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# Turbulence Kinetic Energy budget during the afternoon transition – Part 1: Observed surface TKE budget and boundary layer description for 10 intensive observation period days

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## Abstract

The decay of turbulence kinetic energy (TKE) and its budget in the afternoon period from mid-day until zero buoyancy flux at the surface is studied in a two-part paper by means of measurements from the Boundary Layer Late Afternoon and Sunset  
5 Turbulence (BLLAST) field campaign for 10 Intensive Observation Period days. Here, in Part 1, near-surface measurements from a small tower are used to estimate a TKE budget. The overall boundary layer characteristics and meso-scale situation at the site are also described based upon taller tower measurements, radiosoundings and remote sensing instrumentation. Analysis of the TKE budget during the afternoon  
10 transition reveals a variety of different surface layer dynamics in terms of TKE and TKE decay. This is largely attributed to variations in the 8 m wind speed, which is responsible for different amounts of near-surface shear production on different afternoons and variations within some of the afternoon periods. The partitioning of near surface production into local dissipation and transport in neutral and unstably stratified conditions was investigated. Although variations exist both between and within  
15 afternoons, as a rule of thumb, our results suggest that about 50 % of the near surface production of TKE is compensated by local dissipation near the surface, leaving about 50 % available for transport. This result indicates that it is important to also consider TKE transport as a factor influencing the near-surface TKE decay rate, which in many earlier studies has mainly been linked with the production terms of TKE by buoyancy and wind shear. We also conclude that the TKE tendency is smaller than the other budget terms, indicating a quasi-stationary evolution of TKE in the afternoon transition. Even though the TKE tendency was observed to be small, a strong correlation to mean buoyancy production of  $-0.69$  was found for the afternoon period. For comparison  
20 with previous results, the TKE budget terms are normalized with friction velocity and measurement height and discussed in the framework of Monin–Obukhov similarity theory. Empirically fitted expressions are presented. Alternatively, we also suggest a non-local parametrization of dissipation using a TKE-length scale model which takes

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into account the boundary layer depth in addition to distance above the ground. The non-local formulation is shown to give a better description of dissipation compared to a local parametrization.

## 1 Introduction

The atmospheric boundary layer (ABL) over land is inherently marked by a diurnal cycle. The afternoon transition period can be defined as the period from mid-day maximum heat flux until zero buoyancy flux (Nadeau et al., 2011). It is well-known as a period of turbulence decay in relationship to the diminishing near-surface energy input. This phase of the diurnal cycle is challenging from both an observational and modeling perspective due to its transitory nature and that most of the forcing are small in its later part. The turbulence regime also changes from a mid-day well-mixed convective regime to a more heterogeneous and intermittent state with a residual layer overlying a stably stratified surface layer when entering into the evening transition (Stull, 1988).

Many studies have as discussed in Lothon et al. (2014) provided insight into the late afternoon or evening transitions without being specifically dedicated to this purpose. The recent study of Wingo and Knupp (2015) also points out that observational study has become a priority. In the absence of a specific field campaign with this focus the Boundary Layer Late Afternoon and Sunset Turbulence (BLLAST) experiment was carried out in June and July 2011 at the “Plateau de Lannemezan” in southern France (Lothon et al., 2014). The site is located on a plateau of about 200 km<sup>2</sup> about 600 m a.s.l. and a few kilometer from the Pyrenean foothills and about 45 km from the highest peaks of the Spanish border.

In general, it may be concluded from the extensive review of existing literature provided in Lothon et al. (2014) that the decay of turbulence depends on the formulation of the decrease in the surface-atmosphere exchanges. For instance, the prescribed surface sensible heat flux or surface temperature affects the decay, but no consensus

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on an exact relationship between forcings and TKE decay rate has been reached. Several studies have described the governing TKE budget in sheared convective boundary layers and surface layers using measurements (Wyngaard and Coté, 1971; Caughey and Wyngaard, 1979; Högström, 1990; Frentzen and Vogel, 1992) and LES results for convective boundary layers (e.g. Moeng and Sullivan, 1994; Pino et al., 2003). See also discussions in Fedorovich and Conzemius (2008). In addition Kumar et al. (2006) and Rizza et al. (2013) conducted LES of the diurnal cycle, whereas van Driel and Jonker (2011) carried out an idealized study and analysis of periodically varying surface heat flux and its impact on boundary layer height and TKE.

Recent simulations (Darbieu et al., 2015), have also been used to study TKE and other turbulence characteristics such as anisotropy, evolution of spectra and integral length scales during the afternoon transition. This has also been studied by Pino et al. (2006) using large-eddy simulation, Grant (1997) by observations and by Goulart et al. (2003, 2010) with a theoretical spectral model and LES data. Turbulence kinetic energy and its decay during the afternoon transition have also been specifically studied from measurements by Nadeau et al. (2011) who also managed to model the near surface TKE relatively successfully based on a formulation for heat flux and dissipation ignoring other influences. Little attention has, however, been given to transport of TKE in many of the earlier studies with reasonable arguments that it will not affect the bulk TKE level when integrating over the entire turbulent boundary layer (Nieuwstadt and Brost, 1986; Nadeau et al., 2011). Over a limited vertical extent such argument needs, however, to be examined further. The study by Dupuis et al. (1997) for instance suggests that a significant near-surface transport of TKE can occur in homogeneous conditions over ocean. Shear production of TKE has also been discussed as a cause that can maintain near-surface TKE even when the buoyancy flux decays at the end of the afternoon, but no study has, to our knowledge, specifically focused on the TKE budget during the afternoon transition from an observational perspective to assess the relative importance of these factors.

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In this study, we present a TKE budget from field observations and use it to discuss the governing terms that influence TKE decay rate in the surface layer over a grass surface during the afternoon transition. Our analysis is based on 10 Intensive Observation Period (IOP) days using measurements from the small Divergence Site tower (see Fig. 1) located at the so-called Site 1 from the BLLAST field campaign (Lothon et al., 2014). We then follow-up our results with simple modeling of TKE in our companion paper Nilsson et al. (2015).

The main datasets and methods used in this study are presented in Sect. 2. For further information on the BLLAST dataset, see also the overview paper Lothon et al. (2014). In Sect. 3, some overall boundary layer characteristics are described to guide the reader about the variation of surface layer statistics in relationship to the larger-scale variations in wind and mixed layer depth that occur between the 10 IOPs. In Sect. 4, an hourly near-surface turbulence kinetic energy budget is presented for each afternoon period and a classification based upon wind speed and the size and variation of the dominant TKE budget terms is presented. Furthermore, mean TKE tendency or decay rate for the afternoons is presented. Relationships between TKE tendency and observed dissipation rate, shear and buoyancy effects are also presented. The TKE budget is normalized using a local friction velocity and measurement height for comparison to previous studies. Observed near-surface variation of dissipation rate with height is also investigated further. Finally, a non-local parametrization of dissipation is proposed and evaluated. This is followed by summary and conclusions in Sect. 5.

## 2 Data and methods

### 2.1 Data screening and treatment

Here we describe the main datasets used in this study and provide details about screening and treatment of the data. Turbulence data (20 Hz) of wind components ( $u$ ,

$v$  and  $w$ ) and sonic temperature  $T_s$  measured with Campbell Scientific anemometer-thermometers (CSAT) at the Divergence Site tower as well as Ultra High Frequency (UHF) wind profiler data is downloadable from the website (BLLAST, 2015).

### 2.1.1 Smoothing and gapfilling of UHF wind fields

The data set of UHF wind profiler data is available at an average temporal resolution of 5 min and vertical spatial resolution of 75 m starting at a height of 175 m. We use the UHF profiler data and radiosoundings from Site 1 (closest to the two towers). There was also a second UHF profiler operating during the field campaign (5.1 km away) which gave similar results (Said et al., 2012). The data loss was less than 2 % below 1900 m (on average about 0.7 %). An increasingly smaller data coverage is found for the layers above, at 2350 m it was about 10 % missing values and at 3000 m around 33 %. There was also some more frequent data loss at the lowest level (2.4 %) compared to the second lowest (0.74 %).

We used software from Garcia (2010) to do gapfilling and smoothing of the data set. The data were first placed on a uniform time-height grid by observational minute and using the 75 m vertical resolution. Then a smoothing parameter  $S$  of  $10^{-1}$  was used with 5 repeated iterations and an extra smoothing in time using a 5 min running mean value was used for time series from each vertical level. The larger the value  $S$ , the more smoothing obtained, see Garcia (2010) and accompanying matlab function, *smoothn*. No robust value of the smoothing factor  $S$  was obtained. The performance was, however, deemed as satisfactory for the most part, except for a period in the early morning and before sunrise on 26 June when the method caused the smoothed wind speed to be clearly underestimated. Also on some other periods in the morning or stable nighttime conditions the performance is less good than in unstable conditions.

At times, the gap filled wind direction fields can be argued to miss too much of the real variability that was indicated by the available non-gapfilled and un-smoothed data (and sometimes at the 60 m-tower). This was more frequent on days with low wind speed, but the smoothed and gap filled fields were nevertheless used to describe the

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overall boundary layer behavior in wind in Sect. 3 (and Appendix A). The time-height smoothed fields were also needed for reasonable tracking of persistent wind speed gradients near the inversion, which was otherwise at times obscured by more random fluctuations in the wind field (less persistent in both time and vertical direction).

### 2.1.2 Screening and treatment of turbulent time-series from tower measurements

After manually checking time-series, of wind and temperature, the four upper measurement levels at the small Divergence Site tower (2.23, 3.23, 5.27 and 8.22 m) were chosen for the main analysis and TKE budget calculations. Out-of-range values above 100 or below  $-100$  of any wind component or temperature were first removed from all time-series. Outliers outside plus minus 4 standard deviations from the mean value for each hour were also removed before further calculations. Each hourly time-series was also manually checked and suspicious “noisy” periods were error-flagged. If any 10 min period during an hour had less than 90 % of data coverage that hour was excluded from TKE budget calculations. Linear interpolation was applied when needed. Most of the time the data loss was small (less than 2 %).

This procedure may seem restrictive, but most excluded data belonged to non-IOP days and/or stable conditions (when further considerations should be taken into account). For instance, shallow drainage flows, a mountain-plain circulation and on some occasions, a low-level jet require special treatment of the evaluation of shear production at times when the wind profile was observed to be reverse or non-monotonic (Nilsson et al., 2014; Nauta, 2013; Román-Cascón et al., 2015).

Fluxes were calculated in a rotated coordinate system (Kaimal and Finnigan, 1994, natural wind coordinates with double rotation). We will use an overbar to denote a 10 min averaging operator. For TKE budget terms a subsequent averaging over 1 h is, however, used to reduce scatter and study the more slow trends of the different terms. For a moderate boundary layer wind speed of  $5 \text{ m s}^{-1}$  a 10 min sample would in a simple calculation with Taylors hypothesis correspond to a distance of about 3 km.

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Topographical differences within 2–4 km around the site, on the plateau, are smaller than further away from the site. Therefore, choosing this averaging time may limit some complexity related to topography. Near the surface, fluctuations in TKE and variance values from one 10 min period to the next was not as large as found on the 60 m-tower.

5 At the 60 m-tower also the quality of spectra in the high-frequency range appeared more noisy and questionable and budget calculations were not performed.

**2.2 Determination of the terms in the turbulence kinetic energy budget**

The governing equation for TKE in a sheared convective boundary layer under the assumption of horizontally homogeneous turbulence and no advection is given by Stull (1988):

$$\underbrace{\frac{\partial E}{\partial t}}_{\text{TKE Tendency}} = \underbrace{-\overline{u'w'}}_{\text{Shear production}} \frac{\partial U}{\partial z} + \underbrace{\frac{g}{\bar{\theta}} \overline{w'\theta'_v}}_{\text{Buoyancy production}} - \underbrace{\frac{\partial \overline{w'E'}}{\partial z}}_{\text{Turbulent transport}} - \underbrace{\frac{\partial \overline{w'p'}/\rho_0}{\partial z}}_{\text{Pressure transport}} - \underbrace{\epsilon}_{\text{Dissipation}} \quad (1)$$

Here TKE (=  $E$ ) denotes  $1/2 (\overline{u'^2} + \overline{v'^2} + \overline{w'^2})$ , where  $u'$ ,  $v'$  and  $w'$  are instantaneous deviations of, respectively, the along-wind, cross-wind and vertical wind components from their respective mean values.  $U$  is the magnitude of the mean wind, which varies with height  $z$ ;  $g$  is acceleration of gravity;  $\bar{\theta}$  is mean absolute temperature;  $\theta'_v$  is the instantaneous deviation of virtual temperature from its mean value;  $\rho_0$  is air density;  $p'$  is the instantaneous deviation of air pressure; and  $\epsilon$  is the mean dissipation rate of TKE.

We have given the buoyancy term the subscript buoyancy production of TKE since we limit our study to the afternoon period before stable stratification starts. Hence, it is always a positive term in our case. The physical interpretation of the six terms in Eq. (1) from left to right is hence: local time rate of change of TKE; shear production



of TKE; buoyancy production of TKE; vertical divergence of the turbulent transport of TKE; vertical divergence of the pressure transport of TKE; and dissipation rate of TKE.

### 2.2.1 Tendency of turbulence kinetic energy

5 Firstly, we determined TKE ( $= E$ ) values for every 10 min sample followed by forming a 1 h running mean TKE time-series. This was done to avoid studying very temporary fluctuations in TKE which showed little correlation to, for instance, the generally decaying sensible heat flux during the afternoon transition. A second-order finite difference approximation was then applied to the running mean timeseries to obtain estimates of TKE tendency at 12:30, 13:30, etc. UTC for the afternoon.

10 The variations in TKE on shorter time-scales may potentially be related to advection of TKE, temporary shading from clouds causing changes in the near surface energy balance, fast variations in near-surface wind gradients and fluxes or other effects causing non-stationarity in TKE (and especially in horizontal wind variances). Here we will, however, focus on the more persistent slow trends and changes observed in  
15 TKE in relationship to persistent changes in the other budget terms.

### 2.2.2 Shear production of TKE

This term is evaluated from the shearing stress  $\overline{u'w'}$  and the mean wind gradient at each height (2.23, 3.23, 5.27, 8.22 m) with turbulence measurements. Shearing stress was calculated from measured time-series of vertical and along wind velocity components. A polynomial expression was fit between wind speed and logarithmic  
20 height to estimate the wind gradient at all four heights. The calculation procedure was compared to using a second-order finite difference approximation to estimate the wind gradient for the 3.2 and 5.3 m level. The results indicated only small differences.

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### 2.2.3 The buoyancy production term

This term requires only the measurement of the turbulent flux of virtual temperature, which is nearly equal to the corresponding flux of the directly measured “sonic” temperature at each turbulence level, and measurements of the mean temperature.

5 The 8.2 m temperature was chosen as reference temperature  $\bar{\theta}$ .

### 2.2.4 Dissipation

Dissipation ( $D = -\epsilon$ ) or dissipation rate,  $\epsilon$  was estimated from spectra. Power spectral densities for the  $w$  component premultiplied by frequency  $nS_w(n)$  were plotted on a log-log scale against frequency  $n$ . According to Kolmogoroff (1941), and further assuming  
10 Taylors hypothesis to be valid, the spectral curves in the inertial subrange are predicted to be straight lines with  $-2/3$  slope in this representation,

$$nS_w(n) = \frac{4}{3}\alpha_1\epsilon^{2/3}\left(\frac{2\pi n}{U}\right)^{-2/3},$$

so that

$$\epsilon = \frac{2\pi n}{U} \left[ \frac{3nS_w(n)}{4\alpha_1} \right]^{3/2}.$$

15 Here  $\alpha_1$  is the universal Kolmogorov constant  $\approx 0.52$  (Wyngaard and Coté, 1971; Högström, 1996) and  $n$  must be in the range with  $-2/3$  slope. In practice each hour of data analysed was split into 8 periods of 7.5 min and dissipation rate was estimated by fitting a line to a range of wave numbers above 0.1 and then using the obtained relationship to calculate dissipation rate using the equation shown above. The mean value and standard deviation of the 8 estimates was calculated and the mean value  
20 is used as an average dissipation rate estimate for the hour. We chose to use the vertical wind spectra for our calculation of dissipation since it appeared less influenced by non-stationarity than the horizontal wind components.

## 2.2.5 Transport

Transport is given by two parts, pressure transport and turbulent transport. Pressure transport,  $T_p = -\frac{\partial \overline{w'p'}/\rho_0}{\partial z}$ , is well-known to be very difficult to measure directly. We attempted to calculate the pressure velocity covariance from a microbarometer and vertically displaced sonic anemometer at the so-called “small-scale heterogeneity site” (which is located about 100 m away from the 60 m tower and 400 m away from the Divergence Site tower). There was, however, no clear leveling off in Ogive curves and the results were very scattered for this parameter. Hence, due to the uncertainty in this parameter, estimates of this term are not reported.

The turbulent transport,  $T_t = -\frac{\partial \overline{w'E'}}{\partial z} = -\frac{1}{2} \frac{\partial}{\partial z} \left( \overline{w'u'^2} + \overline{w'v'^2} + \overline{w'w'^2} \right)$ , was also calculated directly for each turbulence level at the Divergence Site. Although the sum of the third-order moments often showed a diurnal cycle, the uncertainty introduced by taking a vertical gradient, led to large scatter in estimates of the turbulent transport term. In fact the profile of estimated  $\overline{w'E'}$  was found to be mostly non-monotonic regardless of choice of averaging time and pre-filtering procedure.

Therefore, we believe that a better estimate of the total transport (being equal to the sum of turbulent and pressure transport) is obtained from the residual of the TKE budget. Hence, we determine the total hourly transport value  $T$  by the following calculation:

$$T = \frac{\partial E}{\partial t} - S - B - D,$$

where the other budget terms have been averaged for each hour centered around 12:30, 13:30, etc. UTC for the afternoon period. It should be noted that  $T$  thereby absorb errors in the terms on the right hand-side and possibly influence from horizontal transport.

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### 3 Summary of overall boundary layer situation and its use for interpretation of surface layer TKE budget

Here, we summarize some of the atmospheric conditions for 10 IOP days. The description is based on boundary layer depths from radiosoundings (using a maximum potential temperature gradient criteria), UHF wind profiler (determined from reflectivity based on the refractive index of air, which is related to pressure, temperature and specific humidity, see Cohn and Angevine, 2000) and lidar (see Fig. 2). Wind speed and direction from tower measurements and the lowest UHF profiler level are presented in Figs. 3 and 4. In Appendix A, also a day-by-day description divided up into the four main observational periods 19–20, 24–27, 30 June–2 July, and 5 July are provided based on temperature and humidity (from the 60 m-tower and radiosoundings) and a more detailed view of height time-variation of wind from UHF (see Figs. A1 and A2). The site longitude is around  $0.21^{\circ}$  E, consequently UTC, very similar to local solar time, is used as the time reference hereafter.

For even further information about the synoptic situation and standard radiosounding we also refer the reader to the Day-by-day description of IOPs in Blay-Carreras (2013) and the Day-by-day analysis of synoptic and meteorological conditions (Nilsson, 2014) with more figures that were used to characterize the situation for these 10 IOP days. These reports are found on the BLLAST webpage (BLLAST, 2015), which also has a collection of other BLLAST related studies.

For these 10 IOPs many different conditions in terms of boundary layer depth, wind speed and moisture conditions occurred. This was found even though, mainly being fair-weather days with generally no or small amount of cloud cover, except on 24 and 30 June which did have some more clouds (Lothon et al., 2014). The boundary layer depth (here shown in Fig. 2), estimated from lidar measurements, was broadly categorized based on its evolution in Lothon et al. (2014) with 19 June and 1 July having a rapid growth and leveling inversion in the afternoon. For 20, 24, 25, 30 June and 2 July instead a more typical growth and leveling inversion was found (Lothon et al., 2014)

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and for 26, 27 June and 5 July the situations were categorized with slower growth and rapidly decreasing inversion top in the late afternoon. On 5 July for the late afternoon the top inversion was more diffuse than on some of the other days. Identifying the inversion based on potential temperature gradient gave sometimes a different result with higher boundary layer depth estimate.

From the UHF wind profiler data provided in Appendix A it is clear that the overall boundary layer flow situation involves an upper wind speed gradient which is often present, for at least 6 out of 10 days, possibly excluding 25–30 June when it was weaker and/or more diffuse. The height of the strong wind speed gradient marks a dynamical separation of the boundary layer flow with northerly or easterly wind (in daytime) from the dominant westerly flow above. The north-easterly boundary layer wind is most of the time linked with a mountain-breeze circulation on the site. The mainly westerly or weak flow above the boundary is related to the synoptic weather situation on the different days. When the boundary layer flow, related to the complex meso-scale situation at the site, encounters and mixes with the flow above, a layer of reduced wind speed in the upper parts of the boundary layer also occurs, as can be observed for several days (see Fig. A1 and for instance 20, 25, 26 June and 1, 2, and 5 July).

On some of the warm days (25–27 June) the wind direction in the boundary layer is more easterly in daytime. This is related to a low-pressure area in the lower troposphere over the Gulf of Lion in the Mediterranean (Lothon et al., 2014). Wind speed is (as seen from Figs. 4 and A1) variable in both time and space, but the lowest UHF level is quite representative of the boundary layer flow up to some height where the wind turns, and mixing of easterly boundary layer flow and westerly synoptic or meso-scale flow occurs. Wind speed below 100 m is less than  $5 \text{ ms}^{-1}$  most of the days except on 26, 27 June and end of 5 July.

Smaller differences in wind characteristics are generally observed on the 60 m-tower and the small tower between the days, than in the boundary layer in general. Wind direction is reasonably consistent on both towers and the lowest UHF level during

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daytime, but once the buoyancy flux becomes negative (marked by a vertical black line in Fig. 3), the wind direction on the small tower often shifts rapidly towards south (19, 20, 24, 25, 30 June and 1, 2 July). This turning is related to a shallow drainage flow which was further studied by Nauta (2013) for some days and for 2 July also by Román-Cascón et al. (2015). This wind turning in the shallow layers near the surface related to very local terrain-induced effects precedes the setup of a common larger-scale mountain breeze circulation (Román-Cascón et al., 2015) which is often recognized in time series about 2–3 h later. The mountain breeze circulation for this site has been studied by meso-scale modeling (Jiménez and Cuxart, 2014, 2015).

When the atmosphere is stably stratified, it is important to remember that the surface TKE budget gives very limited information about upper layers. For unstably stratified conditions there is, however, no reason to believe that such decoupling issues exist, and as we shall see in Sect. 4.3, mixed-layer dynamics (linked with boundary layer depth) has an influence on dissipation rate even very near the surface. Surface layer wind is used in the TKE budget analysis in the following sections. Many of the variations in observed surface layer wind on the small tower is, however, clearly linked and caused by variations in boundary layer wind observed on the 60 m-tower and by the UHF profiler. Therefore this instrumentation provides important additional information for interpretation of surface layer results.

When comparing sensible heat fluxes shown in Lothon et al. (2014) to the overall boundary layer description presented here it is also clear that warmer days (e.g. 26 and 27 June) in general have lower fluxes and colder days higher fluxes (e.g. 19, 24 June and 1 July). This is linked to the ground-air temperature difference on the different days. This is an important factor in determining the size of the buoyancy production term in the turbulence kinetic energy budget during the afternoon transition. The moisture content is also important although this may become even more important in the evening and night (not studied in detail here) as indicated by the higher observed specific humidity reported in Table A1.

## 4 TKE budget and near surface analysis

### 4.1 Overview and classification of observed TKE budget for 10 IOP days

In Fig. 5, we present the observed hourly TKE budget for each afternoon transition period from 12:00 UTC (normalized time 0) to zero buoyancy flux (normalized time 1) for all 4 levels of the small Divergence Site tower. The measurement levels (2.23, 3.23, 5.27 and 8.22 m) are shown as dashed, dash-dotted, full and dotted lines.

For buoyancy production (in blue), only very small height variations are observed and a general decrease during the afternoon is observed for all days. On 30 June, this general picture is partly interrupted by the presence of clouds changing the energy balance. The warmest days, 26 and 27 June with maximum temperature reaching about 32 °C, had less buoyancy production in comparison to for instance 19, 24 June and 1 July which were colder (19, 18, 24 °C).

Also, the dissipation rate (in black) is observed to have a general decrease during the afternoon transition for 8 out of 10 IOP days. Most significant deviations are found on 27 June and 5 July. These days indicate a clear increase of dissipation rate at the end of the afternoon, related to an increase in shear production as a response to the 8 m wind speed increase during the afternoon. Also, 19 June and 1 July have temporary increases in the hourly mean local dissipation rate estimates. This is most clearly seen at the lowest measurement level in response to variations in local shear production during these afternoon periods. Hence, shear production plays an important role near the surface in the TKE budget for most of these 10 IOP days, but clearly has the most pronounced height dependence out of all budget terms. This implies that its effect as a production term is more localized and acting near the surface compared to the buoyancy contribution. The strongest dissipation rate is also found closest to the surface, but the height variation of dissipation is smaller.

Given that the TKE tendency (in green) is much smaller (two order of magnitudes) than the other budget terms this implies that the sum of turbulent and pressure transport (in magenta) compensate for remaining height variation in the budget.

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Because the tendency term of TKE is much smaller than the other budget terms we will refer to the hourly TKE as evolving in a quasi-stationary way. We note that this is sometimes considered to have the more strict definition that an equilibrium between production terms and dissipation exist, such that the tendency term becomes small (under assumption of small transport). Here, we use the term quasi-stationary to mean that the tendency of TKE is small in comparison to the other budget terms without requiring that the transport term be smaller than the dissipation or production terms. This result of quasi-stationarity is consistent with the observed slowly evolving mean TKE levels in LES for a large part of the afternoon of 20 June as described in Darbieu et al. (2015). Although, the TKE tendency then increased somewhat in the late afternoon in the large-eddy simulation a threshold of about  $-1.1 \times 10^{-5} \text{ m}^2 \text{ s}^{-3}$  was used in Darbieu et al. (2015) to indicate the faster decay, and this is still quite a small TKE tendency.

The height variation of transport is found to mainly be linked with local shear production. We will refer to the sum of turbulent and pressure transport as simply transport unless stated otherwise. It is worth noting that the transport term calculated as a residual (as discussed in Sect. 2.2.5) should be regarded as the most uncertain term in the budget, but despite this, it is consistently a negative term in the TKE budget. This implies a transport of near-surface produced turbulence to the surrounding environment and upper parts of the boundary layer. On 30 June, in relationship to changing cloud cover, the transport was found to be temporarily a positive term in the budget. On a few other occasions (such as for instance 19 June) this also occurred when the dissipation estimates were found to be more uncertain (or variable as noted from calculation of a standard deviation value of the dissipation within hour, not shown here).

To investigate general differences between the different days, we calculated statistics for each budget term during the afternoon period. These statistics are provided in Appendix B and some of the most important findings are discussed here. In Tables B1 and B2, we report the mean value (and standard deviation) for wind speed, shear



production, buoyancy production, transport and dissipation. Table B1 refers to the 2.23 m level and Table B2 the 8.22 m level. Note also that a scale factor of  $10^{-3}$  has been used for the budget terms.

It is important to note from Tables B1 and B2 that the variation between highest and lowest mean value for the different afternoons for shear production is as large as  $6.7 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  for the 2 m level (and  $3.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  for 8.22 m level). This can be compared with the buoyancy production variation that is only  $1.5(1.4) \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  between the different afternoons. As we observed that these two terms are the dominant production terms in the near-surface budget and transport acts as a sink term transporting TKE out of the near-surface layers, we could expect variations in dissipation and transport between different afternoons to be mostly related to variations in shear production this close to the surface. To some extent, the less dominant variations in buoyancy production on different afternoons explain variations in near-surface dissipation (and transport) as already seen from the overall decreasing trend of dissipation rate and buoyancy flux in Fig. 5. This is a main basis for simple modeling attempts of turbulence decay (Nadeau et al., 2011) in convectively dominated conditions. However, our data reveals that the role of shear and transport may be equally if not more important to take into account for modeling of sheared convective surface layers. It is worth commenting on the wind. Although weak (the afternoon mean values are always less than  $3 \text{ m s}^{-1}$ ) the relative importance of shear is stressed here. The variation between maximum and minimum afternoon mean values for transport is as large as  $4.4(1.9) \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  and for dissipation  $4.0(3.5) \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  for 2.23 (8.22) m. Larger variations in both the transport and dissipation term compared to the buoyancy term is observed for both measurement levels.

In Table B3, we show TKE mean values for the afternoon, early afternoon (between 12:00 and 13:00 UTC) and late afternoon (last 30 min), as well as the average TKE tendency for the afternoon. Values are given both for 2.23 and 8.22 m level. Comparing TKE mean values and mean wind speed for the afternoon from Tables B1 or B2 does show that the three lowest TKE mean values occurring on 30 June, 2 and 5 July had

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the lowest wind speed and 25 June, which had the highest wind speed also had the highest mean afternoon TKE value.

There are of course exceptions from the rule that a higher wind speed lead to a higher TKE level that needs to be further discussed. In Fig. 6, we show the mean wind profiles for the 10 afternoons and have placed the same color on the two most similar profiles to facilitate further discussions to come. It is directly clear that 24 June and 5 July (in red) have essentially equal mean wind for the afternoon as a whole, yet from Table B3 we note that average TKE values are higher for 24 June. This is likely related to a higher mean buoyancy production of about  $3.4 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  (the highest in the data set) in comparison to about  $1.9 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  for 5 July, which is the lowest in the data set. Hence, several terms need to be considered to understand the observed variations in TKE. It is also worth noting that the higher mean TKE value for 24 June in comparison to 5 July is due to the early afternoon TKE being higher, but in the late afternoon the TKE level is higher for 5 July. This is mostly related to an increase of wind and shear production at the end of the afternoon on 5 July (see Fig. 5). This is only one example mentioned to illustrate the need for several explanatory factors when interpreting the behavior of TKE and TKE decay during the afternoon transition, as well as the evolution of the “forcings”.

Nevertheless, it is interesting to note that a relatively high negative correlation ( $-0.69$ ) between the mean afternoon TKE tendency and mean afternoon buoyancy production exist as shown in Fig. 7a. This is interpreted to imply that in the case of a strong buoyancy production (both before and during the afternoon) TKE levels in mid-day are higher and therefore TKE decay rate during the afternoon can become higher. However, it is always small in comparison to other budget terms. A weaker positive correlation ( $0.33$ ) is found between TKE tendency and shear production, implying that turbulence will decay more slowly during a more shear-driven afternoon as seen in Fig. 7b. This is in general agreement with reduced TKE decay rates for the afternoon found in large-eddy simulation when including wind shear (Pino et al., 2006) and is also discussed using a theoretical spectral model and LES data by Goulart et al. (2003,

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2010). Best linear fit expressions have been included in both (a) and (b). Attempts were done to non-dimensionalize surface layer TKE tendency itself with measurement height and friction velocity and correlate it with various non-dimensional parameters such as  $z/L$ ,  $z_i/L$  but it gave decreased correlation in comparison to relating tendency directly to buoyancy production as in Fig. 7a.

We do a broad summarizing classification of the 10 different afternoons in Table 1 based on the TKE budget mean values of Tables B1 and B2. In Part 2, when attempting to model TKE and TKE decay, we discuss more details and variations.

For this broad classification we take as starting point the terms of largest variation at the 2 m-level as a reference level for this classification. The days were placed into 3 categories (higher, moderate and weaker) in terms of mean wind speed, with 20, 25, 26 and 27 June having the higher mean wind speeds and 30 June and 2 July the weakest winds of the data set. A marker “X” denotes placement in a category. When the variation within the afternoons justifies that only part of the afternoon belongs to a given category we denote in parentheses “(p)”. For the moderate category, we also indicate with “h” or “l” if the variable mainly departs toward the lower or higher category. In a similar way shear production, transport and dissipation are classified into 3 categories (higher, moderate and weaker). For buoyancy production, the variations were smaller and only two categories (higher and moderate) are used. For dissipation, we also mark the special cases of 27 June and 5 July with increasing dissipation during the afternoon with “inc” within parenthesis.

If the mean value of shear production at the 2 m level is above  $3.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$ , it is considered higher (marked with bold font) and, if it is lower than  $2.0 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$ , it is considered weaker (marked with underlining). The moderate category is marked in italics. These arbitrary limits illustrate an expected correspondence between the mean afternoon wind speed and classification based on mean shear production for these afternoons, but is clearly a relative classification since mean afternoon wind speed was always below  $3 \text{ ms}^{-1}$ .

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For transport, a mean value below  $-2.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  at the 2 m-level was considered stronger transport out of the near-surface layers and a mean value above  $-1.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  is marked as weaker. Bold font and italics are added on the days with higher shear production to illustrate that on these afternoons the transport is also higher or moderate. Underlining is instead added for days with weaker or moderate shear production with partly lower shear production during the afternoon, and it can be seen that these have weaker or moderate transport values.

For dissipation, a mean value equal or lower than  $-4.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  at the 2 m-level is classified as having higher dissipation and above  $-3.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  is considered to have lower dissipation. Bold font and underlining are added for days with higher shear production and these are found to have higher or moderate dissipation, whereas the two days with weakest shear production did have the weakest dissipation (marked with underlining and italics). However, also 5 July, which had variable wind during the afternoon, had weaker dissipation and 19 June had higher dissipation, despite its moderate to partly lower shear production. For 19 June, it is hence not possible to draw the conclusion that higher dissipation rate is caused by high shear production but rather it may be the higher buoyancy production that is the cause.

Finally, for buoyancy production, we have classified higher buoyancy production to imply a mean value for the afternoon of above  $2.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  and moderate to mean below this limit.

## 4.2 Normalization of the TKE budget terms

To compare these new measurements and estimated TKE budget terms in the context of earlier studies, we first investigate the behaviour of each term in the budget after normalization by friction velocity  $u_*$  and measurement height  $z$ , as suggested in MO-similarity theory. Here friction velocity was defined from longitudinal shear stress,  $u_*^2 = -\overline{u'w'}$ .

After normalization of Eq. (1) with friction velocity and measurement height and including a von Karman constant value  $k$  (set equal to 0.4 in the analysis), the governing equation for turbulence kinetic energy reads:

$$\underbrace{\frac{kz}{u_*^3} \frac{\partial E}{\partial t}}_{\text{Tendency}} = \underbrace{-\frac{kz}{u_*} \frac{\partial U}{\partial z}}_{\text{Shear production}} + \underbrace{\frac{kz g}{u_*^3 \theta} \overline{w' \theta'_v}}_{\text{Buoyancy production}} - \underbrace{\frac{kz}{u_*^3} \frac{\partial \overline{w' E'}}{\partial z}}_{\text{Turbulent transport}} - \underbrace{\frac{kz}{u_*^3} \frac{\partial \overline{w' p' / \rho_0}}{\partial z}}_{\text{Pressure transport}} - \underbrace{\frac{kz}{u_*^3} \epsilon}_{\text{Dissipation}} \quad (2)$$

5 which can be rewritten in MO-similarity notation:

$$\underbrace{\frac{kz}{u_*^3} \frac{\partial E}{\partial t}}_{\text{Tendency}} = \underbrace{\phi_m}_{\text{Shear production}} + \underbrace{\phi_b}_{\text{Buoyancy production}} + \underbrace{\phi_T}_{\text{Transport}} + \underbrace{\phi_\epsilon}_{\text{Dissipation}} \quad (3)$$

Here, we have lumped together pressure and turbulent transport terms into one total transport term  $\phi_T$ . In Fig. 8, we show the normalized TKE budget terms as a function of the stability parameter  $z/L$ . Included in the plot are fitted expressions for the budget terms (neglecting the small TKE tendency term).

For buoyancy production the expression by definition simply reads  $-z/L$ .

$$\phi_b = -z/L \quad (4)$$

For shear production, we note that a commonly used form of  $(1 - Az/L)^b$  (Stull, 1988) with  $A$  equal to 15 and  $b$  equal to 1/4, fits the data sufficiently well. However, in neutral conditions our data approaches a mean value of about 0.7 rather than 1.0. Our fitted expression thus reads:

$$\phi_m = 0.7(1 - 15z/L)^{-1/4}. \quad (5)$$

The reason for this lower than usual normalized shear production in near neutral conditions should be further explored. In Fig. 9, we have therefore replotted the

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buoyancy production term (in blue circles) and shear production term (in red circles) as a function of gradient Richardson number. Here, also data outside the afternoon transition period is included to show the behavior also in slightly stable conditions. Two larger horizontal ellipses encircle data for which the buoyancy production term is very small. An average shear production for this group is about 0.7 as observed for the near-neutral data during the afternoon transition just before stable stratification has started. As discussed in Blay-Carreras et al. (2014), at this site, there is a delay period between when the buoyancy flux becomes zero and when the vertical virtual potential temperature gradient becomes zero. Therefore, this group of data has a range of Richardson number of between about  $-0.4$  and  $-0.2$ . Here, Richardson number is the gradient Richardson number,  $Ri_g = \frac{g}{\partial U}{\frac{\partial \theta}{\partial z}}$ . This result may, however, not be a general feature of the afternoon and evening transition as discussed by Jensen et al. (2014, 2015) who obtained different results with other data sets. It is interesting to note however, that for this data set when the  $Ri$  number is close to zero and the buoyancy flux is close to zero, such as for the data encircled with the smaller vertical ellipses in Fig. 9, a mean value of shear production of about 1.0 is observed. These observations may be interpreted to imply that in more stationary neutral conditions (when both flux and gradient are small) we observe the consensus value of 1.0, but in the case of still transitional behavior from convective eddies in the afternoon transition until and around the time of zero buoyancy flux we observe lower values of normalized shear production.

For dissipation, we note a variety of different results in the literature (Wyngaard and Coté, 1971; Caughey and Wyngaard, 1979; Frenzen and Vogel, 1992; Albertson et al., 1997; Pahlow et al., 2001). Here, we choose to fit a linear expression to  $z/L$ . Our fitted expression becomes:

$$\phi_\epsilon = 0.45(1 - 1.2z/L), \quad (6)$$

which suggests a weaker normalized dissipation rate in near neutral conditions (of about 0.5). Wyngaard and Coté (1971) and Caughey and Wyngaard (1979) find a value

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of 1.0, which would imply no total transport in neutral conditions (assuming the normalized shear production in neutral conditions is 1). Our value is closer to the value 0.61 suggested by Pahlow et al. (2001); Albertson et al. (1997) and considering our observed low shear production and measurement uncertainty these numbers may be considered comparable.

For the sum of turbulent and pressure transport term (to be consistent with observed small TKE tendency) our expressions in Eqs. (4)–(6) then suggest:

$$\phi_T = 0.46z/L - 0.7(1 - 15z/L)^{-1/4} + 0.45 \quad (7)$$

For  $z/L$  below  $-1$ , this is approximately a linear equation,  $0.5z/L$ , and implies somewhat lower transport than a study focused on this imbalance term by Dupuis et al. (1997), who found a best fit linear relationship of  $0.69z/L$  using an extensive oceanic data set. In the neutral limit, our fitted value of  $-0.25$  implies a larger transport than suggested by Caughey and Wyngaard (1979) (0.0) and Dupuis et al. (1997) ( $-0.17$ ) but lower than the value suggested from Albertson et al. (1997) of  $-0.39$ . In a near-neutral range our expression is non-linear as a consequence of the non-linearity of the shear production term. A similar non-linearity is also suggested by the expression given by Caughey and Wyngaard (1979) to come both from shear production and their expression of dissipation rate. In their case, the transport term also becomes positive for a range of near neutral  $z/L$  values. Högström (1990) also observed positive transport values in neutral conditions. As previously discussed, we only observed a few occasions of positive transport values related to clouds and/or larger uncertainty in the dissipation estimates, and this effect is not included in our mean expression.

### 4.3 Alternative parametrization of dissipation including effects of boundary layer height

An alternative way to express dissipation in models is to relate it to the turbulence kinetic energy ( $E$ ) or subgrid-scale energy ( $e$ ) and a dissipation length scale  $l_e$ .

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For instance, Nadeau et al. (2011) use a relationship  $-2E^{3/2}/z_i$  for dissipation corresponding to a length scale of  $z_i/2$ , see also the more generalized case in Moeng and Wyngaard (1989) and their Eq. (2.3). Near the surface, the expectation is that dissipation becomes dependent on the distance above the ground  $z$  and we will explore these aspects based on our field measurements.

In Fig. 10, dissipation is shown as a function of  $E^{3/2}/z$  averaged for the afternoon. The height dependence of the data is displayed in Fig. 10a by assigning different colored circles (black, blue, magenta and red) to the 4 measurement heights 2.23, 3.23, 5.27 and 8.22 m. Higher dissipation rate is found closer to the ground and at any given measurement level there is a variation in dissipation related to the characteristics of each afternoon. Two best fit linear relationships are included. One of them (full line) is forced through origin because it may be natural to assume that dissipation is zero when TKE is zero. In Fig. 10b, however, a colored symbol is assigned to each afternoon and it becomes clear that the dissipation dependence on the variable  $E^{3/2}/z$  is weaker for each afternoon than implied by the full line forced through origin. It is in fact closer to the dependence implied by the dashed line  $y = -0.0060x - 0.0019$ , which is a best fit on all measurement points. The slope value  $-0.0060$  lies within the one standard deviation range of the mean  $-0.0044 \pm 0.0017$  that was found when fitting each afternoon independently to the expression  $y = kx + A$  and then taking an average of all the fitted slope values  $k$ . For the intersect values  $A$  with the  $y$  axis a mean value of  $-0.0023 \text{ m}^2 \text{ s}^{-3}$  with standard deviation  $9.3 \times 10^{-4}$  was found by this procedure. Thus, we can conclude with some certainty that non-zero intersection values with the  $y$  axis exist in this representation. We interpret this to imply that a variation in dissipation exist which should not be related to height above the surface.

In Fig. 11, we further explore this non-local variation of dissipation by plotting the intersection values  $A$  as a function of  $-E^{3/2}/z_i$ . Here, mean afternoon TKE values and mean boundary layer depth  $z_i$  determined from lidar and UHF profiler were used. For 26 June no boundary layer height data was available from the lidar. Larger symbols



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are used to denote when lidar data have been used and each afternoon is color-coded and use the same symbols as in previous figures. It can be seen that a positive correlation between the parameters exist and two best fit lines are included. The full line based on  $z_i$  determined from UHF profiler data suggest a slope value of about 2.1 and the dashed line corresponding to lidar data suggests a slope value of 2.2. Both expressions have a small negative intersection value for the  $y$  axis of  $-1.6 \times 10^{-4}$  and  $-1.1 \times 10^{-4} \text{ m}^2 \text{ s}^{-3}$  respectively which cannot be concluded to differ much from a value of 0 given the uncertainty in the variables. We note that the slope value of 2.2 corresponds to less deviation from zero of its intersection value with the  $y$  axis and therefore we use this as a slope value representative for the data set.

Our final alternative form for expressing dissipation as a function of TKE and a dissipation length scale then becomes:

$$D = -\frac{E^{3/2}}{l_e} = -E^{3/2} \left( \frac{2.2}{z_i} + \frac{0.006}{z} \right) \quad (8)$$

when combining the fitted slope values in Figs. 10 and 11. Here, the suggestion is that the distance from the ground  $z$  and boundary layer depth  $z_i$  act in parallel to decide the governing dissipation length scale  $l_e$ . It is worth noting that our coefficient value of 2.2 does not depart very much from the proposed value of 2.0 by Nadeau et al. (2011) or 1.92 by van Driel and Jonker (2011) based on other data sets, suggesting it may have some general validity. Equation (8) also implies that for heights higher than about 2.73% of the boundary layer depth the contribution from the  $z$  dependent term is less than 10% of the  $z_i$  dependent term. The expression then differs only about 10% of what Nadeau et al. (2011) used when modeling dissipation in very convective situations.

Figure 12 shows dissipation estimated from Eq. (8) (in b) and from (Eq. 9):

$$D = -\frac{u_*^3}{kz} (0.45(1 - 1.2z/L)) \quad (9)$$

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in Fig. 12a as implied by the fitted linear relationship of normalized dissipation to the stability parameter  $z/L$  in Eq. (6). We have in this final evaluation used all 53 h of data during the afternoon transition period for which all required parameters for both models were available. Boundary layer depth estimates from the UHF wind profiler were used to also be able to include data from 26 June.

Both models behave relatively similar for cases with low observed dissipation ( $> -0.0025$ ) whereas the  $z/L$  model has a tendency to overestimate dissipation for larger observed values of dissipation and a bias of  $-9.3 \times 10^{-4} \text{ m}^2 \text{ s}^{-3}$  was found. The bias for the TKE/lengthscale parametrization was  $-4.9 \times 10^{-4} \text{ m}^2 \text{ s}^{-3}$  also suggesting a slight overestimation of dissipation rate. The centered root mean square difference was  $1.8 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  for the  $z/L$  model and about half ( $0.93 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$ ) for the TKE/lengthscale model. The linear correlation coefficient between measurement and model was lower for the  $z/L$  model (0.70) compared to the TKE/lengthscale model which had 0.80. Finally, the standard deviation of the  $z/L$  model was found to be  $2.5 \times 10^{-3}$  and  $1.4 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$  for the TKE/lengthscale model, which should be compared to the observed standard deviation of  $1.5 \times 10^{-3} \text{ m}^2 \text{ s}^{-3}$ . In 4 out of 4 skill scores the TKE lengthscale model, which takes into account of boundary layer depth and height above the surface, was hence found to better represent the observed dissipation than the stability dependent  $z/L$  model. It should be noted that both models include 2 fitting parameters and no explicit stability dependence have been included for the TKE lengthscale model. However, it may be argued to include an implicit stability dependence since the magnitude of TKE depends on stability. It should also be recognized that only afternoon data is considered here and other parts of the diurnal cycle such as morning transitions could be studied in future work.

## 5 Summary and conclusions

Using radiosoundings, UHF wind profiler and tower measurements, we summarized an overall description of the prevailing boundary layer situation for 10 Intensive

Observation Period days. This characterization showed that many different conditions in terms of boundary layer depth, wind speed and moisture conditions occurred on these days, despite being mainly high-pressure fair weather situations. Some common features are recognized, such as:

- Mainly westerly flow above the boundary layer and an easterly or northerly flow in the daytime boundary layer (linked with mountain-plain circulation for most of the days), turning in the evening and nighttime. As the boundary layer flow encounters and mixes with the flow above, a layer of reduced wind speed is also observed for several days.
- Wind direction at a small tower (2–8 m), a taller tower (30–60 m) and the lowest UHF wind profiler level (at 175 m) was found to be relatively consistent in daytime and afternoon, but with larger variability in the UHF estimates.
- In the evening, after the buoyancy flux switched sign and stable stratification has begun, the wind direction at the small tower turned rapidly towards south for several of the days related to a shallow drainage-flow. At the 60-m-tower and above a more slow and/or delayed turning was observed which is related to a mountain-plain circulation.

These observations are important to emphasize for a couple of reasons:

- In stable stratification, near-surface TKE budget analysis was concluded to provide very little information about atmospheric conditions above the very near-surface layers. This is because of decoupling issues, and effects of shallow drainage flow, as well as the mountain-plane circulation related to larger-scale topography and some occasions of nocturnal low-level jets.
- During unstable stratification, in the afternoon transition our surface layer analysis can, however, also be informative of what is occurring above in the mixed-layer since the two layers are more closely coupled to each other. The height variation

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of TKE budget terms could in these conditions be used to interpret also how the mixed layer has an influence on surface layer dynamics.

The afternoon transition was studied using TKE budget analysis. Here, we focused on the slow and persistent changes in TKE budget terms that are well described by an hourly TKE budget analysis, leaving shorter time scales and more temporary fluctuations of TKE for future studies. Several important results were reached:

- All terms of a turbulence kinetic energy budget except those of transport could be determined directly from field measurements near the surface on an hourly basis for 10 fair-weather afternoons. This allowed calculation of the total transport as a residual from the other budget terms.
- The TKE tendency term was found to be much smaller than all the other budget terms suggesting that the surface-layer turbulence evolves in a quasi-stationary way during the afternoon transition. Even though TKE tendency was small, we found a relatively high correlation coefficient ( $-0.69$ ) between mean afternoon TKE tendency and mean afternoon buoyancy production.
- We found that several explanatory factors are needed to be able to interpret the behavior of TKE and TKE tendency during the afternoon transition. Both near-surface wind speed (causing shear production) and buoyancy production of TKE were found to be important production terms at 2–8 m, even though mean afternoon winds were less than  $3 \text{ m s}^{-1}$  for all days. The shear production term has stronger height dependence than does buoyancy production. Buoyancy therefore becomes more important for the TKE budget with increasing height.
- Larger variations between afternoons were observed in shear production, transport as well as dissipation compared to buoyancy production. This implies that all these terms are important to take into account of in modeling of sheared convective surface layers.

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- A summarizing classification of the 10 IOP afternoons showed that in general windier days of the field campaign (20, 25, 26 and 27 June) had a higher transport of TKE out of the near-surface layers as well as often a higher or moderate dissipation of TKE. Afternoons with weaker wind (30 June and 2 July) instead had less transport and weaker dissipation. But for a more complete picture also buoyancy production, as a key forcing, needs to be considered (e.g. 19 June) as well as consideration of variations within the afternoons.
- Normalization of TKE budget terms by friction velocity and measurement height and fitting of empirical expressions (Eqs. 4–7) revealed both similarities and differences to earlier studies. Around the time of zero buoyancy flux the average of normalized shear production values was about 0.7 (30% lower than in most findings). In slightly stable stratification with both small buoyancy flux and small virtual potential temperature gradient the mean value of normalized shear production showed the consensus result of 1.0.
- As a rule of thumb our data can be argued to suggest that about 50% of the near surface production of TKE is locally dissipated, leaving about 50% available for transport. However, empirically fitted expressions (Eqs. 4–7) represent better some of the observed subtleties and non-linear effects of stratification.
- For dissipation we also alternatively proposed a non-local parametrization using a TKE-lengthscale model which takes into account of boundary layer depth and distance above ground. The non-local formulation was found to give a better description of dissipation of turbulence kinetic energy and is hence suggested to provide an important component for simple modeling of surface layer TKE, while still taking into account of non-local influences. Such modeling is attempted in our companion paper Part 2.

## Appendix A: Description of boundary layer conditions for 10 IOP days

### A1 19–20 June 2011

The weather conditions were dominated by a cloud-free high-pressure situation with very few disturbances in incoming short-wave radiation (Nilsson, 2014). A general warming trend from around 12 °C in the morning of 19 June and reaching about 19 °C in the afternoon (on the 60 m-tower level) was observed. 20 June was warmer around 20 °C in the morning and reaching about 25 °C in the afternoon. Relative humidity remained relatively unchanged between the two days being about 60 % in the morning and decreasing to about 45–50 % in the afternoon before increasing again in the evening.

The boundary layer depth from Fig. 2 shows similar maximum depths of about 1100 m for the two days, but 19 June has been classified as having a rapid growth and leveling inversion in late afternoon whereas 20 June had a more typical growth and leveling inversion (Lothon et al., 2014).

Both days were characterized by moderate westerly winds (higher than about 8 ms<sup>-1</sup>) above the boundary layer most of the time (see Figs. A1 and A2). After the time of the evening transition on 20 June at around 19:00 UTC the greatest upper wind gradient marked in black was more diffuse and found to occur mainly around 2000 m. This height marks a dynamical separation of the boundary layer flow with more northerly (19 June) or easterly (20 June) wind from the dominant westerly flow above. Wind speed is (as seen from Figs. A1 and 4) variable in both time and space. At 175 m (the lowest UHF profiler level) it was around 5 ms<sup>-1</sup> for a large part of the day, afternoon and in the evening on 20 June. As can be seen from Fig. A1, this level is quite representative of the boundary layer flow up to some height where the wind turns, and reduced wind speed is observed. On 19 June, winds were generally lighter in the boundary layer, around 2–3 ms<sup>-1</sup> in mid-day and decreasing in the evening.

Wind speed near the surface show less differences between the 60 m-tower (shown in greenish colors) and the small tower (shown in bluish colors) comparing the two

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days than the 175 m level, which is more representative of the boundary layer flow. Wind direction is reasonably consistent on both towers and the lowest UHF level during daytime on both days. But once the buoyancy flux becomes negative (marked by a vertical black line in Fig. 3) the wind direction on the small tower shifts rapidly towards south due to a shallow drainage flow. A later and less abrupt turning is observed on the 60 m tower and the lowest UHF profiler level.

### A2 24–27 June 2011

24 June may be considered as the start of a general warming period which lasted until the evening of 27 June. Temperatures increased from about 11 °C in the morning of 24 June to about 18 °C in the afternoon and then only decreased about 3 °C until morning of 25 June. The next days had a similar behavior with maximum temperature of about 24 °C for 2 June decreasing 2 °C until morning of the next day (Nilsson, 2014). 26 June later reached a maximum temperature for the time period of about 32 °C. From the afternoon of 26 June the temperature dropped 6 °C until morning of 27 June which temporarily also reached 32 °C before mid-day, before stabilizing at around 30 °C for a large part of the afternoon.

These days can also be characterized as high pressure fair-weather situation before the passage of an approaching frontal system reaching the site around 02:00 UTC on 28 June. The cloud cover varied among the days, 24 June had some clouds (mostly cirrus) for most of the day, but decreasing amounts in the afternoon from 14:30 UTC. 25 June was completely cloud free, whereas clouds were observed on 26 June starting around 14:00 UTC. 27 June was cloud-free until late afternoon around 16:30 UTC when some pre-frontal clouds (mainly cirrus) occurred. Relative humidity for the afternoon was about 50–60 % on 24 June (hence comparable to 19 and 20 June) but less for the warmer days: 30–40 % on 25 June; 25–35 % on 26 June and 30–50 % for 27 June. As noted in Lothon et al. (2014) the less typical windier and warmer conditions were related to the presence of a low-pressure area in the lower troposphere over the Gulf of Lion in the Mediterranean Sea.

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The maximum boundary layer depth on 24 June was similar to 19 and 20 June (1100 m) with a more typical growth and leveling behavior. 25 June was also given this classification in Lothon et al. (2014). As can be seen from Fig. 2, the boundary layer depths are, however, lower for the three warmer days of the field campaign and 26 and 27 June were also classified as having slower boundary layer growth and rapidly decreasing top inversion in late afternoon. This being in strong contrast to most of the other days. This has been partly explained as a consequence of less sensible heat flux during the warm period (Lothon et al., 2014) and possible effects of subsidence (Pietersen et al., 2014).

24 June also experienced a strong westerly flow above the boundary layer, as 19 and 20 June, which however got weaker as time progressed and in the afternoon and evening mainly moderate upper wind gradients (between 0.5 and 1.0  $\text{m s}^{-1}$  change in 100 m) was observed. The flow in the boundary layer was also weak for 24 June and wind directions was variable among westerly, north-westerly and northerly in daytime turning towards easterly and southerly flow in the evening and nighttime. The weaker upper winds above the boundary layer persisted also for 25, 26 and 27 June. For 25 and 26 June there was, however, upper wind speed gradients above 1  $\text{m s}^{-1}$  change in 100 m, but not always as persistent in time as for 19, 20 June and a large part of 24 June.

For both 25 and 26 June the boundary layer flow was stronger with persistent easterly winds turning to southerly in nighttime. An average wind speed at 175 m of about 6–7  $\text{m s}^{-1}$  for 25 June and 5  $\text{m s}^{-1}$  for 26 June makes these two days the overall windiest IOP days studied. For 27 June the wind speed and direction was, as can be seen from Figs. 3 and 4, more variable. Increasing wind speed from very low in the morning to about 5–6  $\text{m s}^{-1}$  as an average for the afternoon and evening at 175 m was observed. The wind direction at the same time turning clock-wise from north-westerly in the morning to southerly in the evening and westerly in nighttime at the 175 m level.



30 June occurred in the aftermath of a cold frontal passage on the previous day and had some stratocumulus clouds in the morning followed by cumulus for most of the day and clearing skies in the evening. Pressure started to rise significantly mid-day and during 1 July and remained relatively high also on 2 July (Nilsson, 2014). Both 1 and 2 July were mainly cloud-free except for a short period in the morning of 1 July, and some low stratocumulus started to appear at the end of 2 July. The three days make up another warming period with a similar diurnal cycle with temperatures increasing about 9, 8 and 7 °C in the morning to maximum afternoon values of 19, 21 and 24 °C on 30 June, 1 and 2 July respectively. Relative humidity being 50–60 % on 30 June and about 30–40 % for both 1 and 2 July.

On both 30 June and 1 July boundary layer depth was observed to be high reaching around 1500 m according to both UHF and radiosounding estimates. On 2 July it was reduced to about 1000 m, comparable to some of the other more typical days of the field campaign. 2 July as well as 30 June were also classified as having a more typical growth and inversion leveling (Lothon et al., 2014), whereas 1 July had a more rapid growth of the boundary layer during the morning explained by a merging of the boundary layer with the residual layer from the previous night (Blay-Carreras et al., 2013).

30 June had mainly weak winds in the boundary layer (below 4 ms<sup>-1</sup> at 175 m most of the time). Above the high boundary layer depth of 1500 m there was an upper wind speed gradient with more than 1 ms<sup>-1</sup> change in 100 m, but winds were mainly below 7 ms<sup>-1</sup> also above this layer of wind speed increase (and below 2500 m). Wind direction in the upper region was mainly from west as for most days and quite variable in the boundary layer as can be expected in low wind conditions. The wind direction stabilized somewhat to mainly north-westerly flow below 500 m in the evening, after the buoyancy flux turned negative and the wind speed also had increased.

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1 July and especially 2 July had higher wind speed (and still westerly flow) above the boundary layer and mainly easterly (2 July) and north-easterly (1 July) flow in the boundary layer. On both days a turning towards south took place in the evening after stable stratification started. This shift of wind direction was slow and delayed and evolving to a full southerly flow at 175 m later in comparison to the earlier and more rapid wind direction shifts observed near the surface on the two towers. The turning hence started first near the surface and later at higher levels with the onset of a mountain-plain circulation.

**A4 5 July 2011**

Finally the last IOP day studied was a completely cloud-free warm day reaching up to 26 °C around 15:00 UTC with a typical diurnal cycle in temperature, but perhaps somewhat more variable relative humidity ranging from 65 to 70 % in the morning down to 30 % in mid-day before rising again in late afternoon and evening. Relative humidity is of course affected by the diurnal cycle of temperature and in fact for 5 July the specific humidity near the surface according to the standard radiosoundings at 11:00, 17:00 and 23:00 UTC (Blay-Carreras, 2013) remained relatively constant at 7 g kg<sup>-1</sup>. Table A1 summarizes specific humidity from these radiosoundings showing a significant moistening of the near-surface layer at 23:00 UTC compared to mid-day values for most of the IOPs. Such moistening of near-surface layers have previously been reported by Busse and Knupp (2012), Bonin et al. (2013) and Mahrt (1999) discussed it as a consequence of a slower decay of latent heat flux than the strength of turbulence and boundary layer depth during evening events. The vertical profile of specific humidity in stable conditions was noted most of the time to have a significant curvature with decreasing moisture at higher levels (Blay-Carreras, 2013).

Boundary layer depth on 5 July was somewhat lower compared to 2 July following a general decreasing trend from the high values observed on 30 June. Potential temperature gradients were often weak especially in the afternoon making boundary layer depth determination based on strongest gradient below 2500 m more difficult to

use than for some of the other days. UHF estimates nevertheless gave estimates of about 1000 m as maximum for the afternoon, but with a more diffuse top inversion in late afternoon (and a slower growth before mid-day).

For 5 July the wind speed was again weak in the boundary layer but increasing during the late afternoon and evening and at the same time winds were turning anti-clockwise from east or north-easterly flow towards mainly west-north-westerly. At the same time, the flow just above the boundary layer also turned anti-clockwise from west or north-westerly towards southerly flow. The upper winds were mainly weak to moderate (5–11  $\text{ms}^{-1}$ ) and quite variable in time and height.

## Appendix B: Afternoon statistics of mean wind speed and TKE budget terms

Mean afternoon statistics for the dominant terms of the turbulence kinetic energy budget and mean wind speed for the afternoons are provided in Tables B1 and B2. In Table B3 also the mean afternoon TKE, early afternoon TKE and late afternoon TKE values are reported, as well as the TKE tendency for each afternoon at 2.23 and 8.22 m.

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which all have contributed in a significant amount. BLLAST field experiment was hosted by the instrumented site of Centre de Recherches Atmosphériques, Lannemezan, France (Observatoire Midi-Pyrénées, Laboratoire d'Aérodologie). Its 60m tower is partly supported by the POCTEFA/FLUXPYR European program. The authors thank also Yannick Bezombes, Solène Derrien and Frédérique Saïd for their involvement in the measurements used here. Fleur Couvreur and Patrick Augustin are acknowledged for their contribution to the estimates of the PBL depth. BLLAST data are managed by SEDOO, from Observatoire Midi-Pyrénées. See <http://bllast.sedoo.fr> for all contributions. Since 2013, the French ANR supports BLLAST analysis.

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**Table 1.** TKE budget classification of the 10 IOP afternoons. Here, winds speed, shear production, transport and dissipation have been classified into 3 categories (“h” = higher, “m” = moderate, “w” = weaker) and the buoyancy production into two categories (“h” = higher and “m” = moderate) based on the mean values for the afternoon (see text for exact limits). Furthermore in parentheses “p” denotes if only part of the afternoon is considered to belong to the category. For the moderate category an extra letter “l” or “h” indicate if the variable is mainly departing towards the lower or higher category. For dissipation two days are denoted with (“inc”) to indicate that dissipation increased during the afternoon. To interpret some of the main effects of higher or weaker wind speed on the TKE budget, combinations of underling, italics and bold font have been added to the table (see text for further explanation).

Category	Wind speed			Shear production			Buoyancy production		Transport			Dissipation		
	h	m	w	h	m	w	h	m	h	m	w	h	m	w
19 June		X			<i>X(pl)</i>		X				<u>X</u>	X		
20 June	<b>X(p)</b>			<b>X(p)</b>			X(p)		<b>X(p)</b>				<b>X</b>	
24 June		<i>X(pl)</i>			<i>X(pl)</i>		X			<u>X(pl)</u>			<u>X(pl)</u>	
25 June	<b>X</b>			<b>X</b>			X(p)		<b>X</b>			<b>X</b>		
26 June	<b>X(p)</b>			<b>X</b>			X		<b>X(p)</b>			<b>X(p)</b>		
27 June	<b>X(p)</b>			<b>X(p)</b>			X		<b>X</b>				<b>X(inc)</b>	
30 June			<u>X</u>			<u>X</u>	X(p)	X(p)			<u>X</u>			<u>X</u>
1 July		<i>X(pl)</i>			<i>X(pl)</i>		X(p)				<u>X</u>		X(ph)	
2 July		<u>X</u>			<u>X</u>		X(p)				<u>X(p)</u>			<u>X</u>
5 July		<i>X(ph)</i>			<i>X(ph)</i>		X		X(pl)					X(inc)

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**Table A1.** Near-surface specific humidity from standard radiosoundings [ $\text{g kg}^{-1}$ ].

Day	11:00 UTC	17:00 UTC	23:00 UTC
19 June	5.5	6.5	8 <sup>a</sup>
20 June	8	8	12 <sup>a</sup>
24 June	6	6	7 <sup>a</sup>
25 June	6	6	9 <sup>a</sup>
26 June	7	10 <sup>a</sup>	10 <sup>a</sup>
27 June	9	11	14
30 June	6	6	8
1 July	5	6	8 <sup>a</sup>
2 July	5.5	5.5	7 <sup>a</sup> ( <sup>b</sup> )
5 July	7	7	7

<sup>a</sup> denotes marked curvature in vertical profile of humidity.<sup>b</sup> denotes that a sounding at 20:30 UTC was used when no standard radiosounding was available.

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**Table B1.** Afternoon statistics of wind speed, shear production, buoyancy production, transport and dissipation for a measurement height of 2.23 m. Here, the mean value (and standard deviation) for each afternoon period was calculated from the hourly TKE budget results presented in Fig. 5. Note the scale factor  $10^{-3}$  for the TKE budget terms.

	Wind speed at 2.23 m	Shear production	Buoyancy production	Transport	Dissipation
Unit and scale factor	$\text{ms}^{-1}$	$10^{-3} \text{ m}^2 \text{ s}^{-3}$	$10^{-3} \text{ m}^2 \text{ s}^{-3}$	$10^{-3} \text{ m}^2 \text{ s}^{-3}$	$10^{-3} \text{ m}^2 \text{ s}^{-3}$
19 June	1.73 (0.48)	2.3 (0.7)	3.2 (1.5)	-0.2 (0.7)	-5.4 (1.7)
20 June	1.96 (0.35)	3.8 (1.6)	2.9 (1.6)	-2.8 (1.9)	-4.0 (1.3)
24 June	1.60 (0.54)	2.1 (1.1)	3.4 (1.7)	-2.1 (1.1)	-3.5 (0.8)
25 June	2.31 (0.24)	7.8 (1.2)	2.4 (1.5)	-4.3 (1.7)	-6.1 (0.9)
26 June	2.12 (0.26)	6.9 (2.4)	2.1 (0.1)	-4.6 (1.6)	-4.5 (0.9)
27 June	2.00 (0.50)	4.3 (3.2)	1.9 (1.1)	-2.5 (1.3)	-3.7 (0.9)
30 June	1.39 (0.42)	1.5 (1.1)	2.2 (1.2)	-0.4 (0.7)	-3.3 (0.3)
1 July	1.75 (0.57)	2.6 (1.5)	2.8 (1.6)	-1.1 (0.8)	-4.3 (2.4)
2 July	1.47 (0.53)	1.1 (0.6)	2.3 (1.4)	-1.2 (0.9)	-2.1 (0.7)
5 July	1.60 (0.69)	3.0 (4.0)	1.9 (1.2)	-1.5 (1.8)	-3.4 (1.3)

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**Table B2.** Afternoon statistics of wind speed, shear production, buoyancy production, transport and dissipation for a measurement height of 8.22 m. Here, the mean value (and standard deviation) for each afternoon period was calculated from the hourly TKE budget results presented in Fig. 5. Note the scale factor  $10^{-3}$  for the TKE budget terms.

	Wind speed at 8.22 m	Shear production	Buoyancy production	Transport	Dissipation
Unit and scale factor	$\text{ms}^{-1}$	$10^{-3} \text{m}^2 \text{s}^{-3}$	$10^{-3} \text{m}^2 \text{s}^{-3}$	$10^{-3} \text{m}^2 \text{s}^{-3}$	$10^{-3} \text{m}^2 \text{s}^{-3}$
19 June	1.97 (0.55)	0.5 (0.6)	3.2 (1.4)	-0.5 (0.9)	-3.3 (1.2)
20 June	2.24 (0.38)	2.5 (1.1)	3.1 (1.8)	-2.3 (2.0)	-3.4 (1.1)
24 June	1.84 (0.64)	0.5 (0.6)	3.4 (1.6)	-1.6 (0.9)	-2.3 (0.6)
25 June	2.75 (0.28)	3.7 (0.6)	2.5 (1.5)	-1.3 (1.4)	-4.9 (0.7)
26 June	2.52 (0.30)	3.4 (1.4)	2.3 (0.4)	-2.5 (1.2)	-3.3 (0.7)
27 June	2.29 (0.65)	2.2 (1.9)	2.1 (1.1)	-1.4 (0.6)	-2.9 (1.0)
30 June	1.61 (0.50)	0.5 (0.4)	2.2 (1.2)	-0.6 (0.9)	-2.0 (0.2)
1 July	2.00 (0.68)	0.8 (0.5)	2.9 (1.3)	-1.1 (0.4)	-2.5 (1.4)
2 July	1.65 (0.61)	0.2 (0.6)	2.4 (1.2)	-1.2 (0.9)	-1.5 (0.6)
5 July	1.83 (0.92)	0.9 (1.1)	2.0 (1.0)	-0.7 (0.3)	-2.1 (0.7)

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**Table B3.** Afternoon TKE statistics for the 10 IOPs for measurement heights of 2.23 and 8.22 m. TKE mean value: for the afternoon, for early afternoon (between 12:00 and 13:00 UTC) and last 30 min of the afternoon transition is shown. Also shown is the average TKE tendency for each afternoon (note the scale factor  $10^{-5}$  for the column on the right).

Unit and scale factor	TKE mean value for the afternoon		TKE mean value for the early afternoon 12:00–13:00 UTC		TKE last 30 min of the afternoon transition		Average time rate of change of TKE	
	$\text{m}^2 \text{s}^{-2}$		$\text{m}^2 \text{s}^{-2}$		$\text{m}^2 \text{s}^{-2}$		$10^{-5} \text{m}^2 \text{s}^{-3}$	
Height	2.23 m	8.22 m	2.23 m	8.22 m	2.23 m	8.22 m	2.23 m	8.22 m
19 June	0.94	1.01	1.19	1.30	0.37	0.39	-4.1	-4.6
20 June	1.00	1.11	1.10	1.19	0.57	0.70	-2.6	-2.5
24 June	0.94	1.01	1.14	1.24	0.50	0.57	-3.2	-3.4
25 June	1.08	1.20	1.15	1.26	0.97	1.09	-1.1	-1.1
26 June	0.96	1.05	1.02	1.12	0.89	0.96	-2.5	-3.0
27 June	0.94	1.05	0.99	1.09	0.96	1.12	-0.2	+0.2
30 June	0.78	0.84	0.81	0.89	0.60	0.64	-1.1	-1.2
1 July	0.99	1.10	1.24	1.35	0.69	0.74	-3.4	-3.7
2 July	0.83	0.90	0.92	0.96	0.53	0.59	-2.4	-2.3
5 July	0.83	0.90	1.01	1.08	0.62	0.66	-2.4	-2.6

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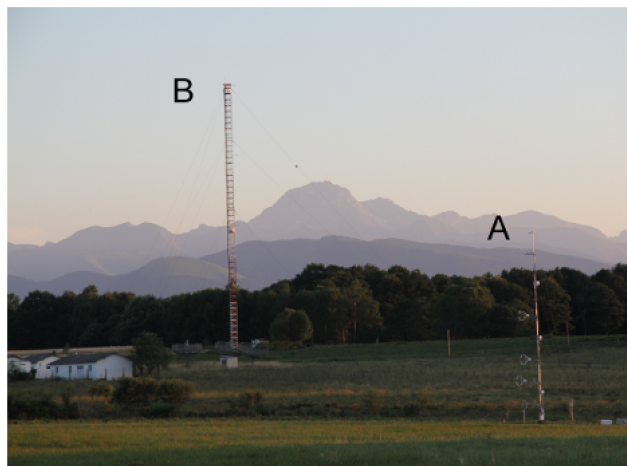
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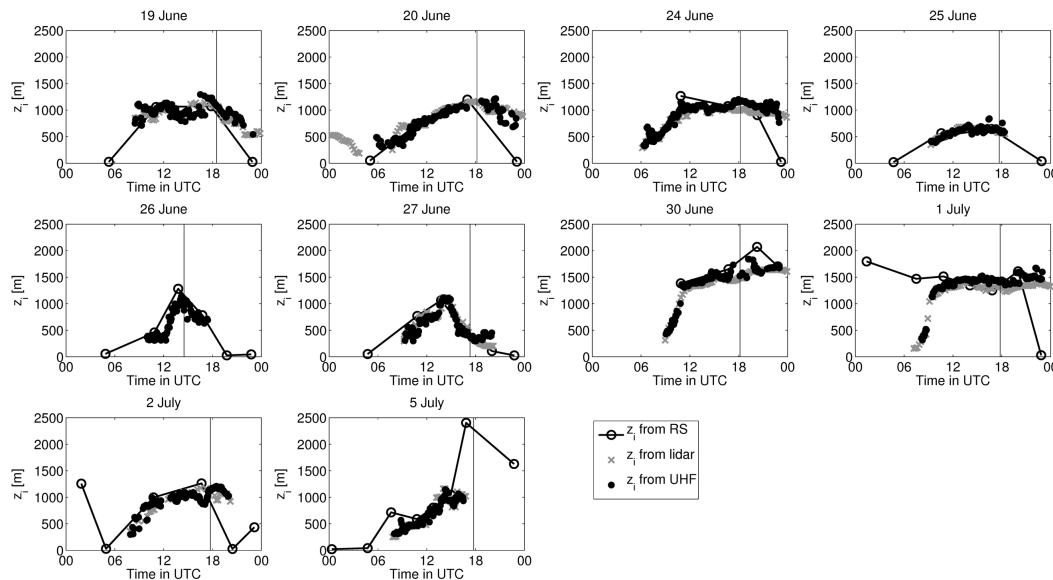


**Figure 1.** The figure is showing the two main measurement towers and the Pyrenees mountain range in the background. The small Divergence Site tower is marked with A and taller 60-m-tower is marked with B.

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**Figure 2.** Boundary layer depth ( $z_b$ ) estimates from (black dots) UHF wind profiler (based on reflectivity), (grey crosses) aerosol lidar (based on backscatter) and from (open circles) radiosoundings (based on the strongest potential temperature gradient). A vertical line has been included to mark the timing of zero buoyancy flux at surface.

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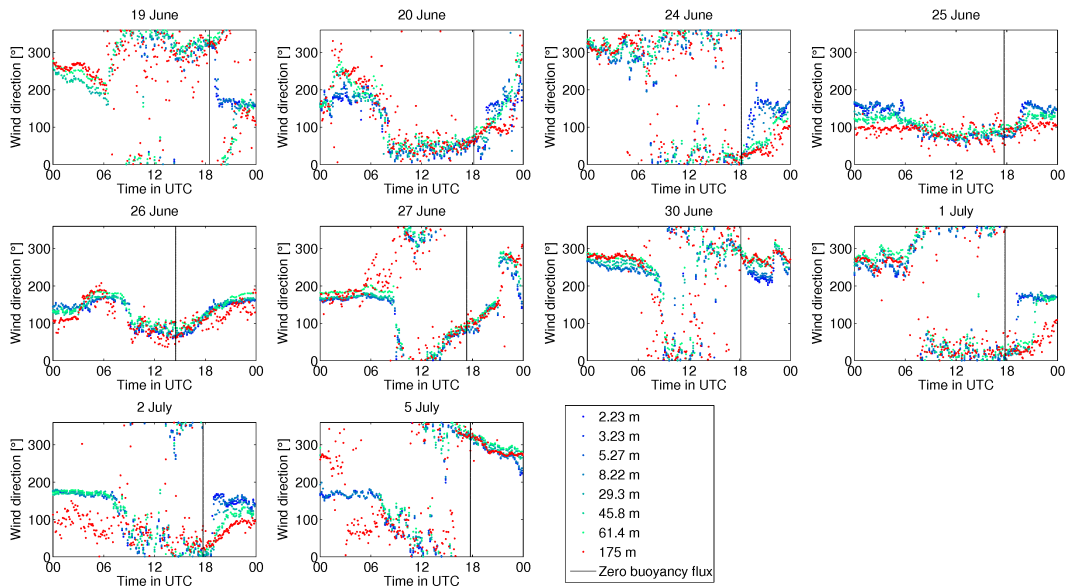
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**Figure 3.** Time series of wind direction for each IOP day, color-coded on the measurement height such that the small-tower measurements (2–8 m) is shown in bluish colors, high tower (30–60 m) in greenish colors and the lowest UHF profiler level (175 m) is shown in red. A vertical line is inserted to show the timing of zero-buoyancy flux for each day.

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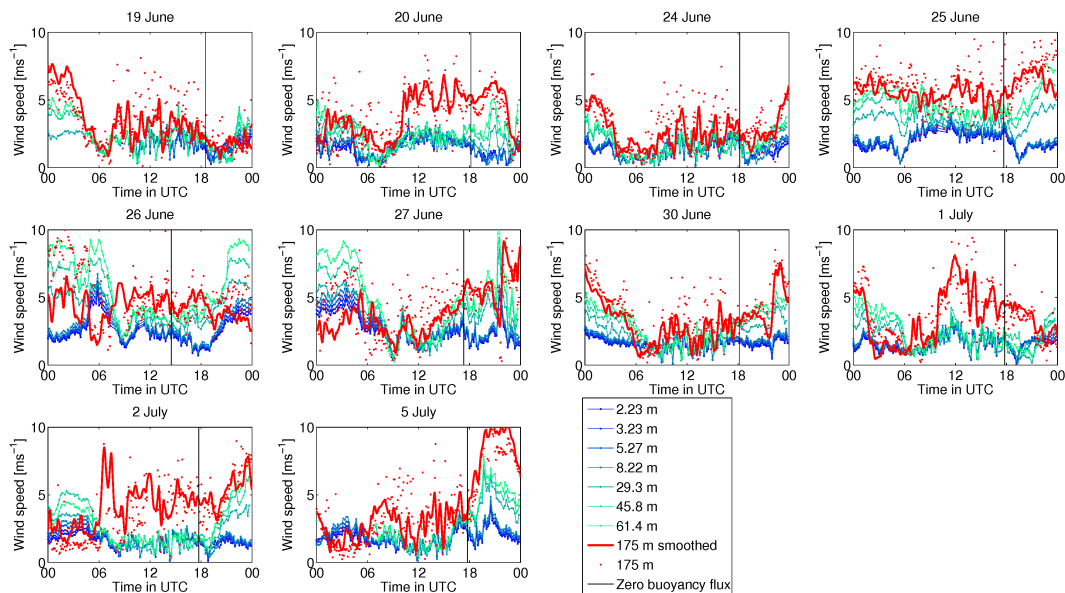
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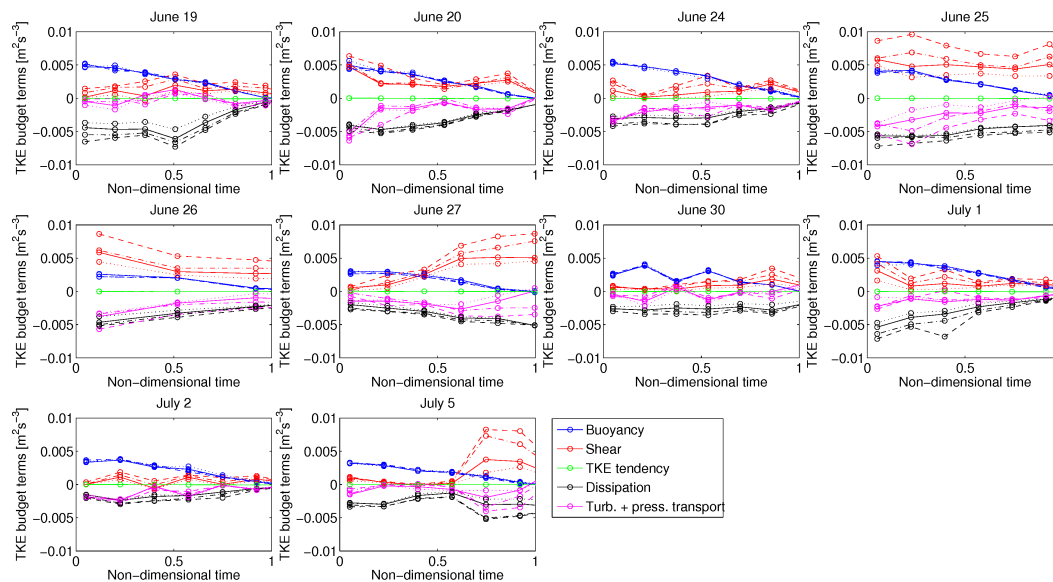


**Figure 4.** Time series of wind speed with the same color-coding as used in Fig. 3. Here also a 10 min height-time smoothed red line is shown for the UHF profiler data at 175 m.

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**Figure 5.** Turbulence kinetic energy budget terms is shown on the y axis as a function of normalized time for the afternoon period between 12:00 UTC (denoted 0) and time of zero-buoyancy flux (denoted 1). Here, dashed lines show the 2.23 m results, dash-dotted 3.23 m, full lines 5.23 m and dotted lines 8.23 m. The colors denote the different budget terms: buoyancy production (blue), shear production (red), dissipation (black), TKE tendency (green) and transport (magenta).

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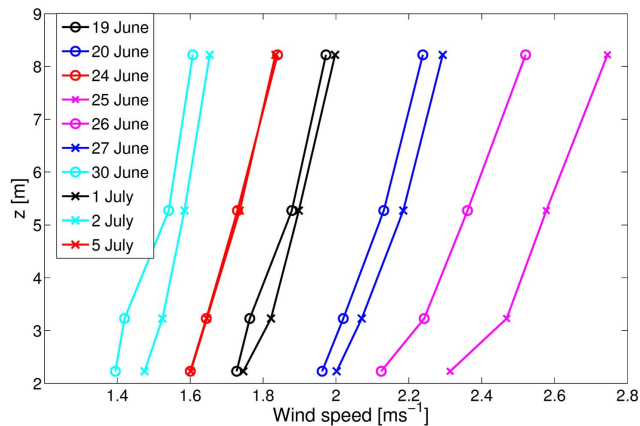
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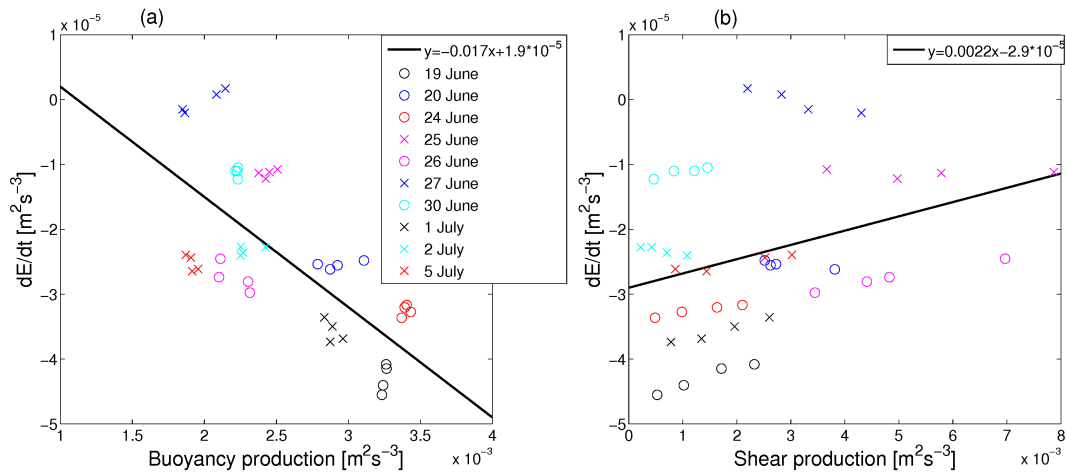


**Figure 6.** Vertical profile of mean near-surface wind speed for all 10 IOP afternoons with measurements at the small Divergence Site tower.

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**Figure 7.** Average TKE tendency for each afternoon is shown as a function of Buoyancy production in panel (a) and Shear production in panel (b).

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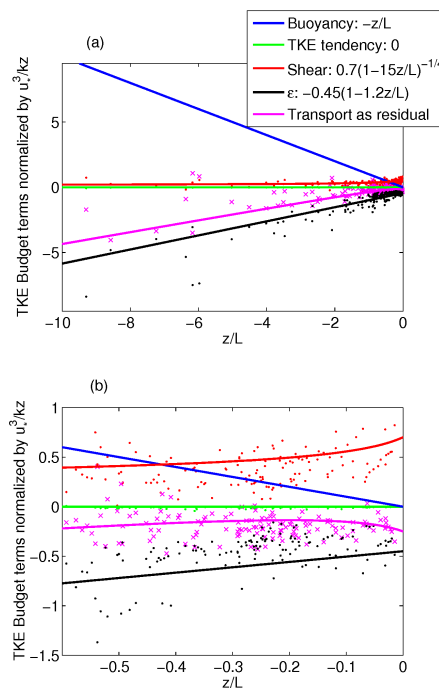
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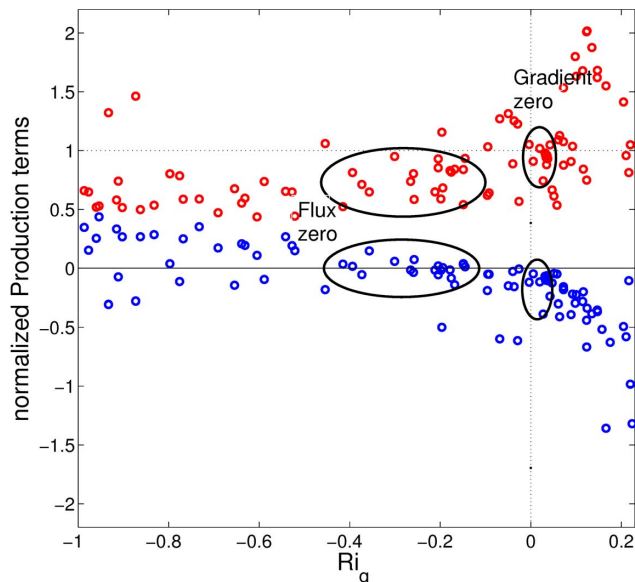
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**Figure 8.** Normalized hourly TKE budget terms for the 10 afternoons shown as a function of the stability parameter  $z/L$  in panel (a) a range of  $-10$  to  $0$  is used on the x axis and in panel (b) the near-surface data within range  $-0.6$  and  $0$  is shown. Data are shown with colored dots and suggested fitted expressions is shown with colored lines, Buoyancy production (blue), TKE tendency (green), Shear production (red), Dissipation (black) and Transport (magenta). There were two more outlier data value (not shown) placed at  $z/L = -48.2$  ( $-37.7$ ) with normalized Shear production =  $0.24$ , ( $0.21$ ), Transport =  $-26.3$  ( $-20.8$ ), Dissipation =  $-22.1$  ( $-17.0$ ) and Tendency =  $0.10$  ( $0.05$ ) also indicating that in the free convection limit the buoyancy production is balanced by dissipation and transport.

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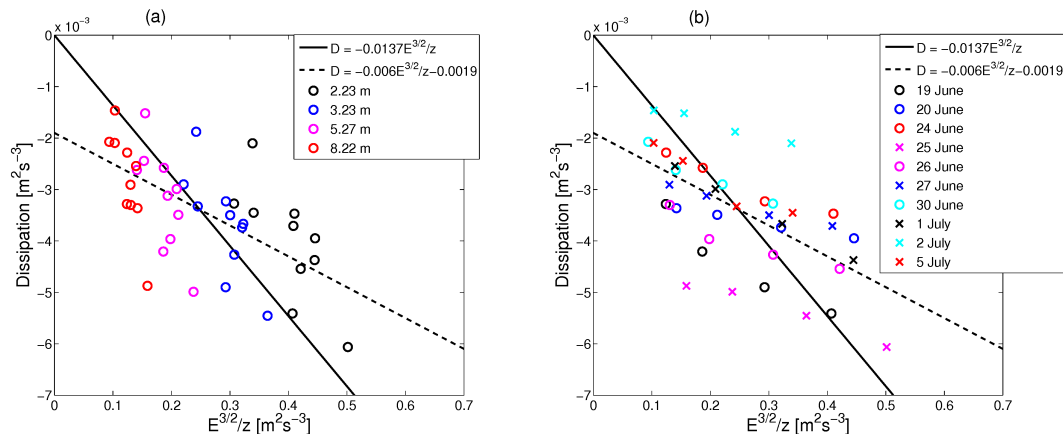


**Figure 9.** Normalized production terms (Buoyancy production =  $-z/L$  in blue and Shear production in red) for near neutral (including also other data outside the afternoon period) is shown as function of Richardson number. Two larger horizontal ellipses encircle some data for which the buoyancy flux is very small, but Richardson number remains in the range between about  $-0.2$  and  $-0.4$ , and normalized shear production averages to about  $0.7$ . Two smaller vertical ellipses encircle some data for which both the buoyancy flux is small and Richardson number is small, and normalized shear production averages to about  $1.0$ .

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**Figure 10.** Dissipation is shown as a function of TKE and height near the surface. In panel (a) the 4 measurement heights 2.23, 3.23, 5.27 and 8.22 m have been assigned different colors (black, blue, magenta, red) to emphasize the height dependence of the data. In panel (b) instead each afternoon have been assigned with a different color to distinguish between different days. Two best fit linear expressions have also been included. The full line expression assumes that the line goes through origo and the dashed line is without this assumption.

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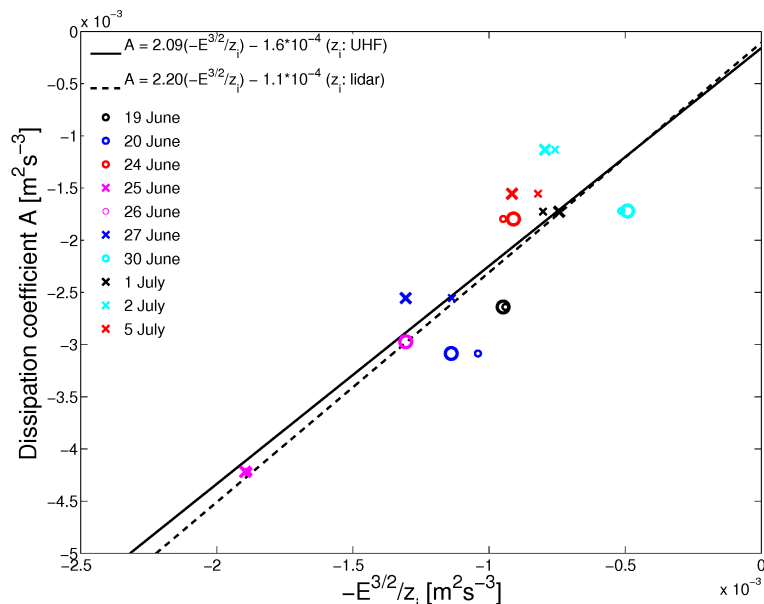
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**Figure 11.** Dissipation coefficient  $A$  as a function of mean afternoon TKE and mean afternoon boundary layer height determined from lidar and UHF profiler. Two best fit linear expressions (full and dashed line) have been included for using the UHF profiler and lidar  $z_i$  estimates. Large and small symbols correspond to using lidar and UHF profiler data respectively.

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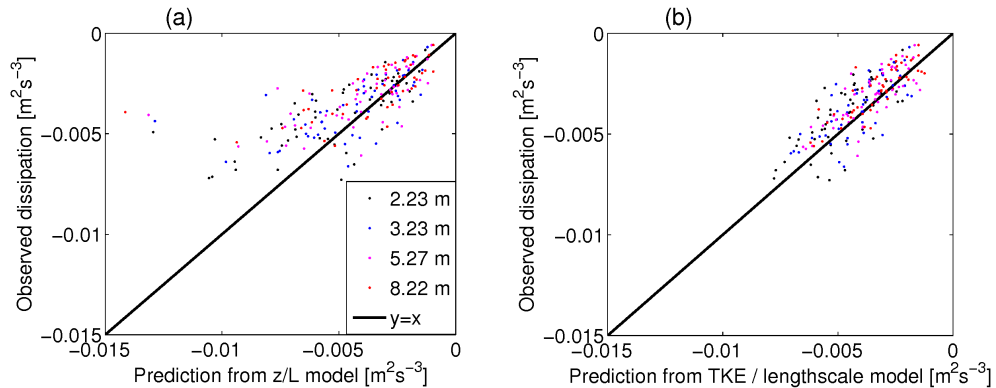
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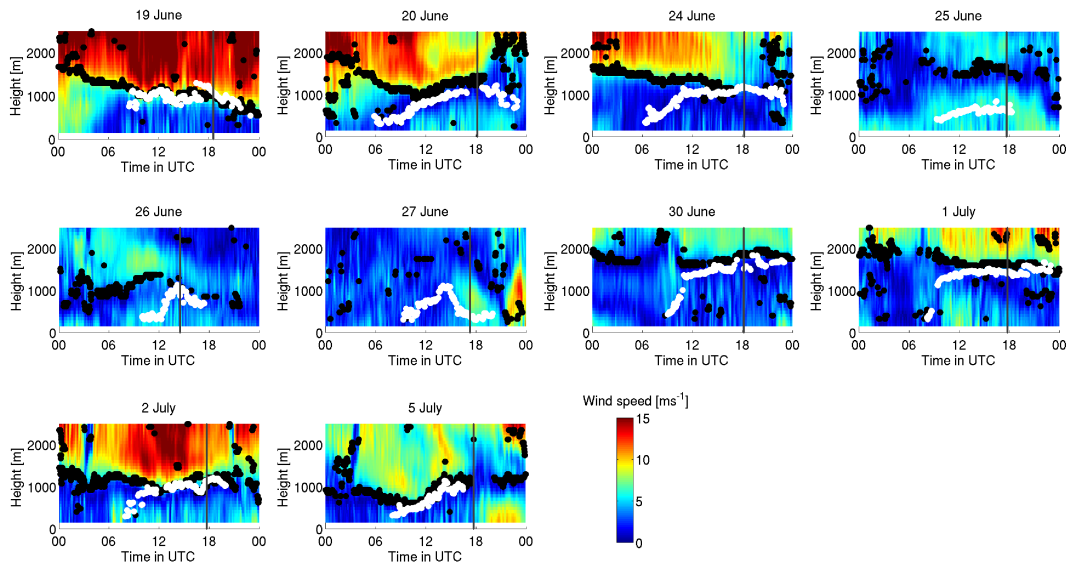


**Figure 12.** Comparison between observed and predicted dissipation is shown for a model based on  $z/L$  in panel (a) and based on TKE and a dissipation lengthscale taking into account of measurement height and boundary layer depth in panel (b). Data shown as black, blue, magenta and red dots denote 2.23, 3.23, 5.27 and 8.22 m measurement height respectively.

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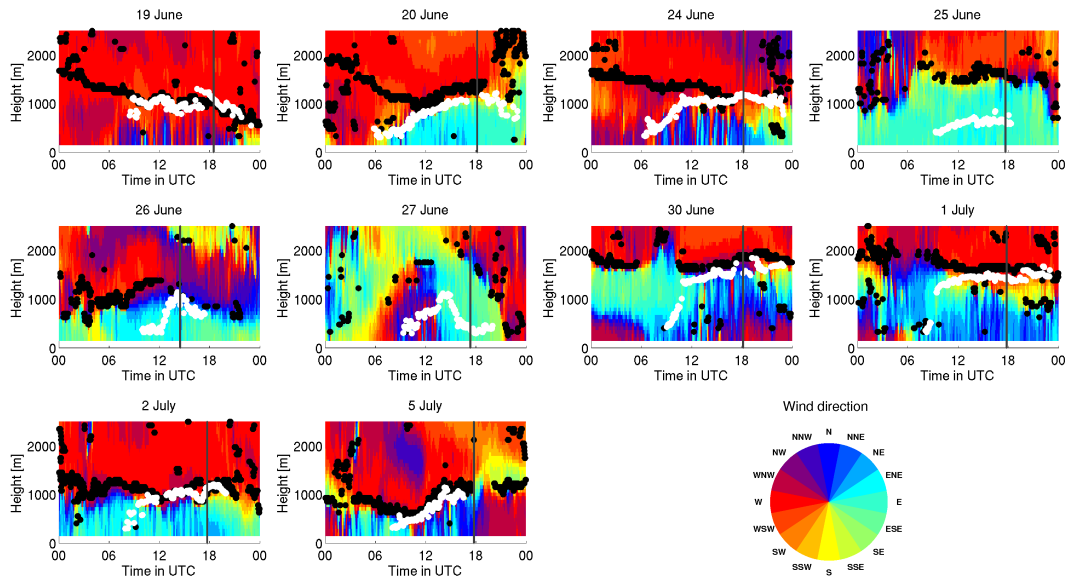


**Figure A1.** Wind speed from UHF profiler between 175 and 2500 m. Strong local maxima in wind gradient ( $> 1 \text{ ms}^{-1}$  change in 100 m) are shown in black. Also shown in white is boundary layer depth estimates from the UHF wind profiler. A vertical line has been included to mark the timing of zero buoyancy flux at surface.

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**Figure A2.** Wind direction from UHF profiler data between 175 and 2500 m. The strongest wind speed gradient identification (black dots) most of the time separates the large-scale westerly flow that persists above from the during daytime often opposing easterly (or northerly) flow below. Also, shown in white is the boundary layer depth estimates from the UHF wind profiler. A vertical line has been included to mark the timing of zero buoyancy flux at surface.

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