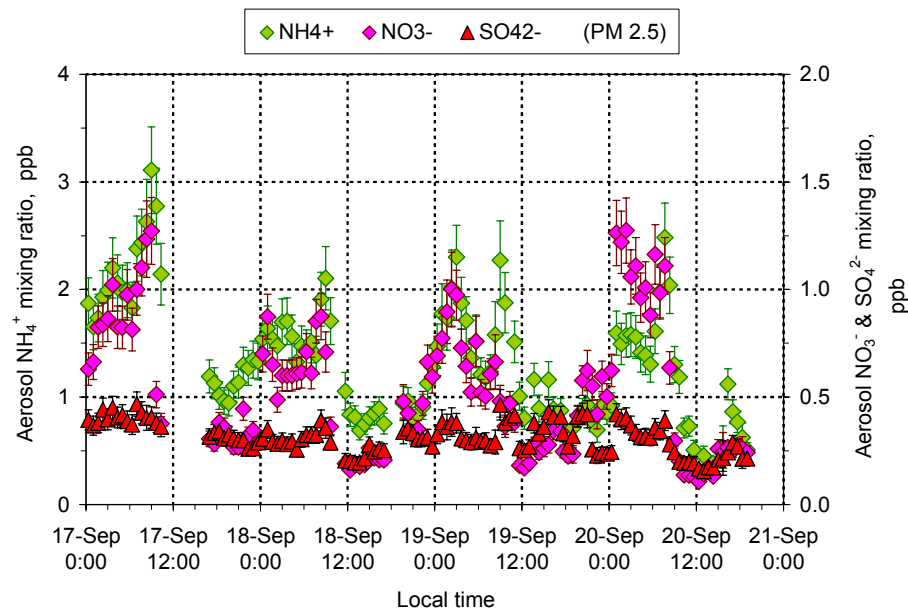


**Fig. 8.** Diel variations of HCl and SO<sub>2</sub> during 17 to 20 September 2002 (biomass burning season) at FNS. Error bars indicate measurement uncertainty for each data point.

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**Fig. 9. (a)** Diel variations of aerosol  $\text{NH}_4^+$ ,  $\text{NO}_3^-$  and  $\text{SO}_4^{2-}$  (fine fraction,  $<2.5\ \mu\text{m}$ ) during 17 to 20 September 2002 (biomass burning season) at FNS. Error bars indicate measurement uncertainty for each data point.

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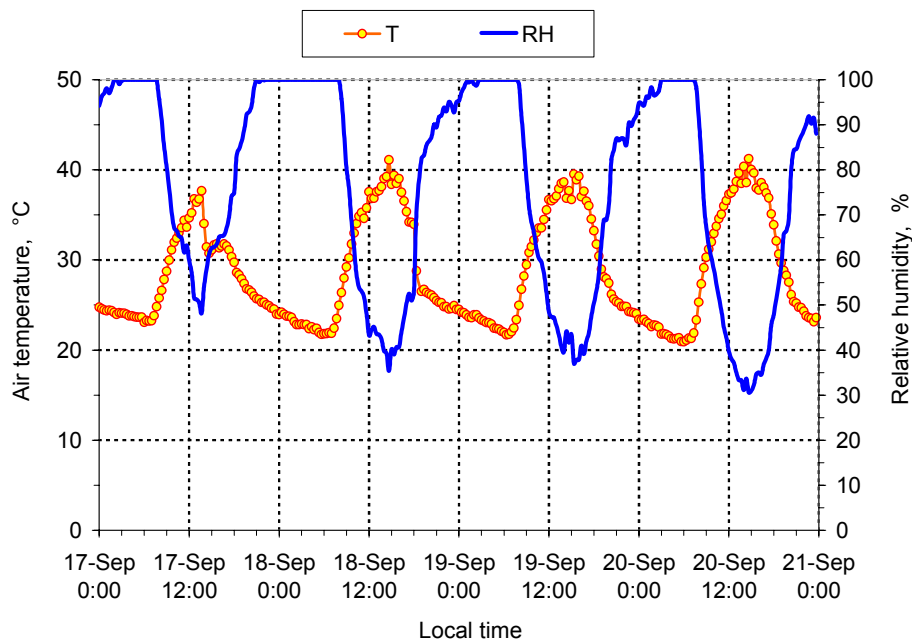
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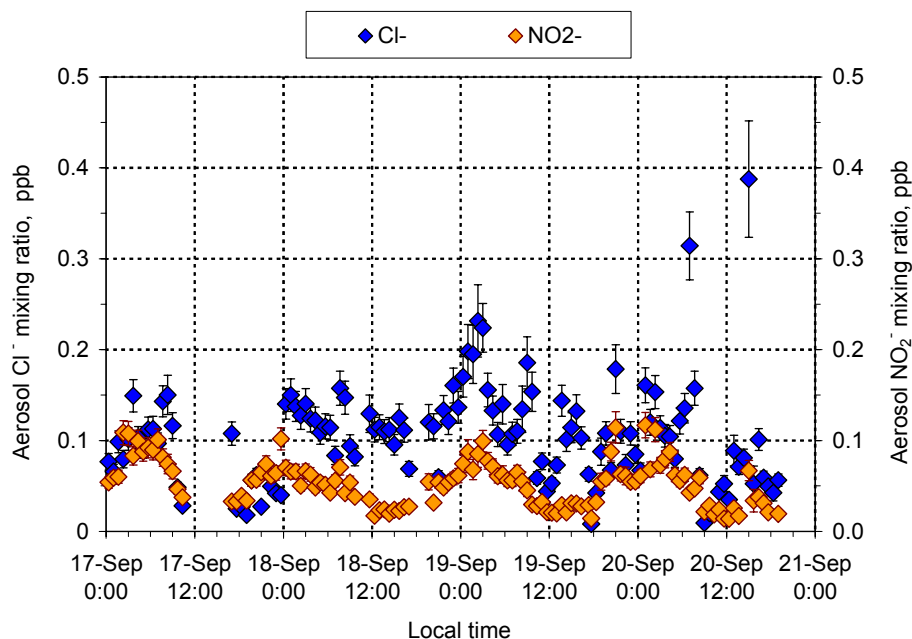


**Fig. 9. (b)** Diel variations of air temperature and relative humidity measured in the polyethylene conduit during 17 to 20 September 2002 (biomass burning season) at FNS.

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**Fig. 10.** Diel variations of aerosol  $\text{Cl}^-$  and  $\text{NO}_2^-$  (fine fraction,  $<2.5\ \mu\text{m}$ ) during 17 to 20 September 2002 (biomass burning season) at FNS. Error bars indicate measurement uncertainty for each data point.

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