



## Supplement of

# Measurement report: Wintertime aerosol characterization at an urban traffic site in Helsinki, Finland

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## 1 SUPPLEMENT

**Table S1.** List showing which compounds were analysed from each sample types and which detector was use.

	Canister Samples	In situ Samples	Tube Samples		Canister Samples	In situ Samples	Tube Samples
Ethane	FID			4-Ethyltoluene		MS	MS
Ethene	FID			1,3,5-Trimethylbenzene		MS	MS
Propane	FID			2-Ethyltoluene		MS	MS
Propene	FID			1,2,4-Trimethylbenzene		MS	MS
2-Methylpropane	FID			1,2,3-Trimethylbenzene		MS	MS
Butane	FID			Hexane		MS	MS
Ethyne	FID			Heptane		MS	MS
T-but-2-ene	FID			Octane		MS	MS
But-1-ene	FID			Nonane		MS	MS
Cis-but-2-ene	FID			Decane		MS	MS
2-Methylbutane	FID			Undecane		MS	MS
n-pentane	FID			Dodecane		MS	MS
1,3-butadiene	FID			Tridecane		MS	MS
T-pent-2-ene	FID			Tetradecane		MS	MS
Pent-1-ene	FID			Pentadecane		MS	MS
Isoprene	FID			Furfural		MS	MS
α-pinene		MS	MS	Benzyl alcohol		MS	MS
Camphene		MS	MS	1,3-Diethylbenzene		MS	MS
Myrcene		MS	MS	o-cresol		MS	MS
β-pinene		MS	MS	1,4-Diethylbenzene		MS	MS
Carene		MS	MS	2-Propyltoluene		MS	MS
p-Cymene		MS	MS	p-cresol		MS	MS
Limonene		MS	MS	2-Ethyl-p-xylene		MS	MS
1,8-Cineol		MS	MS	1,2,4,5- Tetramethylbenzene		MS	MS
Terpinolene		MS	MS	1,3,5-Triethylbenzene		MS	MS
β-caryophyllene		MS	MS	1,4-Dibutylbenzene		MS	MS
Benzene		MS	MS	Naphthalene		MS	MS
Tetrachloromethane		MS	MS	Acenaphthylene		MS	MS
Toluene		MS	MS	Acenaphthene		MS	MS
Ethylbenzene		MS	MS	Fluorene		MS	MS
p/m-xylene		MS	MS	Anthracene		MS	MS
Styrene		MS	MS	Phenanthrene		MS	MS
o-xylene		MS	MS	Fluoranthene		MS	MS
Propylbenzene		MS	MS	Pyrene		MS	MS
3-Ethyltoluene		MS	MS				

**Table S2.** Instruments at the Traffic Supersite.

Traffic Supersite			
Quantity	Instrument		
Chemical composition of aerosol	Soot Particle Aerosol Mass Spectrometer (SP-AMS,		
particles	Aerodyne Research Inc.)		
Chemical composition of particulate	Aerosol Chemical Speciation Monitor (ACSM, Aerodyne		
matter	Research Inc.)		
Volatile organic compounds (VOCs) and	In situ thermal desorption-gas chromatograph-mass		
intermediate volatile organic compounds	spectrometer (TD-GC-MS)		
(IVOCs)			
Gaseous sulfuric acid	Nitrate based chemical-ionization atmospheric-pressure-		
	interface time-of-flight mass spectrometer (nitrate CI-API-		
	TOF-MS, Aerodyne Research Inc.)		
Mobility distribution of ions (0.8–40 nm)	Neutral cluster and Air Ion Spectrometer (Airel Ltd)		
and size distribution of particles (2-40			
nm)			
Concentration of SO <sub>2</sub>	Enhanced Trace Level SO <sub>2</sub> Analyser (Thermo Scientific <sup>™</sup> ,		
	•		
	Model 43i-TLE)		
Particle concentration (size range >7 nm	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756)		
Particle concentration (size range $>7$ nm (D <sub>p</sub> 50), and the maximum detectable	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756)		
Particle concentration (size range >7 nm $(D_p50)$ , and the maximum detectable particle size > 3 $\mu$ m)	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756)		
Particle concentration (size range >7 nm $(D_p50)$ , and the maximum detectable particle size > 3 $\mu$ m) Particle concentration (> 5.4 nm $D_p50$ )	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model		
Particle concentration (size range >7 nm $(D_p50)$ , and the maximum detectable particle size > 3 $\mu$ m) Particle concentration (> 5.4 nm $D_p50$ )	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20)		
Particle concentration (size range >7 nm ( $D_p50$ ), and the maximum detectable particle size > 3 µm) Particle concentration (> 5.4 nm $D_p50$ ) Particle activation size distribution	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.)		
Particle concentration (size range >7 nm $(D_p50)$ , and the maximum detectableparticle size > 3 $\mu$ m)Particle concentration (> 5.4 nm $D_p50$ )Particle activation size distributionbetween 1 and 4 nm.	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.) and nano-Condensation Nucleus Counter (A11 nCNC,		
Particle concentration (size range >7 nm $(D_p50)$ , and the maximum detectable particle size > 3 $\mu$ m) Particle concentration (> 5.4 nm $D_p50$ ) Particle activation size distribution between 1 and 4 nm.	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.) and nano-Condensation Nucleus Counter (A11 nCNC, Airmodus Ltd.)		
Particle concentration (size range >7 nm $(D_p50)$ , and the maximum detectableparticle size > 3 $\mu$ m)Particle concentration (> 5.4 nm $D_p50$ )Particle activation size distributionbetween 1 and 4 nm.Black carbon concentration	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.) and nano-Condensation Nucleus Counter (A11 nCNC, Airmodus Ltd.) Multi-Angle Absorption Photometer (MAAP, Thermo		
Particle concentration (size range >7 nm ( $D_p50$ ), and the maximum detectable particle size > 3 µm)Particle concentration (> 5.4 nm $D_p50$ )Particle activation size distribution between 1 and 4 nm.Black carbon concentration	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.) and nano-Condensation Nucleus Counter (A11 nCNC, Airmodus Ltd.) Multi-Angle Absorption Photometer (MAAP, Thermo Electron Corporation, Model 5012)		
Particle concentration (size range >7 nm ( $D_p50$ ), and the maximum detectable particle size > 3 µm)Particle concentration (> 5.4 nm $D_p50$ )Particle activation size distribution between 1 and 4 nm.Black carbon concentrationBlack carbon concentration	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.) and nano-Condensation Nucleus Counter (A11 nCNC, Airmodus Ltd.) Multi-Angle Absorption Photometer (MAAP, Thermo Electron Corporation, Model 5012) A dual spot aethalometer (AE33, Magee Scientific)		
Particle concentration (size range >7 nm ( $D_p50$ ), and the maximum detectable particle size > 3 µm)Particle concentration (> 5.4 nm $D_p50$ )Particle activation size distribution between 1 and 4 nm.Black carbon concentrationBlack carbon concentrationAlveolar lung deposited surface area	Model 43i-TLE) Condensation Particle Counter (CPC, TSI model 3756) Condensation Particle Counter (CPC, Airmodus model A20) An Airmodus Nanoparticle Diluter (AND, Airmodus Ltd.) and nano-Condensation Nucleus Counter (A11 nCNC, Airmodus Ltd.) Multi-Angle Absorption Photometer (MAAP, Thermo Electron Corporation, Model 5012) A dual spot aethalometer (AE33, Magee Scientific) Pegasor AQ <sup>TM</sup> Urban instrument (Pegasor Ltd.)		

Particle size distribution (size range : 3–	The Differential Mobility Particle Sizer (Vienna type		
950 nm)	Differential Mobility Analyser, DMA) and Airmodus A20		
	CPC)		
Concentration of CO, CO <sub>2</sub> , and CH <sub>4</sub>	Gas analyser for CO, CO <sub>2</sub> and CH <sub>4</sub> (Picarro G2401, Picarro		
	Inc.)		
Samples for PAH analyses	Daily PM <sub>10</sub> filter sampling		
Samples for sugar anhydride analyses	PM <sub>1</sub> filter sampling (one or two samples per day)		
Concentration of PM <sub>2.5</sub> and PM <sub>10</sub>	Fidas 200 (Palas)		
Nitrogen oxides (NO <sub>x</sub> )	APNA 370 (Horiba)		
Ozone (O <sub>3</sub> )	APOA 370 (Horiba)		
Carbon monoxide (CO)	APMA 360 (Horiba)		
Carbon dioxide (SO <sub>2</sub> )	LI-7000 (LICOR)		
Particle scattering coefficient	Nephelometer (model 3610, TSI)		

**Table S3.** Instruments at the UB Supersite (SMEAR III).

Mast (31 m, agl)			
Quantity	Instrument		
Air temperature (4, 8, 16 and 31 m)	Platimun resistance thermometer (Pt-100)		
Wind (4, 8, 16 and 31 m)	2D ultrasonic anemometer (Thies Clima 2.1x)		
Global radiation (31 m)	Kipp and Zonen CNR1		
Reflected global (31 m)	Kipp and Zonen CNR1		
Longwave radiation in (31 m)	Kipp and Zonen CNR1		
Longwave radiation out (31 m)	Kipp and Zonen CNR1		
Photosynthetic Active Radiometer	Kipp and Zonen PAR lite		
(PAR, 31 m)			
Reflected PAR (31 m)	Kipp and Zonen PAR lite		
Flux of momentum and heat (Eddy	Ultrasonic anemometer (Metek USA-1)		
Covariance, 31)			
Flux of CO <sub>2</sub> and H <sub>2</sub> O (Eddy Covariance,	High frequency gas analyser (Li-Cor 7500 & 7000, infra-		
31)	red absorbtion)		
Total number concentration flux of	Water Condesation Particle Counter (WCPC, TSI-3781)		
aerosol particles (Eddy Covariance)			
(2-4 m agl)			
Particle size distribution (size range : 3–	The Differential Mobility Particle Sizer (Hauke-type		
950 nm)	DMA, 10.9 cm+TSI 3025; Hauke-type DMA, 28 cm+TSI		
	3010)		
Particle concentration (size range >7 nm	Condensation particle counter (CPC, TSI 3756)		
(Dp50), and the maximum detectable			
particle size > 3 $\mu$ m)			
Particle size distribution (size range:	Aerodynamic particle sizer (APS, TSI 3321)		
0.5–20 nm)			
Particle size distribution (size range:	Nano Condensation Nucleus Counter System (Airmodus		
1.3-4.5 nm)	A11 nCNC)		
Mobility distribution of ions (0.8–40 nm)	Neutral cluster and Air Ion Spectrometer (Airel Ltd)		
and size distribution of particles (2-40			
nm)			
Nitrogen oxides (NO <sub>x</sub> )	Chemiluminescence + thermal converter (TEI42S)		

Ozone (O <sub>3</sub> )	IR-absorption photometer (TEI49)			
Carbon monoxide (CO)	Non-dospersive infrared (NDIR) absorption (Horiba			
	APMA 370)			
Sulphur dioxide (SO2)	UV-flurescence (Horiba APSA 360)			
PM <sub>2.5</sub> and PM <sub>10</sub>	TEOM 1405 (Thermo Scientific)			
Physicum roof (29 m agl)				
Wind	Cup anemometer (Vaisala WAA141)			
Air temperature	Platimun resistance thermometer			
Sea level pressure	Barometer (Vaisala HMP243)			
Relative humidity	Platimun resistance thermometer + thin film polymer			
	sensor (Vaisala DPA500)			
Dew point temperature	Platimun resistance thermometer + thin film polymer			
	sensor (Vaisala DPA500)			
Precipitation	Weighting rain gauge (Ott Pluvio)			
Global radiation	Kipp and Zonen CNR1			
Reflected global	Kipp and Zonen CNR1			
Longwave radiation in	Kipp and Zonen CNR1			
Longwave radiation out	Kipp and Zonen CNR1			
PAR	Kipp and Zonen PAR lite			
Reflected PAR	Kipp and Zonen PAR lite			
Visibility	PWD			

- 12 Table S4. Average concentrations of measured components during the traffic (averages without episodes) dominated period on
- 13 workdays and weekends and their averages during four different episodes at the UB Supersite. PN concentration at UB Supersite was

14 measured using an ultrafine CPC (Dp > 2.5 nm).

Compound	Traffic	Traffic	E1	E2	E3
	workdays	weekends	22.1.2022	31.1.2022	13.2.2022
			15:00	07:00	12:00
			23.1.2022	5.2.2022	17.2.2022
			10:00	16:00	23:00
$PN(p \ cm^{-3})$	7403	5295	12063	13056	6991
$LDSA \ (\mu m^2 \ cm^{-3})$	3.8	3.5	13.0	13.7	9.8
<b>PM</b> <sub>2.5</sub> ( $\mu g m^{-3}$ )	1.2	1.3	6.3	7.3	5.6
<b>PM</b> <sub>2.5-10</sub> (µg m <sup>-3</sup> )	1.8	1.9	1.2	3.0	3.1
<b>NO</b> ( $\mu g \ m^{-3}$ )	1.5	1.3	b.d.l	10.5	2.7
$NO_2 (\mu g \ m^{-3})$	9.4	6.7	11.0	24.5	16.2
<b>BC</b> ( $\mu g m^{-3}$ )	0.18	0.17	0.91	0.98	0.70
<b>CO</b> (ppb)	141	147	197	236	192
<b>CO</b> <sub>2</sub> ( <i>ppm</i> )	427	428	433	443	432
CH4 (ppb)	2014	2020	2049	2076	2055
$O_3 (\mu g m^{-3})$	59	64	57	29	51
Total particulate organics	0.59	0.47	1.83	1.90	2.84
$(\mu g m^{-3})$					
Sulphate ( $\mu g m^{-3}$ )	0.24	0.30	1.21	1.62	1.01
<i>Nitrate</i> ( $\mu g m^{-3}$ )	0.22	0.13	1.35	0.65	1.35
Ammonium (µg m <sup>-3</sup> )	0.24	0.27	0.88	0.71	0.83
Chloride ( $\mu g m^{-3}$ )	0.03	0.03	0.05	0.02	0.12

15

**Table S5**. Filter steps of the PDA for the figure S17.

Filter	Parameter	Traffic	UB
step		Supersite	Supersite
Deriative filter (IQR)	IQR factor	1.7	1.7
	Window size	24 h	24 h
Threshold filter	Upper threshold	$10^4 \text{ cm}^{-3}$	$10^4 {\rm ~cm^{-3}}$
	Lower threshold	$60 \text{ cm}^{-3}$	$60 \text{ cm}^{-3}$
Neighboring points filter	On/off	On	On
Median filter	Median time interval	30 min	30 min
	Median deviation factor	1.5	1.5
Sparse data filter	Sparse window	30	30
(no. of data points)	Sparse threshold	24	24

### **18 Table S6.** Filter steps of the PDA for the Figure 7.

Filter	Parameter	Traffic	UB
step		Supersite	Supersite
Deriative filter (IQR)	IQR factor	1.7	1.7
	Window size	24 h	24 h
Threshold filter	Upper threshold	$30^5 \text{ cm}^{-3}$	$30^{5} \text{ cm}^{-3}$
	Lower threshold	$60 \text{ cm}^{-3}$	$60 \text{ cm}^{-3}$
Neighboring points filter	· On/off	On	On
Median filter	Median time interval	30 min	30 min
	Median deviation factor	1.5	1.5
Sparse data filter	Sparse window	30	30
(no. of data points)	Sparse threshold	24	24



Figure S1. Measurement setup inside the Aerosol and Trace-gas mobile laboratory.

22



23

24 Figure S2. The measurement timeline of the Aerosol and Trace-gas mobile laboratory. Measurement activity is denoted with letters M

25 (main street/Traffic Supersite), S (side street), D (driving), and D' (driving only along main street).



Figure S3. Time series of PN, LDSA, NO<sub>x</sub>, CO, BC and PM<sub>2.5-10</sub> at the Traffic Supersite and at the UB Supersite during the
 measurement period. The cut size of the CPC at the Traffic Supersite is 5.4 nm and at the UB Supersite 7 nm.



30

Figure S4. Diurnal variation of particle number concentration measured at the main street by an ATMo-Lab CPC (Dp<sub>50</sub>: 2.5 nm) and at the Traffic Supersite CPC (Dp<sub>50</sub>: 5.4 nm) on workdays and on weekends. Different episode time periods are denoted by the label. Geometric mean is used for averaging. Note that the ATMo-Lab did not measure continuously next to the Supersite as it was also utilised in driving measurements during the measurement days. Also, the ATMo-Lab measured during a shorter period between 18 January to 16 February 2022. Diurnal variation hours consisting of less than 30 minutes of measurement data were discarded.





Figure S5. Diurnal variation of particle number concentration measured at the main street by ATMo-Lab on workdays and on weekends. Cut-off sizes (Dp<sub>50</sub>: 2.5 nm and 10 nm) of the used instruments are indicated by the legend. Episode times are excluded from the data and geometric mean is used for averaging. Diurnal variation hours consisting of less than 30 minutes of measurement data were discarded.



42

43 Figure S6. Time series of organics, sulphate, nitrate, ammonium and chloride at the Traffic Supersite and at the UB Supersite during

4.4 the measurement period.



**Figure S7.** Average particle number size distributions measured with DMPS at the Traffic Supersite and at the UB Supersite stations

48 during non-episodic situation and during the three episodes.



50 Figure S8. Daily 4-hour back trajectories during the episodes (local time).



52 Figure S9. Mass spectra of the six factors obtained from PMF analysis.



**Figure S10.** Time series of the six factors obtained from PMF analysis.



- 58 Figure S11. Pies showing the relative abundances of measured chemical components (left) and relative abundances of calculated
- 59 organic fractions (right) during the whole campaign, during the three episodes (E1-E3) and during the traffic related time (non-
- 60 episodes) at the Traffic Supersite.



61

- 62 Figure S12. Hourly diurnal variations of concentrations of PN, BC, NO<sub>x</sub>, PM<sub>2.5</sub>, PM<sub>2.5-10</sub>, and LDSA without episodes during
- 63 workdays at the Traffic Supersite (black) and at the UB Supersite (violet) stations.
- 64



65

66 Figure S13. Hourly diurnal variations of concentrations of PN, BC, NO<sub>x</sub>, PM<sub>2.5</sub>, PM<sub>2.5-10</sub>, and LDSA without episodes during

67 weekends at the Traffic Supersite (black) and at the UB Supersite (violet) stations.



Figure S14. Hourly diurnal variations of concentrations of calculated organic fractions HOA, BBOA, SV-OOA, LV-OOA, LV-OOA
 BB, and Tr-OOA without episodes at the Traffic Supersite during workdays.



weekends

- Figure S15. Hourly diurnal variations of concentrations of calculated organic fractions HOA, BBOA, SV-OOA, LV-OOA LV-OOA BB, and Tr-OOA without episodes at the Traffic Supersite during weekends.
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Figure S16. (a) CPC Traffic Supersite, 1 min resolution. (b) CPC UB Supersite, 1 min resolution. Data gaps (assigned to one) are
shown in the bottom.

79



80



83

#### 84 The meteorological preprocessor MPP-FMI

85 The meteorological pre-processing model of the Finnish Meteorological Institute (MPP-FMI) is based on the method of

86 van Ulden and Holtslag (1985), in which the parameterization of boundary layer is evaluated with energy budget

87 method using synoptic weather observations and meteorological sounding data as input. A brief overview of the

method is given in the following, based on detailed descriptions of the method in Karppinen et al. (1997, 1998, 2000),

- and Backman et al. (2017).
- 90

- 91 Evaluation of scaling parameters  $u_*, \theta_*$  and L
- 92 The main boundary layer parameters include friction velocity ( $u_*$ ), temperature scale for turbulent heat transfer ( $\theta_*$ ), and
- 93 Monin Obukhov length (L), which are evaluated from synoptic weather observations. In addition, potential temperature
- 94 profiles from meteorological soundings are used for estimating the mixing height.
- 95 According to surface-layer similarity theory, friction velocity (u\*) is related to vertical profile of wind speed:

96 
$$u_* = \frac{U(z)k}{ln(\frac{z}{z_0}) - \psi_m(\frac{z}{L}) + \psi_m(\frac{z_0}{L})}$$
, (1)

97 where U(z) is wind speed at height z,  $z_0$  is the roughness length, and k is the von Karman constant. The stability 98 functions  $\psi_m$  used are

- 99  $\psi_m = (1 16z/L)^{1/4} 1$  for L < 0, and
- 100  $\psi_m = -17(1 e^{-0.29z/L})$  for L > 0. (2)
- 101 The temperature scale for turbulent heat transfer ( $\theta_*$ ) is a function of the turbulent heat flux at the ground surface (H<sub>o</sub>) 102 and the friction velocity:

103 
$$\theta_* = -\frac{H_o}{\varrho_a c_p u_*}$$
, (3)

104 where  $\rho_a$  is the density of air, and  $c_p$  is the specific heat capacity of air. Temperature scale can also be presented as

105 
$$\theta_* = \frac{k[\theta(z_2) - \theta(z_1)]}{ln(\frac{z_2}{z_1}) - \psi_h(\frac{z_2}{L}) + \psi_h(\frac{z_1}{L})}$$
, (4)

106 where  $z_1$  and  $z_2$  are arbitrary heights in the surface layer,  $\theta$  is the potential temperature, and  $\psi_h$  are the stability functions 107 for heat:

108 
$$\psi_h = 2ln\left(\frac{1+y^2}{2}\right)$$
, where  $y = (1 - 16z/L)^{1/4}$  for L < 0, and  
109  $\psi_h = -5z/L$  for L > 0. (5)

110 The Monin-Obukhov length is defined as

111 
$$L = \frac{T_2 u_*^2}{kg\theta_*},$$
 (6)

112 where  $T_2$  is the air temperature at the height of 2 m, k is the von Karman constant, and g is the acceleration of gravity.

114 The energy budget at the ground surface in a stationary and horizontally homogeneous boundary layer can be presented 115 as

116  $H_o + \lambda E_o = Q^* - G$ , (7)

117 where  $\lambda E_o$  is the latent heat flux, Q\* is the net radiation flux, and G is the conductive heat flux to the ground. The net 118 radiation flux can be written as

119 
$$Q^* = Q_i^* + \Delta Q^*$$
, (8)

120 where  $Q_i^*$  is the radiation flux in an isothermal atmosphere, and  $\Delta Q^*$  is the deviation from this in the real atmosphere, 121 evaluated as

122 
$$\Delta Q^* = 4\sigma T_r^3 (T_r - T_0)$$
, (9)

- 123 where  $T_r$  is the air temperature at reference height of 50 m,  $T_0$  is the surface radiative temperature, and  $\sigma$  the Stefan-
- $124 \qquad \text{Boltzmann constant. } Q_i^* \text{ can be expressed as the sum of net shortwave radiation } (K^*), \text{ net longwave radiation } (L_{\text{net}}) \text{ and }$
- 125 longwave radiation from clouds (L<sub>c</sub>):

- 126  $Q_i^* = K^* + L_{net} + L_c$ . (10)
- 127 The estimation of latent heat flux is based on Penman-Monteith equation

128 
$$\lambda E_o = \alpha \left[ \frac{s}{s+1} (Q^* - G) + \varrho_a c_p u_* \theta_d \right].$$
(11)

- 129 where  $\alpha$  is the Priestley-Taylor parameter ( $0.5 \le \alpha \le 1.0$ ),  $\theta_d$  an empirical temperature scale (0.033 K), and S is the slope
- of saturation enthalpy curve. The Priestley-Taylor parameter is estimated from solar elevation angle, precipitation,temperature and snow depth.

Combining equation (11) with wind profile equation (1) and the definition of L in equation (6), the temperature scalecan be presented as

134 
$$\theta_* = \left(\frac{\alpha S}{S+1} - 1\right) \left[\frac{Q^* - G}{\varrho_a c_p u_*}\right] - \alpha \theta_d . \quad (12)$$

135 The radiation fluxes in equation (7) are presented in terms of measured meteorological parameters. The

parameterization is mostly based on van Ulden and Holtslag (1985), complemented with parameterizations based on experimental data from Jokioinen observatory in southern Finland, as described in Karppinen et al. (1997, 1998). The

net shortwave radiation is computed from surface albedo and measured incoming radiation, and the net longwave

radiation is a function of surface radiative temperature. The radiation from clouds is evaluated using the observed

amount of low and mid-level clouds, and cloud base temperature, which is computed using adiabatic temperature

141 profile and observed cloud base height, and taking into account the seasonal variation of albedo with empirical

142 regression equations based on data from Jokioinen. Ground heat flux can be presented as

143 
$$G = -A_G(T_r - T_0)$$
, (13)

where  $A_G$  is an empirical constant (5 Wm<sup>-2</sup>K<sup>-1</sup>). The surface radiative temperature is not observed directly. The temperature difference can, however, be eliminated (van Ulden and Holtslag, 1985). For unstable boundary layer, equations (8) and (9) are combined with equation (13), and  $\Delta Q^*$  is presented as  $\Delta Q^* = -A_H Q^*$ , where  $A_H$  is an empirical coefficient. For stable boundary layer, equations (8), (9) and (13) are combined and temperature difference is presented using potential temperature profile equation

149 
$$T_r - T_0 = \theta_* \left( 30 + \frac{z_r}{kL} \right) - \Gamma_d z_r$$
, (14)

150 where  $z_r = 50$  m and  $\Gamma_d$  is the dry adiabatic lapse rate (0.01 Km<sup>-1</sup>). The scaling parameters u\*,  $\theta$ \* and L are solved with 151 an iterative procedure by varying L and using both equation (12) and profile equation (4).

152

#### 153 Evaluation of mixing height in winter

154 The method of generating the hourly time series of mixing heights is different for winter and summer periods. As this 155 study concerns only the winter season, the method for winter is described in detail in the following.

Evaluation of mixing height is based on routine midday (12 UTC) and midnight (00 UTC) sounding data. In winter, the
 boundary layer is mostly stable or near neutral in Finland. The mixing height h at time t is expressed in terms of friction
 velocity u\*:

159 
$$h(t) = s(t)u_*(t)$$
, (15)

where s is the linear interpolation coefficient, applied to compute the mixing heights between two consecutive soundings, e.g., the coefficient for hours between 00 and 12 UTC is

162 
$$s(t) = s(00) + (s(12) - s(00))\frac{t}{12}$$
. (16)

163 The parameter s at midday and midnight is computed from corresponding mixing heights, which are evaluated by

analyzing the vertical potential temperature profiles of soundings. The first two significant levels, i.e., levels for which the vertical profile of temperature direction differ significantly from a straight line, are selected from the sounding. The

166 potential temperature gradient  $g_1$  is calculated between these levels:

167 
$$g_1 = \frac{\theta_2 - \theta_1}{z_2 - z_1},$$
 (17)

- 168 where  $\theta$  is the potential temperature and z is the corresponding height of the level.
- 169 If the first gradient is greater than 0.01, the mixing height is
- 170  $h^* = \frac{4.5}{g_1 + 0.005}$  . (18)
- 171 If the gradient is between 0 and 0.01, a test temperature  $\theta_h$  is calculated:
- 172  $\theta_h = \theta_1 + g_1 h^*$ . (19)

173 If the potential temperatures of the sounding do not exceed  $\theta_h$ ,  $h^*$  is the mixing height. If a significant level i with

- 174 potential temperature above  $\theta_h$  exists, the mixing height is linearly interpolated between the lowest such level and the 175 previous significant level:
- 176  $h = min\left[z_i^* + \frac{\theta_h \theta_i^*}{\theta_i \theta_i^*}(z_i z_i^*), h^*\right],$  (20)
- 177 where  $\theta_i$  and  $\theta_i^*$  are the potential temperatures of the level i and the previous significant level, and  $z_i$  and  $z_i^*$  are the 178 corresponding heights of the level.
- 179 The simple dry parcel intersection method (Holzworth, 1964) is used to estimate the mixing height for unstablesituations.
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