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# The impact of shipping emissions on air pollution in the Greater North Sea region – Part 1: Current emissions and concentrations

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Abstract. The North Sea is one of the areas with the highest ship traffic densities worldwide. At any time, about 3000 ships are sailing its waterways. Previous scientific publications have shown that ships contribute significantly to atmospheric concentrations of  $NO_x$ , particulate matter and ozone. Especially in the case of particulate matter and ozone this influence can even be seen in regions far away from the main shipping routes. In order to quantify the effects of North Sea shipping on air quality in its bordering states, it is essential to determine the emissions from shipping as accurately as possible. Within the Interreg IVb project Clean North Sea Shipping (CNSS) a bottom-up approach was developed and used to thoroughly compile such an emission inventory for 2011 that served as the base year for the current emission situation. The innovative aspect of this approach was to use load dependent functions to calculate emissions from the ships' current activities instead of averaged emission factors for the entire range of the engine loads. These functions were applied to ship activities that were derived from hourly records of Automatic Identification System signals together with a data base containing the engine characteristics of the vessels that traveled the North Sea in 2011. The emission model yielded ship emissions among others of  $NO_x$  and  $SO_2$  in high temporal and spatial resolution that were subsequently used in a chemistry transport model in order to simulate the impact of the emissions on pollutant concentration levels. The total emissions of nitrogen reached 540 Gg and of sulfur oxides 123 Gg within the North Sea - including the adjacent western part of the Baltic Sea until 5 degrees W. This was about twice as much of those of a mediumsized industrialized European state like the Netherlands. The relative contribution of ships to, for example,  $\mathrm{NO}_2$  concentration levels ashore close to the sea can reach up to 25 % in summer and 15 %in winter. Some hundred kilometers away from the sea the contribution was about 6 % in summer and 4% in winter. The relative contribution of the secondary pollutant  $NO_3^-$  was found to reach 20% in summer and 6% in winter even distant from the shore.

#### 1 Introduction

Land based sources of  $SO_2$  and  $NO_x$  have decreased substantially in Europe during the last 20 years, partly because of technical progress in the sectors of traffic, heating and industrial production, and partly because of the political and economic changes in Eastern Europe since 1990. In contrast, measures to control ship emissions were disregarded for a long time. Since a few years, however, the awareness of air pollution by shipping in particular concerning the emission of precursors for particulates has been rising (Eyring et al., 2005a, b; Lauer et al., 2009; Dentener et al., 2006) and political options to decrease ship emissions are discussed. Ship traffic in the North Sea is now recognized by its adjacent states as a relevant source for air pollutants because future projections show that this traffic is likely to grow further during the coming decades (Project, 2014). For this reason, the North Sea is designated an Emission Control Area (ECA) with the objective to reduce the emissions of  $NO_x$  and  $SO_2$ . Since November 2007 ships have been obliged to use fuel with a sulfur content not higher than 1.5 %. This limit was lowered to 1 % in July 2010 and to 0.1 % as of January 2015. In addition, from January 2010 the EU sulfur directive requires ships to use fuel with 0.1% or less in EU harbors. The introduction of a nitrogen control area in the North Sea was planned for 2016. However, this plan is suspended at the moment. In the second greenhouse gas study commissioned by the International Maritime Organisation (IMO) both the increase of ship traffic for the next 40 years and implications of introducing ECAs on emission factors for  $NO_x$  and  $SO_2$  are described (Buhaug et al., 2009). Reducing emissions, however, does not necessarily allow to draw conclusions about the actual concentration levels distant from the sources. This is even more true for secondary pollutants like particulate ammonium sulfate, ammonium nitrate or ozone that undergo chemical transformations while being transported in the atmosphere. In this study, an emission inventory for ships in the North Sea for 2011 was created with a bottom-up modeling approach. The main purpose, however, was to use these emissions with a chemistry transport model (CTM) in order to quantify the effect of sea going ships on air quality (with regard to NO<sub>2</sub>, SO<sub>2</sub>, ozone and PM) in middle and northern Europe. 2011 was supposed to be one of the first years of recovery after the world economic crisis at the end of the 2000s, and hence, representative for the current situation of the transport of goods.

Formerly, when little was known about ship activities and the emission behavior of their engines, the only way to estimate emissions of air pollutants from ships was to estimate fuel consumption by means of fuel sales numbers and multiply them with emission factors per units of fuel burned. This method is described in the CORINAIR guidelines (EEA, 2013) and it is partly used to date by the European member states in order to report national emissions to the European Union. It bears, however, large uncertainties because the amount of fuel bunkered in Northern Europe is not necessarily the same amount of fuel consumed there. Deriving emissions that depend only on the mass of fuel and the sulfur or carbon content in that fuel. However, the emissions of substances like

 $NO_x$ , CO, hydrocarbons and particulate matter (PM) depend strongly on combustion temperature and fuel to air ratio, which are related to the engine load.

With the introduction of the Automatic Identification System (AIS) for ships it became much easier to track ship movements and estimate their actual engine loads provided the necessary engine characteristics are known. When the Clean North Sea Shipping project (CNSS) started, emission factors were only available as constant values that had to be multiplied by the energy or fuel consumption of a ship (Denier van der Gon and Hulskotte, 2010; Matthias et al., 2010). One of the first studies about AIS based ship emissions in the North Sea was published by MARIN (2011). The authors of that study calculated ship emissions of the year 2009 for the Netherlands Continental Shelf and extrapolated these emissions to the whole North Sea by means of ship traffic density maps from the Safety Assessment Model for Shipping and Offshore on the North Sea (SAMSON). Hammingh et al. (2012) used the MARIN emission inventory for a study about the impact of introducing a Nitrogen Emission Control AREA (NECA) on the environment and human health in the North Sea. In 2012, Jalkanen et al. (2012) published a study about a ship emission model (STEAM2) that followed an approach similar to the one presented here, also combining AIS signals with a ship characteristics data base. On the one hand, the calculation of the instantaneous engine power is very elaborate in the STEAM2 model, using for example a ship resistance model while the model presented here uses only the ratio between design speed and actual speed. On the other hand, the model presented here uses different emission factor functions for different engine types, vessel sizes and pollutants while Jalkanen et al. (2012) derived load dependency of emission factors from only a few measured engines. Jonson et al. (2014) used results from the STEAM2 emission model for 2011 to estimate the contribution of ships to pollutant concentrations and depositions over Europe and Johansson et al. (2013) extended STEAM2 for a study of the evolution of shipping emissions in northern Europe. Another study about the contribution of ships to air pollution that investigated also health effects and external costs was published by Brandt et al. in 2013 (Brandt et al., 2013). It may be valuable to compare the different models and their results in detail, which is, however, beyond the scope of this study. Instead, the plausibility of the ship emissions presented here and their contribution to air pollution was evaluated by performing statistical tests with observed concentrations available from the European Monitoring and Evaluation Programme (EMEP) network (EMEP, 2015).

#### 2 Ship-emissions model

First of all, the bottom-up approach we followed to estimate ship emissions for the year 2011 required activity data about the ships traveling the North Sea. As one of the most effective ways to derive ship activities the evaluation of signals from the automatic identification system (AIS) was established in recent time (Jalkanen et al., 2012). In order to avoid collisions, all ships bigger than 100 gross tons (GT) are obliged to broadcast such a signal every six seconds to indicate – amongst others – their identification number, position, moving status, direction and speed over ground. Some enterprises like IHS Fairplay store these signals for further evaluation and make them available for purchase. On the basis of AIS data it is possible to follow the route of a single ship and to estimate its energy demand, fuel consumption and pollutant exhaust along this route.

The second requirement for a bottom-up inventory are activity based emission factors for different ship types. Such a set of emission factors in the form of load dependent functions resulted from a study of Germanischer Lloyd (GL) (Zeretzke, 2013) within the Inrerreg IVb project Clean North Sea Shipping (CNSS). The engine characteristics needed to calculate the engine loads were taken from a data base acquired from IHS Fairplay combined with one from GL. The model approach developed in this study uses these functions together with interpolation routines, which allows for simulation of ship emissions at nearly arbitrary temporal and spatial resolution. In order to use the ship emissions in a chemistry transport model (CTM) they had to be transferred from latitude-longitude positions to a regularly spaced Eulerian grid.

#### 2.1 Ship routes derived from AIS data

The AIS data base that was acquired from IHS Fairplay contains hourly updated AIS data in the OSPAR region II, defined within The Convention for the Protection of the marine Environment of the North-East Atlantic (the OSPAR Convention) for the whole year 2011 (Fig. 1). According to this data, about 3000 ships with a valid IMO number were active in the North Sea on average per hour in 2011. However, the spatial density of the hourly signals appeared to be too sparse for creating gridded emissions at a resolution required by the used chemistry transport model set up. In addition to this, the coverage of received AIS signals is low in some regions, especially on the open sea. Therefore, the broadcast positions along a ship track were interpolated linearly to complete tracks and to get enough points for transferring the track to the Eulerian grid. Several routes were predefined that ships would use to circumnavigate certain capes or coastlines. In case an interpolated track point was positioned on land it was moved to the appropriate predefined route. The vessel whose track was to be reconstructed was identified by its International Maritime Organisation (IMO) or Maritime Mobile Service Identity (MMSI) number contained in the AIS data.

In order to elaborate a temporal emission profile of the ship activities – and hence emissions – the ship emissions for 2011 were calculated as 52 weekly sums (Fig. 2). Using weekly and not daily or hourly data reflects the necessity of having enough points to reconstruct and complete ship tracks. The procedural steps were as follows:

- 1. Read data sets from the AIS data base of one week.
- 2. Subset the weekly AIS data by one vessel (IMO or MMSI number).
- 3. Sort by time stamp: this yields the track of one ship in one week sailing the North Sea.

- 4. Interpolate the ship track so that it consists of equidistant points. The distance between the track points is set to  $\frac{1}{3}$  of the length of a grid cell. Make sure the track does not lead over land.
- 5. Calculate speed at every track point.

#### 2.2 Handling erroneous records in the AIS data

#### 2.2.1 Implausible ship movements

AIS signals that contained a requested IMO number but did obviously not belong to the current track resulted in an unrealistic movement of the ship. For example: A ship could jump from the German coast to Norway and back. These signals and the therein contained track points were detected in case the calculated speed between two track points was 20 % higher than the maximum of all reported speeds in the AIS signals of this track. The second one of these points was then removed from the track and the track was recalculated with the remaining points. If there was more than one implausible point in the track they were removed recursively. The assumption was that the preceding points in the track reflected correct AIS signals. The pitfall is, of course, that the correct points could have been removed and erroneous ones kept.

#### 2.2.2 Mooring ships with unknown demooring point of time

In some cases the AIS signal of a ship disappeared for some time while the ship was mooring and did not reappear immediately after it had demoored. Then, the calculated voyage time between the mooring place M and the next captured AIS position T was too long and the calculated speed was too low (the threshold is 40% of speed over ground at position T). When this was detected the speed over ground at position  $T \operatorname{sog}(T)$  was assumed for the whole journey between M and T. In that case, the demooring point of time  $\operatorname{clock}(M)$  was calculated with the formula below. This approach did not consider that it takes some time until a vessel reaches its cruising speed. The same procedure was applied to correct low speeds in the case where a ship leaves the domain and returns many hours later.

$$\operatorname{clock}(M) = \operatorname{clock}(T) - \frac{\operatorname{distance}[MT]}{\operatorname{sog}(T)}$$
 (1)

#### 2.3 Attribute ship characteristics to track

Ships in the AIS data base were usually identified by their unique IMO number. In some cases where the IMO number of a record in the data base was missing or invalid, vessels were identified by the MMSI number of their broadcasting devices. In cases where the same IMO number corresponded to more than one MMSI number, the most frequently found pair was chosen to identify the IMO number of a vessel. By means of the IMO number of the vessel – whose weekly track was reconstructed as explained above – the technical characteristics needed to calculate the emissions of that track were selected from a ship characteristics data base that was also acquired from IHS Fairplay or in a second one provided by GL. If the IMO number was present in both data bases and the values were contradictory the values of the IHS data base were used.

All vessels in the data base were divided into seven types (tankers, bulk ships, cargo ships, cruise ships, ferries, tugs and other vessels) and nine size classes defined by gross tonnage (GT). In several cases single characteristics were missing for a ship. To account for these gaps a look-up table was compiled containing median values per ship class and type whose values were used if not found in the data base. For non-numeric characteristics like fuel type the most frequent one was taken. If no median could be calculated for a particular class the median of a neighboring class was taken (see Appendix A1).

These medians are used to complete missing data if feasible as follows:

- The GT and type of that ship was found: use class medians for missing characteristics.
- IMO is valid but not found in data bases; AIS contains a valid ship type: use medians of the peak of the frequency distribution for this ship type (Fig. 3).

#### 2.4 Emission factors

In the ship emission model presented here methods for calculating fuel consumption and pollutant emissions developed at Germanischer Lloyd (GL) (Zeretzke, 2013) were implemented. For fuel consumption and, hence, SO<sub>2</sub> emissions and NO<sub>x</sub> emissions, these methods consist of functions to calculate load dependent factors in g (kWh)<sup>-1</sup>. Specific functions were developed for different engine applications, namely E3 (propeller-law-operated main and propeller-law-operated auxiliary engine application), E2 (constant-speed main propulsion application including diesel-electric drive or variable-pitch propeller installations) and D2 (constant-speed auxiliary engine application) as well as different engine sizes defined by their maximum continuous rating in kW (MCR). For some of the particulate pollutants, namely black carbon, secondary organic aerosols and mineral ash where no functional relationships could be found constant emission factors for all engine loads were used. The emission factors and functions were found by evaluating a data base of 446 test bed measurements. The resulting formulas and emission factors are summarized in appendix A.

#### 2.4.1 SO<sub>2</sub>

The  $SO_2$  emissions are directly dependent on the fuel consumption and the sulfur content of the fuel. The fuel consumption was calculated using the appropriate functions differentiating between engine type and size (appendix A) and the energy consumption as described in 2.5. The sulfur fuel content is dependent on the type of fuel used, which is unfortunately unknown for most of the ships in our vessel data base. Therefore, we decided to use the speed of the engines to determine the fuel used. Zeretzke (2013) assumes that 95 % of the engines running at between 60 and 300 rpm use heavy fuel oil (HFO) while only 70 % of the engines running at between 300 and 1500 rpm use HFO. The remaining vessels only use marine diesel oil (MDO). According to the MARPOL regulations in 2011 (IMO, 2008) the sulfur fuel content of the vessels while moving in the North Sea ECA was set to 1 % for ships running on HFO and 0.2 % for ships using MDO. If ships using HFO were sailing outside the ECA, the average sulfur content of the HFO allowed in international shipping of 2.7 % was used.

#### 2.4.2 NO<sub>x</sub>

Because the emissions of  $NO_x$  are not linearly related to the fuel consumption, Zeretzke (2013) developed a separate set of functions to calculate load dependent emission factors for  $NO_x$ . These functions differ not only by engine type and size but also consider the year of build because vessels built after 2000 had to comply to TIER I regulations while ships built after 2011 complied to TIER II. The test bed measurements revealed that the emissions of vessels having TIER I specifications were 23 % lower than the officially allowed TIER I value. Therefore, the emission factor for ships built before 2000 was determined by calculating the factor with the formula for the TIER I regulation and multiplying this by 1.6, which considers also the recommendations of Mollenhauer and Tschöke (2007) who estimate that pre-TIER engines emit on average 30 % more  $NO_x$  than TIER I engines. The test bed measurements were carried out with MDO, which has a very low nitrogen content. This means that the formulas for calculating the  $NO_x$  emission factors consider only  $NO_x$  from atmospheric  $N_2$ . Because, according to Zeretzke (2013), the nitrogen content of HFO of up to 0.6 % should not be neglected, our model considers  $NO_x$  emissions of 5.6 g kg<sup>-1</sup> HFO burned.

In addition to new ships, built after 2000, TIER I standards become also applicable to existing engines that were installed on ships built between January 1, 1990 and December 31, 1999, with a displacement of at least 90 liters per cylinder and rated output of at least 5000 kW, subject to availability of an approved engine upgrade kit (IMO, 2008). However, we did not consider this because there was no information in the engine data base whether an engine complied to TIER I and we did not find any information about how many ships built in the nineties were actually retrofitted. To assess the error this negligence would introduce into the model we counted the number of vessels in each class built between 1990 and 2000. Weighting the percental NO<sub>x</sub> emissions with the relative number of potentially retrofitted vessels per class reveals that 13 % of the NO<sub>x</sub> emissions was caused by vessels built between 1990 and 2000 that had a MCR of more than 5000 kW (Table 1). Considering the pre-TIER factor of 1.6, means that the overestimation of NO<sub>x</sub> emissions were 8 % at maximum. Assuming further that for half of these vessels upgrade kits were available we estimate the overestimation in NO<sub>x</sub> emissions at 4 %.

#### 2.4.3 Particulates

The particle emissions that were measured at GL included sulfuric acid and sulfate, mineral ash, black carbon (BC) and primary organic carbon (POA). Other than on load directly the emission factors for particulate species depend on the type of fuel and fuel consumption – hence, indirectly on the engine load. The emissions of particulate sulfate was calculated in the model assuming that 5% of the sulfur in the fuel is emitted as sulfuric acid. The chemistry transport model CMAQ does not distinguish between sulfate and sulfuric acid but treats both as sulfate aerosol.

Both BC and POA were analyzed by a sequential thermal carbon analyzer separating organic from non-organic carbon, which ensured a minimum overlap between BC and POA (VDI, 1996, 1999). Because of the dependency of BC emissions on the sulfur content in fuels (Kurok, 2008; Lack and Corbett, 2012) there are different emission factors for MDO and HFO. The emission factors proposed for the non-carbon ash fraction assume that this ash consists of metal oxides, it does not take into account that some metals form metal sulfates. As the percentage of sulfates in this mineral ash is unknown and the mineral ash fraction is small, we decided to use these emission factors without any sulfate correction (Table 2).

#### 2.5 Emission calculation

Energy consumption, fuel consumption and the emissions of  $NO_x$ ,  $SO_2$ , mineral ash, sulfuric acid, black carbon (BC) and primary organic carbon (POA) were calculated for every track point where the calculated speed was larger than 2 kn. 2 kn was assumed to be the threshold indicating that the ship was neither mooring nor maneuvering. This means, of course, that the emissions of ships in ports are underestimated. According to Hammingh et al. (2012) port emissions account for ca. 10 % of the  $NO_x$  emissions in the North Sea, half of which is emitted from ships at berth. Extrapolating the  $NO_x$  emissions of 2011 in the port of Antwerp, which was estimated for the CNSS project, to the five biggest North Sea ports suggested an underestimation of 6.4 %. Because ports cover only a small part of the entire area of the applied regional model, we considered this lack to be acceptable. In future versions the inclusion of a port emissions model is planned.

Consumption and emissions depend on the actual load L of the ship which was calculated with the speed at MCR and the calculated actual speed (scalc). Calculating the energy consumption E was then straightforward using MCR, the actual load and the time difference between two track points  $\Delta t$ .

$$L = \left(\frac{\text{speed}_{\text{MCR}}}{\text{scalc}}\right)^3 \tag{2}$$

$$E = L \times \text{MCR} \times \Delta t \tag{3}$$

For auxiliary engines the load for moving ships was kept constant at 0.3 following a suggestion by Whall et al. (2002). In a sensitivity model run we increased the auxiliary engine load to 0.4 and found that this would increase the total fuel consumption on the North Sea by 4 %. Fuel consumption and pollutant emissions Em were calculated by multiplying the energy consumption *E* with specific emission factors EF in g (kWh)<sup>-1</sup> (appendix A2 and A3). These emission factors are a function of load *L*, propulsion type *P* (application E2, E3, D2), fuel type *F* (Heavy Fuel Oil or Marine Diesel Oil) and year of build *Y*.

$$\mathbf{EF} = f(L, P, F, Y) \tag{4}$$

$$Em = EF \times E \tag{5}$$

The load was kept between 1 and 0.25 because the emission factors are only applicable for this range according to Zeretzke (2013). If the design speed of a ship (speed<sub>MCR</sub>) was lower than the maximum reported speed over ground (sog) along the track – corrected for implausible track points – speed<sub>MCR</sub> was set to max(sog). However, the actual speed and engine load of a vessel is influenced by external effects like currents and wind. Applying this artificially increased design speed to conditions without or contrary external effects would lead to underestimations of the vessel's engine load. Through a sensitivity run we estimated for vessels of class 6 (which have the largest share in fuel consumption) a worst case underestimation of ca. 9%. On the other hand, external effects can also lead to overestimations, so that the underestimations for the entire year on the whole North Sea may be far below 9%. The most appropriate way to deal with external effects would be to take them directly into account provided these effects were known. This would require, however, a lot of data (for example about the ship's hull, draught, fouling, wind, currents, wave height) that were not available. In our opinion, estimating all these variables would introduce many hardly quantifiable uncertainties.

Loads lower than 0.25 were set to 0.25. An exception was the calculation of BC emissions because it is known that these increase significantly at low loads. We used the formulas below to calculate a correction factor for BC emissions  $f_{BC}$ . They were derived as a piece-wise linear fit to an average relation between engine load and BC emissions shown in a diagram by Lack and Corbett (2012).

$$f_{BC} = \frac{6 - 0.12 \times L}{1.2} \qquad 0 < L \le 0.25$$

$$f_{BC} = \frac{3 - 0.052 \times (L - 0.25)}{1.2} \qquad 0.25 < L \le 0.50$$

$$f_{BC} = \frac{1.7 - 0.02 \times (L - 0.50)}{1.2} \qquad 0.50 < L \le 0.75$$

$$f_{BC} = \frac{1.2 - 0.008 \times (L - 0.75)}{1.2} \qquad 0.75 < L \le 1 \qquad (6)$$

#### 2.6 Transferring the line sources to the model grid

The last step was to transfer these line source emissions to the grid cells of the model domain. The model domain consists of equally spaced grid cells in a Lambert conformal projection. Therefore, the track points defined by latitude-longitude coordinates were converted to Lambert x-y coordinates. Next, the grid cells in which the track points lie were found and all emissions in a cell summed up and added to the domain.

#### **3** Ship emission inventory

Most of all, the exhaust of pollutants is connected with the fuel consumption and, thus, with the energy demand of the ships. Therefore, the sections of the North Sea where the highest emissions of pollutants occurred were those where the majority of the big ships with high energy demand sail. These are the English Channel and the route along the North Sea coast between Belgium and Germany because the largest ships head for the three biggest ports in Europe, Rotterdam, Antwerp and Hamburg. From there, goods are distributed to smaller ports with medium-sized ships that account for regional and inner-European shipping. The main routes for medium-sized ships extend between central-western Europe and Scandinavia. It is a fundamental plausibility check for the bottom-up emission approach that these main shipping lanes could be reconstructed from the AIS data base (Fig. 4). Thus, the emissions of smaller ships were spread all over the North Sea while the large vessels that only sail certain routes along the coasts were responsible for the peak values there.

Table 3 shows the share of ships of different sizes concerning total fuel consumption,  $NO_x$  and  $SO_2$  emissions on the North Sea. It quantifies also the differences normalized by the number of ships per size class – representing differences between average ships of the size classes – and the differences normalized by the transport volume per size class. It is evident that the share of air pollution of the large ships was big if single ships were compared but small if it was related to the freight volume of the ships. This suggests that using large vessels to transport large amount of goods causes less emissions than using smaller vessels for the same amount of goods, provided, of course, that the large vessels use their full freight capacity. In this comparison, however, it should be kept in mind that the amount of goods distributed by medium sized ships to smaller ports in the North and Baltic Sea depends on the freight shipped with large vessels from all over the world. The total calculated ship emissions in 2011 in the study area were lower than those of the big industrial countries like Germany, UK and France, but higher than those of smaller countries (Fig. 5).

A closer look at Table 3 reveals that the relations are not exactly the same for all pollutants. The exhaust of sulfuric acid and  $SO_2$  depends both on the fuel consumption and on the sulfur contents of the fuels used. On the one hand, the specific fuel consumption in g (kWh)<sup>-1</sup> of smaller ships is higher than that of bigger ones. On the other hand, 95 % of the large ships use high sulfur fuel (1.0,% S within SECA) in contrast to 75 % of the medium-sized ships, so that it could be expected

that the share of sulfur emissions for larger ships was higher even if the share in fuel consumption was lower. This relation should be reversed for  $NO_x$  exhaust because the combustion temperature in smaller engines is higher which promotes the creation of oxidized nitrogen (Zeretzke, 2013). In our data set of 2011, this effect appeared to be only weakly pronounced. Ships larger than 60 000 GT consumed 83.1 % of the fuel while causing 83.6 % of SO<sub>2</sub> and 82.7 % of the NO<sub>x</sub> emissions, whereas smaller ships consumed 16.9 % of the fuel and caused 16.4 % of the SO<sub>2</sub> and 17.3 % of the NO<sub>x</sub> emissions (Table 3).

The total ship emissions in 2011 for the model area, which covers the North Sea and the adjacent western part of the Baltic Sea (unitl 5 degrees W), amounted to 540 Gg for NO<sub>x</sub> and 123 Gg for SO<sub>2</sub>. At the same time, the officially reported emissions for the North Sea were 798 Gg for NO<sub>x</sub> and 192 Gg for SO<sub>2</sub> (EMEP/CEIP, 2014). Even if the areas are not the same the differences seem to be remarkable. Recent investigations by Vinken et al. (2014) using satellite data suggested that the officially reported ship emissions might be overestimated by about 35 %. In 2015, EMEP revised the emissions provided through their website to 644 Gg for NO<sub>x</sub> and 162 Gg for SO<sub>2</sub> (EMEP/CEIP, 2015). The reason for the revision is, however, not explained. Table 4 illustrates the variation of ship emission estimates by different models. A further discussion of these differences would require to investigate the differences of the methods applied to create the inventories, which is not intended in this paper.

#### 4 Model set up for the chemistry-transport simulations

The contribution of shipping to air quality in the North Sea area can be determined by combining accurate emission inventories with advanced three-dimensional chemistry transport (CTM) models. A CTM imports emissions and uses meteorological data like wind speed, wind direction, radiation and temperature to simulate transport and chemical transformation of pollutants in the atmosphere. In this way, the CTM developed by the US Environmental Protection Agency, called Community Multi-scale Air Quality (CMAQ) model, was used to calculate air concentrations of a number of pollutants depending on the input emissions. The CMAQ model was used in its version 4.7.1 with the CB05 chemistry mechanism (Byun and Ching, 1999; Byun and Schere, 2006). It was run on a 24 x 24 km<sup>2</sup> Lambert conformal grid for an entire year with a spin up time of 2 weeks and a data output time step of one hour. The model uses 30 vertical layers reaching approximately 10.000 m at the top, the lowest two layers having a height of 36 m. Boundary conditions for the model were from the TM5 global chemistry transport model system (Huijnen et al., 2010). The meteorological fields that drive the chemistry transport model were produced with the COSMO-CLM mesoscale meteorological model for the year 2008 (Rockel et al., 2008). This year was chosen because it did not include very unusual meteorological conditions in central Europe and can therefore be considered to represent average weather conditions in Europe. The simulation of atmospheric chemical processes

is of particular importance for estimating concentrations of secondary pollutants which are not emitted directly but formed from emitted gases by chemical reaction. The most prominent one is ozone, whose formation is influenced by  $NO_x$ . Also very important for health and environment is secondary particulate matter that emerges from gaseous emissions, mostly  $NO_x$  and  $SO_2$ , and constitutes the largest portion of the noxious fine particulate matter. Emissions from other sources like traffic, industry, households and agriculture as well as shipping emissions from outside the domain of the ship emissions model were taken from official European emission inventories (EMEP/CEIP, 2014) and made model ready with the Sparse Matrix Operator Kernel Emissions model for Europe (SMOKE-EU (Bieser et al., 2011)). Model runs were performed both using all available emissions including the ship emission inventory and using land based emissions exclusively. The resulting concentration differences between these runs revealed the impact of shipping emissions.

#### **5** Simulation results

#### 5.1 Validation of simulations through comparison to observations

Several air pollutants are routinely measured by European authorities. They are available for download via the EMEP internet sites (EMEP, 2015) and can be used to validate model results. Even if it must be taken into account that the location where the measurement takes place may not be fully representative for the model grid cell this location belongs to and the overall measurement uncertainty of the observations is not known this comparison provides a good indication for the plausibility of the simulated concentrations. The comparison involves both a graphical comparison of concentration time series and the calculation of some statistical parameters. The authors decided to use only those stations for model evaluation at which values were provided on more than 200 days.

The agreement between measurements and simulations is different at different measurement stations. Very low background concentrations are usually both difficult to measure and to predict correctly with models. For assessing the agreement between observations and simulations the correlation coefficient and the normalized mean bias (NMB) were used (Tables 5 through 7). With only a few exceptions both the measured and modeled concentrations were found to be not normal but logarithmically distributed. In these cases, the mean values shown are geometric means and the correlation was calculated as Spearman rank correlation. Only the NMB was calculated from original concentration values because the authors regarded it as a non-parametric estimator.

Without knowing the measurement conditions and the observation site it is hardly possible to explain the differences exactly. Nonetheless, some cautious but plausible conclusions can be drawn.

#### 5.1.1 Assessment of the base case model results

Because observations of  $NO_2$  are usually available as daily averages, the hourly model output was also recalculated to daily mean values. The resulting time series were compared to the daily mean

of observations at measurement stations in North Sea bordering states (Fig. 6). As often seen with air quality models, CMAQ tended to predict lower  $NO_2$  concentrations than measurements would suggest (Bessagnet et al., 2014), which can be seen by the negative NMB. If the time profile of the predicted values resembles that of the observations and if peak values in the measurements are met by the predictions a correlation should be found. Without testing the significance of the correlation explicitly we consider a correlation coefficient of more than 0.5 to indicate a correlation whereas we speak of a good correlation at values of 0.7 and above. Concerning  $NO_2$ , 17 out of 29 stations had a correlation coefficient of at least 0.7, whereas only three showed a coefficient below 0.5 (Table 5). Stations with low correlation are those that lie in a difficult heterogeneous terrain like rocky coastal areas or on a small island in the sea or where the background concentrations are very low with no peaks but only random variations of the signal.

 $SO_2$  concentrations are generally lower than  $NO_2$  concentrations. This may be a reason for the correlation coefficients being lower than for  $NO_2$ . None of the 15 available stations showed a correlation coefficient higher than 0.7 (Table 6). At least, seven of them had a value of more than 0.5. Another reason for low correlations could be that  $SO_2$  shows nearly no seasonality. In contrast to this,  $O_3$  expresses the most significant seasonality of all investigated substances. As the model succeeded in modeling this seasonal concentration differences, only three out of 36 stations seemed to show no correlation at all. On the other hand, only seven stations showed a good correlation, which reflects the difficulties in modeling the short term variability of ozone (Table 7).

Similar to ozone, nitrate  $(NO_3^-)$  is not directly emitted from the engines, but rather formed in the air by chemical reactions of NO<sub>2</sub>. Only about 5 % of the fuel sulfur is emitted as sulfuric acid aerosol whereas most of the particulate sulfate is produced in the atmosphere from SO<sub>2</sub>. Ammonium nitrate constitutes the major part of inorganic particulate matter. As the formation of these particulates is a complicated and not yet fully understood process the model results are presumably less reliable than for gaseous compounds. Also, the sampling and measurement process is fairly complicated. The agreement between model and observations seemed to be better for nitrate than for sulfate. On the other hand, much less stations were available to evaluate the nitrate simulations (Tables 8 and 9). Six out of nine stations with nitrate measurements presented a correlation coefficient higher than 0.7 while none of the 24 stations for sulfate did. The reason for this is probably the weak seasonality of sulfate in contrast to nitrate. The concentrations of particulate nitrate are notably dependent on ammonia concentrations in the atmosphere, and these are higher in summer than in winter. In contrast, particulate sulfate is nearly invariant to the concentration variations of ammonia.

In order to investigate differences when using the official EMEP emissions, we performed an additional base case run using the EMEP emissions for 2011 EMEP/CEIP (2015). It turned out that the simulation results differ only a little. At the stations along the North Sea coast that showed signifficant differences between the base case and the no ship case 5 the median annual difference for NO<sub>2</sub> was  $0.09 \,\mu g \,m^{-3}$ . Thus, it cannot be clearly decided which model performs better.

#### 5.1.2 Differences between the base case and the no-ship-emissions case

It is evident that ship emissions increase the background concentrations of pollutants at the coast. Therefore, the model bias of the under-predicted substances like NO<sub>2</sub> decreases at coastal stations. This can be shown exemplary for the Danish island Anholt (Fig. 7) where the NMB changed from to -0.69 to -0.37 (Table 5). Some peaks that had been missed by the simulations without ship emissions were met. For this reason, not only the bias decreased but also the correlation increased at some stations if ship emissions were included. The significance of the increase of correlation between simulations and observations was tested by calculating the Fisher *z* transformation of the two correlation coefficients for the different model runs and testing the alternative hypothesis "greater than" at a significance level of 0.9. This means, it was accepted that the correlation at a certain station increased by including ship emissions if the probability of this assumption was larger than 90 %. The significance of the difference of model biases was validated by performing a one-sided *t* test between the model results with and without including ship emissions. As mentioned above, values were logarhythmized if necessary. It can be stated that those stations where bias and correlation were enhanced significantly are most likely to be influenced by ship emissions.

Concerning  $NO_2$  significant correlation increases could be stated for Zingst, Keldsnor, Anholt, Yarner Wood, Lullington Heath, St. Osyth and Raö – the latter also lying on an island like Anholt. In the densely populated Netherlands and Belgium where concentrations are generally higher than in other coastal regions around the North Sea the relative contribution of ships was quite small. Actually, no significant concentration increase could be found for the Belgian stations, and in the Netherlands an increase could only be found for stations close to the sea. For the rest of the studied area all stations close to the sea showed concentration increases and even Neu Globsow in the German hinterland.

Only four stations in the Baltic Sea (the most western part of the Baltic Sea was also in the model domain) showed significantly increased correlations concerning  $SO_2$ . However, stations that showed increased  $NO_2$  concentrations also showed increased  $SO_2$  concentrations which underlines the influence of ships for these sites. When looking at  $O_3$  one would expect that the correlations only were increased at those stations where also  $NO_2$  had a better correlation. There were, however, three stations, Westerland, Zingst and Ulborg where increased correlations for ozone could be verified, but not for  $NO_2$ . This can neither be unambiguously explained by ship emissions nor by the model chemistry. On the one hand,  $O_3$  lives longer than  $NO_2$ , which could be the reason that the ship influence is easier to detect with  $O_3$ . On the other hand, the three mentioned measurement stations lie close to the shipping lanes and the atmospheric life-time of the substances might not play such a big role. Therefore, the ambiguities could also be an issue of the measurement data. There were in total 8 stations with increased ozone correlations, all of them placed close to the sea.

It was already mentioned that it is both difficult to model and to measure particulate  $NO_3^-$ , and therefore it is no surprise that no significant increase of correlation coefficients between the two

model runs could be confirmed. The same can be said about particulate sulfate with one exception at Keldsnor. All stations where the modeled  $NO_2$  concentrations increase significantly also presented significantly increased nitrate concentrations. The same relation would be expected between  $SO_2$  and sulfate. It could, however be not confirmed for the stations Waldhof, Birkenes and Vredepeel. In this regard, it should be mentioned that results of statistical testing only allow to state that the effect could not be verified. They are always dependent on the underlying data and do not necessarily reflect reality. Still, it can be generalized that the concentration levels for particulates increased at stations close to the shipping lanes.

#### 5.2 Concentration patterns over Northwest Europe

The highest pollutant concentrations typically occurred over land at highly populated or industrialized areas. Some of these areas in France, Belgium, Holland and UK lie relatively close to the shore and therefore experienced moderate concentration increases by ship emissions. While sites east of the English Channel showed increases of about 10 % much smaller increases were calculated along the eastern coast of the UK (see for example  $NO_2$ , Fig. 8). The reason is that pollutant plumes from the shipping lanes passing the Channel are transported towards the continent by the prevailing westerly and south-westerly wind directions. During this transport, they are partly removed from the atmosphere by wet and dry deposition. In less populated areas such as Scotland and large parts of Scandinavia pollution levels were generally lower than in the regions mentioned above. This is why the relative pollution increase by ships was up to 50 % in summer and between 10 and 20 %in winter. Apart from the presence of other sources, the relative influence of ship exhaust on air pollutant concentrations also depends on the reaction rates of primary pollutants to form secondary pollutants. These are higher at higher temperatures, which would increase concentrations of secondary pollutants in summer and decrease them in winter. On the other hand, the coagulation of particulates is retarded at lower temperatures, which would suggest lower concentrations of particle bound secondary pollutants like  $NO_3^-$  and  $SO_4^{2-}$  in summer. Northern Germany and Denmark can be considered as coastal regions and are surrounded by numerous shipping lanes. Here, the contribution of shipping emissions to NO<sub>2</sub> is around 15 % in winter and 25 % in summer. Similarly, the contributions concerning  $SO_2$  are about 12 % in winter and 30 % in summer (Fig. 9). Some hundred kilometers away from the sea in the German hinterland the contributions to SO<sub>2</sub> are 5 % in summer and 2% in winter while for the secondary particulate sulfate the contributions are 8% in summer and 3% in winter (Fig. 10).

Along the major shipping lanes between UK and Germany the pollution levels were comparable to those of moderately polluted regions in Europe. However, the concentration maps (Figs. 8 through 14) indicated that nowhere in the investigated domain the contribution of ship emissions to any pollutant was 100 %. This means that emissions produced ashore and substances that enter the domain through the boundaries were transported over the North Sea. Where these influences were

low the contribution of ship emissions were the highest, provided ships operated in these regions. The most significant example for this was the western entrance to the English Channel where the ship emissions were responsible for over 90 % of NO<sub>2</sub> and SO<sub>2</sub> concentrations.

#### 5.2.1 NO<sub>2</sub> and SO<sub>2</sub>

While for  $NO_2$  and  $SO_2$  the overall concentrations were higher in the colder months Figs. 8 and 9 suggest that the absolute contribution of ships is lower in these months. One of the largest sources of land based pollution is heating, which is subject to seasonality. Therefore, the relative contribution of ship engines to pollution levels is lower in winter than in summer because, while the shipping activity is only slightly higher in summer, significantly more pollution from land based sources is produced in winter than in summer. Due to the relatively high emissions of land based sources in winter only slight concentration changes over land in a small slice at the land-sea border were noticeable. In summer, this slice was a little broader indicating that the shipping influence could be recognized further inland than in winter.  $SO_2$  concentrations were a little lower than  $NO_2$  concentrations. The relative contribution of ships within the North Sea was also a little lower with the general spatial pattern being similar. However, the influence of ships was high at the northern and western domain borders because the ships are allowed to use there fuel with higher sulfur content.

### 5.2.2 PM<sub>2.5</sub>

The maps of simulated  $PM_{2.5}$  concentrations suggested in some regions a large relative contribution from ships in the summer months even far inland. This emphasized that the influence of ship emissions on particulate matter in general could be seen further away from the shipping lanes than it is the case for  $NO_2$  and  $SO_2$ , the most important precursors of these secondary pollutants. The influence of ship emissions was further emphasized by the fact that concentration peaks in the time-series (Fig. 12) were accompanied by relatively large reductions if ship emissions had been omitted. The main constituents of  $PM_{2.5}$  are ammonium sulfate and ammonium nitrate, whereas nitrate and sulfate originate from oxidation of  $NO_2$  and  $SO_2$ . While these oxidation reactions are taking place the pollutant plumes can be transported inland (Fig. 13). The reaction rates depend, however, on temperature, solar radiation and the availability of reaction partners like OH and  $NH_3$ , which means that the reaction conditions are much better in summer than in winter. Furthermore, ammonia emissions are lower in winter, which additionally limits the formation of ammonium nitrate and enhances the dry deposition of gaseous nitric acid. Low ammonia emissions, however, have no effect on ammonium sulfate because in ammonia limited conditions the ammonium sulfate production is preferred over ammonium nitrate production.

#### 5.2.3 Ozone

The formation of ozone is, most of all, driven by solar radiation and temperature. Thus, there is a clear summer to winter gradient. It is also evident that the contribution of ships can selectively be very significant, both in terms of increasing the  $O_3$  levels noticeably and decreasing them. The latter is the case in the Channel where massive emissions of  $NO_x$  in the absence of VOCs result in degradation of ozone. Figure 14 illustrates that ozone concentrations were increased by more than 10% along the Scandinavian coasts where no other relevant  $NO_x$  sources but enough VOC was present to form additional ozone.

For the purpose of assessing air quality, ozone concentrations are usually denoted as eight-hour maximum concentrations. This is the maximum of eight-hour means calculated as gliding average for one day. A value of  $120 \,\mu g \, m^{-3}$  was recommended by WHO in 2000 as the value below which health risks are low. The same value has been defined as a target value in the EU recommending that it should not be exceeded on more than 25 days per year within three subsequent years. An analysis of the daily 8 h maximum ozone values in selected coastal regions around the North Sea (Fig. 1) revealed that in Germany, the Netherlands and Belgium and in the UK a concentration of  $120 \,\mu g \, m^{-3}$  was exceeded on more than 25 days (Table 10). Excluding shipping emissions reduced this number significantly in the UK and in Germany. In the Netherlands and Belgium the effects were much smaller because of the high NO<sub>x</sub> emissions from other sources.

#### 6 Summary and conclusions

A multi-model approach to evaluate the impact of shipping on air quality was developed and applied to the North Sea and its bordering states for the year 2011. This approach involved developing a bottom-up emissions model for sea going ships and integrating this into a well established modeling system (COSMO-CLM, SMOKE-EU and CMAQ) to simulate atmospheric transport and chemical transformations of the emitted pollutants.

It is evident that the predictive ability of the modeling system for compounds that tend to be underestimated by the model improves by including ship emissions – particularly in coastal regions. An evaluation of the correlation and the bias between measured and modeled concentrations suggested that the agreement between model and observations improved generally at coastal stations. The less polluted a measurement site is by land-based sources like traffic or industry, the more enhancement of the prediction could be observed. This underlines both the necessity to include a proper representation of shipping emissions into emission inventories for air quality modeling and the plausibility of the model presented here.

The greatest benefit of an advanced bottom-up approach like the one presented here is the possibility to use it for creating and evaluating sophisticated emission scenarios (Matthias et al., 2015).

Running the chemistry transport model CMAQ with and without including ships in the emission inventory revealed that high relative contributions to primary gaseous pollutants concentrated at hot spots along the main shipping lanes. At the same time, the relative contribution to secondary pollutants like particulates and ozone was lower but distributed over a larger area. Even if the contribution of ships to concentration levels of air pollutants in densely populated areas is low it is possible that ship emissions rise the background concentrations sufficiently high that threshold values are more likely to be exceeded and air pollution standards missed.

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	class	NOx	retrofit	NOx share
5	< 10000	7.8	23.8	1.9
6	< 30000	24.5	24.5	6
7	< 60 000	18.7	26.5	5
8	< 100000	21.1	1.8	0.4
9	$\geq 100000$	7.3	0	0

Table 1. Ratio of  $NO_x$  emissions per size class and ships built between 1990 and 2000 (retrofit) and the share of these ships in total  $NO_x$  emissions in %

Table 2. Emission factors for BC, POA and mineral ash in  ${\rm g}\,({\rm kWh})^{-1}$ 

application	fuel	E3	E2	D2
BC	HFO	0.06	0.06	0.15
	MDO	0.03	0.03	0.15
POA		0.1	0.1	0.15
mineral ash	HFO	0.1	0.1	0.1
	MDO	0.01	0.01	0.01

**Table 3.** Percentile share of different ship sizes in fuel consumption and emissions within the model domain in 2011; middle: normalized by the number of ships in every class; right: normalized by the transported freight volume in every class (estimated from the gross tonnage).

					normalized by counts		normalized by freight			
class	GT	fuel	$\mathrm{SO}_2$	$NO_x$	fuel	$\mathrm{SO}_2$	$NO_x$	fuel	$\mathrm{SO}_2$	$NO_x$
2	< 1600	1.6	1.6	1.4	0.9	0.9	0.8	34.1	33.9	31.9
3	< 3000	1.7	1.7	1.6	0.6	0.6	0.5	5.6	5.6	4.9
4	< 5000	16.8	16.8	17.6	2.6	2.6	2.7	14.9	14.7	16.2
5	< 10000	7.9	7.9	7.8	3.7	3.8	3.6	12.1	12.3	12.3
6	< 30 000	25.1	25.4	24.5	9.1	9.4	8.8	10.4	10.7	10.6
7	< 60 000	18.7	18.8	18.7	14.9	15.2	14.8	8.4	8.5	8.8
8	< 100000	21.3	21	21.1	28.6	28.6	28	8.2	8.1	8.4
9	$\geq 100000$	7	6.8	7.3	39.6	39	40.8	6.4	6.2	6.9

 Table 4. Comparison of ship emissions in the North Sea in Gigagrams estimated in different studies.

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study	$NO_x$	$\mathrm{SO}_2$	remarks
EMEP	789	192	emissions 2011, designated ECA zone excluding ports
			(EMEP/CEIP, 2014)
EMEP	644	162	emissions 2011, designated ECA zone excluding ports,
			revised in 2015 (EMEP/CEIP, 2015)
MARIN	472	177	emissions 2009, designated ECA zone including ports
			(MARIN, 2011)
Johansson	648	151	emissions 2011, designated ECA zone including ports
			(Johansson et al., 2013)
This study	540	123	emissions 2011, designated ECA zone, area between 5
			degrees West and 12 degrees East excluding ports

		base case	e		no ships		obse	observations	
station	corr	NMB	mean	corr	NMB	mean	mean	# samples	
Offagne	0.7	-0.33	1.3	0.71	-0.36	1.25	2.1	332	
Eupen	0.62	0	3.08	0.6	-0.04	2.9	3.27	344	
Vezin	0.72	-0.25	2.86	0.72	-0.27	2.75	4.28	346	
Westerland	0.77	-0.62	0.55	0.76	-0.76	0.29	1.44	349	
Waldhof	0.83	-0.43	1.13	0.82	-0.47	1.05	2.37	350	
Neuglobsow	0.74	-0.28	0.96	0.76	-0.33	0.87	1.51	359	
Schmücke	0.71	-0.16	1.38	0.71	-0.18	1.35	1.79	355	
Zingst	0.72	-0.38	1.1	0.61	-0.61	0.54	1.95	359	
Keldsnor	0.71	-0.39	1.2	0.57	-0.67	0.49	2.04	344	
Anholt	0.65	-0.45	0.72	0.45	-0.73	0.3	1.38	322	
Eskdalemuir	0.45	-0.41	0.62	0.44	-0.45	0.57	1.41	364	
Yarner Wood	0.54	-0.42	0.82	0.45	-0.54	0.62	1.57	245	
High Muffles	0.72	-0.09	1.27	0.71	-0.14	1.14	1.57	287	
Aston Hill	0.64	-0.21	0.97	0.64	-0.26	0.89	1.6	295	
Bush	0.67	-0.54	0.87	0.67	-0.56	0.81	2.24	258	
Harwell	0.7	-0.01	2.56	0.68	-0.05	2.42	2.52	310	
Ladybower Res.	0.66	0.11	2.08	0.66	0.07	2.01	2.16	251	
Lullington Heath	0.65	-0.31	1.54	0.53	-0.46	1.05	2.52	360	
Narberth	0.56	-0.66	0.31	0.55	-0.75	0.18	1.42	350	
Wicken Fen	0.73	-0.07	2.25	0.73	-0.12	2.11	2.64	355	
St. Osyth	0.74	-0.34	2.06	0.61	-0.47	1.54	3.18	324	
Market Harborough	0.82	-0.14	2	0.82	-0.18	1.9	2.67	365	
Eibergen	0.8	-0.36	2.39	0.81	-0.39	2.23	4.64	361	
Vredepeel	0.79	-0.45	3.06	0.78	-0.47	2.89	6.49	365	
Cabauw	0.74	-0.32	3.33	0.77	-0.39	2.89	5.62	364	
De Zilk	0.77	-0.44	2.03	0.78	-0.55	1.38	4.18	337	
Birkenes	0.39	0.76	0.5	0.33	0.53	0.43	0.26	361	
Hurdal	0.46	3.04	2.1	0.44	2.98	2.05	0.45	360	
Råö	0.6	-0.5	0.53	0.53	-0.73	0.27	1.12	364	

Table 5. Comparison of simulated NO<sub>2</sub> concentrations with observations in  $\mu g m^{-3}$ . Values that are significantly different between the base case and the no-ships case are printed in bold.

		base case	e		no ships		observations		
station	corr	NMB	mean	corr	NMB	mean	mean	# samples	
Westerland	0.45	0.17	0.21	0.44	-0.15	0.08	0.32	242	
Waldhof	0.53	0.85	0.47	0.53	0.76	0.41	0.31	237	
Neuglobsow	0.58	0.48	0.34	0.61	0.37	0.27	0.29	240	
Schmücke	0.65	0.4	0.58	0.66	0.37	0.55	0.49	311	
Zingst	0.43	0.45	0.46	0.26	-0.09	0.15	0.37	236	
Tange	0.63	0.61	0.14	0.59	0.3	0.1	0.12	350	
Keldsnor	0.68	0.53	0.49	0.54	-0.06	0.19	0.35	339	
Anholt	0.62	0.11	0.21	0.44	-0.31	0.09	0.22	339	
Ulborg	0.52	0.4	0.12	0.47	0.1	0.07	0.12	340	
Narberth	0.07	-0.78	0.22	0.05	-0.85	0.1	1.64	245	
Wicken Fen	0.33	-0.2	1.34	0.33	-0.23	1.29	2.11	363	
Bilthoven	0.32	0.43	1.27	0.31	0.34	1.16	1.03	224	
Vredepeel	0.49	1.38	1.25	0.48	1.32	1.19	0.65	251	
De Zilk	0.45	0.45	1.27	0.42	0.32	1.04	1.2	254	
Råö	0.38	-0.25	0.15	0.23	-0.5	0.07	0.26	346	

Table 6. Comparison of simulated SO<sub>2</sub> concentrations with observations in  $\mu g m^{-3}$ . Values that are significantly different between the base case and the no-ships case are printed in bold.

	base case			no ships		observations		
station	corr	NMB	mean	corr	NMB	mean	mean	# samples
Westerland	0.66	0.09	72.15	0.58	0.06	70.63	63.42	365
Waldhof	0.75	0.28	64.57	0.74	0.26	63.88	45.73	365
Neuglobsow	0.68	0.25	68.27	0.65	0.23	66.82	54.45	365
Schmücke	0.69	0.04	67.81	0.69	0.03	67.25	64.21	365
Zingst	0.68	0.29	70.37	0.62	0.26	68.94	54.62	365
Keldsnor	0.69	0.22	71.34	0.62	0.19	69.62	58.29	365
Ulborg	0.7	0.09	72.23	0.64	0.06	70.12	66.16	332
Lille Valby	0.69	0.24	67.81	0.64	0.21	66.18	54.89	365
Eskdalemuir	0.62	0.21	67.38	0.64	0.18	66.28	54.31	346
Yarner Wood	0.53	0.22	74.37	0.54	0.2	73.26	60.84	344
High Muffles	0.64	0.17	66.72	0.65	0.14	65.39	55.17	313
Strath Vaich Dam	0.55	-0.04	69.67	0.56	-0.06	68.31	72.64	324
Aston Hill	0.69	0.02	71.22	0.71	0	69.85	69.92	314
Great Dun Fell	0.46	0.2	68.12	0.48	0.17	67	55.85	362
Harwell	0.64	0.31	66.34	0.65	0.29	65.32	50.83	354
Ladybower Res.	0.75	0.12	65.93	0.75	0.1	64.52	58.83	357
Lullington Heath	0.62	0.22	72.57	0.6	0.21	72.12	59.69	359
Narberth	0.49	0.26	76.52	0.51	0.23	75.05	60.03	267
Auchencorth Moss	0.64	0.14	68.76	0.64	0.11	67.35	60.43	359
Weybourne	0.71	0.07	64.45	0.71	0.05	64.18	60.3	361
St. Osyth	0.63	0.29	69.5	0.59	0.29	69.45	53.91	336
Market Harborough	0.78	0.16	65.77	0.78	0.14	64.6	56.5	365
Lerwick	0.54	0.02	70.51	0.5	0	69.03	68.44	356
Eibergen	0.78	0.65	59.75	0.78	0.63	59.58	31.78	357
Kollumerwaard	0.71	0.31	69.08	0.71	0.29	67.94	52.85	348
Vredepeel	0.7	0.51	70.27	0.7	0.49	69.23	46.43	286
Cabauw	0.69	0.56	70.25	0.69	0.54	69.43	44.95	281
De Zilk	0.63	0.49	71.18	0.64	0.48	70.65	47.72	312
Birkenes	0.5	0.2	65.86	0.46	0.17	63.97	54.76	353
Prestebakke	0.59	0.13	64.69	0.55	0.09	62.66	57.43	365
Sandve	0.62	0.07	71.36	0.58	0.03	68.8	66.57	365
Hurdal	0.51	0.06	54.01	0.51	0.04	52.87	50.76	365
Bredkälen	0.46	-0.07	52.69	0.46	-0.09	51.76	56.76	356
Råö	0.62	0.13	69.84	0.54	0.09	67.35	61.65	365
Norra-Kvill	0.56	0.03	61.83	0.5	0	59.99	58.07	365
Grimsö	0.54	0.11	57.86	0.52	0.08	56.42	52.18	365

**Table 7.** Comparison of simulated  $O_3$  concentrations with observations in  $\mu g m^{-3}$ . Values that are significantly different between the base case and the no-ships case are printed in **bold**.

**Table 8.** Comparison of simulated  $NO_3^-$  concentrations with observations in  $\mu g m^{-3}$ . Values that are significantly different between the base case and the no-ships case are printed in bold.

		base case	e		no ships		observations	
station	corr	NMB	mean	corr	NMB	mean	mean	# samples
Waldhof	0.71	-0.06	0.22	0.71	-0.16	0.18	0.32	236
Neuglobsow	0.75	0.16	0.19	0.75	0.03	0.15	0.3	234
Zingst	0.74	-0.13	0.24	0.72	-0.29	0.16	0.45	235
Oak Park	0.84	-0.15	0.09	0.82	-0.27	0.07	0.17	255
Malin Head	0.8	-0.31	0.06	0.78	-0.4	0.04	0.11	310
Carnsore Point	0.81	-0.38	0.07	0.79	-0.47	0.06	0.19	347
Kollumerwaard	0.56	0.07	0.58	0.53	-0.07	0.44	0.79	239
Birkenes	0.35	-0.16	0.05	0.34	-0.3	0.04	0.1	298
Hurdal	0.26	1.28	0.1	0.26	1.06	0.09	0.07	295

		base case	e		no ships		obse	ervations
station	corr	NMB	mean	corr	NMB	mean	mean	# samples
Westerland	0.55	-0.04	0.61	0.52	-0.14	0.54	0.62	242
Waldhof	0.5	-0.25	0.56	0.49	-0.3	0.51	0.7	236
Neuglobsow	0.48	-0.18	0.54	0.47	-0.26	0.48	0.64	240
Zingst	0.52	-0.13	0.6	0.47	-0.29	0.47	0.64	241
Tange	0.55	-0.04	0.45	0.5	-0.13	0.41	0.44	355
Keldsnor	0.56	-0.07	0.6	0.48	-0.22	0.49	0.61	340
Anholt	0.6	-0.12	0.48	0.54	-0.22	0.41	0.53	339
Ulborg	0.45	0.05	0.54	0.39	-0.03	0.49	0.48	353
Eskdalemuir	0.43	0.3	0.39	0.39	0.18	0.36	0.26	333
Lough Navar	0.29	0.41	0.38	0.26	0.3	0.34	0.22	213
Barcombe Mills	0.48	-0.11	0.59	0.45	-0.2	0.52	0.59	280
Yarner Wood	0.52	0.03	0.53	0.45	-0.11	0.45	0.42	268
High Muffles	0.41	0.32	0.49	0.33	0.21	0.45	0.34	232
Oak Park	0.5	-0.02	0.4	0.44	-0.11	0.36	0.34	257
Malin Head	0.5	-0.07	0.44	0.46	-0.15	0.4	0.44	335
Carnsore Point	0.58	-0.18	0.5	0.56	-0.25	0.45	0.58	348
Bilthoven	0.41	0.1	0.67	0.39	0.02	0.62	0.51	308
Kollumerwaard	0.37	0.15	0.59	0.32	0.05	0.53	0.43	348
Vredepeel	0.35	0.17	0.7	0.36	0.11	0.66	0.49	322
De Zilk	0.34	0.29	0.69	0.29	0.16	0.62	0.43	351
Birkenes	0.41	0.37	0.35	0.35	0.28	0.32	0.2	347
Hurdal	0.21	1.23	0.37	0.18	1.11	0.34	0.15	359
Bredkälen	0.26	0.69	0.23	0.24	0.54	0.21	0.12	334
Råö	0.63	-0.21	0.43	0.6	-0.28	0.38	0.52	357

Table 9. Comparison of simulated  $SO_4^{2-}$  concentrations with observations in  $\mu g m^{-3}$ . Values that are significantly different between the base case and the no-ships case are printed in bold.

Table 10. Annual number of exceedances of the ozone threshold of  $120 \,\mu g \, m^{-3}$ . For the regions represented see Fig. 1.

	Region 1	Region 2	Region 3	Region 4	Region 5
all emissions	9	19	27	46	29
without ships	4	6	14	42	18



Figure 1. Modeling domain with the borders of the OSPAR region II and the cells that were defined as representative coastal areas.



Figure 2. Monthly deviation from the annual mean fuel consumption in the North Sea in %.



Figure 3. Distribution of ship types across classes.



Figure 4. NO<sub>x</sub> emissions of cargo ships between 5000 and 10 000 GT (left) and > 100 000 GT (right).



Figure 5. Total  $NO_x$  and  $SO_2$  emissions of ships in 2011 compared to some country emissions.



Figure 6. Locations of the EMEP measurement stations used for model evaluation.



Figure 7.  $NO_2$  concentration time series at Anholt.



Figure 8.  $\mathrm{NO}_2$  in summer and winter and the relative contribution of ship emissions.



Figure 9.  $\mathrm{SO}_2$  in summer and winter and the relative contribution of ship emissions.



Figure 10.  $SO_4^{2-}$  in summer and winter and the relative contribution of ship emissions.



Figure 11.  $\mathrm{NO}_3^-$  in summer and winter and the relative contribution of ship emissions.



Figure 12.  $PM_{2.5}$  time-series. Concentrations averaged over the Dutch and Belgian coast (area 4) and the negative bias if ship emissions were excluded.



Figure 13.  $\mathrm{PM}_{2.5}$  in summer and winter and the relative contribution of ship emissions.



Figure 14.  $O_3$  in summer and winter and the relative contribution of ship emissions.

# Appendix A: Supplementary information on ship engine characteristics and emission factor functions

#### A1 Median engine characteristics per ship type and class

The tables summarize class medians of characteristics for ship engines. MCR is the maximum continuous rating in kW, speed the vessel's design speed in kn, RPM the engine speed in revolutions per minute, Y the year of build and power aux. the installed power of auxiliary engines in kW.

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	_	_	_	_	_
2	< 1600	_	-	-	-	_
3	< 3000	749	11.5	750	1995	328
4	< 5000	2400	12.5	600	1997	550
5	< 10000	4690	15.5	500	2004	1213
6	< 30 000	10 400	19	127	2002	2284
7	< 60 000	21 068	22	104	2005	7400
8	< 100 000	57 100	25	102	2005	9416
9	$\geq 100000$	68 640	24.9	104	2010	13 188

Table A.1. Class medians for cargo ships.

Table A.2. Class medians for bulk carrier.

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	_	_	_	_	_
2	< 1600	882	11.5	574	1977	216
3	< 3000	882	11	428	1977	390.5
4	< 5000	2794	12.4	530	1977	435.5
5	< 10000	3884	13.5	228.5	2002	735
6	< 30 000	7080	14	127	2002	1595
7	< 60 000	9480	14.5	113	2008	1890
8	< 100000	16 860	14.5	91	2009	2400
9	$\geq 100000$	22 700	14.5	78	2009	6343

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	_	_	_	_	_
2	< 1600	809	11	413	1985	307.5
3	< 3000	809	12	720	1994	852
4	< 5000	2640	13	600	1996	1201
5	< 10000	4440	14	210	2002	1845
6	< 30 000	8562	14.5	127	2003	2826.5
7	< 60 000	12 240	14.9	105	2005	2768
8	< 100000	16 859	15.3	92	1999	2999
9	$\geq 100000$	28 972.5	16	79	2002	4828

Table A.3. Class medians for tanker.

**Table A.4.** Class medians for cruise ships. As a majority of the cruise ships use their main engines instead of auxiliary engines to generate electricity, 40% of the MCR was used as total power of auxiliary engines. The value of 40% was derived from evaluating cruise ships with no diesel electric engines.

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	_	_	_	_	_
2	< 1600	_	-	_	_	_
3	< 3000	1060	12	1175	2001	-
4	< 5000	3520	15.75	1000	1998	-
5	< 10000	5516	16	750	1987	-
6	< 30000	13 232	18.9	520	1996	-
7	< 60000	23 514	20	600	1984	-
8	< 100000	57 500	22	514	2006	-
9	$\geq 100000$	71 400	22	514	2006	_

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	409	12.8	2100	1995	174
2	< 1600	1900	12.8	1800	1978	174
3	< 3000	1900	15	1050	1987	715
4	< 5000	5884	17.5	850	2004	1292
5	< 10000	8000	17.5	600	1997	1768
6	< 30000	15 479	20	510	1994	3785
7	< 60 000	30 400	22	500	1988	6720
8	< 100000	32 400	21.9	1225	1986	6153
9	$\geq 100000$	_	-	_	_	_

Table A.5. Class medians for ferries.

Table A.6. Class medians for tugs.

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	882.5	10.2	1800	2000	48
2	< 1600	2940	12	1000	2004	315
3	< 3000	2940	13.25	750	2007	1060
4	< 5000	12 000	14	750	2008	1222.5
5	< 10000	16320	16.75	750	2008	2482
6	< 30 000	_	-	_	_	-
7	< 60 000	_	-	_	_	-
8	< 100 000	_	-	-	-	_
9	$\geq 100000$	_	-	_	_	-

class	GT	MCR	speed	RPM	Y	power aux
1	< 100	932	11	2100	1980	70.5
2	< 1600	1618	12	1800	1983	391
3	< 3000	1618	12.8	1000	1994	1065
4	< 5000	5280	14	750	1990	978
5	< 10000	8632	14.4	750	2001	930
6	< 30000	12942.5	14.6	720	1998	1648
7	< 60 000	30 1 56	14.1	500	2008	1007
8	< 100000	_	_	_	_	_
9	$\geq 100000$	-	-	-	_	-

Table A.7. Class medians for other vessels where no type specification could be found.

#### A2 Functions for calculating specific fuel consumptions depending on engine load

In the formulas f(x) is the specific fuel consumption  $\log (kWh)^{-1}$  and  $0.25 \le x \le 1$  is the fractional load.

# A2.1 Application E2: constant-speed main propulsion application (including diesel-electric drive or variable-pitch propeller installations)

MCR < 2000kW	$f(x) = 102x^2 - 170x + 274$
$2000 \geq \mathrm{MCR} < 10000 kW$	$f(x) = 102x^2 - 171x + 260$
$MCR \ge 10000 kW$	$f(x) = 40.1x^2 - 53.2x + 191$

# A2.2 Application E3: propeller-law-operated main and propeller-law-operated auxiliary engine application

MCR < 2000 kW	$f(x) = 67.9x^2 - 84.0x + 239$
$2000kW \ge \mathbf{MCR} < 15000kW$	$f(x) = 47.2x^2 - 74.7x + 210$
$MCR \ge 15000 kW$	$f(x) = 46.1x^2 - 69.2x + 201$

#### A2.3 Application D2: constant-speed auxiliary engine application

 $f(x) = 254.9x^{-0.029}$ 

#### A3 Functions for calculating specific NO<sub>x</sub> emissions depending on engine load

In the formulas f(x) is the specific NO<sub>x</sub> emission in g (kWh)<sup>-1</sup> and  $0.25 \le x \le 1$  is the fractional load.

#### A3.1 Application E2 TIER I

MCR < 2000kW	$f(x) = 0.696x^2 - 1.18x + 9.07$
$2000kW \ge \mathbf{MCR} < 10000kW$	$f(x) = -6.36x^3 + 11.5x^2 - 7.43x + 12.3$
$MCR \ge 10000 kW$	$f(x) = -12.5x^2 + 16.3x + 8.71$

### A3.2 Application E2 TIER II

MCR < 2000 kW	$f(x) = 4.15x^2 - 5.39x + 7.91$
$2000kW \ge \mathrm{MCR} < 10000kW$	$f(x) = -15.3x^3 + 28.0x^2 - 14.5x + 11.2$
$MCR \ge 10000 kW$	$f(x) = -13.4x^2 + 16.7x + 8.64$

# A3.3 Application E3 TIER I

MCR < 2000kW	$f(x) = -12.1x^3 + 27.3x^2 - 20.8x + 12.5$
$2000kW \ge \mathrm{MCR} < 15000kW$	$f(x) = -13.8x^3 + 23.8x^2 - 15.2x + 17.0$
$MCR \ge 15000 kW$	$f(x) = -25.7x^3 + 44.3x^2 - 25.2x + 19.7$

# A3.4 Application E3 TIER II

MCR < 2000kW	$f(x) = -7.25x^3 + 18.2x^2 - 15.5x + 10.7$
$2000kW \ge \mathbf{MCR} < 15000kW$	$f(x) = -14.8x^3 + 27.7x^2 - 19.0x + 17.2$
$MCR \ge 15000 kW$	$f(x) = -32.0x^3 + 57.2x^2 - 31.6x + 18.6$

# A3.5 Application D2 TIER I

f(x) = -0.005x + 14.7

### A3.6 Application D2 TIER II

 $f(x) = 0.891 \log(x) + 1.18$