



Supplement of

Highly time-resolved chemical characteristics and aging process of submicron aerosols over the central Himalayas

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2 **Section S1 HR-ToF-AMS operation**

3 A PM_{2.5} cyclone was installed before the sampling line to remove coarse particles. A Nafion dryer was then used to keep the
4 relative humidity of aerosol particles below 30 % before sampling into the HR-ToF-AMS. Ambient particles are sampled into
5 the instrument through a critical orifice and focused into a concentrated and narrow beam through an aerodynamic lens.
6 Particles are then accelerated into the sizing vacuum chamber and obtain different velocities for particles with different sizes
7 due to the supersonic expansion induced by a pressure difference between the two chambers. Meanwhile, a mechanical
8 chopper with two radial slits located 180° apart is used to intercept the focused particle, and then the time of flight (P-ToF)
9 from the chopper to the vaporizer is measured to obtain the aerodynamic size of particles. After passing through the sizing
10 chamber, particles are directed onto a resistively heated surface (600 °C) under a high vacuum and ionized by a 70 eV
11 electron impact, before finally being detected by a high-resolution mass spectrometer. There are two different operation
12 modes in HR-ToF-AMS, i.e., V-mode (detection limits of about 10 ng m⁻³) and W-mode (~5000 m/Δm) with different
13 signal-to-noise ratio (S/N). In this study, we only used V-mode in consideration of the relatively low aerosol mass
14 concentration level and low S/N ratio over the TP.

15 **Section S2 Calculation and evaluation of the acidity of submicron aerosols**

16 Bulk acidity of PM₁ was generally evaluated following the methods in Zhang et al. (2007) and Schueneman et al. (2021). The
17 mass concentration of ammonium was predicted by assuming to fully neutralize these HR-ToF-AMS measured sulfate,
18 nitrate, and chloride using the following equation:

19

$$\text{Predicted ammonium} = 18 \times \left(\frac{2 \times \text{SO}_4^{2-}}{96} + \frac{\text{NO}_3^-}{62} + \frac{\text{Cl}^-}{35.5} \right) \quad (\text{S1})$$

20 The mass concentration ratio of measured ammonium to predicted ammonium can be further calculated to be an indicator to
21 evaluate the bulk acidity of submicron aerosols. In this study, linear regression analysis between the mass concentrations of
22 measured and predicted ammonium was performed to evaluate the bulk acidity of submicron aerosols (Fig. S2). Aerosol
23 particles are generally considered to be “acidic” if the calculated ratio is obviously lower than 1 and to be “more acidic” if the
24 ratio is lower than 0.75, whereas a ratio that roughly near to 1 or larger than 1 indicates the particles are “bulk neutralized”
25 and even there are more excess ammonium that needed to be neutralized. Note that the validity of using this method is based
26 on the assumption that the influence from nitrogen- or sulfur-containing organic ions (e.g., organic acids and organic nitrogen
27 compounds) as well as the mineral and metal ions are negligible (Zhang et al., 2007).

28 **Section S3 The box model description**

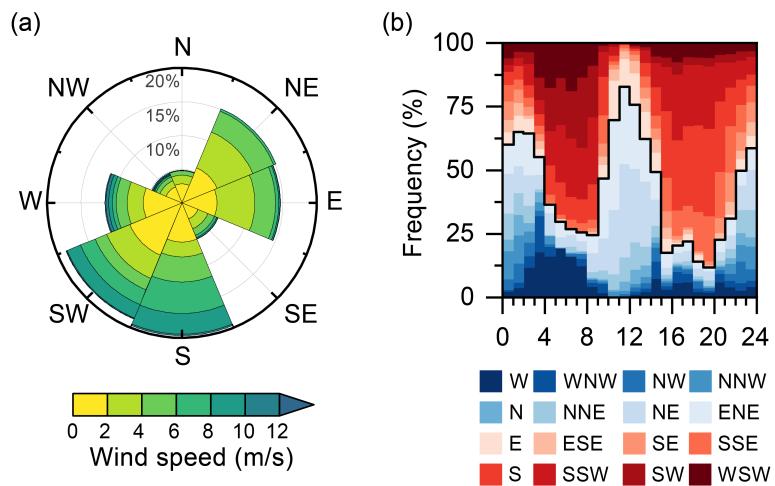
29 Based on the box model described in Chen et al. (2021), the formation rate of species i is given by:

30

$$\frac{dc_i}{dt} = \frac{Q_i}{H(t)} + R_i - \frac{v_{d_i} c_i}{H(t)} + \frac{u}{\Delta x} (c_i^0 - c_i) + \frac{1}{H(t)} \frac{dH}{dt} \Big|_{dH/dt > 0} (c_i^a - c_i) \quad (\text{S2})$$

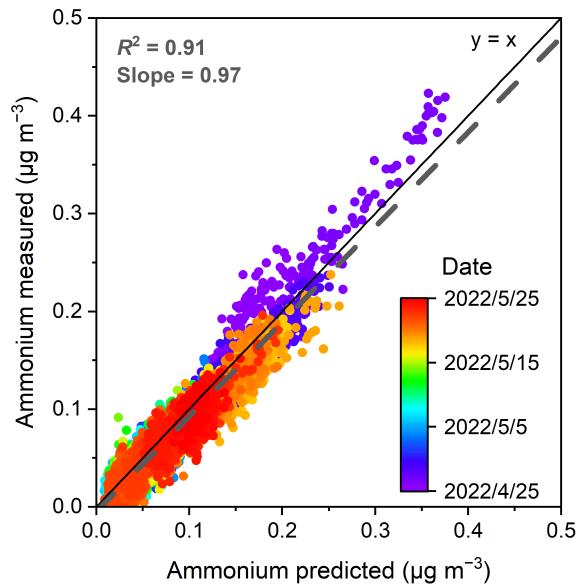
31 where $H(t)$ is the ABLH, Q_i is the emission rate, R_i is the chemical production and loss rate, v_{d_i} is the deposition velocity, c_i^0
32 is the background concentration of species i, c_i^a is the aloft concentration of species i, and u is the wind speed (with a
33 constant Δx direction).

34 **Figures**



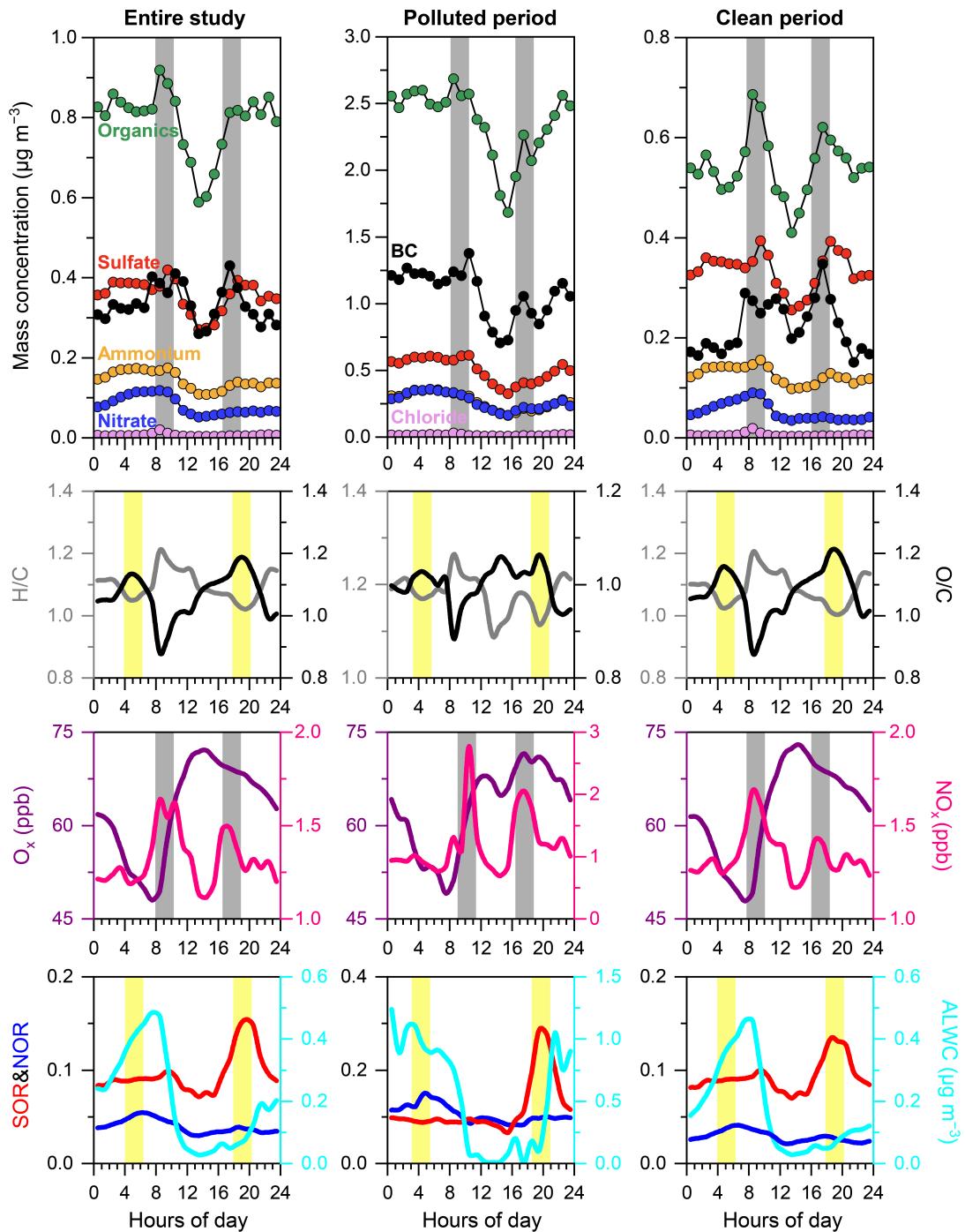
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36 **Figure S1.** (a) The wind rose plot colored by wind speed during the field study period and (b) the diurnal variation of wind
37 direction.



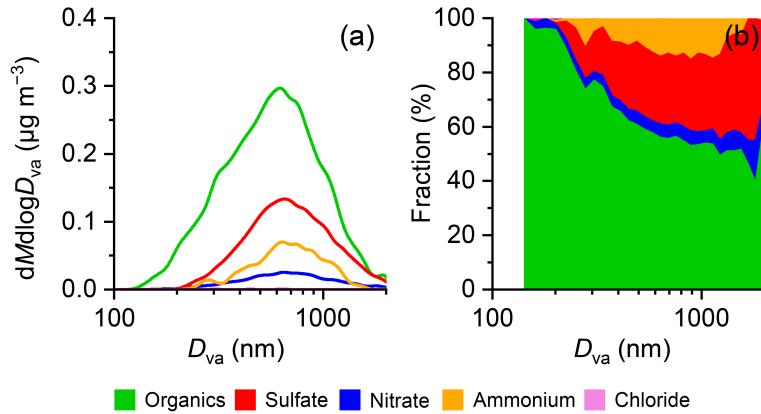
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39 **Figure S2.** Scatterplot and linear regression (grey dashed line) of measured ammonium versus predicted ammonium.



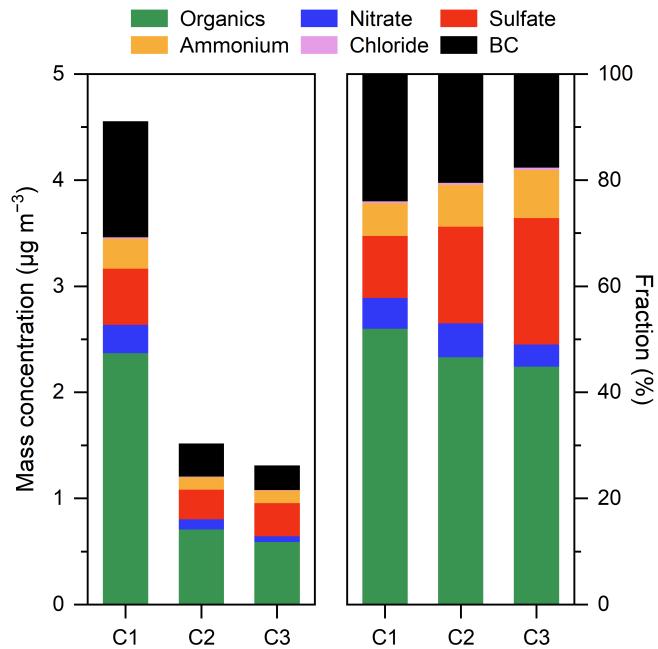
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41 **Figure S3.** Diurnal variations of PM₁ species, elemental ratios, gas indicators, SOR, NOR and ALWC during the entire study,
42 polluted period and clean period. The grey shadows mark the potential transport periods with peaks of PM₁ species and NO_x.
43 The yellow shadows mark the oxidation processes.



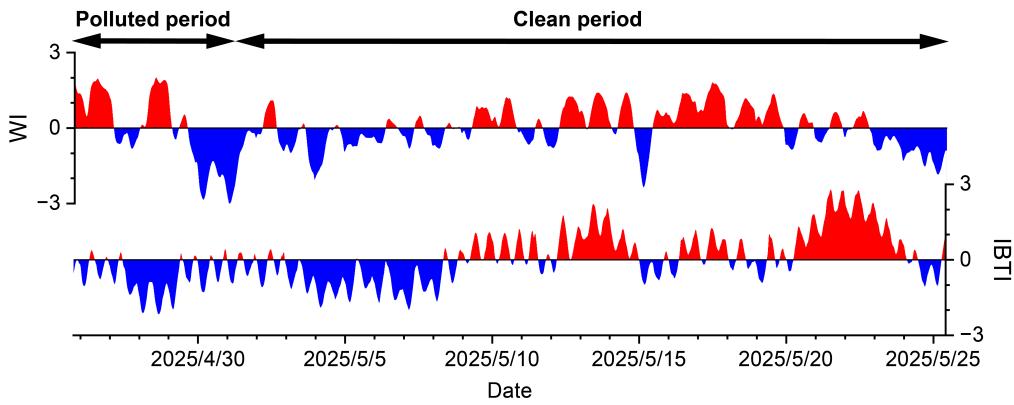
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45 **Figure S4.** (a) Averaged mass size distributions of NR-PM₁ and (b) the fraction of species as a function of particle sizes.



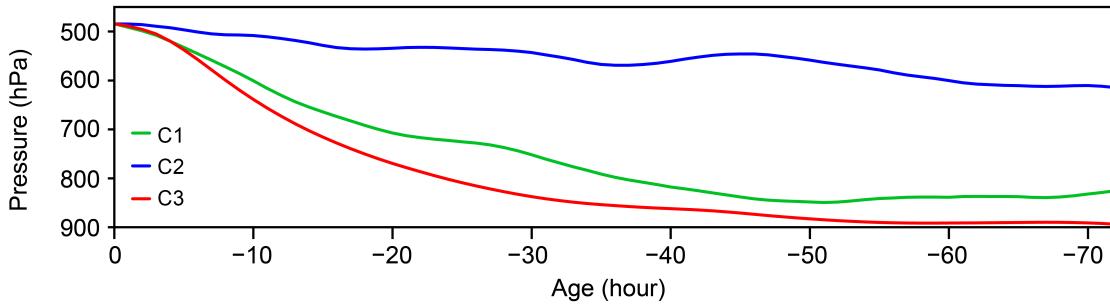
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47 **Figure S5.** The PM₁ mass concentration and fraction of each trajectory cluster during polluted period and clean period.

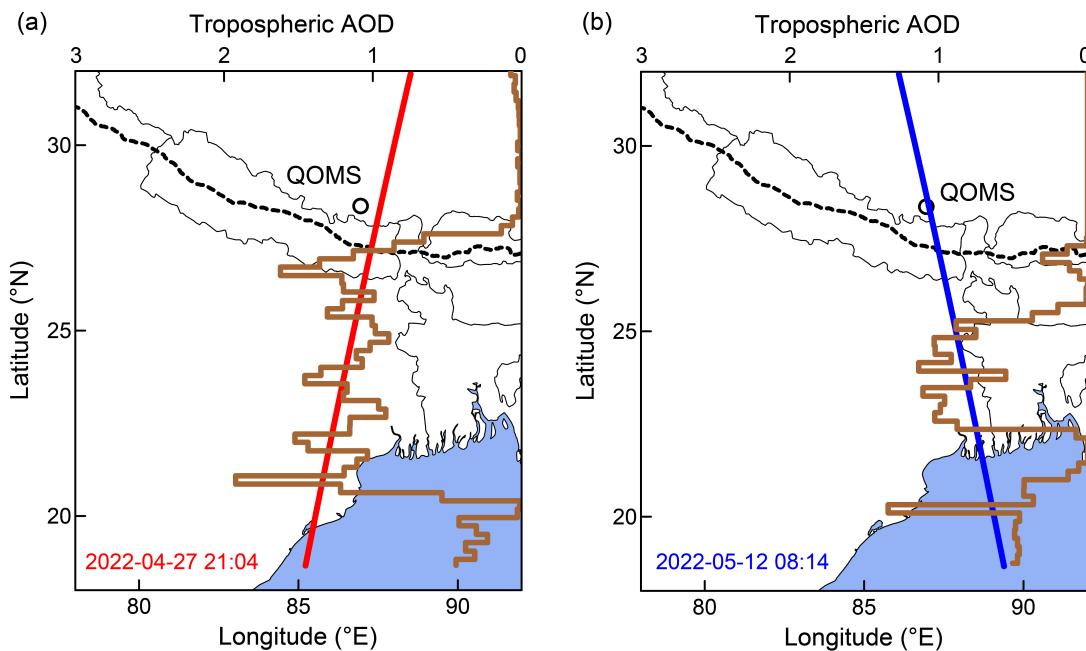


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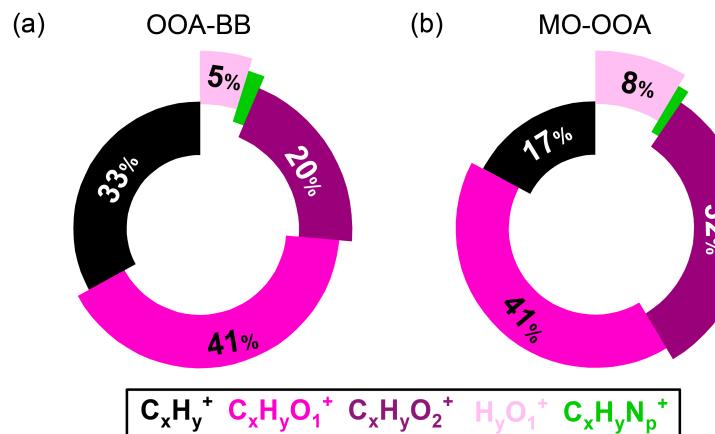
49 **Figure S6.** The westerlies index (WI) at QOMS and India-Burma Trough index (IBTI) during the study.



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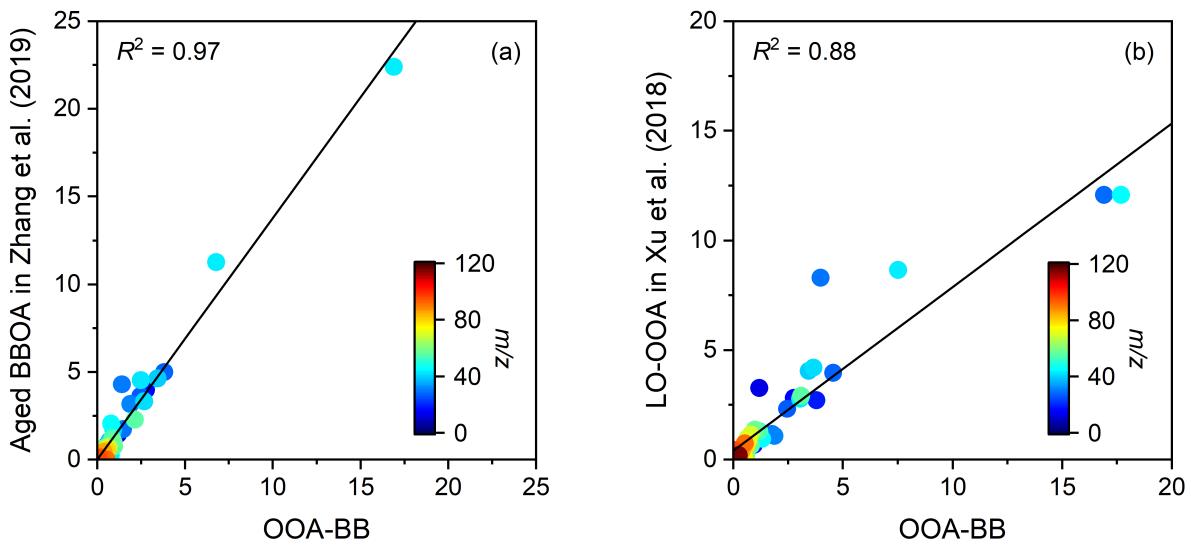
51 **Figure S7.** The atmospheric pressure of three backward-trajectory clusters.

52

53 **Figure S8.** The Tropospheric AOD along the CALIPSO tracks on (a) 27 April and (b) 12 May 2022. Dashed black lines
54 represent Tibetan Plateau boundary.

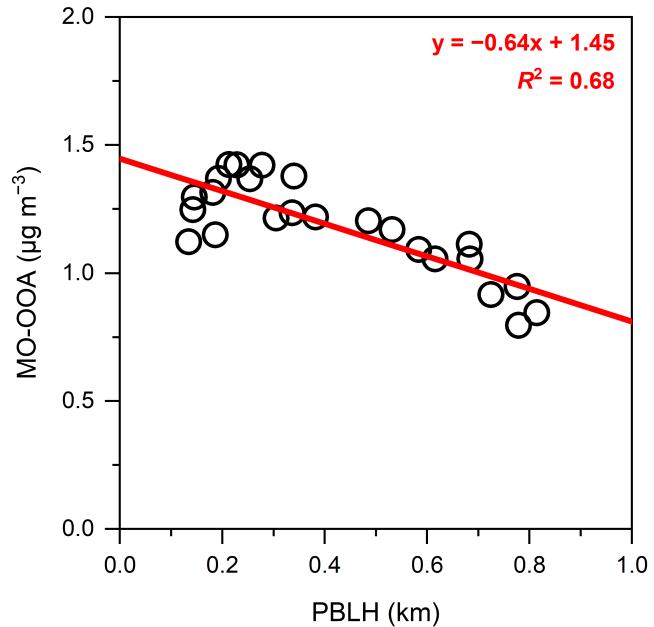
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56 **Figure S9.** Five ion categories to (a) OOA-BB and (b) MO-OOA for the entire study.



57

58 **Figure S10.** Comparisons between the OOA-BB HRMS identified in this study and HRMS determined from (a) Zhang et al.
59 (2019) and (b) Xu et al. (2018).



60

61 **Figure S11.** MO-OOA concentration as a function of ABLH in the polluted period.

62

63 **Table S1.** Pearson correlation coefficients and linear regression slopes for OOA factors with O_x, SOR, ALWC, and NOR grouped by daytime (solar radiation > 0)
 64 and nighttime (solar radiation = 0). “ns” represents the slope is not significantly non-zero at $p = 0.05$.

	Day			Night		
	Σ OOA	MO-OOA	OOA-BB	Σ OOA	MO-OOA	OOA-BB
O _x	$r = 0.58$ slope = 0.072 ± 0.007	$r = 0.65$ slope = 0.035 ± 0.003	$r = 0.50$ slope = 0.036 ± 0.004	$r = 0.72$ slope = 0.060 ± 0.004	$r = 0.69$ slope = 0.028 ± 0.002	$r = 0.68$ slope = 0.032 ± 0.002
SOR	$r = 0.66$ slope = 15 ± 1	$r = 0.67$ slope = 6.8 ± 0.5	$r = 0.62$ slope = 8.3 ± 0.8	$r = 0.74$ slope = 9.9 ± 0.5	$r = 0.80$ slope = 5.2 ± 0.2	$r = 0.62$ slope = 4.8 ± 0.4
NOR	$r = 0.60$ slope = 12 ± 1	$r = 0.61$ slope = 5.6 ± 0.5	$r = 0.56$ slope = 6.9 ± 0.7	$r = 0.86$ slope = 16 ± 0.6	$r = 0.80$ slope = 7.7 ± 0.3	$r = 0.79$ slope = 8.3 ± 0.4
ALWC	$r = 0.31$ slope = 0.74 ± 0.2	$r = 0.12$ slope = $0.12 \pm 0.1^{\text{ns}}$	$r = 0.42$ slope = 0.62 ± 0.1	$r = 0.77$ slope = 1.2 ± 0.09	$r = 0.80$ slope = 0.52 ± 0.04	$r = 0.71$ slope = 0.67 ± 0.06

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