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The Balances of Mixing Ratios and Segregation Intensity: A Case Study from the Field
(ECHO 2003)

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Reply to Anonymous Referee #1

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We thank this referee for his very detailed and extremely helpful review. Two main remarks are given followed by a number of specific comments:

I have two main remarks: (1) The observational data used in the research is rather limited. I realized that this measurements are very difficult to be taken, and the data analysis and interpretation is very difficult. The study only used 22 block of 10 minutes. This insures a satisfactory quality to calculate mean statistics, but for higher-order moments is not enough to obtain robust statistics. Have they additional data set that can be used to further support their findings and obtain more reliable statistics? (2) I found the paper with more than 24 figures very lengthy and with some repetitions. I will recommend to the authors to shorten the paper and remove unnecessary figures. By so doing, the paper will be more accessible to potential readers

The first main remark addresses the robustness of statistics for third moments which appear in our equation (5) – (12). The second asks to revise the paper with respect to

- a) some repetitions and
- b) *unnecessary figures*.

A Part of these comments is also given by referee #2. But we separately answer to each of these reviews with reference to each other if we think this is appropriate.

Reply to the main remarks:

It is true that the number of 22 blocks of 10 minutes field data from ECHO 2003 for the further analysis of segregation in the isoprene – OH – system is limited. But, to our knowledge, no comparable additional analysis of such experimental data is published elsewhere up to now.

We described this data set and how it was obtained during the ECHO field study together with first steps of an analysis in detail in our paper in Atmos. Chem. Phys. 10. 6215 – 6235. Initiated by the further discussion on these results in addition with some comments given by

the reviewers (of this paper in ACP10) and some colleagues (see our acknowledgements) we stepped further into the analysis of these field data from the ECHO – campaign 2003.

One of these aspects is to present an analysis of these field data in terms of the theoretical frame also used to model the interactions of turbulence, convection and chemical reactions, e.g. to apply these equations (5) – (12) (and also (1) – (4)) for data analysis. This concept (widely applied in experimental studies of physics and chemistry in the ABL (e.g. Stull, 1988; Sorbjan, 1989; Lenschow, 1982) should provide results for a further analysis of the relative importance of transport / mixing versus chemical reactions on segregation intensity I_s . This procedure also keeps the experimental data rather independent from specific properties of models, and, therefore, allows an intercomparison with results published – for example – by Patten et al. (2001) and Ouwersloot et al. (2001) or – as proposed by this referee – also Vinuesa et al. (2003).

Doing this, first to fourth moments of all quantities are calculated. For the first and second order moments we calculated errors and presented the *uncertainty of the covariance* in I_s and for I_s itself in Figs. 9, 10, 12. We now will add the presentation of errors also for the first and second moments in a supplement and for the terms in Eq. 5 and Eq. 6 in an extended Table 3. As the uncertainty in mean values, standard deviations and variances is significantly smaller than for second and third moments and I_s , we did not present these small deviations in figures. But – as mentioned – we will now add this information on numerical values in the text and (e.g. chapter 3.2.4) with references to the new supplement and an extended table as given below. As an example the revised Table 3 will therefore read as follows:

Table 3

Term	Range	Mean Error (%)
S	$< 6 \cdot 10^{-8}$	$\pm 30 \%$
TPI_k	$6 \cdot 10^{-7}$ to $6 \cdot 10^{-6}$	$\pm 43 \%$
$TPOH_k$	$6 \cdot 10^{-7}$ to $6 \cdot 10^{-6}$	$\pm 48 \%$
A_{1k}	$< 10^{-6}$	$\pm 36 \%$
A_{2k}	$< 2 \cdot 10^{-7}$ ($< 10^{-4}$)	$\pm 50 \%$ ($\pm 30 \%$)
D	$< 10^{-10}$	$\pm 60 \%$
R_{ij}	$< 4 \cdot 10^{-4}$	$\pm 16 \%$

The third moments appear in terms $RES(a)$ and $R_{ij}(b)$. R_{ij} is a sum of two terms (eq. (10)), one the product of the mean concentration of OH times the variance of isoprene and the other (C_{ij}) a sum of triple correlations.

a) RES is a linear combination of two terms composed of products of second order moments and gradients of mean quantities and three terms (A_{1k} , A_{2k} , TT_k) with the divergence of the wind field and of third moments and gradients of second moments.

To explain which terms become important for the final analysis we introduced chapter 4.2. But – concerning the comments of reviewer #1 (but also reviewer #2) – this presentation is revised with respect to

- 1) a more detailed description why a number of terms can be neglected in eq. (5) respectively eq. (9) or finally eq. (12) and
- 2) a further consideration on errors to prove the reliability of our analysis and to describe the influence of uncertainties on the results especially in triple correlations (see above: revised Table 3).

According to the requirements given by both referees, the revised version will have the following structure also to shorten the paper and the number of figures:

1. Introduction
2. Field site and summary of measurements (short summary, details in a supplement; e.g. instruments, calibration, site description, distribution of isoprene sources)
3. Observed relationships between OH and isoprene
4. Balance equation of the mixing ratio (was Chapter 2)
5. Segregation intensity (was Chapter 3)
6. Balance equation for the covariance and segregation intensity (was Chapter 4).
(To shorten the paper, former chapters 4.4 and 5.1 will be mainly shifted to the supplement with Figs. 16 – 18. Only Fig. 19 will remain in the paper together with a related discussion.)
7. Reaction and transport (was chapter 5)
(Fig. 20 will be shifted to the supplement)
8. Summary (was chapter 6)

The additional information on the experiment will cover several aspects like the following:

- 1) During ECHO 2003 all components of the wind vector (u_k) and the temperature T were measured throughout the canopy (30 m) between 2 m and 41 m above ground in 9 heights with a time resolution of 10 Hz (chapter 3.1, Dlugi et al., 2010, ACP10, 6215 - 6235). In addition, 8 psychrometer (with time resolution of about 0.066 Hz for T and specific humidity q) were installed at the same heights except 41 m. Therefore

first up to fourth moments of wind velocity components and temperature and their mixed moments (e.g. also third moments like $\overline{u'_k u'_l T'}$) could be calculated.

One can compare the terms of the interactions of the temperature – velocity field (u_k , T) (and with less time resolution the humidity – velocity (u_k , q) and temperature – humidity – field (T, q)) to the terms in eq. (5), respectively eq. (9), or eq. (12). This is done in a way that q is replaced by isoprene and T by OH. The compounds isoprene and OH could be only measured with higher time resolution at one height of 37 m (7 m above mean canopy height).

But vertical profiles for *mean quantities* with time resolution of about 180s (OH) and 600s (isoprene) are available from measurements of others as cited in chapter 1 of Dlugi et al. – (2010, ACP10, 6215 - 6235). Therefore the vertical gradients of time integrated mean values of u_k , T, q and isoprene (ISO) as well as OH are available if the mixed terms (with spatial gradients) are calculated. In addition the covariances (*fluxes*) for momentum, heat, humidity and isoprene as well as OH could be calculated from the measured data. The results for isoprene, OH and heat are presented in the same reference (Dlugi et al., 2010) together with covariances between T or the *sonic temperature* T_s and mixing ratios e.g. of OH, isoprene and HO₂. This gives some more insight into the influences of transport and emission of BVOCs on OH mixing ratio at the measuring height.

The following remarks will be presented in a supplement:

We often found small negative values of $\overline{T'_s OH'}$ together with small positive values of $\overline{T'_s ISO'}$ or $\overline{T'_s HO_2'}$ (Fig. 9 in Dlugi et al., 2010, ACP10, p. 6228).

This indicates – for example – that warm canopy surfaces tend to emit isoprene which immediately reacts with OH causing a negative correlation between T_s (or T) and OH. This is also shown by the result that a positive (- upward directed -) sensible heat flux is observed together with negative (downward directed) fluxes of OH. The OH – fluxes are only caused by the chemical reactions with isoprene and other compounds (see our Tables 1 and 2). Therefore we used the factor f in terms of OH – reaction with isoprene versus OH – reaction with all others (measured) reactants. We will repeat these findings from the cited reference in chapter 4.3.2 of our paper.

The magnitude of terms TPI_k , $TPOH_k$ and A_{1k} is directly estimated from measured data. This estimate is given in Tab. 3 together with the directly calculated values for term $S \leq 6 \cdot 10^{-8} \text{ ppb}^2 \text{ s}^{-1}$. We did not mention in the text – but will do in a supplement for the revised version – that the percentage change in vertical gradients

of T, q, ISO and OH in the height interval $23m \leq z \leq 41m$ around canopy top ($z=h_c=30m$) is comparable within $\pm 28\%$ during that experimental period. Therefore vertical profiles (and relative changes of local gradients) are comparable. All scalar quantities show maxima inside the canopy in the range $0.77 < z/h_c < 1$ and decreases with increasing height above canopy. Therefore the signs of the mean gradients are the same.

The influences of horizontal gradients of \bar{T} , \bar{q} , \bar{u}_k and \overline{ISO} are estimated from additional measurements at two other towers aligned along mean main wind direction. Results from one of them – the *west-tower* (see Spirig et al. 2005) – describe also the diurnal behavior of isoprene fluxes. OH is controlled only by chemical reactions on a *local* scale of some m^3 as discussed in Dlugi et al. (2010). Therefore the horizontal gradient of OH is purely determined by the horizontal gradient of mixing ratios of chemical compounds acting as sources and sinks as given in Appendix A of the paper under review in eq. (A1).

We found empirically $(\partial \bar{c}_l / \partial x_k) \approx a_l \cdot \sigma_{OH} (\Delta x_k)^{-1}$ with $\Delta x_k = 3 m$ for all reactants (Index *l*) including isoprene. σ_{OH} is given in our Fig. 4 with $0.2 < \sigma_{OH} / \overline{OH} < 0.45$ for OH from Fig. 5. Therefore the calculated mean local vertical gradient of OH (as given in the text) of about $3 \cdot 10^{-5} ppb m^{-1}$ is larger than the mean horizontal gradient of about $1 \cdot 10^{-5} ppb m^{-1}$ but still is of the same order of magnitude.

Conclusions:

- In TPI_k the horizontal gradient has to be multiplied by the horizontal component of the turbulent flux of isoprene which is smaller by one order of magnitude than the vertical component $\overline{w'c_i}$. Therefore, within an uncertainty of less than 10%, only the vertical contribution remains for term TPI_k , e.g. TPI_3 ($k=3$; see chapter 4.1).
- For term $TPOH_k$ the calculated vertical turbulent flux of OH is about a factor of 3 larger than the horizontal contribution and the total sum is – therefore – less than $4 \cdot 10^{-5} ppb m^{-1}$. In the related formulation in line 20 of page 12934 only *the OH – flux* is mentioned without the explanation that here all three terms are added. Therefore we will revise this sentence. But the conclusion $TPI_k \approx TPI_3 \approx TPOH_k$ (see Table 3) still remains.
- The discussion on the *advection of covariance* A_{1k} by the influence of the divergence of the mean flow field is correct. But the term *advection of covariance with the mean flow* A_{2k} in chapter 4.2 (line 4 - 13) needs further discussion. As mentioned in our text we found by the analysis of the data (!)

that $R_{ij} \approx \text{RES}$ can only be fulfilled together with $S \approx 0$ (!) if also the horizontal derivatives in A_{2k} contribute to RES! Therefore, we propose that our description on page 12935 (line 4 - 13) and 12936 (line 1 - 10) will be extended with respect to the findings described in chapters 4.3.3 (with reference also to Fig. 18, 19) and 4.4 but also 5.1 (line 16 - 24).

The mean error given in the revised Table 3 (see above) is larger for triple products than for second order terms like covariances. The spatial derivatives of these quantities are estimated according to mixed moments composed of fluctuations of specific humidity q and temperature T (second moments) and u_k , q and T (third moments). For the error analysis, we replaced T by OH and q by isoprene and assumed that the spatial derivatives are the same. For the error analysis of A_{1k} and A_{2k} the relative errors of q and T are replaced by those of OH and isoprene. The same holds for term TT_k . This allows to estimate the influence of different processes on the covariance $\text{cov}(\text{ISO}, \text{OH})$ and I_s by an order of magnitude estimation (Chapter 4.2 and Appendix B). The finding $\text{RES} \approx R_{ij}$ (Eq.7, 9) is only possible if the horizontal gradients in A_{2k} significantly contribute to the magnitude of this term (see revised Table 3, number in brackets). Many studies assume that these terms are negligible.

b) The dominant term in R_{ij} is the normalized variance of isoprene. This term has a mean error of only 7%. The second term CH_{is} is dominated by term IV3 from Eq. 6. This triple correlation has a mean error of about 64%, but contributes only by about 10-16% to the budget of I_s in Eq. 12. Therefore the mean error of R_{ij} is only 16% (see revised Table 3). (The term C_{ij} is composed only of third order terms. The Eq. (6) will be extended by the notation of terms (I3 to V3 from Fig. 11) and the same notation will be also written in Tab. 4. The numerical values for these terms have very different orders of magnitude (Tab. 4), and, therefore, only terms III3 and IV3 contribute to the numerical values resulting in eq. (6) or finally in Eq.(12). This simplifies the discussion on errors especially for third order moments.)

Finally, a revised paper will also cover the following corrections:

- The English language will be improved.
- The Structure of the paper: will be significantly revised according to the suggestions of Referee 1 and 2 in order to provide an improved guideline to the reader.
- The robustness of results and errors of the results will be discussed in detail (see detailed response to general remarks).
- The size of the paper will be reduced by transferring some material (including figures) into a new Supplement.

Specific comments:

1. *In the introduction there is some confusion on the definition of the Damkohler number first introduced as the time scale of a specific chemical reaction, but later on used as a time scale of a chemically active species. I recommend to clarify it.*

In a revised version we will clarify that in general the Damköhler number Da is introduced *as the time scale of a specific reaction* and that – for the (isoprene + OH) - system within the context of this study – Da is always used with respect to the time scale of a reactant (isoprene) with respect to the active species OH.

2. *Section 2. In Equation (1), and since they focus entirely their research on isoprene and the hydroxyl radical, it is perhaps handier and clearer to substitute c_i and c_j by iso and oh .*

We specified $c_i = \text{isoprene}$ and $c_j = \text{OH}$ in line 19 on page 12922, because the general description in eq. (5) – eq. (12) makes it easier to follow the derivation. In addition, if we refer to the specific comment 14., one can give a more general formulation, because even if $S \approx 0$ is not valid, only an additional term has to be considered – e.g. for NO and O_3 . We will extend the paper by a list with all notations to support the reader.

3. *Section 2.1. (lines 17 on page 12920 to 3 on page 12921). Quoting them: 'variation of only 4.7 % in k_{ij} '. This leads to 4.7 % difference in chemical reaction rate. Therefore, the influence of this variable is of the same magnitude as the effect that is investigated (e.g. Fig. 22). This does not seem a valid justification to use a constant k_{ij} in the analysis.*

a) If k_{ij} varies by 4.7% – e.g. for a value of $k_{ij}[\text{ISO}] \cdot [\text{OH}] = 3 \cdot 10^{-4} \text{ ppb s}^{-1}$ in Fig. 2 – this is an uncertainty of $1.41 \cdot 10^{-5} \text{ ppb s}^{-1}$.

b) For a variation of 4.7% in Fig. 18 a value of $1.5 \cdot 10^{-4} \text{ ppb s}^{-1}$ on the ordinate could be shifted by about $\pm 7 \cdot 10^{-6} \text{ ppb s}^{-1}$, which is about ± 1 mm on the scale chosen in the online version of Fig. 18 in ACP. To compare with the range of ten data points: They cover a range of about 80 mm.

c) I_s itself is only influenced by the application of a mean value of k_{ij} in term RE_{is} . To classify these aspects for the reader, we will add the description of the systematic uncertainty in k_{ij} and its consequence in a new supplement, where we will also discuss the results of error analysis for first to third moments.

4. *Section 2.1. The flux divergences is calculated a residual term and therefore includes contributions of the horizontal advection and horizontal turbulent advection. In order to avoid misunderstandings I will recommend to name it in a different way.*

Yes, both terms need to be named in a revised version.

5. *Section 2.1 (line 27 on page 12921 to lines 3 on page 12922): since the 'flux divergence' is actually a residual term, calculated with the mean reaction rate, it is not surprising that it*

has a linear relation with a high correlation coefficient. This could also indicate that the observations are wrong. For example, when in this analysis, the mean reaction rate would be multiplied by a factor 1000, the 'flux divergence' would be virtual equal to the negative of the mean reaction rate since it is the residual term. This would lead to a linear relation with correlation coefficient 1. The conclusion that 'advection is not significant in our case' can therefore not be drawn on this argument.

The storage term and the flux divergence are of same order of magnitude. The chemical term is smaller than about one order of magnitude. Therefore chemistry influences the flux divergence to a lesser extent than any other mixing or transport process. We therefore revise our statement.

6. Section 3.2.1 (pages 12923, 1 20-23) It will be interesting if a similar relation holds for isoprene.

In Appendix A we describe that OH is locally produced and – itself – is not transported! Therefore a definition of a Damköhler number – as applied by Patton et al. (2001) for isoprene with respect to OH – is not meaningful. Formally OH is not transported but if we calculate an effective τ_t for the volume of $1 - 3 \text{ m}^3$ (where OH is produced and destructed) by the wind velocity we end up with $\tau_t > 3 \text{ s}$ for $\tau_c < 0.2 \text{ s}$ (Dlugi et al., 2010, ACP 10). Therefore $\tau_c \ll \tau_t$, and with $k_{ij} = 2.3 \text{ ppb}^{-1} \text{ s}^{-1}$ and $\overline{ISO} \approx 1 \text{ ppb}$ this leads to

$$\tau_t / \tau_c = D_{iso} > [\text{large number } (> 15)] \cdot 2.3 \text{ ppb}^{-1} \text{ s}^{-1} > 30$$

and OH is in the very fast reacting range, as required (line 20, page 12916).

7. Section 3.2.2. (lines 20-23) Related to the previous point, the authors seem to indicated that entrainment of isoprene (quoting them: " ... some hundred meters above the surface ... ") is an important processes influencing the reactivity behaviour. Van Stratum et al. (AGP 12, 5329-5341) (see Figure 6) presented a budget of reactants where entrainment was a relevant process (at least during the large ABL morning growth). Could they clarify and discuss the role of entrainment in the analysis of the observations?

The information on vertical transport was obtained from local measurements of w at the main tower. At his day (25 July, 2003) convective clouds modulated solar UV-radiation (e.g. photolysis of O_3 and NO_2) and – according to descriptions in literature for comparable situations (e.g. Stull, 1988) – should have influenced ABL characteristics. The ABL morning growth by heat (and moisture) transfer from the surface is therefore modified by the influence of cloud's downdrafts and updrafts moving through the experimental area. At measuring height we found a mixed influence of shear driven and convective turbulence (see our chapter 5.2.2). We – therefore – cannot quantify the role of entrainment from CBL – scaling but only the role of net downward transport in this ABL near the canopy top.

During the measuring campaign several flights with a motor – glider performed by Dr. Bruno Neininger, showed that

a) the isoprene mixing ratio decreased with height above canopy as in Davis (1992) respectively Davis et al. (1994): *J. Geophys. Res.* 99 (D12), 25587 – 25598, and
 b) that the variances of ISO and temperature T also decreased with height as described for T e.g. in Stull (1988). We will add this information and a comparison to results by van Stratum et al. (ACP 12) in the new supplement.

8. *Section 3.2.4 In the comparison with LES results, I was wondering how representative it is to compare surface layer measurements influenced by canopy effect with large-eddy simulations that are mainly representative for mixed-layer properties.*

The results from model calculations and measurements are different and we discuss possible reasons. The paper of Ouwersloot et al. (2011) shows the *horizontal spatial correlation between isoprene and OH* in their Fig. 6. We compare their data given to levels down to $h_z = 0$ m with our correlation coefficients for time averaged quantities. Here we suppose that time averaged quantities and spatially averaged quantities can be compared also for this chemical system (see Shu, 1976; Sorbjan, 1989; Stull, 1988; Panofsky, Dutton (1984): *Atmospheric turbulence, models and methods for engineering applications*, Wiley, N. Y.). It might be that their subscale turbulence parameterization causes a higher correlation (coefficient) near the surface than determined by us from local measurements in some type of a mixed layer (see: Katul et al., 1997; cited in our paper). This can be the case if their pdf's for isoprene are less skewed than found in our measurements (e.g. Fig. 6c, Dlugi et al. (2010), ACP10, 6215 – 6235). But they found this behavior (correlation coefficient $r > 0.85$) throughout the ABL (with height h) up to about $z/h < 0.90$ for homogeneous and heterogeneous conditions.

9. *Section 4.1 (equation 5). The introduction of Equation (5) is very confusing. First they mentioned that the advections terms are neglected and thereafter are included (term $A2k$ for instance). I recommend to introduce it in a systematic and clearer way.*

The advection is given in eq. (5) although others neglect this term in their model studies. We will introduce eq. (5) in a text of a revised version without the restrictions mentioned in line 5 – 6 on page 12930 according to this recommendation.

10. *Equation 10. The use of C_{ij} can bring confusion when comparing with the concentration. I recommend to use another notation.*

We will add a list of all symbols in a revised version also with the definition for C_{ij} . A bold letter **C** with indices ij (\mathbf{C}_{ij}) refers to the chemical term (**C**) with triple correlations between compounds i, j with concentrations c_i and c_j . The definition – by a comparison between eq. (6) and (10) – will be explicitly written in the list of symbols to avoid any misunderstanding.

11. Section 4.1 (equation 5). The introduction of Equation (5) is very confusing. First they mentioned that the advections terms are neglected and thereafter are included (term $A2k$ for instance). I recommend to introduce it in a systematic and clearer way. 12- Section 4.1 (equation 11) Equation (11) does not seem right: the + sign should be a minus. From Eq. (8) there is within \square basically $RES - kij (Cij + cj ci^2)$. This results, after division by $kij ci$ in $- Cij/ci - cj/ci ci^2$. So, the + sign should be a minus. Could they check the consistency of the sign?

Is answered by 9.

12. Section 4.1 (equation 11) Equation (11) does not seem right: the + sign should be a minus. From Eq. (8) there is within \square basically $RES - kij (Cij + cj ci^2)$. This results, after division by $kij ci$ in $- Cij/ci - cj/ci ci^2$. So, the + sign should be a minus. Could they check the consistency of the sign?

Thank you for this remark. Yes, there is a printing error which occurred by the transfer process and could not be corrected by the ACP administration. Therefore both terms have a negative sign. This error will be corrected in a revised version. The calculations of related data and the presentation in Figs. were also checked and are found to be all correct.

13. Section 4.2 (page 12934, line 20). A question that perhaps deserve some attention is if a radical fast compound like OH is transported vertically by turbulent motions. Has the OH-turbulent flux a physical meaning? What is the accuracy of the measurement of the OH-flux?

The OH flux is a net result of the chemical reaction with compounds coming mainly from below to the measuring volume. The calculated flux $\overline{w'OH'} = r_{w,OH} \cdot \sigma_w \cdot \sigma_{OH}$ is mainly determined by $r_{w,OH}$ and to a lesser extent by σ_{OH} . As stated in Dlugi et al. (2010), ACP10, 6215 – 6235, in chapters 3.5 and 5.2.1 the OH – flux is *underestimated* by -37% by the influence of the correlation coefficient. A comparison (not published) for the OH – flux for a 40 minute time interval compared to the 10 minutes interval shows a statistical error of 18%. A maximum loss of 13% for fluxes compared to instruments which sample from the same volume and with 10 Hz (instead of 0.2Hz) is theoretically estimated from these measurements during ECHO 2003 which is smaller than our estimate for the statistical error (18%) and a systematic error of -37% (underestimation of fluxes; Tab. 4 of Dlugi et al. (2010) , ACP10, 6215 – 6235). For the calculation in this paper we did correct for this systematic error! The accuracy of the measurements of w is $\pm 0.007 \text{ ms}^{-1}$ by the procedures described by Dlugi et al. (2010). For the OH – mixing ratios we found a mean relation $OH'/std \text{ dev}(OH) > 4.2$ as error of a single measurement for 0.2 Hz (as given in Dlugi et al. (2010)). We will add this information and a short description of calibration

procedures to measure wind components in the supplement, because also referee 2 asked for such details.

14. Section 4.2 (page 12935, line 20). *Although the large-eddy simulation loses accuracy within the atmospheric surface layer, I think it can be interesting, at least qualitatively, (and for the sake of completeness of the discussion) to include a comparison with the co-variance budget presented by Vinuesa et al. (Tellus 55B, 935-949, 2003) for the NO-NO₂-O₃ triad to determine if the vertical distribution and the order of magnitude of the different contributions of the co-variance equation is similar.*

In this paper we analyze the reaction between isoprene and OH from available measurements (see our *general remarks*). These were *point measurements*! This analysis is done also with respect to an influence of other reactants on the *available OH* for this reaction with isoprene. A comparison with the concept published by Vinuesa et al. (Tellus 55B, 935 – 943, 2003) requires that not only surface fluxes of the reacting compounds, but also entrainment fluxes are available for the calculation of their dimensionless concentrations respectively mixing ratios (see their eq. 9).

As pointed out before (see point 7.), the *CBL – scaling* according to the concept applied also by Vinuesa et al. (2003) should not be applied to the ABL on 25 July 2003 at this site because we had a cloud topped boundary layer. But if we calculate z_i - despite the observed conditions - we need a CBL – height of $z_i \approx 1500 \text{ m}$ e.g. to compare with observed variances of isoprene according the concept applied in their chapter 6 for a bottom- up transported compound for $c_b = \text{ISO}$.

The bottom of clouds was estimated to be between 650 m at 10:00 CET and 800 m at 13:30 CET and their vertical extent was about 200 – 400 m. Therefore their top was about 1000 m – 1200 m. For this height the calculated variances of isoprene were only in agreement with observed values if the corresponding isoprene entrainment flux would be 40% of the surface flux. Compared to findings by B. Neininger during ECHO 2003 and the results published by Davis (1992, 1994) this is rather unlikely (see: Comment 7). Therefore, albeit vertical *pumping* by clouds may modify the vertical profiles of scalars and their variance in a comparable way as done by convective transport (in the cloud free (!) CBL), the comparison is rather qualitative.

In any case, OH is not transported and a dimensionless concentration scale for OH cannot be justified because the OH – flux is only a result of its local chemical reactions! Therefore for the available set of data we cannot perform a robust comparison based on our data and the set of equations published by Vinuesa et al. (2003).

On the other hand they calculate segregation also for a chemical mixture including a compound RH which has a reaction rate with OH with $k = 1.8 \text{ ppb}^{-1} \text{ s}^{-1}$ not far from the rate constant $k_{ij} = 2.3 \text{ ppb}^{-1} \text{ s}^{-1}$ for (ISO + OH). They obtained an average value

of the intensity of segregation for the CBL between $0.2z_i$ and $0.8z_i$ of $I_s = -0.17$ (see their Table 3) for the *complex chemistry* case from their LES model runs. Although the conditions are different we will cite and discuss their results and add this information also to Fig. 22. Their second value of $I_s = -0.23$ is obtained from a parameterization if the covariance (in our eq. (3)) is replaced by our eq. (4) and using results of their LES model. This higher value is compatible to results with a higher correlation coefficient of about 0.95.

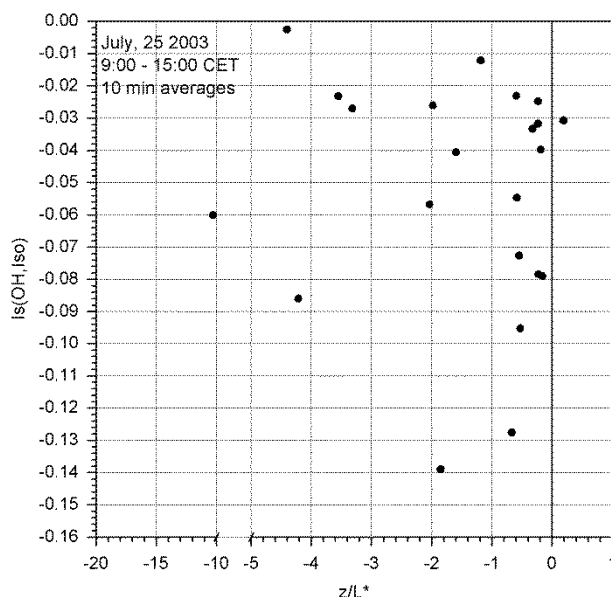
15. *Connected to the previous comment, the diffusion term seems to have a different meaning and order of magnitude in the research presented by Patton et al. (2001) and Vinuesa et al. (2003) (see for instance Figure 7). In the LES studies, the term is representing a dissipation at the smaller scales and it is comparable in order of magnitude to the other terms in the co-variance equation (gradient production, chemistry or turbulent transport). In turn, in this observational research, this term represent a molecular diffusion term and it is smaller compared to the other terms (see discussion at lines 23-25 at page 12935). Could the authors comment on this differences?*

We used the equation with molecular diffusion term D which is important at the boundaries because our measurements were near boundaries (canopy, tower). They disregard this term in the volume of the flow because there it is small compared to others. Their term D in the LES studies is composed of the contributions of *subgrid scale dissipation*, which is still turbulent dissipation below the spatial scale they resolved (for example 1 – 10 m or larger).

For this spatial scale, *turbulent diffusivity* is comparable to values larger than about $10^{-2} \text{ m}^2 \text{ s}^{-1}$ compared to $D \approx 10^{-5} \text{ m}^2 \text{ s}^{-1}$ for molecular diffusion in our Eq.5. Therefore their Term D is of influence. This influence correctly increases with decreasing distance to the boundary (as shear driven turbulence intensity increases).

16. *Section 5.2.2. In view of the completeness of the research and the temporal evolution of the atmospheric stability, it is perhaps interesting to show a figure of I_s as a function of a stability parameter like z/L or the Richardson gradient number.*

We did a complete analysis on the behavior of $\text{cov}(\text{ISO}, \text{OH})$, I_s and other quantities like variances, skewness and kurtosis but also mixed third moments as function of stability parameter. The requirement (also by Reviewer #2) is that we remove *unnecessary figures*. If we add this information $-I_s = f(z/L)$ or $-I_s = f(R_i)$ we will therefore add this figure to the supplement where we also shortly discuss this result. No clear dependence on z/L^* for I_s is visible. This may be caused also by the finding that the mixing processes above *tall* canopies in general do not scale with standard surface layer scaling parameter schemes. In this layer phenomena as in a mixed layer are observed and scaling might be better with mixing layer height and u^* (e.g. Katul et al., 1997; Katul et al., 1998: Journal Applied Meteorol., 37, 1533 – 1546).



17. General comment on figures and data treatment. In view of the uncertainties associated to the simultaneous measurements of turbulence and fast atmospheric compounds, I will recommend the use of error bars in all the figures.

We follow this recommendation and give the required information in the revised Table 3 and in Figures of the revised version.

18. Figure 22 is a very good summary of the observational results of I_s combined with the buoyancy surface forcing. In order to complete and integrate with the numerical studies, it is perhaps interesting to include some representative results reported by Patton et al. (2003) and additional point for I_s under homogeneous surface conditions. The I_s value from Ouwersloot et al. (2011) in Fig. 22 and line 28 of page 12947 is indeed for a numerical simulation with $\Delta H_v = 0$, but this experiment considers still differences in isoprene emissions (0.7 ppb m/s) and is therefore NOT representative for homogeneous surface conditions. To truly compare for homogeneous conditions, use their HOM experiment: $I_s = -0.070$. As can be expected, this result also fits better with the other values in Fig. 22. It is possible to combine both values, explaining the difference.

Yes, we will present now both values and explain the differences. But we will also point out here that the ECHO – site is not a homogeneous site! Therefore we used their I_s value for $\Delta H_v = 0$ instead of the value for HOM.

But in a revised version we will also add in the supplement additional information on the distribution of isoprene sources around the main tower.

19. Appendix A: f is not the relative reaction rate for OH consumption by isoprene compared to total OH consumption, but compared to OH consumption by other compounds. However, it is stated (line 22 of p 12953) that f is an estimation to calculate the relative isoprene sink from the reaction with OH, so it would make more sense to calculate f as

the relative reaction rate for OH consumption by isoprene compared to total OH consumption. Why this discrepancy?

The formulation in line 22 (page 12953) is misleading and should better read: “... f to calculate the isoprene sink relative to the sink by other compounds for the reaction with OH”.

We have chosen this formulation of f because we found a better dependence of I_s on OH_{mod} than on $OH_{measured}$ (Fig.6). In addition, I_s and the correlation coefficient better follow the term $ISO \cdot OH_{mod}$ for all categories of f (see our Fig.24 and the 2 following figures here). We will refer to these results in a supplement of the revised version.

