



## Supplement of

# Kerb and urban increment of highly time-resolved trace elements in $PM_{10}$ , $PM_{2.5}$ and $PM_{1.0}$ winter aerosol in London during ClearfLo 2012

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#### 1 Supplement A: RDI backup filter and PM<sub>1.0</sub> cut off analysis

#### 2 RDI backup filter analysis

RDI backup filters (Balston 050-11-BQ 2  $\mu$ m, microfiber, fluorocarbon resin binder) from the ClearfLo winter campaign were immersed in water and sonicated for about 1.5 hrs. One filter per measurement site was available. Total sulphate (SO<sub>4</sub><sup>2-</sup>) mass was obtained by analysing the solutions with ion chromatography and converted to concentrations by dividing by the total air volume that passed through the filter during the campaign.

9 Table S1 compares the S concentrations from the RDI  $PM_{1.0-0.3}$  stage with S (from 10  $SO_4^{2-}$ ) collected by the backup filter. The sum of both (Total S <1µm) is compared 11 with S from AMS sulphate measurements. The ratio in the last column reveals mass-12 closure between the RDI and AMS within 20%.

13

14 Table S1. Comparison between S from RDI PM<sub>1.0-0.3</sub> fractions and backup filters

15 (S from  $SO_4^{2-}$ ) with S from the AMS (S from  $SO_4$ ). Units in ng m<sup>-3</sup>. The ratio of S

16 in the RDI to the AMS is given in the last column (ratio of RDI Total S <1  $\mu$ m to

17 **AMS S).** 

	RDI			AMS	Ratio
Site	PM <sub>1.0-0.3</sub> S	S in backup filter	Total S <1 μm	S	RDI : AMS
MR	178	398	576	476	1.21
NK	159	405	564	607	0.93
DE	212	359	571	715	0.80

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#### 19 **RDI PM<sub>1.0</sub> cut off analysis**

As noted in the main text, elements whose mass is dominated by the  $PM_{1.0}$  fraction are typically underestimated by RDI-SR-XRF relative to external measurements like the AMS and 24-hr filter measurements. One explanation is that the collection efficiency of the RDI  $PM_{1.0}$  stage is smaller than expected, e.g. by a larger-thanexpected size cut off. We therefore performed new laboratory measurements of the RDI size-dependent collection efficiency, and compare to earlier characterisations by Bukowiecki et al. (2009) and Richard et al. (2010). 27 Figure S1 shows the setup used for the collection efficiency measurements. 28 (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>, NH<sub>4</sub>NO<sub>3</sub> and NaCl particles were nebulized, dried and size-selected 29 using a differential mobility analyser (DMA, TSI, Inc., Shoreview, MN, USA), and then 30 sampled with the RDI. The DMA was operated with sample and sheath flow rates of 31 0.3 and 3.0 L min<sup>-1</sup>, respectively. A condensation particle counter (CPC1, TSI, Inc., Shoreview, MN, USA) with a flow rate of 1.0 L min<sup>-1</sup> was continuously connected at 32 33 the inlet stage of the RDI to measure the particles entering the RDI, and to correct for 34 fluctuations in nebulizer performance. A second line led to an additional CPC (CPC2, 35 1 L min<sup>-1</sup>) and an Aerodyne aerosol mass spectrometer (AMS, Aerodyne Research, Inc., Billerica, MA, USA) with a flow rate of 0.1 l min<sup>-1</sup>. This line could be connected at 36 the inlet, after the PM<sub>2.5-1.0</sub> (B) stage or after the PM<sub>1.0-0.3</sub> (C) stage. Measurements 37 38 following the B and C stages were made by connecting the line to a small hole in the 39 lid covering these stages, resulting in sampling of the air flow at a 90° angle (see 40 picture in Figure S1). The total flow through the system was controlled by a mass 41 flow controller connected to a clean air generator pumping air into the nebulizer and 42 RDI simultaneously. The RDI was operated using three wheels with freshly mounted 43 6-µm polypropylene foils coated with Apiezon to minimize particle bouncing effects, 44 to simulate ambient field measurements. Tests ruled out differences in 45 measurements on the top or bottom side of the lid at the B and C stages. For the final 46 results, all data was collected at the bottom side of the B and C stages.



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48 Figure S1. Setup of the collection efficiency measurements of the RDI PM<sub>1</sub>

49 impactor stage. The line with the AMS and CPC2 was connected at the inlet,

50 after the  $PM_{2.5-1.0}$  or after the  $PM_{1.0-0.3}$  stage. The picture of the RDI shows the 51 connection at the bottom side of the lid of the  $PM_{1.0-0.3}$  stage.

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53 As noted above, measurements were conducted at the RDI inlet, after the B stage 54 impactor (nominal size cut = 1.0 µm) and after the C stage impactor (nominal size cut 55 = 0.1  $\mu$ m). RDI collection efficiency at each stage is defined as 1 minus transmission. 56 To correct for fluctuations in nebulizer concentrations, all data for a given set of 57 CPC2/AMS measurements were normalized to a constant inlet (CPC1) 58 concentration. Transmission from the inlet across the B stage impactor was between 59 90 and 100% for all sizes (aerodynamic diameter  $D_a < 950$  nm), indicating negligible 60 particle losses and/or unintended collection of small particles. C stage collection 61 efficiency (CE<sub>c</sub>) was therefore calculated using Eq. (S1):

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63 
$$CE_{C} = 1 - \left(Conc_{C} * \frac{CPC1_{ref}}{CPC1_{measC}}\right) / \left(Conc_{B} * \frac{CPC1_{ref}}{CPC1_{measB}}\right)$$
  
64 (S1)

65 Concentrations were measured using both CPC2 and the AMS. For large particles, 66 where the fraction of multiple charged particles passed by the DMA is negligible, 67 these two methods yield similar results. For smaller particles, collection efficiency as 68 calculated by the CPC2 is biased low due to the presence of multiple charged 69 particles with larger diameters, as clearly evidenced from AMS size distributions. For 70 simplicity, we therefore present only the AMS results here. RDI collection efficiencies 71 are calculated by fitting a lognormal distribution to each mode and using the resulting 72 mass concentrations in Eq. S 1. This allows simultaneous calculation of RDI 73 collection efficiencies for several sizes, providing an internal consistency and stability 74 check for the measurements.

75 Figure S2 shows the collection efficiency of the PM<sub>1.0-0.3</sub> (C stage) nozzle for two 76 RDIs (RDI1 and RDI2) as a function of D<sub>a</sub> for NH<sub>4</sub>NO<sub>3</sub> particles. D<sub>a</sub> is calculated from 77 AMS size measurements, assuming a density of 1.74 and a Jayne shape factor 78 (DeCarlo et al., 2004) of 0.8. Cut points are estimated by a sigmoidal fit to the 79 collection efficiency curves, and yield different cut points for the two RDIs. RDI1 has 80 a cut point of 290  $\pm$  25 nm and RDI2 a cut point of 410  $\pm$  15 nm. This discrepancy 81 was investigated using RDI2 equipped with the PM<sub>1.0-0.3</sub> nozzle of RDI1 (RDI2 (nozzle 82 RDI1)), demonstrating that the difference between the two RDIs is governed by nozzle performance, because the cut point of this system is  $300 \pm 20$  nm and therefore closer to the RDI1 performance. Similar cut points for the various systems were obtained using (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> and NaCl particles (not shown).



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Figure S2. Collection efficiency of the RDI PM<sub>1.0-0.3</sub> impactor stage as a function
of aerodynamic diameter.

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90 Measurements of the nozzle sizes under a microscope reveal small differences 91 between the RDIs. A 1.0 µm cut point at the B stage impactor is obtained with a 92 nozzle size of 0.68 x 10 mm. The RDI1 and RDI2 B stage nozzles were 0.70 x 10 93 mm, and a third RDI that was used at Marylebone Road during ClearfLo had a size of 94 0.71 x 10 mm. The C stage nozzle size should measure 0.30 x 10 mm for a cut point 95 of 0.1 µm. However, the nozzle sizes were 0.30-0.31 x 10, 0.30-0.32 x 10 and 0.32 x 96 10 for RDI1, RDI2 and the third RDI, respectively. We expect the deviations from 97 these measurements from the machining of the nozzles, resulting in higher cut points 98 than expected for the PM<sub>1.0</sub> stage, and possibly also for the PM<sub>2.5-1.0</sub> stage.

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#### 100 Conclusions

101 The  $PM_{1.0-0.3}$  collection efficiency curves are different for the two RDIs. RDI2 has a 102 larger small-end cut point of 410 ± 15 nm than RDI1 of 290 ± 25 nm. RDI2 with the 103  $PM_{1.0-0.3}$  nozzle of RDI1 resulted in a similar cut point of RDI1 of 300 ± 20 nm. The 104 slightly larger nozzles than theoretically calculated are the likely reason for the 105 observed increase in the small-end cut point of the  $PM_{1.0-0.3}$  nozzle and thus in 106 reduced particle collection at the C stage.

### 108 Supplement B: Additional tables and figures

- 109
- 110 Table S2. Fit coefficients and Pearson's R values for elements measured with
- 111 the RDI (PM<sub>10-2.5</sub>, PM<sub>2.5-1.0</sub> and PM<sub>1.0-0.3</sub> fractions summed to total PM<sub>10</sub> and
- 112 averaged to 24 hrs) relative to 24-hr  $PM_{10}$  filter measurements. Data points were
- 113 fitted with an orthogonal fit and forced zero intercept.

Element	Fit coefficient	Pearson's R	
Na	1.98	0.87	
Mg	2.19	0.99	
AI	1.79	0.88	
K	0.52	0.78	
Ca	0.78	0.94	
Ti	1.04	0.86	
V	0.17	0.64	
Cr	0.41	0.29	
Mn	1.49	0.91	
Fe	0.93	0.96	
Ni	0.82	0.56	
Cu	1.33	0.94	
Zn	0.71	0.94	
Sr	1.49	0.74	
Мо	2.93	0.86	
Sn	0.43	0.97	
Sb	1.44	0.90	
Ва	1.67	0.91	
Pb	0.41	0.53	



Figure S3. Same as Figure 5, but for NK with mean, median and 25-75<sup>th</sup> percentile trace element concentrations split in four wind direction sectors (N, E, S, W) normalized to the global median concentration per element for PM<sub>10-2.5</sub> (top), PM<sub>2.5-1.0</sub> (middle) and PM<sub>1.0-0.3</sub> (bottom). See section 4.2.2 for the definition of the wind direction sectors.



Figure S4. Same as Figure 5, but for DE with mean, median and 25-75<sup>th</sup> percentile trace element concentrations split in four wind direction sectors (N, E, S, W) normalized to the global median concentration per element for  $PM_{10-2.5}$  (top),  $PM_{2.5-1.0}$  (middle) and  $PM_{1.0-0.3}$  (bottom). See section 4.2.2 for the definition of the wind direction sectors.



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Figure S5. Wind roses as a function of wind direction (angle) and wind speed (diameter) at (a) BT Tower, color-coded by NO<sub>x</sub> concentrations at MR, (b) BT Tower, color-coded by NO<sub>x</sub> concentrations at NK, (c) DE, color-coded by NO<sub>x</sub> concentrations at DE for the RDI sampling periods (see Table 1).



Figure S6. Same as Figure 6, but with mean, median and 25-75<sup>th</sup> percentile kerb increment values for trace elements at MR relative to NK for PM<sub>10-2.5</sub> (top), PM<sub>2.5-</sub>  $_{\rm 1.0}$  (middle) and PM  $_{\rm 1.0-0.3}$  (bottom) split in N, E, S and W wind sectors. See section 4.2.2 for the definition of the wind direction sectors. 



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Figure S7. Same as Figure 7, but for all other elements: P, K, Br, Zn, Pb (regional background); Mg (sea salt), Al, Ca, Ti, Sr (mineral dust); Cl (sea salt), V, Cr, Mn, Ni (traffic-related); Cu, Zr, Mo, Sn, Ba (brake wear). Diurnal cycles of 2-hr median concentrations for  $PM_{10-2.5}$  (left),  $PM_{2.5-1.0}$  (middle) and  $PM_{1.0-0.3}$ (right) at MR, NK, DE split in SW and NE wind sectors. See section 4.2.2 for the definition of the wind direction sectors. Hour of day is start of 2-hr sampling period, so 00:00 means sampling from 00:00 to 02:00.















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Figure S8. Same as Figure 8, but for all other elements: P, K, Br, Zn, Pb
(regional background); Mg (sea salt), Al, Ca, Ti, Sr (mineral dust); Cl (sea salt),
V, Cr, Mn, Ni (traffic-related); Cu, Zr, Mo, Sn, Ba (brake wear). Weekly cycles of

174 2-hr median concentrations for  $PM_{10-2.5}$  (left),  $PM_{2.5-1.0}$  (middle) and  $PM_{1.0-0.3}$ 175 (right) at MR, NK, DE.



179 (Figure S8, continued)









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