

Abstract

Thermal-optical evolved gas analysis (TOEGA) is a conventional method for classifying carbonaceous aerosols as organic carbon (OC) and elemental carbon (EC). Its main source of uncertainty arises from accounting for pyrolyzed OC (char), which has similar behavior to the EC originally present on the filter. Sample composition can also cause error, at least partly by complicating the charred carbon correction. In this study, lab generated metal salt particles, including alkali (NaCl, KCl, Na₂SO₄), alkaline-earth (MgCl₂, CaCl₂) and transition metal salts (CuCl₂, FeCl₂, FeCl₃, CuCl, ZnCl₂, MnCl₂, CuSO₄, Fe₂(SO₄)₃), were deposited on a layer of diesel particles to investigate their effect on EC and OC quantification with TOEGA. Measurements show that metals reduce the oxidation temperature of EC and enhance the charring of OC. The split point used to determine classification of EC vs. OC is more dependent on changes in EC oxidation temperature than it was on charring. The resulting EC/OC ratio is reduced by 0–80% in the presence of most of the salts, although some metal salts increased reported EC/OC at low metal to carbon ratios. In general, transition metals are more active than alkali and alkaline-earth metals; copper is the most active. Copper and iron chlorides are more active than sulfates. The melting point of metal salts is strongly correlated with the increase of OC charring, but not with the reduction of EC oxidation temperature. Other chemistry, such as redox reactions, may affect the EC oxidation. A brief discussion of possible catalytic mechanisms for the metals is provided.

1 Introduction

Ambient aerosols are composed of inorganic species, such as sulfate, nitrate, ammonium, trace metals, and carbonaceous material consisting principally of OC and EC (also known as black carbon, BC). Carbonaceous materials make up a large fraction of ambient aerosols (Zhang et al., 2007). OC and EC play important roles in climate, health and other atmospheric processes, thus there is great interest in quantifying OC

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and EC in aerosol particles.

Carbonaceous aerosol ranks as some of the most difficult aerosol to measure, with uncertainties of at least 30–50% (e.g., Huebert and Charlson, 2000). OC and EC are usually determined by thermal-optical protocols. One such protocol is the National Institute of Occupational Safety and Health (NIOSH) method 5040 with correction by thermal-optical transmission (TOT) (Chow et al., 2001; NIOSH, 1999). Briefly, a filter sample is exposed to a prescribed temperature protocol first in an inert (helium, He) environment and then in an oxidizing (He/oxygen mixture, He/O₂) atmosphere. Ideally, OC volatilizes in the He-mode of the analysis, while EC combusts in the oxidizing atmosphere at high temperatures. A major complication is that a fraction of the OC chars, or pyrolyzes, in the inert mode of the analysis. This pyrolyzed organic carbon (POC) requires an oxidizing atmosphere to evolve off the filter, similar to EC. To account for pyrolysis, the transmittance of laser light through the sample is monitored and used to split the total carbon (TC) into OC and EC. The OC-EC split is generally defined as the point where the transmittance level returns to its initial level after a transient reduction of laser response due to OC charring. This point frequently intersects a large peak, so that a shift in the peak by a few seconds in either direction has a significant impact on the carbon mass allocated as OC or EC.

A handful of recent studies have suggested the sample composition, either organic or inorganic, can influence the evolution of carbon from filters, causing errors in TOEGA (Peterson et al., 2001). EC in aged and remote aerosols has been observed to evolve at considerably lower temperatures (450–550 °C instead of 550–700 °C) than in urban aerosols (Huffman, 1996). EC in ambient aerosols evolved at 30–40 °C lower temperatures than in highway vehicle samples (Turner and Hering, 1990). EC in biomass-burning aerosols was also oxidized at lower temperatures compared to diesel particles (Novakov and Corrigan, 1995a). Mixing ambient aerosols with tunnel exhaust can lower diesel soot oxidation temperatures by 100–150 °C, a phenomenon attributed to the non-carbonaceous constituents of particles (Turner and Hering, 1994; Grosjean et al., 1994). A suite of laboratory studies demonstrated that small amounts of many

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2 Experimental

2.1 Diesel exhaust particles

DEP were produced by a four-stroke, air-cooled direct injection 4.8-kW diesel generator (L70V6, Yanmar Corporation) at maximum load. The generator has been verified to produce particles that are well within the range observed for particle emissions from heavy duty diesel trucks in terms of OC and EC content, primary particle size, size distribution and fractal dimension of agglomerates (Chung et al., 2008). The generator was run on California #2 ultra low sulfur fuel (less than 15 ppmw sulfur), and was allowed to warm up for 10 min prior to collection of samples. DEP were collected 10 cm away from the generator's exhaust outlet without dilution, onto pre-fired quartz filters (47 mm, Pall Life Sciences) at a flow rate of 30 L min⁻¹ for 1–2 min. Blanks were collected for 4±1 s. One set of diesel samples was used as diesel controls; ambient or metal particles were collected on top of the other samples.

2.2 Ambient aerosols

Ambient total suspended particles (TSP) were collected on the roof of the math sciences building on the campus of University of California at Los Angeles (UCLA) during 5–7 December 2007. TSP was collected onto Teflon (47 mm, Pall Life Sciences), quartz, and pre-DEP loaded quartz filters simultaneously, at 30 L min⁻¹ for 2 to 6 h. The Teflon filters were used for mass and metal analysis of ambient aerosols. The clean and pre-DEP loaded quartz filters were used for OC and EC analysis of the ambient and the mixed ambient/diesel aerosols, respectively.

2.3 Metal salt particles

Thirteen 2.5 wt% metal salt solutions (NaCl, KCl, MgCl₂, CaCl₂, FeCl₂, FeCl₃, CuCl₂, CuCl, MnCl₂, ZnCl₂, Na₂SO₄, CuSO₄, Fe₂(SO₄)₃) were prepared by dissolving the metal salt powders (Acros, Sigma, or Alfa Aesar, purity >98%) in purified de-ionized

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water (18 M Ω). Metal salt solutions were aerosolized into a 2 m³ Teflon chamber for 30 min at a flow rate of 3.5 L min⁻¹. Prior to an experiment, the chamber was flushed with purified air for 1 h, and then filled with purified air for about 15 min. The resulting background particle concentration was <20 cm⁻³. The resulting metal salt particles were collected onto pre-DEP loaded quartz filters, usually at 30 L min⁻¹ for 10–120 s. The sampling time was determined by the desired metal to carbon mass ratio (M/C), typically in the 0.01–0.5 range, similar to that in ambient aerosols (Krudysz et al., 2008; IMPROVE, 2010). Metal control filters were created by collecting chamber aerosol onto pre-fired quartz filters at 30 L min⁻¹ for 47–540 s. The mass concentrations and size distributions of metal aerosols were monitored with a scanning mobility particle sizer (SMPS, 3081 DMA, 3100 CPC, TSI).

2.4 OC and EC analysis

OC and EC were quantified for 1 cm² punches of the quartz filter samples with a thermo-optical evolved gas analyzer (Sunset Lab Inc.) using the NIOSH 5040 procedure (NIOSH, 1999; Birch and Cary, 1996). Carbon evolving from the filter is oxidized to carbon dioxide, and then reduced to methane for detection with a flame ionization detector (FID). A red laser (670 nm) is used to monitor transmittance through the filter. To account for changes in the laser transmittance as the instrument and filter go through its temperature cycle, eighteen diesel samples were first analyzed for OC/EC, allowed to cool, and then re-analyzed. The resulting transmittance curves were averaged, and the resulting “background” curve was used to correct all sample transmittance curves, by taking the natural log of the transmittance through the sample at a given time point relative to the background trace at the same time point ($\ln I_{\text{sample}} - \ln I_{\text{avg.blank}}$). The resulting corrected sample trace was then smoothed with a nine-point moving average. The split point is set as the time at which the corrected transmittance returns to its initial maximum value. This adjusted split time is smaller than, but highly correlated with, the split time set by the instrument software (adjusted split time = $0.83 (\pm 0.01) \times$ software

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split time, $R^2=0.41$, $p < 10^{-16}$). The adjusted split time (367 ± 56) has a similar standard deviation as the software split time (439 ± 50). At the end of each analysis a 5% CH_4/He standard is injected for calibration. The measured carbon fractions in $\mu\text{g cm}^{-2}$ from the analyzer output were converted to total mass in the filter (μg). We observe that all of the trends reported in this contribution are preserved if we use the output provided by the instrument software.

Most volatilized carbon evolves in the He phase while the temperature is heated stepwise to 250 (90 s), 500 (60 s), 650 (60 s) and 850 °C (90 s), producing four OC fractions. The 98% He/2% O_2 atmosphere is introduced after the oven cools to 600 °C, and oxidized carbon evolves at 650 (30 s), 750 (30 s), 850 (60 s) and 940 °C (120 s), producing three EC fractions. The carbon that evolves in the oxidizing atmosphere until the transmitted light returns to its initial value is termed pyrolyzed organic carbon (POC). POC is subtracted from the sum of EC fractions to obtain the EC concentration. OC is the sum of four OC and the POC fractions. TC is the sum of OC and EC. OC and EC in blanks were $18.6\pm 19.8\%$ and $2.0\pm 4.8\%$ of those in samples, respectively.

2.5 BC analysis

BC content on the pre-DEP loaded quartz filters was characterized by a dual-wavelength (370 and 880 nm) optical transmissometer (Model OT21, Magee Scientific). The relationship between the optical attenuation and the BC concentration (in $\mu\text{g cm}^{-2}$) is given by $\text{ATN}=\sigma \text{BC}$, where $\text{ATN}=-100\ln(I/I_0)$, I and I_0 are the light intensities transmitted through the loaded and blank filters, and σ represents the mass absorption coefficient of BC. We used $16.6 \text{ m}^2 \text{ g}^{-1}$ for σ as suggested by the manufacturer, although the choice of σ is not consequential since it was used to infer relative EC in metal loaded samples.

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2.6 Metal analysis

Quartz (after OC/EC analysis) or Teflon filters were immersed in 10 mL 5% HNO₃ for 24 h. The resulting solutions were filtered and analyzed for metals by inductively coupled plasma atomic emission spectroscopy (ICP-AES, Perkin-Elmer, TJA Radial Iris 1000). A multiple elements stock solution, containing 10 or 20 ppm of each element was prepared from individual element standards (CPI Intl.). 0.01–1.2 ppm element standards were prepared by serial dilution of the stock solution. Zn, Cu, Fe, K, Mg, Mn, Ca and Na in blanks were about 1.4, 1.2, 0.5, 1.0, 0.3, 0.1, 29 and 3.5% of those in samples, respectively.

3 Results

3.1 Effect of ambient aerosols on TOEGA analyses of diesel particles

Table 1 shows the metal and carbon content of ambient TSP samples. The composition was quite variable from day to day; metals and carbon comprised 20–45% and 10–20% of the total particle mass, respectively. The most abundant metals were Na, followed by Ca, Mg and Fe, with K, Si, Cu, Al and Zn also contributing significantly. The metal concentrations, as well as the fraction of carbon and other material in these aerosols are well within the ranges observed by other investigators (Krudysz et al., 2008; IMPROVE, 2010), except for the high sodium levels. High sodium is expected due to the sampling site's close proximity to the coast, and the sea breeze present on sampling days.

Ambient TSP was collected on a layer of diesel particles to investigate the effects of ambient aerosols on the OC/EC analysis of diesel particles by TOEGA. Figure 1 shows the TOEGA results of ambient TSP, diesel, and the two combined for the 5 December sample set. The addition of ambient TSP to diesel particles did not affect the carbon volatilization profile during the inert phase (<320 s); the resulting carbon evolution pro-

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file was a weighted average of the ambient and diesel carbon evolution profiles. In the oxygen phase (>320 s), the small amount of ambient aerosol shifted the oxidation temperature of the low volatility carbon (EC) in diesel particles 180°C earlier; EC in diesel-ambient samples began to oxidize at the same temperature as EC in ambient aerosols. TOEGA results for the samples from 6 December and 7 December were very similar to 5 December; higher M/C did not further reduce the oxidation temperature of diesel EC. The reduction of the EC oxidation temperature, independent of the M/C ratio (over the range investigated), is consistent with the results from Turner and Her-
ing (1994) and Grosjean et al. (1994), who showed that exposure of a highway tunnel sample to inland or coastal ambient aerosols resulted in a $\sim 100^{\circ}\text{C}$ or $\sim 150^{\circ}\text{C}$ reduction of soot oxidation temperature, respectively. The authors suggested that sodium or other components in ambient aerosols catalyzed the oxidation of carbon. These results reiterate that components in ambient aerosols can cause diesel EC to start oxidizing almost immediately after oxygen is introduced, in the region where POC evolves, making accurate separation of OC and EC very difficult.

For the 5 December sample set, the EC/OC ratios were 4.31, 0.14, and 1.49 for diesel, ambient TSP, and the two combined, respectively. Based on the TC mass of diesel ($171\ \mu\text{g}$) and ambient TSP ($28\ \mu\text{g}$) in the combined sample, the weighted EC/OC ratio of the resulting mixture would be 3.72. This ratio is higher than the measured ratio of 1.49, suggesting components of the ambient particles may reduce the EC/OC ratio of diesel particles measured by TOEGA. Similar results were found for the other two sample sets.

3.2 Effect of metal catalysts on TOEGA analyses of diesel particles

Na, K, Mg, Ca, Fe (II, III), Cu (I, II), Mn, and Zn are abundant in ambient aerosols. In this study, chlorides of the above metals were chosen to understand their effects on the OC and EC measurements of diesel particles by TOEGA. Na, Cu(II), and Fe(III) sulfates were also investigated to determine the role of anions.

Comparing the metal mass measured by ICP and SMPS suggests the collected

metal particles were likely a combination of metal hydrates and crystalline metal particles (Table S1, see supplementary material). The mean diameter of the metal particles was between ~70–100 nm (Fig. S1). The mass of metals (exclusive of water and anions) and carbon on the filters fell in the ranges of 5–164 and 27–226 μg , with averages of 36 ± 31 and 108 ± 46 μg , respectively.

3.2.1 Effects on TC

For pure diesel samples, there is a strong correlation between BC measured by optical transmissometer and TC measured by TOEGA, $\text{TC} (\mu\text{g}) = 1.78 \times \text{BC} (\mu\text{g}) - 21.97$ ($R^2 = 0.97$). For metal-loaded diesel samples, we estimated TC (TC_{esti}) from measured BC and the above linear relationship, and compared it to measured TC (TC_{meas}). TC_{meas} is strongly correlated with TC_{esti} ($\text{TC}_{\text{esti}} = 0.998 \times \text{TC}_{\text{meas}} - 0.516$; $R^2 = 0.88$) for all metal-loaded diesel samples (Fig. S2). While there is more scatter for the metal-loaded samples, the slope of regression line is not differentiable from 1, suggesting that the metal catalysts do not affect the TC measurement by TOEGA.

3.2.2 Effects on carbon oxidation

Figure 2 shows average TOEGA thermograms of metal-loaded and pure diesel samples. For 13 diesel controls without metal catalysts, the native EC was oxidized at $\sim 870^\circ\text{C}$, corresponding to the largest peak at ~ 550 s. At this point, 80% of the carbon has evolved from the filter. This point, $T_{0.8}$ is used to compare the effect of metal salts on carbon evolution. With metal catalysts, a more complex carbon evolution profile was observed. Once oxygen is introduced, the carbon begins to oxidize earlier, and some evolves at each temperature step, resulting in the multiple peaks in the oxidative phase. The carbon is also completely removed from the filter at lower temperatures.

Due to the multiple oxidation steps of diesel EC in the presence of metal catalysts, the fraction of carbon conversion as a function of temperature in the oxygen phase was calculated for metal-loaded and pure diesel samples and shown in Fig. S3. It shows

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clearly that metals systematically lower the temperature at which the carbon evolves from the filter.

The average degrees by which each metal salt reduces the native EC oxidation temperature ($T_{0.8}$) are as follows: (in °C) CuCl -133, CuCl₂ -212, CuSO₄ -193, FeCl₂ -145, FeCl₃ -93, Fe₂(SO₄)₃ -54, MnCl₂ -131, ZnCl₂ -64, NaCl -94, Na₂SO₄ -156, KCl -76, MgCl₂ -48, and CaCl₂ -22. Copper (II) species had the largest effect, causing the oxidation of carbon immediately after the addition of oxygen; calcium and magnesium had little effect (MgCl₂ > CaCl₂); iron (II, III), copper (I), manganese, zinc, sodium, and potassium all had moderate effects (KCl > NaCl; CuCl, FeCl₂, MnCl₂ > FeCl₃ > ZnCl₂). The reduced form of iron was more active than its oxidized form; while the oxidized form of copper was more active than its reduced form. The effect of anions on carbon oxidation also varied by metal. Sodium sulfate was more active than sodium chloride, while copper and iron chlorides were more active than sulfates.

The importance of catalyst concentration on EC oxidation was investigated by considering the reduction of $T_{0.8}$ (compared to pure diesel $T_{0.8}$) as a function of M/C ratio. The oxidation reactivity was found to be independent or very weakly dependent on the catalyst concentration for most metals (Fig. S4). Such independence of $T_{0.8}$ on metal loading may be because the quantity of metals that is sufficient to lower the carbon oxidation temperature is below the lowest ratio we used (between 0.03 and 0.37 depending on the metal).

The results indicate that catalytic activity of metal salts depends on the metal, its oxidation state, and to a lesser degree on the associated anions. The general activity follows transition metal > alkali metal > alkaline-earth metal.

A handful of previous studies on the catalytic oxidation of soot support our results. For the oxidation of model soot (Printex-U), CuCl₂ and CuCl were very active, whereas CaCl₂ had little effect (Mul et al., 1998). Cu(NO₃)₂ was the most effective catalyst of the first transition series of elements in carbon-air reactions (Cu(NO₃)₂ ≫ Fe(NO₃)₃ > Mn(NO₃)₂ > Zn(NO₃)₂ (Moreno-Castilla et al., 1985). CuO

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was a better catalyst than Cu_2O and Fe_2O_3 (Neri et al., 1997, 1998; Wang and Haynes, 2003). Cu^{2+} ion was the active form for copper reagents, and copper was more active in the presence of chloride than other anions (Courcot et al., 1998). CuCl_2 could lower the oxidation temperature of diesel soot by $\sim 170^\circ\text{C}$ (Murphy et al., 1981). K reduced the oxidation temperature of BC in biomass aerosols by $\sim 100^\circ\text{C}$ (Novakov and Corrigan, 1995b). Na lowered the combustion temperatures of laboratory-generated (Lin and Friedlander, 1988), biomass ($\sim 100^\circ\text{C}$, Novakov and Corrigan, 1995b), and ambient tunnel ($\sim 50^\circ\text{C}$, (Grosjean et al., 1994) carbonaceous particles.

The catalytic activity of metals on soot oxidation is related to many factors, such as the type of contact between the catalyst and soot, the origin and structure of soot itself, and the catalyst mobility, dispersion, sintering or inhibition, so some variation between studies is inevitable.

3.2.3 Effect on OC charring

Figure 2 shows that during the inert heating phase of TOEGA ($< 320\text{s}$), there is a small decrease in laser transmittance for both metal-loaded and pure diesel samples, indicating some OC charring. The fraction of charred OC was quantified from the change in the transmission signal, calculated as the percent reduction of laser transmittance through the filter during the inert heating phase of TOEGA, i.e. $(\ln I_{\max} - \ln I_{\min}) / \ln I_{\max} \times 100$, where I_{\max} and I_{\min} denote the maximum and minimum transmission signals during the inert phase, respectively. As expected (Yu et al., 2002), char was strongly linearly correlated with the TC loading, which ranged from 35–360 μg per filter, for diesel reference samples (Fig. S5a):

$$\text{char (\%)} = 0.0378 \text{ TC } (\mu\text{g}) - 1.47 \quad (R^2 = 0.92) \quad (1)$$

The effect of metals on OC charring was investigated by calculating the percent change of char for metal-loaded diesel relative to diesel reference samples (Figs. 3 and S6). Char of a metal-loaded diesel sample was calculated from its transmittance profile.

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Since metal-loaded and diesel reference samples have different TC loadings, the reference char was calculated from Eq. (1) using the measured TC for the metal-loaded sample. All tested salts increase char to variable extents (Figs. 3 and S6). Increased charring by transition metal salts was dependent on the M/C ratio, while the effects of alkali and alkaline-earth metals were not. The presence of alkali and alkaline-earth metal salts, NaCl, Na₂SO₄, KCl, MgCl₂, and CaCl₂ caused increases of 26±26%, 65±143%, 107±106%, 90±117% and 52±70% in char, respectively. Figure 3 shows that Cu and Fe increase OC charring rapidly with M/C ratio, following an exponential relationship in the M/C range of 0.03–1.25. For both Fe and Cu salts, chlorides are more active than sulfates. The results also suggest that the oxidation state of the transition metal has little effect on OC charring.

3.2.4 Effects on OC-EC split time

The split time is manually set at the point where the laser transmittance returns to its initial maximum level. For diesel reference samples, the split time was correlated with the TC loading, increasing modestly as TC increased, $t_{\text{split}} \text{ (sec)} = 0.5585 \text{ TC } (\mu\text{g}) + 336.24$ with $R^2 = 0.52$, $p < 0.001$ (Fig. S5b). Heavily loaded filters are less likely to give significant increases in laser transmittance as the oven temperature approaches 900 °C in the inert phase and these filters are therefore likely to have the OC-EC split occur later in the oxygen phase (Peterson and Richards, 2010).

The effect of metals on the OC-EC split of diesel samples was investigated by comparing the OC-EC split between metal-loaded and pure diesel samples normalized to the same TC loading. Generally, the metals lowered the split time, although there were a few scattered samples that had negligible or positive changes (Fig. S7). Most did not show a dependence on M/C ratio, however, CuCl, CuCl₂, FeCl₂, and ZnCl₂ did, with smaller changes in the split time as M/C increased.

Figure 4 shows the relationship between the drop of OC-EC split time and the reduction of EC oxidation temperature ($T_{0.8}$) in the presence of metals. The data show a

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strong positive correlation ($R^2=0.73$) between the two factors, although the variations of both changes are large. No correlation between OC-EC split and OC charring is found (not shown). The result suggests that the location of OC-EC split is more a function of the removal of EC from the filter than OC charring. The split point corrections produced by the instrument software, as with all other analyses, show a similar strong correlation (not shown).

3.2.5 Effects on EC/OC ratio

Figure 5 shows the EC/OC ratio as a function of M/C ratio. Most of the metal-M/C ratio combinations lower the EC/OC ratio by a substantial amount. $\text{Fe}_2(\text{SO}_4)$, FeCl_2 , FeCl_3 , CuSO_4 , Na_2SO_4 , MnCl_2 , and ZnCl_2 have little effect below a threshold M/C ratio, which ranges from approximately 0.1 to 0.4, and above this M/C ratio they lower the EC/OC ratio. CaCl_2 and CuCl both appear to increase the EC/OC ratios, by 25–40% at the low end of M/C ratios (0.03 and 0.06, respectively), but as M/C is increased further, they decrease the EC/OC ratio sharply. Data for KCl and CuCl_2 are difficult to interpret with confidence due to the small number of points and potential that an error in one or two of the points could throw off the conclusion (2 of the 4 diesel controls for these salts are anomalously low). They do however lend credence to the notion that for some salts, the EC/OC ratio will be increased at low M/C ratios. The results for NaCl are not shown as they are scattered and not in agreement with our preliminary data. We note that samples such as the diesel studied here tend to have more variable split points and EC/OC ratios than ambient samples because they char relatively little and thus are more sensitive to the background correction and small temperature dependent changes in the filter and instrument.

As shown in Fig. 2, the transmittance typically reaches a minimum value partway through the 850°C temperature step of the He-mode and then begins increasing, indicating premature evolution of light-absorbing carbon. This loss of light-absorbing carbon in the inert mode could be due to oxidation of POC or native EC due to the

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presence of inorganic materials, such as metal oxides (Chow et al., 2001) or sulfate (Huffman, 1996), which are able to act as oxidizing agents at high temperatures. In addition, metals catalyze the evolution of more carbon in the lower temperature steps of the He/O₂-mode (Figs. 2 and S3). The above likely contribute to the lower reported EC/OC ratios in the presence of metals. However, in principle the laser transmittance should do a reasonable job of correcting for such processes and move the split earlier to compensate. A complication arises from the differences in the absorption cross section of POC vs. EC; POC is usually more absorbing than EC (e.g., Subramanian et al., 2006). This situation can lead to a delayed split point and an underestimate of EC because early evolving EC does not bring the transmission signal back up sufficiently to compensate for the POC that evolves later.

None of the measurable impacts of metals on carbon evolution including its ability to lower the carbon oxidation temperature, to increase OC charring, and to reduce the split time is correlated with its effect on the EC/OC ratio (not shown). Presumably this is because of the interplay between the effects of metals on carbon evolution, i.e. increasing the OC charring in the He-phase, and catalyzing the oxidation of POC and EC both in the He- and He/O₂-phase.

3.3 Catalytic mechanisms

In this study, metal salts were deposited on top of diesel particles. The metal-loaded diesel samples were first heated to ~900 °C in the absence of O₂, allowed to cool, and then reheated to ~900 °C in the presence of O₂. The speciation of metal (chemical forms) during the heating process is likely an important factor in the catalytic mechanism of metals. Initially, most of the metal salts exist as hydrates, which presumably dehydrate during the inert heating phase. Eventually the salts reach their melting point, partially vaporize and likely become oxides. The chemical forms of metals during the heating stages in this study are not known, and it is possible chlorides, oxides, and other oxygen-chloride complexes coexist with elemental forms of the metal.

The catalytic activity of metals is related to its physical and chemical properties. The

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contact between metal and carbon has been found to be an important factor affecting its catalytic activity (Neeft et al., 1996). For metals in loose contact with soot (as in this work), the mobility of a metal is suggested to be a major parameter determining its activity, and the mobility correlates with the melting point (Neri et al., 1997; Neeft et al., 1996; McKee, 1983; Mul et al., 1998; Stanmore et al., 2001). The NIOSH protocol used here reaches temperatures close to 900 °C, above the melting points of all the salts tested. Figure 6 shows that with the exception of FeCl₂, which is excluded from the regression analysis, lower melting points of metal salts are strongly correlated with increasing char ($y=3E+09x^{-2.6228}$, $R^2=0.87$).

The melting point of metal salts is not correlated with the shift in EC oxidation temperature (not shown), likely because the metal salts are converted to other chemical forms (oxides, oxygen-chloride complexes) in the He/O₂-phase. It also suggests that the chemical properties of metal catalysts, beyond simple contact with carbon, play an important role in the oxidation of EC.

Metal chlorides may catalyze the carbon oxidation through the formation of M-O-Cl species; the catalytic cycle is proposed involving activation of oxygen on the surface of the metal(oxy)chloride, followed by transfer of activated oxygen to the carbon surface (Mul et al., 1998). The catalytic effect is due to the fact that carbon adsorbs metal-bound oxygen faster than molecular oxygen. Our observation that copper and iron are more active in the presence of chloride than sulfate lends some credence to the above mechanism. Another mechanism accounting for the catalytic activity of metal chlorides is through the coordination between metal ions and oxygen-containing ligands in diesel particles including O²⁻, OH⁻, H₂O and -COO⁻. The formation of metal-oxygen complexes through coordination of metal ions will greatly change the structure of diesel particles, which will affect its oxidation properties (Yu et al., 2005).

Metal oxides, which may form upon heating, are known to catalyze carbon oxidation through oxygen transfer mechanisms. CuO, Cu₂O, Fe₂O₃, ZnO, MgO, CaO, and K₂O have all been shown to have this activity. Metal oxides that readily change valency (such as Cu and Fe) have been identified as superior catalysts (Silva et al., 1997;

Setzer et al., 1993; Moulijn et al., 1984). The high activity of transition metals observed in this study suggests the possible role of the above mechanism in the oxidation of diesel EC.

4 Discussion and atmospheric implications

Precise quantification of EC is highly desirable due to its relatively large role in climate forcing, in altering the hydrologic cycle when deposited on snow, and because it is commonly used as a tracer for diesel exhaust in urban areas. As we show, the EC and OC measurements of diesel particles by TOEGA is affected by metals in the sample. Metals change the evolution profiles of carbon, catalyzing the oxidation of EC and the charring of OC; and generally reduce the EC/OC ratio. Transition metals are more active than alkali and alkaline-earth metals. Since the effect of metals on the EC/OC ratio depends on both metal and M/C, and further, preliminary measurements in our lab support the catalyst community's suggestion the effects of metals are not simply additive, it is difficult to predict the activity of different metals and the impact of metals on EC/OC analysis of a particular ambient sample. The effect is large however; metals appear to result in negative biases of up to 80%. For a few metal salts, and at low M/C ratios, the EC/OC ratio may be increased as by as much as 40%.

Pure diesel contains variable but usually small amounts of metals. For our diesel particles the M/C ratio for metals tested here is about 0.02, similar to the ultrafine fraction in Southern California (Krudysz et al., 2008). This may itself cause errors in the reported EC; our results suggest the direction of the error could be in the direction of over-reporting EC. For fine mode particles M/C ratios are usually 0.1–0.5, and the upper end of the range may be even higher for PM₁₀ and TSP (Krudysz et al., 2008; IMPROVE 2010 and Table 1), thus underestimates of EC are likely more common in ambient samples. If metals react similarly with different types of carbonaceous aerosols present in ambient aerosols, the measured EC/OC ratio will likely have a variable, low bias except possibly at very low M/C ratios. This is supported by the dramatic

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reductions in EC/OC ratios we observed in our mixtures of diesel with ambient aerosol (Sect. 3.1).

Although more work would clearly be required, including investigation of the effect of aluminum and silicon which may also have catalytic activity, there is potential that existing data sets containing EC, OC and trace metals could be corrected. We also note that adjusting the temperature profile to minimize charring will not necessarily reduce metal-dependent errors in EC/OC splits because the split point is more sensitive to changes in EC oxidation temperature than it is to charring.

Supplementary material related to this article is available online at:

<http://www.atmos-chem-phys-discuss.net/10/16941/2010/acpd-10-16941-2010-supplement.pdf>

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Table 1. Chemical composition of ambient TSP aerosols collected at UCLA, in $\mu\text{g}/\text{m}^3$ for each component.

Variable	5 Dec 2007	6 Dec 2007	7 Dec 2007
Na	6.44	7.48	7.42
Al	0.42	0.27	0.06
Ba	0.15	0.06	0.02
Ca	2.84	1.93	0.49
Cr	0.05	0.02	0.01
Cu	0.37	0.07	0.02
Fe	1.77	0.78	0.19
K	0.47	0.24	0.2
Mg	1.06	0.97	0.85
Ni	0.01	0.01	0
Si	0.75	0.41	0.26
Ti	0.04	0.02	0
V	0.11	0.03	0.09
Zn	0.43	1.25	0.05
TC	15	9	2
EC/OC Ratio ^a	0.14	0.16	0.11
TSP	79	57	22
Metal/Diesel Mass ^b	0.16	1.77	3
EC Ox. Temp Red. ^c	-158	-158	-160

^a In the ambient aerosol.

^b Ratio of the sum of measured metals in ambient aerosol to diesel particle mass added to ambient aerosol. The carbon present in the ambient aerosol is not included.

^c Reduction of diesel EC oxidation temperature, which is assumed to be the temperature at which the largest carbon evolution peak appears in the He/O₂-phase.

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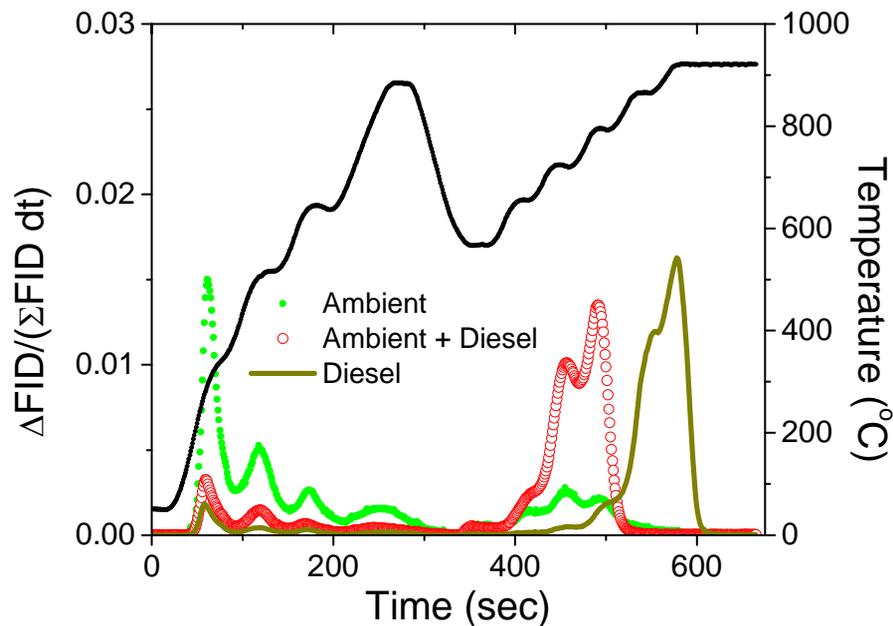


Fig. 1. Carbon evolution profiles for ambient, diesel, and a combination of ambient and diesel particles, for samples collected in 5 December 2007, using the NIOSH protocol. The mass of diesel and ambient particles were 171 μg and 28 μg , respectively. The FID response was normalized to the total FID response for a given sample.

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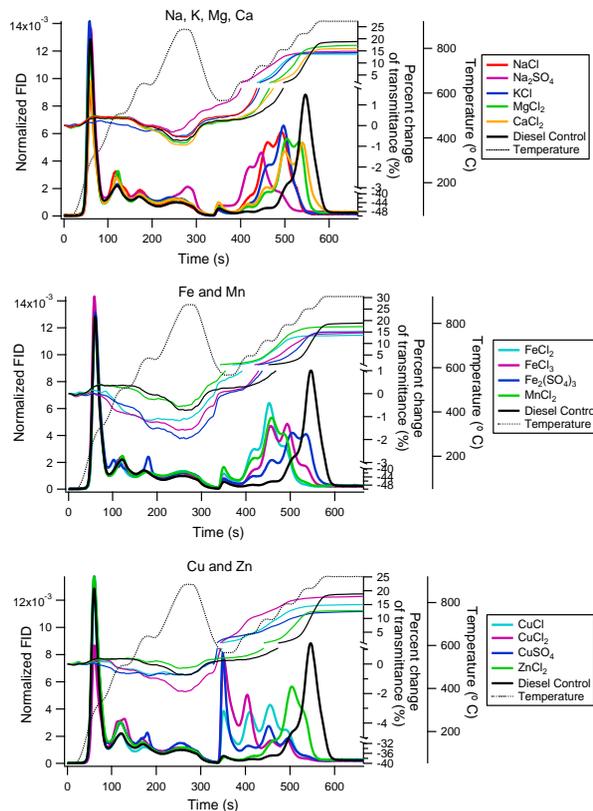


Fig. 2. Carbon evolution profiles of diesel and metal-loaded diesel samples using the NIOSH protocol. For each metal salt, several samples with different metal to carbon ratios were averaged. The diesel control profile is also an average, of 13 samples. The FID response was normalized to the total FID response ($\Delta\text{FID}/\Sigma\text{FID}dt$). Transmittance profiles are shown as percent change relative to the initial transmittance I_0 , i.e. $(\ln I - \ln I_0)/\ln I_0 \times 100$.

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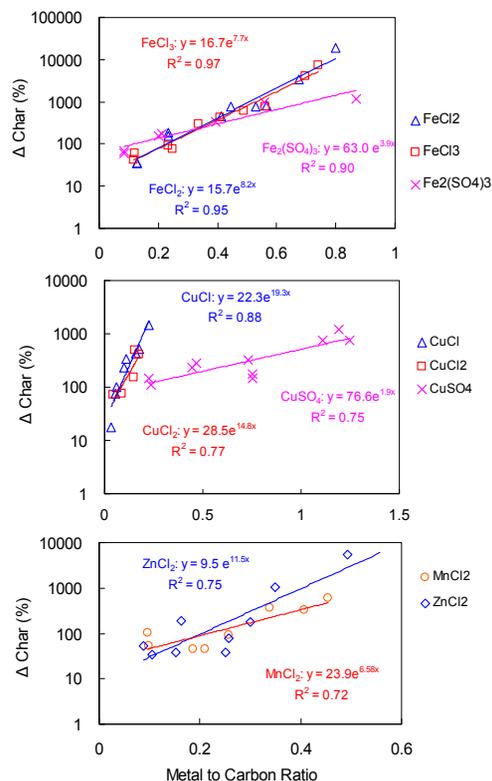


Fig. 3. The percent increase of char as a function of metal to carbon ratio for transition metal-loaded diesel compared to diesel reference samples. The values have been adjusted for the mass of TC (see text). The y axis represents $\frac{([\text{char}]_{\text{metal-loaded diesel sample}} - [\text{char}]_{\text{diesel reference sample with matched TC loading}})}{[\text{char}]_{\text{diesel reference sample with matched TC loading}}} \times 100$. Char: the percent reduction of laser transmittance through the filter during the inert heating phase of TOEGA.

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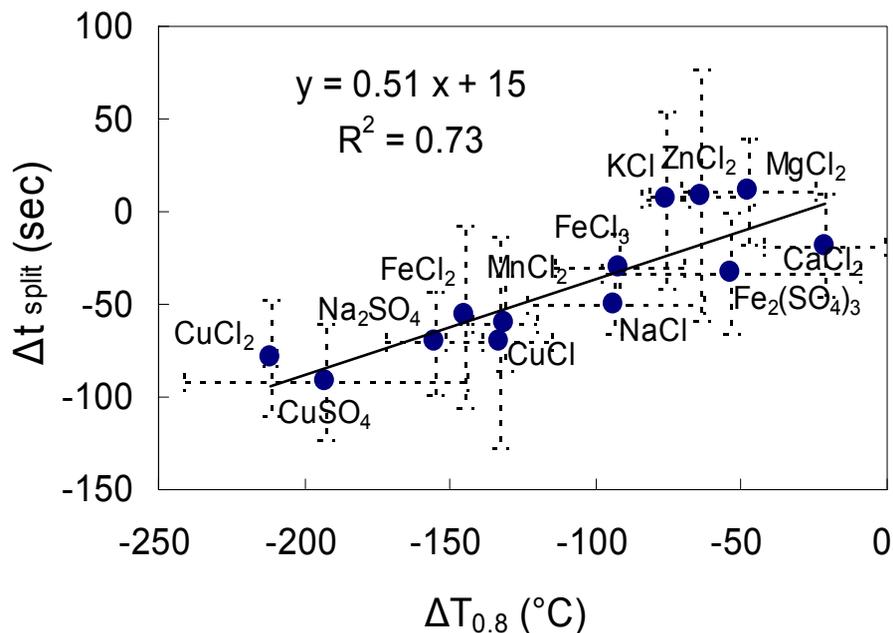


Fig. 4. The reduction of $T_{0.8}$ (temperature at which 80% of the carbon has evolved from the filter) vs. the reduction of OC-EC split time due to the addition of a metal catalyst. The error bars indicate one standard deviation.

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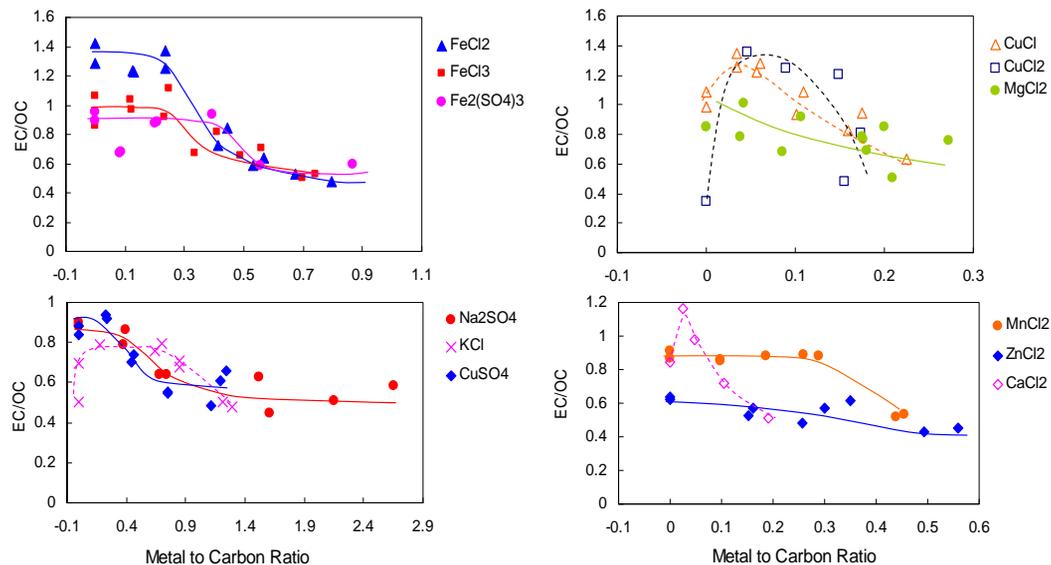


Fig. 5. EC/OC ratio as a function of metal to carbon ratio for metal-loaded diesel and the corresponding diesel reference samples.

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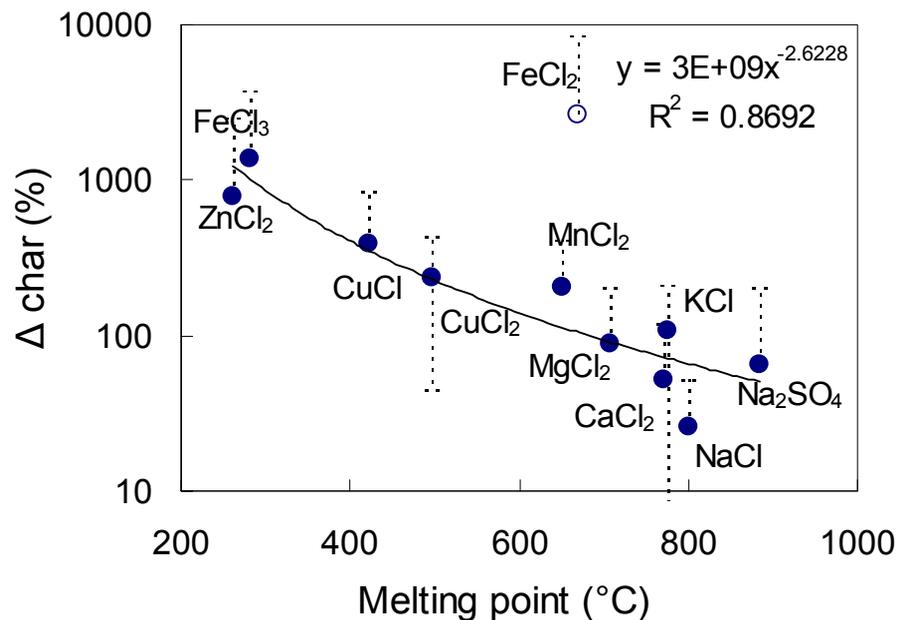


Fig. 6. The percent increase in the fraction of charred OC for metal-loaded compared to diesel reference samples vs. the melting point of metal salts. The error bars indicate one standard deviation.

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