1	Prediction of gas/particle partitioning of polybrominated
2	diphenyl ethers (PBDEs) in global air: A theoretical study
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#### 14 Abstract

Gas/particle (G/P) partitioning for semivolatile organic compounds (SVOCs) is an 15 important process that primarily governs their atmospheric fate, long-range atmospheric 16 transport, and their routes to enter human body. All previous studies on this issue have 17 hypothetically based on equilibrium condition, the results of which do not predict results 18 from monitoring studies well in most cases. In this study, a steady-state model instead of an 19 equilibrium-state model for the investigation of the G/P partitioning behavior for 20 polybrominated diphenyl ethers (PBDEs) was established, and an equation for calculating the 21 partition coefficients under steady state ( $K_{PS}$ ) for PBDEs (log $K_{PS} = \log K_{PE} + \log a$ ) was 22 developed, in which an equilibrium term ( $\log K_{PE} = \log K_{OA} + \log f_{OM} - 11.91$ , where  $f_{OM}$  is 23 organic matter content of the particles) and a nonequilibrium term (loga, caused by dry and 24 wet depositions of particles), both being functions of  $\log K_{OA}$  (octanol-air partition coefficient), 25 are included. It was found that the equilibrium is a special case of steady state when the 26 nonequilibrium term equals to zero. A criterion to classify the equilibrium and 27 nonequilibrium status for PBDEs was also established using two threshold values of  $\log K_{OA}$ , 28  $\log K_{OA1}$  and  $\log K_{OA2}$ , which divide the range of  $\log K_{OA}$  into 3 domains: equilibrium, 29 nonequilibrium, and maximum partition domain; and accordingly, two threshold values of 30 temperature t,  $t_{\text{TH1}}$  when  $\log K_{\text{OA}} = \log K_{\text{OA1}}$  and  $t_{\text{TH2}}$  when  $\log K_{\text{OA}} = \log K_{\text{OA2}}$ , were identified, 31 32 which divide the range of temperature also into the same 3 domains for each PBDE congener. We predicted the existence of the maximum partition domain (the values of  $\log K_{PS}$  reach a 33 maximum constant of -1.53) that every PBDE congener can reach when  $\log K_{OA} \ge \log K_{OA2}$ , or 34  $t \le t_{TH2}$ . The novel equation developed in this study was applied to predict the G/P partition 35 coefficients of PBDEs for our China-SAMP-II program in China and other monitoring 36 programs worldwide, including Asia, Europe, North America, and the Arctic, and the results 37 matched well with all the monitoring data, except those obtained at e-waste sites due to the 38

39 unpredictable PBDE emissions at these sites. This study provided evidence that, the newly developed *steady-state*-based equation is superior to the equilibrium-state-based equation that 40 has been used in describing the G/P partitioning behavior in decades. We suggest that, the 41 investigation on G/P partitioning behavior for PBDEs should be based on steady state, not 42 equilibrium state, and equilibrium is just a special case of steady state when nonequilibrium 43 factors can be ignored. We also believe that our new equation provides a useful tool for 44 environmental scientists in both monitoring and modeling research on G/P partitioning for 45 PBDEs and can be extended to predict G/P partitioning behavior for other SVOCs as well. 46

47

## 49 **1 Introduction**

Atmospheric transport is a major mechanism to move semivolatile organic 50 compounds (SVOCs), including persistent organic pollutants (POPs), from 51 52 source regions to other remote places, including Arctic and Antarctic, where these chemicals have never been produced and used (Barrie et al. 1992; Macdonald et al. 53 2000; Li et al.1998; Li and Bidleman, 2003; Eckhardt and Manø, 2007). The gas/particle 54 55 (also called aerosol) (G/P) partitioning for SVOCs is a very important process that primarily governs their atmospheric fate (Lohmann et al., 2000), since wet and dry 56 depositions and other processes act differently on gaseous and particulate SVOCs, thus 57 58 affecting the efficiency and scope of their long-range atmospheric transport and fate (Bidleman, 1988). In addition, SVOCs are an important class of indoor pollutants that are 59 of great health concern to humans (Weschler and Nazaroff, 2008). The gaseous and 60 particulate SVOCs have different routes to enter human body, and therefore the G/P 61 partitioning for SVOCs has a significant influence on human exposure (Weschler, 2003). 62

The G/P partitioning behavior of SVOCs, *K*<sub>P</sub>, is commonly defined as (Yamasaki et al.
1982, Pankow 1991, Pankow and Bidleman 1991)

65

$$K_{\rm P} = (C_{\rm P}/TSP)/C_{\rm G} \tag{1}$$

where  $C_{\rm G}$  and  $C_{\rm P}$  are concentrations of SVOCs in gas- and particle-phases (both in pg·m<sup>-3</sup> of air), respectively, and *TSP* is the concentration of total suspended particle in air ( $\mu$ g·m<sup>-3</sup>). Thus  $K_{\rm P}$  has a unit of m<sup>3</sup>· $\mu$ g<sup>-1</sup>. In this study, the term of *partition quotient* instead of *partition coefficient*, is used for  $K_{\rm P}$ , because *partition coefficient* is used for equilibrium condition only, and Eq. (1) was not defined under equilibrium condition.

The value of  $K_{\rm P}$ , calculated by Eq. (1) using the monitoring data *TSP*,  $C_{\rm P}$ , and  $C_{\rm G}$ , is denoted as  $K_{\rm PM}$  (subscript "M" in  $K_{\rm PM}$  means measurement). It has been shown that there is a linear relationship between  $\log K_{\rm PM}$  and  $\log K_{\rm OA}$  ( $K_{\rm OA}$  is octanol-air partition coefficient) (Finizio et al. 1997, Harner and Bidleman, 1998, Pankow, 1998) and between  $\log K_{PM}$  and log  $P_L$  ( $P_L$  is sub-cooled liquid vapor pressure) (Pankow, 1987; Bidleman and Foreman, 1987; Pankow and Bidleman, 1991, 1992). The  $\log K_{OA}$ -based model given by

 $\log K_{\rm PR} = m_{\rm O} \log K_{\rm OA} + b_{\rm O} \tag{2}$ 

has been widely used in describing the partitioning behavior for SVOCs, where slope  $m_0$  and intercept  $b_0$  are fitting constants obtained using regression of  $\log K_{PM}$  (from Eq. (1)) against  $\log K_{OA}$ . The subscript "R" in  $K_{PR}$  indicates regression.

Unfortunately, Eq. (2) is not very useful to environmental modelers, since this equation can only be used when the monitoring data of SVOCs concentrations in both gas- and particle-phases are known, while the modelers need the equations to predict environmental behavior, including their concentrations in air with both gas- and particle-phases, based on physicochemical properties of SVOCs, their emissions, climate and meteorological conditions.

Under the conditions of the equilibrium ( $m_0=1$ ), the dominant absorption processes between gas- and particle-phases, and equivalence of octanol to the sorbing organic matter in particle, Harner and Bidleman (1998) derived the following equation,

90

$$\log K_{\rm PE} = \log K_{\rm OA} + \log f_{\rm OM} - 11.91 \tag{3}$$

where  $f_{OM}$  is organic matter content of the particle. The subscript "E" in  $K_{PE}$  indicates equilibrium. In comparison to Eq. (2), Eq. (3) has an advantage to predict  $K_{PE}$  from the values of  $K_{OA}$  and  $f_{OM}$  without the need of real monitoring data.

However, as discussed in the previous publications (Finizio et al., 1997; Cetin and Odabasi, 2007; Tian et al., 2011; Yang et al., 2013; Li and Jia, 2014), Eq. (3) cannot describe accurately the relationship between gas- and particle-phases polybrominated diphenyl ethers (PBDEs). It is evident that Eq. (3) can be applied only in a few cases, such as for less brominated PBDE congeners (such as BDE-17 and -28) or at high temperatures, and becomes inaccurate in most cases, especially for highly brominated PBDE congeners, such as BDE-66,
-85, -99, -100, -153, -154, and -183, or at low temperatures (Yang et al., 2013; Li and Jia,
2014). This has been blamed by the artifacts and nonequilibrium factors (Finizio et al., 1997;
Cetin and Odabasi, 2007; Tian et al., 2011; Su et al., 2006).

Based on a large dataset of more than 700 pairs of air samples in both gas- and 103 particle-phases with a wide ambient temperature range of 60 °C from -22 to +38 °C obtained 104 from our Chinese POPs Soil and Air Monitoring Program, Phase 2 (China-SAMP-II), we 105 investigated G/P partitioning behavior of PBDEs in Chinese air (Yang et al., 2013; Li and Jia, 106 107 2014). We derived for the first time empirical equations to predict the values of slopes and intercepts for both  $K_{OA}$ -based and  $P_L$ -based models as functions of temperature, and thus 108 109 predicted partition quotient  $(K_P)$  without assuming an equilibrium status and free of artifacts 110 (Li and Jia, 2014). The slope  $m_0$  and the intercept  $b_0$  were given as functions of temperature (in °C), 111

112 
$$m_{\rm O}(t) = 0.011t + 0.263$$
 (4)

113 
$$b_0(t) = -(0.135t + 5.006)$$
 (5)

The temperature *t* in Eqs. (4) and (5) is usually a mean value of temperature for a series of sampling events, such as annual or monthly mean temperature at each sampling site. After the values of  $m_0$  and  $b_0$  are calculated using Eqs. (4) and (5), we can use Eq. (2) to calculate the values of  $\log K_P$ . Since this method can be used to predict the values of  $\log K_P$ , we use  $K_{PP}$  (the second "P" in the subscript  $K_{PP}$  indicates "Prediction") instead of  $K_{PR}$  in Eq. (2), and rewrite them as

$$\log K_{\rm PP} = m_{\rm O}(t) \log K_{\rm OA} + b_{\rm O}(t) \tag{6}$$

121 where  $m_0(t)$  and  $b_0(t)$  are given by Eqs. (4) and (5), respectively.

122 It is noteworthy that  $\log K_{PP}$  in Eq. (6) depends on two parameters, temperature *t* and  $K_{OA}$ , 123 which is also a function of temperature, and given by an empirical equation (Harner and 124 Shoeib, 2002)

125

$$\log K_{\rm OA} = A + B/(t + 273.15) \tag{7}$$

where *t* (in  $^{\circ}$ C) is the temperature for each sampling event, and the parameters *A* and *B* are given in **Table S1** in the Supplement for several PBDE congeners. It should be borne in mind that temperature *t* in Eqs. (4) and (5) can be also the temperature for each sampling event, and thus using Eq. (7), we can express  $\log K_{\text{PP}}$  in Equation (6) as a function of a single independent variable of  $\log K_{\text{OA}}$  as (Li and Jia, 2014)

131 
$$\log K_{\text{PP}} (K_{\text{OA}}) = 0.011B (\log K_{\text{OA}} - 12.27) / (\log K_{\text{OA}} - A) - 2.74 \log K_{\text{OA}} + 31.85$$
 (8)

These two Eqs. (6) and (8) have been successfully applied to predict the values of  $K_{\rm P}$  for 132 PBDEs as functions of  $\log K_{OA}$  in air of China and other countries in the north temperate zone 133 134 and also at an Arctic site in East Greenland (Li and Jia, 2014), and our results matched the monitoring data well at background, rural, urban, and suburban sites, but not at e-waste sites 135 due to the unpredictable PBDE emissions at these sites, and the results indicated that our new 136 equations have a better performance than Eq. (3) in describing G/P partitioning behavior of 137 PBDEs in air as functions of  $\log K_{OA}$ . We also found for the first time that the G/P partitioning 138 139 of PBDE congeners can reach a maximum value if the ambient temperature is low enough. A criterion to classify the equilibrium and nonequilibrium status for PBDEs was also 140 established using  $\log K_{OA}$  (Li and Jia, 2014). 141

These equations, however, suffer from two drawbacks. First, these equations derived at the temperature range from -22 to +38 °C, thus cannot be used at temperatures beyond this range; secondly, these equations were obtained empirically, and do not have a strong theoretical foundation. Therefore, in this paper, we study the G/P partitioning behavior of PBDEs in global air in a theoretical way. The objectives of this study are to establish a partitioning model between gaseous and particulate phases for PBDEs, which can reveal the real partitioning mechanism of PBDEs between these two phases and to predict the partition quotients defined in Eq. (1) accurately for PBDEs in air, thus to achieve a capability to address a series of G/P partitioning issues for these chemicals, such as those presented previously (Yang et al., 2013; Li and Jia, 2014).

152

## 153 **2 Theory**

## 154 **2.1 Equilibrium state and steady state**

To develop a new model in simulating G/P partitioning behavior, we need to understand the 155 equilibrium state and steady state for SVOCs in environment. The steady state is a state in 156 which no change occurs with time, or all time derivatives are equal to zero. "Equilibrium 157 implies that phases have concentrations such that they experience no tendency for net 158 transfer of mass" (Mackay 2001). These two terms have been frequently mistaken with each 159 other. In his book (Mackay 2001), Mackay gave examples to explain the difference between 160 these two states, indicating a chemical is in equilibrium between two media (phases) as long 161 as its fugacities in the two media (phases) are equal no mater the system is steady or 162 163 unsteady.

We also noticed that, although equilibrium is actually an ideal event since such a system 164 cannot exist in real environment; this state has been successfully applied in some cases. 165 Good examples are treat air-water exchange for gaseous pesticide 166 to a-hexachlorocyclohexane (a-HCH) (Jantunen and Bidleman, 1996; 1997; Li et al. 2004) and 167 air-soil exchange for gaseous polychlorinated biphenyls (PCBs) (Li et al. 2010). In these two 168 169 examples, the factors other than the diffusion due to random molecular movement were negligible, and the systems can be treated as equilibrium, thus the net flux of 170 171 gaseous a-HCH between air and water, and gaseous PCBs between air and soil are zero. We realized, however, that the exchange of SVOCs between the gas- and particle-phases is 172 different since the advection processes, such as dry and wet depositions, caused by an 173

external force (gravity) on the particles, cannot be ignored in studying the partitioning
behavior of SVOCs between these two phases. Therefore, we suggest that the steady state,
not equilibrium state, should be applied here.

### 177 2.2 G/P partitioning model under steady state

#### 178 2.2.1 Basic equation

179 A model to describe G/P partitioning under steady state for PBDEs is

180

$$N_{\rm G-P} = N_{\rm P-G} + N_{\rm P-S} \tag{9}$$

181 where  $N_{G-P}$  is flux of PBDEs from gas phase to particle phase,  $N_{P-G}$  is flux of PBDEs from 182 particle phase to gas phase, and  $N_{P-S}$  the net flux of particle-bound PBDEs between air and 183 earth surface, such as water body or surface soil. For the sake of simplicity, we only consider 184 dry and wet depositions in  $N_{P-S}$ , which is given by (Mackay 2001)

185 
$$N_{P-S} = f_P(D_D + D_W)$$
 (10)

where  $f_{\rm P}$  is fugacity of particle in air, given by Eq. (S1) in the Supplement with subscript "I" being "P", and  $D_{\rm D}$  is D value of dry deposition of particle-phase PBDEs described by (Mackay 2001)

189

$$D_{\rm D} = U_{\rm D} v_{\rm P} A Z_{\rm P} \tag{11}$$

where  $U_D$  is dry deposition velocity, a typical value being 10 m/h, *A* is the area between air and earth (water or soil), and  $Z_P$  is *Z* value of aerosol, given by Eq. (S3) in the Supplement, and  $v_P$  is the volume fraction of aerosol, given by

193  $v_{\rm P} = 10^{-9} TSP/r$  (12)

where *TSP* is the concentration of total suspended particles in air ( $\mu g \cdot m^{-3}$ ) and  $\rho$  is the density of the particle (kg·m<sup>-3</sup>).

196  $D_{\rm W}$  is D value of wet deposition given by (Mackay 2001)

$$D_{\rm W} = U_{\rm R} Q v_{\rm P} A Z_{\rm P} \tag{13}$$

198 where  $U_{\rm R}$  is rain rate, a typical value being 0.5 (m·year<sup>-1</sup>). Q is a scavenging ratio

199 representing the volume of air efficiently scavenged by rain of its particle content, per unit volume of rain. A typical value for Q of 200,000 may be used. Substituting the above 2 200 Equations in Eq. (10) leads to 201

202 
$$N_{\text{P-S}} = f_{\text{P}} \left( U_{\text{D}} + U_{\text{R}} Q \right) v_{\text{P}} A Z_{\text{P}}$$
(14)

#### 2.2.2 Gas/particle exchange of PBDEs 203

One of the most important issues for investigating the G/P partitioning behavior is the 204 exchange of PBDE between air and particle. We treat each particle as a ball with a mean 205 diameter of d, a volume of  $v=\pi d^3/6$ , surface area  $a=\pi d^2$ , and a mass  $m=\rho v$ , where  $\rho$  is the 206 density of the particle. The number of particles in 1 m<sup>3</sup> of air, n = TSP/m. In air with volume 207 of Ah (h is the height of atmosphere), the total area of the particles is 208

209 
$$A_{\rm P} = 6TSP(g \cdot m^{-3}) \times A(m^2)h(m)/(\rho(g \cdot m^{-3})d(m))$$
(15)

Assuming  $\rho = 1.5 \times 10^6 \text{ g} \cdot \text{m}^{-3}$ ,  $d = 1.0 \times 10^{-7} \text{ m}$  (Rissler et al. 2006),  $h = 1.0 \times 10^3 \text{ m}$ , the above 210 equation becomes 211

213

$$A_{\rm P} = 0.04A \times TSP \tag{16}$$

a surface area of  $A_{\rm P}$ , as shown in **Fig. S1** in the Supplement. The ratio between  $A_{\rm P}$  and A is 214

To be simplified, we treat the particles as a film, called the *particle film*, with a thickness of d,

- $R_P = A_P / A = 0.04 TSP$ (17)215
- 216 which is a linear function of TSP.

In order to study the movement of SVOCs between air and particle, we adapted the method 217 used for the air-soil interface introduced by Mackay (2001). For diffusion, the two-resistance 218 approach is used, and the overall D values is given by 219

220  $1/D_{\rm V} = 1/D_{\rm E} + 1/(D_{\rm A} + D_{\rm H})$ (18)

where  $D_E$  is air boundary layer D value,  $D_A$  and  $D_H$  are diffusion D values of chemical in air 221 and water sub-phases in particle film, respectively. D<sub>E</sub> is deduced as the product of the 222 surface area of the particle film,  $A_P$  (m<sup>2</sup>), a mass transfer coefficient  $k_V$  (m·h<sup>-1</sup>), and the Z 223

value of air  $Z_G$ , given by:

225

$$D_{\rm E} = A_{\rm P} \, k_{\rm V} Z_{\rm G} \tag{19}$$

226 Here,

227

$$k_{\rm V} = B_a / l_a \tag{20}$$

where  $B_a$  is the chemical's molecular diffusivity in air (0.018 m<sup>2</sup>·h<sup>-1</sup> was assumed), and  $l_a$  is an air boundary layer thickness (0.00475 m was assumed) (Mackay 2001).

In comparison to the soil surface in air-soil exchange, the particle-film that we suggested in our model keeps moving within the atmosphere and thus has much more chances to intersect with the chemical in gas phase. Therefore, the mass transfer coefficient will be larger than that given by Eq. (20), and accordingly, a parameter *C* is introduced in Eq. (20), leading to

235

$$k_{\rm V} = CB_{\rm a}/l_{\rm a} \tag{21}$$

Thus the term  $CB_a$  is the chemical's molecular diffusivity for the particle film in air, and its value will be determined later.

Since most of the SVOCs (including PBDEs) are associated with the organic matter of the particles, again for the sake of simplicity, the 2 terms,  $D_A$  and  $D_H$ , in Eq. (18) are neglected, which becomes

241

$$D_{\rm V} = D_{\rm E} = A_{\rm P} k_{\rm V} Z_{\rm G} \tag{22}$$

242 The flux of PBDEs from gas phase to particle phase,  $N_{G-P}$ , becomes

$$N_{\rm G-P} = f_{\rm G} D_{\rm E} \tag{23}$$

and the flux from particle phase to gas phase,  $N_{P-G}$ , is

$$N_{\rm P-G} = f_{\rm P} D_{\rm E} \tag{24}$$

If the term  $N_{P-S}$  is dropped from Eq. (9), i.e., the net flux of particle-bound PBDEs between air and surface is neglected, we will have

248 
$$N_{G-P} = N_{P-G}$$
 (25)

From Eqs. (23) and (24), the fugacities of a chemical in gas phase ( $f_G$ ) and in particle phase ( $f_P$ ) are equal, and thus the steady state becomes equilibrium. Therefore, it is concluded that equilibrium is just a special case of steady state when  $N_{P-S}$  is ignored.

#### 252 **2.3 G/P equations under steady state**

#### 253 2.3.1 G/P partition coefficient under steady state

254 We use Eqs. (10), (23), and (24) into Eq. (9), leading to

255 
$$f_{\rm p}(D_{\rm E} + D_{\rm D} + D_{\rm W}) = f_{\rm G}D_{\rm E}$$
 (26)

By using Eqs. (S6) and (S7) in the Supplement, the above equation leads to

257 
$$C_{\rm p}'/C_{\rm G} = (Z_{\rm P}/Z_{\rm G})(D_{\rm E}/(D_{\rm E}+D_{\rm D}+D_{\rm W})) = K_{\rm PG} (1/[1+(D_{\rm D}+D_{\rm W})/D_{\rm E}])$$

where  $C'_{P}$  (pg/m<sup>3</sup> of *particle*) and  $C_{G}$  (pg/m<sup>3</sup> of *air*) are concentrations of SVOCs in particleand gas-phases, respectively, and  $K_{PG}$  is dimensionless *G/P partition coefficient* under equilibrium (=  $Z_{P}/Z_{G}$ ). Setting a parameter **a** as

261 
$$\mathbf{a} = 1 / [1 + (D_{\rm D} + D_{\rm W}) / D_{\rm E}]$$
 (27)

and the above equation becomes

263 
$$C'_p/C_G = a K_{PG}$$
 (at steady state) (28)

By using Eqs. (S10) and (S11),  $C'_p$  and  $K_{PG}$  are replaced by  $C_p$  and  $K_{PE}$ , respectively, Eq. (28) becomes

266  $(C_{\rm P}/TSP) / C_{\rm G} = a K_{\rm PE}$  (29)

267 Defining a *G*/*P* partition coefficient under steady state,

268 
$$K_{\rm PS} = (C_P / TSP) / C_G \qquad (at \ steady \ state) \tag{30}$$

where  $C_{\rm G}$  and  $C_{\rm P}$  are concentrations of PBDEs in gas- and particle-phases (both in pg·m<sup>-3</sup> of air), respectively, *at steady state*, and the subscript "S" in  $K_{\rm PS}$  indicates steady state. Although Eq. (30) seems the same as Eq. (1) (for  $K_{\rm P}$ ) and Eq. (S8) (for  $K_{\rm PE}$ ), they are different since Eq. (30) is defined under steady state, Eq. (S8) is under equilibrium, and Eq. (1) was defined at neither steady nor equilibrium state. Thus Eq. (29) becomes

$$\log K_{\rm PS} = \log K_{\rm PE} + \log a \tag{31}$$

274

In the above equation,  $\log K_{\text{PE}}$  is designated the *equilibrium term*, given by Eq. (3), and loga is the *nonequilibrium term*. Therefore, we have two predicted partition coefficients: partition coefficient  $K_{\text{PS}}$  under steady state when the system is at steady state, or partition coefficient  $K_{\text{PE}}$  under equilibrium when the system is at equilibrium. Eq. (31) indicates that the equilibrium is just a special case of the steady state when  $\log a = 0$ .

- 280 2.3.2 Nonequilibrium term loga
- 281 In Eq. (27), setting

282 
$$G = C (D_{\rm D} + D_{\rm W}) / D_{\rm E}$$
 (32)

283 Eq. (27) becomes

- 284 a = 1 / (1 + G/C) (33a)
- 285 or
- 286  $\log a = -\log (1 + G/C)$  (33b)
- 287 Substituting Eqs. (11), (13) and (19) in Eq. (32), which leads after some manipulations,

288 
$$G = 2.09 \times 10^{-10} f_{\rm OM} K_{\rm OA}$$
(34)

289 Thus, as  $K_{\text{PE}}$ , loga is also a function of  $f_{\text{OM}}$  and  $K_{\text{OA}}$ .

## 290 **2.4 loga as functions of logKOA and temperature**

**Fig. S2** in the Supplement depicts variation of loga as functions of log $K_{OA}$  and temperature *t* with C=5. As shown in **Fig. S2A**, the function of loga versus log $K_{OA}$  is a curve shared by all PBDE congeners, showing that when log $K_{OA} < \sim 10.4$ , loga = 0, the state is equilibrium. In contrast with the function of loga versus log $K_{OA}$ , the functions of loga versus *t* are different for different PBDE congeners, as shown in **Fig. S2B** in the Supplement. This figure explains why light PBDE congeners, such as BDE-17 and -28, can reach equilibrium state much more easily than heavy PBDE congeners. It is obvious from **Fig. S2B** that the curves of BDE-17 and -28 deviate significantly from zero at a low temperature (~  $-10^{\circ}$ C), indicating that the values of loga are equal or close to 0 at a wide range of environmental temperature ( $t > -10^{\circ}$ C). For highly brominated congeners, BDE-153 for example, the values of loga deviates significantly from zero even when  $t < +40^{\circ}$ C, causing the equilibrium state at a much narrower ambient temperature range for this chemical ( $t > +40^{\circ}$ C) than BDE-17 and -28.

#### 303 **2.5 Threshold values of log***K***OA** and temperature

Since all the equations to calculate the parameter  $K_{PE}$  and  $K_{PS}$  link only the PBDE parameter 304  $\log K_{OA}$ , it may be advantageous to explore partitioning behavior according to  $\log K_{OA}$ , rather 305 than individual PBDE congeners or homolog groups. Under this consideration, we drew 306  $\log K_{PS}$  -  $\log K_{OA}$  and  $\log K_{PE}$  -  $\log K_{OA}$  graphs, for all PBDE congeners/homologues at an 307 environmental temperature range of -50 to +50 °C, as shown in **Fig. 1**. The straight line (thick 308 blue) for  $\log K_{\rm PE}$  and the curve (red) for  $\log K_{\rm PS}$  can be used for all PBDE 309 congeners/homologues as long as their ranges of  $\log K_{OA}$  are known. Of course, it should be 310 mentioned that the different PBDE congeners have different ranges of  $\log K_{OA}$  at the same 311 temperature span, thus are represented by different portions of the curves in the Fig. 1, 312 accordingly showing different G/P partitioning behaviors. 313

314 There are three cases for G in Eq. (33b).

315 (1)  $G \ll C (D_D + D_W \ll D_E)$ 

316 In this case, Eq. (33b) becomes

317 
$$\log a = -\log (1 + G/C) \approx 0$$
 (35)

318 which is equilibrium state.

319 (2) 
$$G=C(D_D + D_W = D_E)$$

320 In this case, Eq. (33b) becomes

 $\log a = -\log 2 \tag{36}$ 

If we assume that  $f_{OM} = 0.1$  and C = 5, then we have the *first threshold value* from Eqs. (33b) and (34),

$$\log K_{\text{OA1}} = 11.4$$
 (37)

which is very close to the threshold value of  $\log K_{OA} = 11.5$  suggested by Li and Jia (2014). The physical meaning of  $\log K_{OA1}$  is, at this threshold, the data of  $\log K_{PS}$  deviates from  $\log K_{PE}$  by an amount of log 2.

328 (3) G>>C 
$$(D_{\rm D} + D_{\rm W} >> D_{\rm E})$$

329 In this case, Eq. (33b) becomes

330 
$$\log a \approx -\log (G/C) = \log C - \log K_{\text{PE}} - 2.23$$
 (38)

thus  $\log K_{PS}$  in Eq. (31) reaches its maximum value,

332 
$$\log K_{\rm PSM} = -1.53$$
 or  $K_{\rm PSM} = 0.03$  (39)

when G >> C. This is very close to the maximum value of -1.5 suggested by Li and Jia (2014). The maximum value of  $\log K_{PS}$  is clearly shown in **Fig. 1** (the thin blue horizontal line), and

335 we define the *second threshold value* as

336  $\log K_{\text{OA2}} = 12.5$  (40)

As shown in **Fig. 1**, the first threshold value of  $\log K_{OA}$  divides the whole range of  $\log K_{OA}$ into *equilibrium* (EQ) and *nonequlibrium* (NE) *domains*. The second threshold indicates the start of the *maximum partition* (MP) *domain*, in which the values of  $\log K_{PS}$  reach a maximum value of  $\log K_{PSM}$ , which is independent of the values of  $f_{OM}$  and  $K_{OA}$ .

In brief, as shown in **Fig. 1**, the curve of  $\log K_{PS}$ , originally coinciding with the straight line of  $\log K_{PE}$ , increases along with increase of  $\log K_{OA}$ , and separates visibly (by a mount of  $\log 2$ ) from the straight line of  $\log K_{PE}$  at the first threshold value of  $\log K_{OA1}$ , entering the NE domain from the EQ domain. After the second threshold value of  $\log K_{OA2}$ , the curve of  $\log K_{PS}$  enters the MP domain and becomes a horizontal straight line of  $\log K_{PS} = -1.53$ . 346 The values of  $\log K_{OA}$  depend on each PBDE congener and the ambient temperature, as discussed previously (Harner and Shoeib, 2002). Accordingly, we defined two threshold 347 348 values for temperature, the *threshold temperatures*  $t_{TH1}$  and  $t_{TH2}$ , which are the temperatures when  $\log K_{OA}$  of PBDE congeners equals to the threshold values  $\log K_{OA1}$  and  $\log K_{OA2}$ , 349 respectively. As presented in Fig. 2, while the threshold values of  $\log K_{OA1}$  and  $\log K_{OA2}$  are 350 constants for all congeners, the threshold values for  $t_{TH1}$  and  $t_{TH2}$  are different for different 351 352 PBDE congeners. These two threshold temperature values divided the temperature space also into the same 3 domains; the EQ domain when  $t > t_{TH1}$ , the NE domain when  $t \le t_{TH1}$ , and the 353 MP domain when  $t \le t_{TH2}$ . Taking BDE-47 as an example, with its  $t_{TH1} = +11$  °C and  $t_{TH2} = -6$  °C, 354 BDE-47 is in EQ domain when  $t > +11^{\circ}$ C; in NE domain when  $t \leq +11^{\circ}$ C; and in MP domain at 355  $t \leq -6 \,^{\circ}\mathrm{C}.$ 356

#### 357 **2.6 Particle phase fraction**

358 Another important parameter, the fraction of chemical on the particle phase, f (= 359  $C_{\rm P}/(C_{\rm G}+C_{\rm P})$ ), can be calculated from  $K_{\rm P}$  as

360 
$$f_{PX} = K_{PX} TSP / (1 + K_{PX} TSP)$$
 (41)

where the subscript "PX" can be one of "PS", "PE", and "PR". Thus the maximum value of particle phase fraction can be obtained from Eqs. (39) and (41) as

363 
$$f_{PSM} = 0.03 TSP / (1 + 0.03 TSP)$$
(42)

which indicates that, while the maximum partition coefficient  $\log K_{PSM}$  is a constant for all PBDE congeners, it's corresponding maximum value of particle phase fraction is not, but depends on *TSP*. The variation of  $f_{PSM}$  as a function of *TSP* is depicted in **Fig. S3** in the Supplement.

## **369 3. Application of the equations**

#### 370 3.1 G/P partitioning of PBDEs in Chinese Air from China-SAMP-II

In the previous section, we derived an Eq. (31) to predict the values of partition coefficient 371 under steady state  $K_{PS}$ . In this subsection, we used these equations to predict  $K_P$  for air 372 373 samples collected at 15 sites across China under our PBDE monitoring program, 374 China-SAMP-II (Yang et al., 2013, Li and Jia, 2014), and the results will be compared with the predicted values of partition coefficient under equilibrium state K<sub>PE</sub>, obtained using Eq. 375 (3); and the values of *partition quotient*,  $K_{PR}$ , obtained using Eq. (2) with the help of  $K_{PM}$ , 376 377 calculated from Eq. (1) using the monitoring data  $C_{\rm P}$  and  $C_{\rm G}$ . Among the three modeled values ( $K_{PS}$ ,  $K_{PE}$ , and  $K_{PR}$ ),  $K_{PR}$  values are the ones most close to the values of  $K_{PM}$  since 378  $\log K_{\rm PR}$  values are obtained directly from  $\log K_{\rm PM}$  by least squares regression against  $\log K_{\rm OA}$ , 379 and the accuracy of the equations of  $K_{PS}$  and  $K_{PE}$  depends on how their results close to those 380 381 given by  $K_{PR}$ .

382 **Figs. S4 and S5** in the Supplement depict the variations of  $\log K_{PS}$ ,  $\log K_{PE}$ , and  $\log K_{PR}$  as functions of  $\log K_{OA}$  for the 15 sampling sites and 10 PBDE congeners, respectively, both 383 showing the curve of  $\log K_{PS}$  is closer to the regression line of  $\log K_{PR}$  than  $\log K_{PE}$ . It is 384 worthwhile to point out that, for the best match between the results of  $\log K_{PS}$  and  $\log K_{PR}$  for 385 PBDEs, C = 5 was used in Eq. (5) to calculate  $\log K_{PS}$  in air at all the sampling sites with an 386 exception of the site of Waliguan, where C = 50 was used. The reason why much higher value 387 of C was used at this site will be explained later. Fig. S5 also shows that, from the light 388 PBDE congeners to the heavy ones, the ranges of  $\log K_{OA}$  for each PBDE congeners (at 389 temperature range of -22 °C – +38 °C) move from left to right, from smaller than  $\log K_{OA1}$  for 390 BDE-17 to larger than  $\log K_{OA1}$  for BDE-183, or the states that these congeners reside in 391 change from EQ domain to the NE domain, and finally reach the MP domain. 392

393 The 10 regression lines  $(\log K_{PR})$  for the 10 PBDE congeners shown in Fig. S5 are all

presented in **Fig. S6** in the Supplement along with the curves of  $\log K_{PE}$  and  $\log K_{PS}$ , indicating evidently that these 10 lines of  $\log K_{PR}$  change their slopes  $m_0$  along the curve of  $\log K_{PS}$ , not the straight line of  $\log K_{PE}$ , and accordingly, the curve of  $\log K_{PS}$  matches the monitored G/P partitioning data very well for all the 10 PBDE congeners in Chinese air.

We understand that, modelers are most interested in  $K_P$  values as a function of temperature 398 for each PBDE congener. Fig. S7 in the Supplement presents variations of  $\log K_{PS}$ ,  $\log K_{PE}$ , 399 400 and  $\log K_{PR}$  as functions of temperature for the 10 PBDE congeners, indicating that, the curve of  $\log K_{PS}$  matches the line of  $\log K_{PR}$  for each PBDE congener, the highly brominated 401 402 congeners in particular, dramatically well. It is interesting to note that the two threshold temperatures,  $t_{TH1}$  and  $t_{TH2}$ , designed by two vertical dashed lines, increase from the less 403 brominated to highly brominated PBDEs. For example, the value of  $t_{TH1}$  of BDE-17 equals to 404 -16.5 °C, meaning that this compound is in the EQ domain in the most ambient temperature 405 range of  $\geq$ -16.5 °C, while for BDE-183,  $t_{TH1}$ =36.5 °C and  $t_{TH2}$ =15 °C, meaning that this 406 compound is in the EQ domain only when t>36.5 °C, in the NE domain when t $\leq$ 36.5 °C, and 407 in the MP domain when t  $\leq 15.0$  °C. We also calculated the modeled values of log  $K_{PS}$  for 5 408 typical PBDE congeners as functions of temperature from -50 to +50 °C, and the results are 409 given in Fig. S8 in the Supplement, showing that, along with decrease of temperature, the 410 values of  $\log K_{PS}$  for PBDE congeners increase to a maximum partition value; the more highly 411 brominated the congener is, the higher is its value of the first threshold temperature ( $t_{TH1}$ , data 412 413 are not shown) and the second threshold temperature  $(t_{TH2})$ , and thus the higher temperatures at which the congener reaches the NE and MP domains. 414

As shown in **Fig. 1**, the partitioning behavior of PBDEs depends on ambient temperature of sampling events. There are three squares presented in **Fig. 1** indicating the three regions with different temperature ranges, 0 - +50 °C (the orange one), -30 - +30 °C (the green one), and -50 - 0 °C (the blue one). Here, we take the two sampling sites from China-SAMP-II 419 (Yang et al., 2013; Li and Jia, 2014), one is Harbin in the northeast of China, with a sampling 420 temperature range of -22 - +28 °C, within the green square, and the other is Guangzhou in the 421 south of China, with a range of +8 - +38 °C, within the orange square, as examples to show 422 how the threshold values can be used in study the G/P partitioning behavior of PBDEs.

We determined the ranges of  $\log K_{OA}$  for the 10 PBDEs at the site of Harbin (vertical bars) 423 based on the ambient temperature range of -22 - +28 °C at the site, and the results are 424 425 presented in Fig. 3. The two threshold values of  $\log K_{OA}$ ,  $\log K_{OA1}$  and  $\log K_{OA2}$  (the horizontal light blue dashed lines), divide the space of  $\log K_{OA}$  (the left axis) into three domains, the EQ, 426 427 the NE, and the MP domains, and accordingly, the 10 PBDEs in Harbin air can be segregated into 3 groups; BDE-17 and 28 (3-Br homologue) as equilibrium EQ-group, BDE-47 and 66 428 (4-Br homologue) as semiequilibrium SE-group, and others (>4-Br homologues) as 429 nonequilibrium NE-group. The dominant portions of  $\log K_{OA}$  for the EQ-group (purple lines) 430 are under the line of  $\log K_{OA1}$ , i.e., these congeners are mainly in the EQ domain, while the 431 dominant or whole portions of the NE-group (blue lines) are above the line of log  $K_{OA1}$ , 432 indicating that these congeners are in the NE and the MP domains. The SE-group (green lines) 433 is in both the EQ and the NE domains. It is noteworthy that, the major portions of log  $K_{OA}$  for 434 the PBDE congeners in the NE-group were in the MP domain. These three domains can also 435 be identified in the temperature space. In Fig. 3, the two threshold temperatures,  $t_{TH1}$  (the red 436 diamonds) and  $t_{TH2}$  (the red square), are also shown (the right axis), which is similar to **Fig. 2**. 437 In the real ambient temperature range, formed by the two red dashed lines (-22  $^{\circ}$ C and +28  $^{\circ}$ C) 438 at the Harbin site, the major temperature portions of PBDEs in the EQ-group were in the EQ 439 domain (t< $t_{TH1}$ ), those of the NE-group in the NE and MP domains (t $\geq t_{TH1}$ ), and those of the 440 SE-group in both the EQ and NE domains. 441

442 **Fig. 4** presents the  $\log K_{\rm P}$  -  $\log K_{\rm OA}$  graph for the 10 PBDEs in Harbin, which is almost 443 identical to the one contained in the green square of **Fig. 1**. The ranges of  $\log K_{\rm OA}$  for the three groups and their corresponding  $\log K_P$  -  $\log K_{OA}$  diagram are also shown. For example, the log $K_P$  - log $K_{OA}$  diagram for the EQ-group (3-Br homologue), bound by the 2 purple dashed lines, is mainly in the EQ domain, with a small portion in the NE domain; the log $K_P$  - log $K_{OA}$ diagram for the SE group (4-Br homologue), contained by 2 green dashed lines, is mainly in the NE domain, with a small portion in the MP domain; and the log $K_P$  - log $K_{OA}$  diagram for the NE-group (>4-Br homologue), formed by the 2 blue dashed lines, is mainly in the NE and MP domains.

Similar analysis was carried out for the 10 PBDEs at the site of Guangzhou at an ambient temperature range of +8 - +38 °C at the site (Yang et al., 2013), and the results are presented in **Figs. S9 and S10** in the Supplement. The 10 PBDEs at Guangzhou air can also be segregated into 3 groups, BDE-17, -28, and -47 as EQ-group, BDE-66, 99, and 100 as SE-group, and the others, BDE-85, -99, -100, and -183 as NE-group, which are quite different from those for Harbin, caused by the different ambient temperature ranges at the two sites.

We concluded that the PBDEs in Chinese air at 15 sampling sites across China were in the steady state instead of equilibrium state, in realizing that, for less brominated PBDE congeners, BDE-17 and -28, this steady state can be treated as equilibrium state since their nonequilibrium term (loga) can be ignored in comparison to the equilibrium term (log $K_{PE}$ ) in the temperature range of -22 °C to +38 °C (see **Fig. S2B**).

#### **3.2 G/P partitioning of PBDEs in air from other sources**

There are only a few data available in the literature that we can compare to our prediction data.

We predicted the partitioning behavior of gaseous and particle-bound PBDEs in the atmosphere at an e-waste site and a rural site in southern China during 2007-2008 using the information given by Tian et al. (2011). We calculated the values of  $\log K_{PS}$ ,  $\log K_{PE}$ , and

 $\log K_{PR}$  as functions of  $\log K_{OA}$ , and the results are presented in Fig. S11. It is noticeable that 469 our predicted results are obviously better than those obtained by the equilibrium model at the 470 rural site, but not at the e-waste site, where the data from equilibrium model matched the 471 monitoring data better than those predicted using our equation. This seemed unexpected but 472 could possibly be explained by the fact that the emissions of PBDEs from the e-waste site 473 compensated the flux of PBDEs due to dry and wet deposition, leading a situation that 474 475 seemed to be at equilibrium. We cannot, however, accept the point of view that the PBDEs in air at the rural area cannot reach equilibrium, but those in air at the e-waste sites can. 476

477 The G/P partitioning behavior was studied for 7 PBDEs (BDE-28, -47, -99, -100, -153, -154 and -209) at four sites (1 suburban, 2 urban, and 1 industrial) in Izmir, Turkey, in 478 summer and winter in 2004-2005 with a temperature range of 1.8 - 22.4 °C (Cetin and 479 Odabasi, 2007). We calculated the particle phase PBDEs fractions  $f_{PS}$  and  $f_{PE}$ , using Eq. (41) 480 and compared them with the monitoring data, and the results are depicted in Fig. S12. It was 481 noted by the authors that their monitoring data were much lower than the predicted values by 482 the equilibrium equation (f<sub>PE</sub>) (Cetin and Odabasi, 2007), but it is obvious that their results 483 matched our predicted data (f<sub>PS</sub>) very well, among which, the best agreement was observed 484 for BDE-209, the most highly brominated congener of PBDEs. 485

We calculated the G/P partition coefficients for PBDEs in atmosphere of Kyoto, Japan, which were measured in August 2000, and January and September 2001 (Hayakawa et al., 2004), and the variations of  $\log K_{PE}$  and  $\log K_{PS}$  as functions of  $\log K_{OA}$  are presented in **Fig. S13**, indicating obviously that the values of  $\log K_{PS}$  was in a better agreement with the monitoring data than  $\log K_{PE}$ .

491 Air samples were collected from 1 urban, 2 rural, and 1 remote sites near the Great Lakes 492 in 1997-1999 as part of the Integrated Atmospheric Deposition Network (IADN), among 493 which, those taken when the ambient atmospheric temperatures were  $20 \pm 3$  °C were

analyzed for the G/P partitioning behavior of PBDEs, and the log-log relation of  $K_P$  and their subcooled liquid vapor pressures ( $P_L$ ) for BDE-47, -99, -100, -153, and -154 were calculated (Strandberg et al. 2001). By using these data, we calculated both log $K_P$  and f<sub>P</sub> as functions of log $K_{OA}$  for the same 5 PBDE congeners, using the values of  $f_{OM} = 0.2$  and  $TSP = 25 \ \mu g \ m^{-3}$ suggested by Harner and Shoeib (2002), which are presented in **Fig. S14**, along with the predicted results under equilibrium state and steady state. Again the results indicated that the prediction by our new equation is more accurate than those by the equilibrium equation.

### **3.3 G/P partitioning of PBDEs in the Arctic air**

As discussed in the previous sections, each PBDE congener will reach the maximum partition 502 503 domain when  $\log K_{OA} \ge \log K_{OA2}$  or  $t \le t_{TH2}$ . The value of  $t_{TH2}$  of BDE-183 is 15 °C, meaning that BDE-183 in air will be in MP domain when t < 15 °C. The value of  $t_{TH2}$  for BDE-209 504 should be higher ( $\log K_{OA}$ =14.98 for BDE-209 was estimated at 25 °C by Cetin and Odabasi 505 (2007) in comparison to  $\log K_{OA}$ =11.97 for BDE-183 at the same temperature). Accordingly, 506 BDE-209 in arctic air should be in the MP domain, with a constant of  $\log K_{PSM}$  (= -1.53) and 507 the corresponding  $f_{PSM}$  (=0.23 if TSP = 10 mg m<sup>-3</sup> is assumed). This prediction was 508 remarkably in agreement with monitoring data for BDE-209 measured in arctic air at Alert, 509 Canada from 2007 to 2009 with a temperature range between 10 and -50 °C (NCP 2013), 510 lower than the value of  $t_{TH2}$  for BDE-209 (see Fig. 5). The comparisons between the 511 predicted values and the monitoring data at Alert for other values of TSP (= 5 and 2 mg m<sup>-3</sup>) 512 given in Fig. S15 also showed great consistence. It should be stressed from the figure that the 513 values of  $\log K_{PE}$  of BDE-209 are from 3.06 at 10 °C to 8.36 at -50 °C calculated by Eq. (3), 514 which means that the values of  $K_{\text{PE}}$  are from more than 5 orders at 10 °C to 10 orders at -50 515 <sup>o</sup>C of magnitude higher than the monitoring data, a huge error that cannot be tolerated. The 516 corresponding values of f<sub>PE</sub> are 1, indicating that BDE-209 are all in particle phase in the 517 Arctic air predicted by the equilibrium equation, which was not the case given by the 518

monitoring data. In other words, the maximum value 0.23 of  $f_{PSM}$  indicates that, from our prediction, more than half BDE-209 (~0.77) is in gas phase in arctic air, which was confirmed by the monitoring data shown in **Fig. 5**.

We also studied the G/P partition for the 10 PBDEs (BDE-28, -47, -66, -85, -99, -100, -153, -154, -183, and -209) in the Arctic atmosphere in East Greenland Sea in August and September 2009 with a temperature range between -0.5 °C and +6.5 °C (Möller et al., 2011). We calculated the values of  $\log K_{PS}$ ,  $\log K_{PE}$ , and  $\log K_{PR}$  as functions of  $\log K_{OA}$ , and the results are shown in **Fig. S16**. Once again, the equation of  $\log K_{PS}$  had a better performance than the equation of  $\log K_{PE}$ , especially for those congeners in the NE domain with  $\log K_{OA} \ge$  $\log K_{OA1}$ .

529

530 **4. Conclusions and Discussion** 

#### 531 **4.1 G/P partitioning of PBDEs in global air**

Figure At a Glance in the Supplement presents G/P partition coefficients of PBDEs ( $\log K_{PS}$ ) 532 and  $\log K_{\text{PE}}$ ) as functions of  $\log K_{\text{OA}}$  at ambient temperature ranging from -50 to +50 °C, which 533 can be applied at any sites worldwide (the top middle panel, similar to Fig. 1). The three 534 squares in the panel designate the  $\log K_{P}$ -log $K_{OA}$  graphs with three different temperature 535 ranges: 0 - +50 °C, -30 - +30 °C, and -50 - 0 °C, representing the tropical and subtropical 536 climate zones, warm temperate climate zone, and boreal and tundra climate zones, 537 respectively. Monitoring data ( $\log K_{PM}$ ), their regression data ( $\log K_{PR}$ ), and the predicted 538 results  $\log K_{PS}$  and  $\log K_{PE}$  in the three different temperature zones are presented in the figure; 539 the site Guangzhou, China, within the subtropical climate zone, shown in the top-left panel, 540 the site Harbin, China, within the warm temperate climate zone, shown in the bottom panel, 541 and in the site Alert, Canada, within tundra climate zone, shown in the top-right panel, all 542 introduced in the previous sections. The data at these three sampling sites all indicated that 543

the curve of our new equation  $(\log K_{PS})$  are superior to the equilibrium equation  $(\log K_{PE})$  in G/P prediction of partitioning behavior for PBDEs in global air, at the sites in warm temperate, boreal, and tundra climate zones.

#### 547 **4.2 Equilibrium state vs steady state**

Harner and Bidleman (1998) developed in 1998 the Eq. (3), which can predict for the first 548 time the partition coefficients of selected SVOCs in air under the condition of equilibrium 549 between gas- and particle-phases. Four years later, Harner and Shoeib (2002) used this 550 equation to predict the partitioning behavior for 11 PBDE congeners at 25 °C and 0 °C, the 551 results of which, along with the results from our new equation under steady state, are given in 552 Fig. S17 in the Supplement. As shown in the figure, the equilibrium Eq. (3) predicted that, at 553 0 °C, the particle fraction of PBDE congeners can reach as high as ~1, which means that 554 555 PBDE congeners can completely sorbed to the particles. According to our new Eq. (31) under 556 steady state, however, the maximum particle fraction of PBDE congeners was about 0.42 557 when  $\log K_{OA} \ge \log K_{OA2}$ , which was less than half of the highest values predicted by Eq. (3). In other words, we predict that the maximum particle fraction of PBDE congeners in air 558 cannot be more than 50% under steady state if  $TSP < 30 \text{ mg/m}^3$  (See Fig. S3 in the 559 Supplement). In order to support their prediction results, Harner and Shoeib (2002) used the 560 monitoring data of gaseous and particle-bound PBDEs in the Great Lakes air at 20±3 °C 561 (Strandberg et al. 2001). However, as demonstrated in Fig. S14, the prediction by our new 562 equation is much accurate than those by the equilibrium equation. This suggests that PBDEs 563 564 in the Great Lakes atmosphere were in the steady state, not in the equilibrium state.

In brief, we cannot treat the gas- and particle-phases as a closed system for studying G/P partitioning behavior of PBDEs, since the third compartment, the surface of the earth has to be considered. If the nonequilibrium term, loga, in Eq. (31) cannot be ignored, then the fugacities of PBDEs in gas- and particle-phases are not equal, indicating that the system is not at equilibrium but at steady state. For some less brominated PBDEs (such as BDE-17 and -28) at certain temperature, the values of loga is small enough in comparison to the value of  $\log K_{\rm PE}$  in Eq. (31), which is considered as a small perturbation, the system can be considered as equilibrium.

#### 573 **4.3 The maximum partition coefficient**

574 In our previous study (Li and Jia, 2014), we predicted for the first time by an empirical approach the existence of a maximum partition coefficient that every PBDE congener can 575 reach, and was wrongly termed as "saturation state". This prediction was confirmed in this 576 study by a theoretical approach. As shown in **Fig. 1**, the logarithm of the maximum partition 577 578 coefficient log $K_{PSM}$  is equal to -1.53 (or  $K_{PSM} = 0.03$ ) when log $K_{OA} \ge \log K_{OA2}$  (=12.5 for all PBDE congeners), or equally when the ambient temperature is smaller than or equal to  $t_{TH2}$ , 579 which is from -34.5 °C for BDE-17 to 15 °C for BDE-183, and cannot increase linearly along 580 with increase of  $\log K_{OA}$  as predicted by the straight line of  $\log K_{PE}$ . The difference of 581 prediction data between these two equations can be very great. For example, as shown in Fig. 582 1, the difference can reach as high as ~5.5 order of magnitude when  $\log K_{OA} = 17$ . Obviously, 583 the state in the MP domain is a steady state, but not an equilibrium state since the fugacities 584 of PBDEs in gas- and particle-phases are not equal. 585

The best example is the case for BDE-209 in the Canadian Arctic site Alert predicted by 586 our new steady equation discussed previously (Fig. 5). In fact, this is true for any PBDE 587 congener, not for BDE-209 only. As shown in Fig. 1, the blue square with a temperature 588 range of -50 - 0 °C could most likely be the situation for the Arctic atmosphere. Fig. 2 shows 589 that, for the 7 PBDE congeners (BDE-66, -85, -99, -100, 153, -154, and -183),  $t_{\text{TH2}} > 0$  °C. 590 Thus we predict that, as the G/P partitioning behavior is considered, these 7 PBDE congeners 591 592 do not behave differently in the Arctic air, and are all have the same partition coefficient,  $\log K_{PSM}$  = -1.53. Unfortunately, there are no data for the PBDE congeners other than 593

594 BDE-209 available for confirmation of this prediction in the Arctic air.

### 595 **4.4 Comparison to the empirical equations**

The two empirical Eqs. (6) and (8) have been successfully applied to predict the values of  $K_P$ for PBDEs in air of China and other countries in the north temperate zone and also at an Arctic site in East Greenland (Li and Jia, 2014). The Eq. (31) for  $\log K_{PS}$  derived in this study is superior to these empirical equations  $\log K_{PP}$  and  $\log K_{PP}$  ( $K_{OA}$ ) in two ways. First, the steady-state Eq. (31) was derived theoretically, and secondly, this steady-state equation can be used at any ambient temperature, from equator to polar regions, while the empirical equations can only be used at a temperature range of -22 °C to +38 °C.

Comparison between steady-state Eq. (31) for  $\log K_{PS}$  and empirical equations  $\log K_{PP}$  given 603 by Eq. (6) and  $\log K_{PP}(K_{OA})$  given by Eq. (8) in Harbin air at a temperature range of -22 to 604 +28 °C are presented in Fig. 6, and the equilibrium equation  $\log K_{PE}$ , given by Eq. (3), is also 605 included for comparison. It is evident from Fig. 6 that, the straight line  $\log K_{\rm PP}$  deviates 606 607 apparently from the straight line  $\log K_{\text{PE}}$  at  $\log K_{\text{OA}} = \log K_{\text{OA}}$ , and increases linearly with  $\log K_{OA}$ . Different lines of  $\log K_{PP}(K_{OA})$  for different PBDE congeners are able to predict the 608 G/P partitioning behavior of PBDE more accurately than the straight line  $\log K_{PP}$ . It is 609 610 interesting to note that, the different lines of  $\log K_{PP}(K_{OA})$  for different PBDE congeners change their trends along with the single line of steady-state equation  $\log K_{PS}$ , which is the 611 best equation that can be used to predict the G/P partitioning behavior for all PBDE 612 congeners and at all ranges of ambient temperature. 613

## 614 **4.5 The limitation of applications**

In order to derive Eq. (31), several assumptions were made, which include that, the G/P partitioning reached steady state, the annual rainfall was 0.5 m yr<sup>-1</sup>,  $f_{OM} = 0.1$ , C = 5, and some others. This equation, however, has been successfully applied in all situations that we discussed in this study, in which some of the assumptions were not satisfied. We should be 619 aware, however, that the situations in which some abnormal conditions exist, such as heavy wind, heavy rains, or the sampling sites close to e-waste or PBDE manufactures, should be 620 best treated separately. For example, as described in the previous section, the constant C621 622 should be changed from 5 to 50 in Eq. (5) for Site Waliguan. The reason why much higher value of C was used at this site is possibly due to the high wind speed there. At Waliguan, 623 where annual average wind speed reaches 4.6 m/s, and the northwest wind with speed > 10624 625 m/s being quite often in the winter and spring seasons (http://gaw.empa.ch/gawsis/reports.asp?StationID=12), much higher than the other sites; and 626 627 the air sampler was installed at the top of the mountain (see Supplementary Fig. S18), suffering from the highest wind speed without any blocks in the area, causing the higher 628 value of C than those at the other 14 sites. An analytic equation may exist to relate the 629 630 parameter C and the wind speed (and possibly other factors too), but this equation is not 631 available at present and planned for future study. The case for the Chinese e-waste site is also worth to mention. Our equation cannot be used at the e-waste sites and most likely at the 632 PBDE manufacturers as well since the emissions of PBDEs at these sites could be too large 633 and also variable with time so that the steady state cannot be reached or maintained 634

It should be borne in mind that the steady state discussed here is still an idealized scenario 635 since only dry and wet depositions were discussed in the study, other factors, such as 636 humidity and artifacts, will also play roles to a certain extent to affect the G/P partitioning. As 637 638 anticipated, results obtained from this study do not perfectly fit monitoring data. However, this study revealed the major internal factors governing the gas-particle partitioning processes 639 for PBDEs, and explicated how these processes can be more correctly treated as being in 640 641 steady state rather than in equilibrium state. At least, the steady-state model, not the equilibrium-state model, should be applied to analyze the gas-particle relationship of SVOCs, 642 such as PBDEs. Further study for other SVOCs, like PCBs and PAHs, is on the way. 643

#### 645 The Supplement related to this article is available online at

646

#### 647 Author contribution:

Y.F.L. designed the research on the new theory of G/P partitioning of PBDE in air under
steady state; Y.F.L., W.L.M., and M.Y. performed the research; Y.F.L., W.L.M, and M.Y.
analyzed data; and Y.F.L. wrote the paper, with input from W.L.M., and M.Y.

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# 781 Figure captions

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**Figure 1.** Variation of  $\log K_{PE}$  and  $\log K_{PS}$  as functions of  $\log K_{OA}$  with a temperature range of

783 -50 - +50 °C. Two threshold values of  $\log K_{OA}$  ( $\log K_{OA1}$  and  $\log K_{OA2}$ ) are also shown, 784 which divide the space of  $\log K_{OA}$  into three domains: the equilibrium (EQ), the 785 nonequilibrium (NE), and the maximum partition (MP) domains. The three squares 786 designate the  $\log K_{P}$ -log $K_{OA}$  graphs with three different temperature ranges: 0 - +50 °C, 787 -30 - +30 °C, an -50 - 0 °C, representing the tropical and subtropical climate zones, 788 warm temperate climate zone, and boreal and tundra climate zones, respectively.

**Figure 2.** The first and second threshold temperatures,  $t_{TH1}$  and  $t_{TH2}$  for 10 PBDE congeners, which divide the temperature space into the same 3 domains (EQ, NE, and MP).

**Figure 3.** The range of  $\log K_{OA}$  (the left axis) and the threshold temperatures (the right axis) 791 for 10 PBDE congeners in Harbin air at a temperature range of -22 to +28 °C. The 792 ranges of  $\log K_{OA}$  for the 10 PBDE congeners are given by the vertical bars. The 2 793 horizontal light blue dashed lines give the 2 threshold values of  $\log K_{OA1}$  and  $\log K_{OA2}$ , 794 and the red diamonds and red squares present respectively the two corresponding 795 threshold temperatures,  $t_{\text{TH1}}$  and  $t_{\text{TH2}}$ . The former divides the space of  $\log K_{\text{OA}}$  (the left 796 axis) and the later divides the temperature space (the right axis) into three domains: the 797 EQ domain, the NE domain, and the MP domain. Thus the PBDE congeners 798 (homologues) in Harbin air can be segregated into 3 groups; BDE-17 and -28 (3-Br 799 homologue) as equilibrium EQ-group, BDE-47 and -66 (4-Br homologue) as 800 semiequilibrium SE-group, and others (>4-Br homologues) as nonequilibrium 801 802 NE-group.

Figure 4. The  $\log K_{\rm P}$  -  $\log K_{\rm OA}$  diagram for the 10 PBDE congeners in Harbin air at a temperature range of -22 to +28 °C. The EQ Group includes BDE-17 and -28, the SE Group contains BDE-47 and -66, and the rests belong to NQ Group. The range of

806 $\log K_{OA}$  for each group and their corresponding  $\log K_P$  -  $\log K_{OA}$  diagram are also shown.807The  $\log K_P$  -  $\log K_{OA}$  diagram for the EQ Group, boned by 2 purple dashed lines, is808mainly in the EQ domain, with a small portion in NE domain; the  $\log K_P$  -  $\log K_{OA}$ 809diagram for the SE Group, contained by 2 green dashed lines, is mainly in the NE810domain, with a small portion in MP domain; and the  $\log K_P$  -  $\log K_{OA}$  diagram for the NE811Group, formed by the 2 blue dashed lines, is mainly in the NE and MP domains.

Figure 5. The temporal trends of concentrations of BDE-209 in the Arctic air in gas + particle phase (blue line) and in particle phase (green line) at Alert, Canada from 2007 to 2009 (NCP 2013). The purple triangles and red diamonds are the values of f and  $\log K_P$  of BDE-209, respectively, calculated using the concentration data, and match well the values of  $f_{PSM}$  (=0.23) and  $\log K_{PSM}$  (-1.53), respectively (*TSP* = 10 mg m<sup>-3</sup> was assumed).

Figure 6. Variation of  $\log K_{PS}$  (the thick red line, given by Eq. (31)),  $\log K_{PE}$  (the thick dark green line, given by Eq. (3)), and  $\log K_{PP}$  (the thick pink line, given by Eq. (6)) as functions of  $\log K_{OA}$ . The functions of  $\log K_{PP} (K_{OA})$  (the thin lines, given by Eq. (8)) vesus  $\log K_{OA}$  for the 10 PBDE congeners in Harbin air at a temperature range of -22 to +28 °C are also included.

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Figure 1. Variation of  $\log K_{PE}$  and  $\log K_{PS}$  as functions of  $\log K_{OA}$  with a temperature range of -50 - +50 °C. Two threshold values of  $\log K_{OA}$  ( $\log K_{OA1}$  and  $\log K_{OA2}$ ) are also shown, which divide the space of  $\log K_{OA}$  into three domains: the equilibrium (EQ), the nonequilibrium (NE), and the maximum partition (MP) domains. The three squares designate the  $\log K_{P}$ -log $K_{OA}$  graphs with three different temperature ranges: 0 - +50 °C, -30 - +30 °C, an -50 - 0 °C, representing the tropical and subtropical climate zones, warm temperate climate zone, and boreal and tundra climate zones, respectively.

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**Figure 2.** The first and second threshold temperatures,  $t_{TH1}$  and  $t_{TH2}$  for 10 PBDE congeners,

839 which divide the temperature space into the same 3 domains (EQ, NE, and MP).





843 **Figure 3.** The range of  $\log K_{OA}$  (the left axis) and the threshold temperatures (the right axis) for 10 PBDE congeners in Harbin air at a temperature range of -22 to +28 °C. The ranges of 844  $\log K_{OA}$  for the 10 PBDE congeners are given by the vertical bars. The 2 horizontal light blue 845 846 dashed lines give the 2 threshold values of  $\log K_{OA1}$  and  $\log K_{OA2}$ , and the red diamonds and red squares present respectively the two corresponding threshold temperatures,  $t_{TH1}$  and  $t_{TH2}$ . 847 The former divides the space of  $\log K_{OA}$  (the left axis) and the later divides the temperature 848 849 space (the right axis) into three domains: the EQ domain, the NE domain, and the MP domain. Thus the PBDE congeners (homologues) in Harbin air can be segregated into 3 groups; 850 BDE-17 and -28 (3-Br homologue) as equilibrium EQ-group, BDE-47 and -66 (4-Br 851 homologue) as semiequilibrium SE-group, and others (>4-Br homologues) as nonequilibrium 852 NE-group. 853



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Figure 5. The temporal trends of concentrations of BDE-209 in the Arctic air in gas + particle phase (blue line) and in particle phase (green line) at Alert, Canada from 2007 to 2009 (NCP 2013). The purple triangles and red diamonds are the values of f and  $\log K_P$  of BDE-209, respectively, calculated using the concentration data, and match well the values of f<sub>PSM</sub> (=0.23) and  $\log K_{PSM}$  (-1.53), respectively (*TSP* = 10 mg m<sup>-3</sup> was assumed).

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**Figure 6.** Variation of  $\log K_{PS}$  (the thick red line, given by Eq. (31)),  $\log K_{PE}$  (the thick dark green line, given by Eq. (3)), and  $\log K_{PP}$  (the thick pink line, given by Eq. (6)) as functions of  $\log K_{OA}$ . The functions of  $\log K_{PP}(K_{OA})$  (the thin lines, given by Eq. (8)) versus  $\log K_{OA}$  for 10 PBDE congeners in Harbin air at a temperature range of -22 to +28 °C are also included.