

# Supplement to First direct measurements of formaldehyde flux via eddy covariance from a coniferous forest

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## S1 HCHO Permeation Tube Calibration

The FTIR gas cell pressure and temperature were held near ambient. Spectra were acquired and integrated for 1 hr at 1 cm<sup>-1</sup> resolution. The concentration of formaldehyde (HCHO) in the calibration mixture was quantified using HITRAN absorption line lists (Rothman et al., 2005) and a multi-component least squares fitting algorithm (Griffith, 1996). The C-H stretch region of 2620-2920 cm<sup>-1</sup> was chosen as the fitting region. The permeation rate determined via FTIR spectroscopy was found to be significantly lower (~50%) than the rate determined via mass loss over time.

## S2 Error in Flux Measurements

Error resulting from instrument response time was estimated by:

$$\frac{\overline{\Delta w' HCHO'}}{\overline{w' HCHO'}_{meas}} = 2\pi f_m \tau_{HCHO} \quad (S1)$$

where  $f_m$  is the frequency maximum of the weighted cospectrum (Fig. 3a) and  $\tau_{HCHO}$  is the instrument response time, determined from the decay observed upon introducing a sharp concentration change at the front of the inlet (Horst, 1997). The measured instrument response time of ~0.28 s resulted in an estimated error of  $\leq 5\%$ . Error from instrumental noise as a result of the discrete method of detection (i.e. shot noise) was estimated by the following equation:

$$\frac{\overline{\Delta w' HCHO'}}{\overline{w' HCHO'}_{meas}} = \frac{\sigma_w^2 \sigma_{HCHO}^2}{f_s T} \quad (S2)$$

where  $\sigma_x^2$  is the measurement variance in  $x$ ,  $f_s$  is the sampling frequency, and  $T$  is the length of the sampling period (Lenschow and Kristensen, 1986; Ritter et al., 1990). This typically resulted in an error of  $< 4\%$ . Error due to the separation between the HCHO inlet and sonic anemometer was determined by the following cospectral transfer function:

$$T_s(f) = e^{-9.9 \left( \frac{fs}{U} \right)^{1.5}} \quad (\text{S3})$$

where  $f$  is the cospectral frequency,  $s$  is the sensor separation, and  $U$  is the wind speed (Moore, 1986). During BEACHON-ROCS, the separation was  $\sim 0.5$  m and wind speeds typically varied from 0.5 to 4.5  $\text{m s}^{-1}$ , leading to errors ranging from 0.84% to 6.6%. Error resulting from dampening inside the inlet was predicted by the following cospectral transfer function:

$$T_s(f) = e^{-\frac{(2\pi f)^2 \Lambda L a}{u^2}} \quad (\text{S4})$$

where  $f$  is the cospectral frequency,  $\Lambda$  is the attenuation coefficient,  $L$  is the length of tubing,  $a$  is the radius of the tubing inner diameter, and  $u$  is the flow rate through the inlet (Massman, 1991). Dampening was considered for both the main inlet line ( $\Lambda = 1$ ,  $u = 18.7 \text{ m s}^{-1}$ ,  $L = 38.5 \text{ m}$ ) and the internal instrument tubing ( $\Lambda = 20$ ,  $u = 3.5 \text{ m s}^{-1}$ ,  $L = 1 \text{ m}$ ), resulting in a total error of 1.3%. Error resulting from the lag time calculation was calculated using the error in the fitted linear trends. Fluxes were calculated for the lag time range of the  $1\sigma$  error in the trends, then the standard deviation over these fluxes were taken to be the lag contribution to the error. Median daytime error due to lag time was  $\sim 20\%$ .

### S3 HCHO Production via $\text{CH}_3\text{O}_2$ Radical

PA concentrations were calculated with a steady-state model, based on observations in a similar coniferous forest, which predicts the PA steady state concentration ( $[PA]_{ss}$ ) by the steady-state equation:

$$[PA]_{SS} = \frac{P_{MVK} + P_{MACR} + P_{CH_3CHO} + P_{MGLY} + P_{BACE} + P_{PAN}}{L_{NO_2} + L_{NO} + L_{HO_2} + L_{RO_2}} \quad (\text{S5})$$

However, this equation simplifies significantly upon neglect of isoprene oxidation products, as isoprene has been observed to be low at this site (Kim et al., 2010):

$$[PA]_{SS} = \frac{k_{acetal-OH}[CH_3CHO][OH] + k_d[PAN]}{k_{PA\cdot NO_2}[NO_2] + k_{PA\cdot NO}[NO] + k_{PA\cdot HO_2}[HO_2] + k_{PA\cdot RO_2}[RO_2]} \quad (\text{S6})$$

Reactions of PA radical with NO and  $RO_2$  have a unity yield of methylperoxy radical ( $\text{CH}_3\text{O}_2$ ) (Atkinson et al., 2006), while reaction with  $HO_2$  has a 40% yield through methyl hydrogen peroxide (Hasson et al., 2004; Jenkin et al., 2007; Dillon and Crowley, 2008).  $\text{CH}_3\text{O}_2$  has a net unity yield of HCHO via reactions with NO,  $RO_2$  (Tyndall et al., 2001; Atkinson et al., 2006), and  $HO_2$  (Fried et al., 1997), which permits us to assume all  $\text{CH}_3\text{O}_2$  radicals quickly react to form HCHO. This leads to a production rate of HCHO from PA radicals of:

$$P_{HCHO}^{PA} = P_{CH_3O_2}^{PA} = [PA]_{SS} \cdot (k_{PA\cdot NO}[NO] + k_{PA\cdot RO_2}[RO_2] + 0.4 \cdot k_{PA\cdot HO_2}[HO_2]) \quad (\text{S7})$$

Similarly, OH-initiated oxidation of methane produces  $\text{CH}_3\text{O}_2$  radicals (and thus HCHO) with unity yield. Methane concentrations were assumed to be constant at 1.7 ppm<sub>v</sub>.

#### S4 Aerodynamic and Laminar Sublayer Resistance

$R_a$  is the aerodynamic resistance, the resistance to transfer between the measurement height and the surface (Monteith, 1965).

$$R_a = \frac{\bar{u}(z-d)}{u_*^2} - \frac{\Psi_H(\xi) - \Psi_M(\xi)}{k \cdot u_*} \quad (\text{S8})$$

where  $z$  is measurement height A.G.L.,  $d$  is the displacement height ( $2/3 \times h$ ),  $\bar{u}(x)$  is the wind speed at height  $x$ ,  $k$  is the von Karman constant ( $\sim 0.4$ ), and  $\Psi_H$  and  $\Psi_M$  are the sensible heat and momentum integrated stability corrections (Dyer, 1974), which are a function of the stability parameter  $x_i = (z-d)/L$ , where  $L$  is the Obukhov length. Typical values of  $R_a$  range from  $8 \text{ s m}^{-1}$  at mid-day to  $30 \text{ s m}^{-1}$  at night.  $R_b$  is the laminar sublayer resistance, the resistance to molecular diffusive transport through the viscous layer surrounding leaf surfaces (Jensen and Hummelshoj, 1995, 1997).

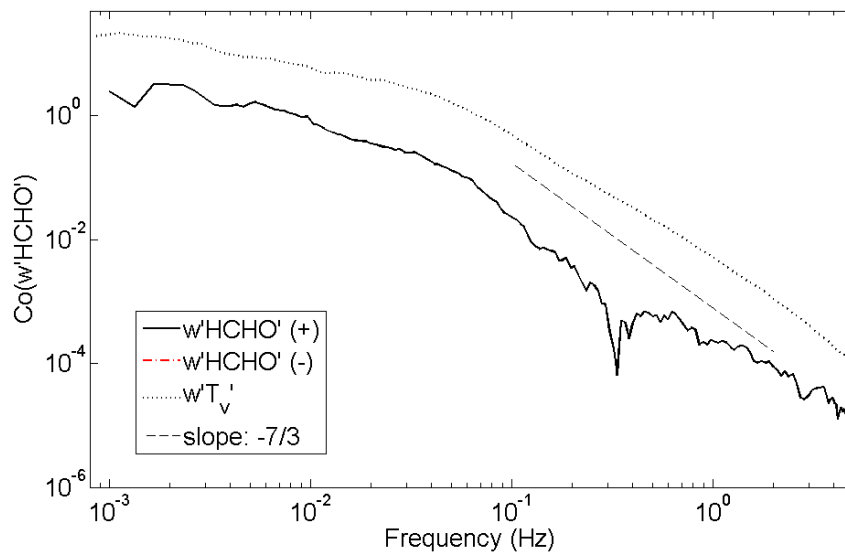
$$R_b = \frac{\nu}{u_* \cdot D_{HCHO}} \cdot \left[ \frac{100 \cdot l \cdot u_*}{LAI^2 \cdot \nu} \right]^{1/3} \quad (\text{S9})$$

$\nu$  is the pressure-corrected kinematic viscosity of air ( $1.7 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$ ),  $D_{HCHO}$  is the pressure-corrected diffusion coefficient for HCHO ( $1.7 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$ ) (Wesely, 1989; Massman, 1998), and  $l$  is the “characteristic length scale”, or thickness, of a pine needle (1 mm). Typical values of  $R_b$  range from  $16 \text{ s m}^{-1}$  at mid-day to  $32 \text{ s m}^{-1}$  at night.

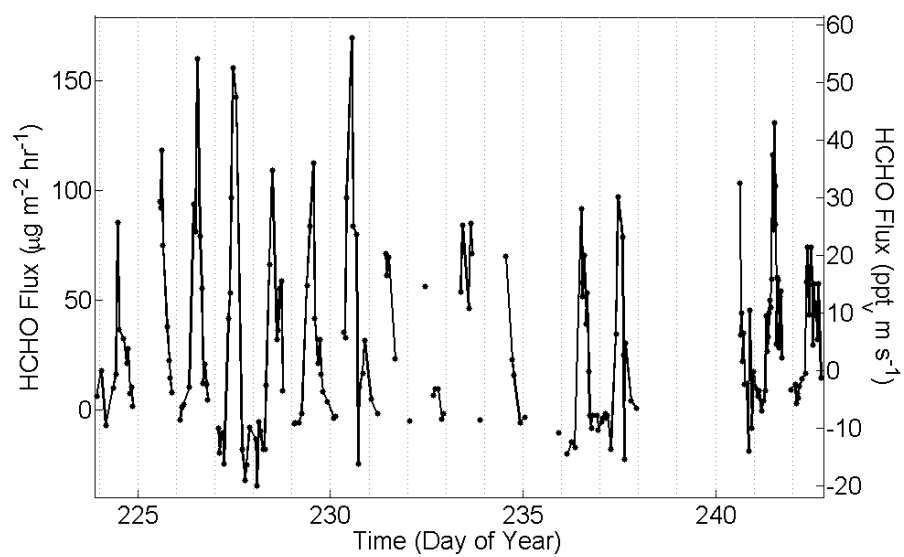
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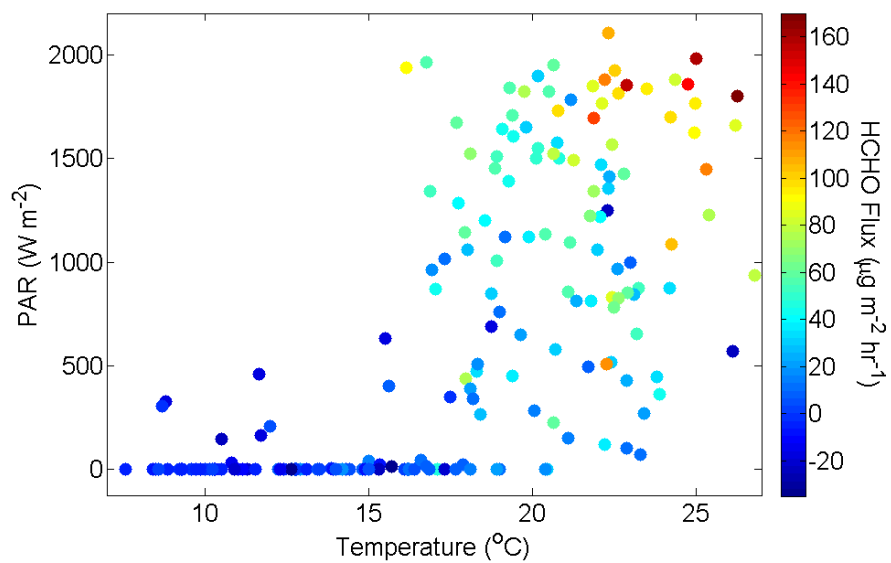
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**Fig. S1.** Average cospectra of HCHO and virtual temperature with vertical wind speed during half-hour periods from 10 AM to 2 PM over entire measurement period. To compensate for noise, cospectra were binned into 200 bins spaced equally in frequency, and each bin was averaged. The red dot-dashed region in  $w'HCHO'$  denotes negative contributions to flux. The positive  $w'HCHO'$  points designate a positive covariance, whereas negative  $w'HCHO'$  points designate negative covariance .



**Fig. S2.** Time series of HCHO flux over entire flux measurement period (11 - 30 August). Data has been corrected for unstationary conditions.



**Fig. S3.** Temperature and PAR dependence of HCHO flux during BEACHON-ROCS.



**Table S1.** Comparison of detection limits and time resolution of HCHO measurement techniques.

Technique	$3\sigma$ Detection Limit	Reference
Quantum Cascade Laser Spectroscopy	$\sim 96$ ppt <sub>v</sub> in 1 s	McManus et al. (2010)
Tunable Diode Laser Spectroscopy	$\sim 180$ ppt <sub>v</sub> in 1 s	Weibring et al. (2007)
Proton Transfer Reaction-Mass Spectrometry	300 ppt <sub>v</sub> in 2 s	Wisthaler et al. (2008)
Hantzsch Derivatization	75 ppt <sub>v</sub> in 1 min	Wisthaler et al. (2008)
Madison Ti:Sapphire LIF	$\sim 51$ ppt <sub>v</sub> in 1 s	Hottle et al. (2009)
Madison FILIF (field)	$\sim 300$ ppt <sub>v</sub> in 1 s	this work
Madison FILIF (laboratory)	$\sim 25$ ppt <sub>v</sub> in 1 s	this work

**Table S2.** Chemical production and loss rates and yields for zero-dimensional box model. All rate constants have units of  $\text{cm}^3\text{molec}^{-1}\text{s}^{-1}$  unless otherwise specified.

Reaction	HCHO Yield	Yield Reference	Rate Constant T = temperature (K)	Rate Constant Reference
MBO + OH	0.33	a	$8.2 \times 10^{-12} \times e^{610/T}$	d
$\alpha$ -pinene + OH	0.19	b	$1.2 \times 10^{-11} \times e^{440/T}$	d
$\beta$ -pinene + OH	0.51	c	$7.89 \times 10^{-11}$	b
Methanol + OH	1.0	d	$2.85 \times 10^{-12} \times e^{-345/T}$	d
3-carene + OH	0.28	c	$8.68 \times 10^{-11}$	b
Acetaldehyde + OH	1.0	d	$4.4 \times 10^{-12} \times e^{365/T}$	d
CH <sub>4</sub> + OH	1.0	d	$1.85 \times 10^{-12} \times e^{-1690/T}$	d
PAN → PA + NO <sub>2</sub>	-	-	(*) $k_0 : 4.9 \times 10^{-3} \times e^{-12100/T}$ (*) $k_\infty : 5.43 \times 10^{16} \times e^{-13830/T}$ (**) $F_c : 0.31$	d
PA + NO <sub>2</sub>	-	-	(*) $k_0 : 2.7 \times 10^{-28} \times (T/300)^{7.1}$ (*) $k_\infty : 1.2 \times 10^{-11} \times (T/300)^{0.9}$ (**) $F_c : 0.31$	d
PA + NO	1.0	d	$7.5 \times 10^{-12} \times e^{290/T}$	d
PA + HO <sub>2</sub>	~0.4	e,f,g	$5.2 \times 10^{-13} \times e^{980/T}$	d
PA + RO <sub>2</sub>	1.0	d	$2.0 \times 10^{-12} \times e^{500/T}$	d
MBO + O <sub>3</sub>	0.5	a	$1.0 \times 10^{-17}$	d
$\alpha$ -pinene + O <sub>3</sub>	0.28	c	$6.3 \times 10^{-16} \times e^{-580/T}$	d
$\beta$ -pinene + O <sub>3</sub>	0.65	c	$1.5 \times 10^{-17}$	b
3-carene + O <sub>3</sub>	0.25	c	$3.61 \times 10^{-17}$	b
HCHO + OH	-	-	$5.4 \times 10^{-12} \times e^{135/T}$	d

a. Carrasco et al. (2007)

b. Atkinson and Arey (2003)

c. Lee et al. (2006)

d. Atkinson et al. (2006)

e. Hasson et al. (2004)

f. Jenkin et al. (2007)

g. Dillon and Crowley (2008)

\* Units:  $\text{s}^{-1}$

\*\* Unitless

**Table S3.** Noon model case results in  $\mu\text{g m}^{-2} \text{hr}^{-1}$  by species.

Species	Base	VOC-I	E350	VOC-II
<i>Production:</i>				
Litter Emission	8.43 (25%)	8.43 (7%)	8.43 (6%)	8.43 (15%)
MBO + OH	8.35 (24%)	83.5 (74%)	8.35 (6%)	8.35 (14%)
PPine Emission	4.24 (12%)	4.24 (4%)	105 (78%)	4.24 (7%)
PA	3.99 (12%)	3.99 (4%)	3.99 (3%)	3.99 (7%)
CH <sub>4</sub> + OH	2.76 (8%)	2.76 (2%)	2.76 (2%)	2.76 (5%)
CH <sub>3</sub> CHO + OH	2.10 (6%)	2.10 (2%)	2.10 (2%)	2.10 (3%)
CH <sub>3</sub> OH + OH	1.16 (3%)	1.16 (1%)	1.16 (1%)	1.16 (2%)
$\beta$ – pinene + OH	0.67 (2%)	0.67 (1%)	0.67 (<1%)	6.69 (12%)
$\alpha$ – pinene + OH	0.61 (2%)	0.61 (1%)	0.61 (<1%)	6.11 (11%)
Other MT + OH	0.49 (1%)	0.49 (<1%)	0.49 (<1%)	4.93 (9%)
MBO + O <sub>3</sub>	0.48 (1%)	4.80 (4%)	0.48 (<1%)	0.48 (1%)
3 – carene + OH	0.33 (1%)	0.33 (<1%)	0.33 (<1%)	3.26 (6%)
Other MT + O <sub>3</sub>	0.32 (1%)	0.32 (<1%)	0.32 (<1%)	3.17 (6%)
$\alpha$ – pinene + OH	0.14 (<1%)	0.14 (<1%)	0.14 (<1%)	1.41 (2%)
$\beta$ – pinene + O <sub>3</sub>	0.04 (<1%)	0.04 (<1%)	0.04 (<1%)	0.40 (1%)
3 – carene + O <sub>3</sub>	0.03 (<1%)	0.03 (<1%)	0.03 (<1%)	0.30 (1%)
<i>Loss:</i>				
Dry Deposition	-19.30 (69%)	-22.37 (72%)	-27.19 (76%)	-19.30 (69%)
Photolysis	-4.90 (17%)	-4.90 (16%)	-4.90 (14%)	-4.90 (17%)
OH	-3.84 (14%)	-3.84 (12%)	-3.84 (11%)	-3.84 (14%)