



Supplement of

Impact of HO_2 / RO_2 ratio on highly oxygenated α -pinene photooxidation products and secondary organic aerosol formation potential

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9 S1 Sulfuric acid calibration for MION-APi-LTOF

The calibration source setup used by us was described in detail by KüRten et al. (2012) and was recently applied to a newer model of the MION chemical ionization inlet by He et al. (2023). In short H_2SO_4 is produced via the reaction of SO_2 with OH in a calibration source directly in front of the instrument. OH is produced via the photolysis of water from a humidified N_2 flow and the H_2SO_4 concentration is varied by variation of the humidified inflow.

The expected H_2SO_4 concentration is calculated with an open-source python library provided by Shen and He (2023). The model simulates the necessary gas phase chemistry based on a set of differential equations and uses two-dimensional convection-diffusion-reaction equations to take into account the losses of H_2SO_4 in the tubing. All that is needed for this calculation is the dimensions of the exact calibration setup. Details about the model can be found in He et al. (2023).

- 18 For the analyte signal we used the signal sum of the detected product ions HSO₄-, H₂SO₄(NO₃)- and H₂SO₄(HNO₃NO₃)- and
- 19 normalized the signal with the sum of the NO₃- ion and (HNO₃NO₃)- cluster. The resulting calibration curve can be found in
- **Figure S1**. The calibration yielded a calibration factor of $7.0 \cdot 10^9$ molecules cm⁻³·ncps⁻¹, which is in the range of calibration
- 21 factors reported before for different NO₃-MION inlets, for comparison see Rissanen et al. (2019)
- 22 $(1.4 \cdot 10^9 \text{ molecules} \cdot \text{cm}^{-3} \cdot \text{ncps}^{-1})$ and He et al. (2023) $(1.3 \cdot 10^{10} \text{ molecules} \cdot \text{cm}^{-3} \cdot \text{ncps}^{-1})$.



23

24 Figure S1: Calibration curve NO₃-MION-CIMS for H₂SO₄ calibration set-up

25 S2 Particle loss rate constant determination in SAPHIR STAR

The particle loss rate in the SAPHIR STAR chamber was determined by observation of the seed concentration decay in the chamber after stop of the particle addition. The exponential decay was fitted logarithmic as shown in **Eq. (S1)** and the lifetime $\tau_{Particle} (k_{particleLoss} = \frac{1}{\tau_{Particle}})$ was determined. t is the time since start of the decay (time since seed addition stop) and τ and b are fitted for.

$$ln(normalized signal) = -\frac{1}{\tau} * t + b$$
(S1)

30 Exemplary the result of the fit for the total surface concentration measured in the SMPS is shown in Figure S2. The

31 determination via AMS sulfate and ammonium signal as well as the number concentration measurement gave similar results.

32 Therefore, the average determined particle lifetime in the chamber of 54 minutes was used. The residence time in the chamber

33 was 63 minutes which shows that the seed particles are lost only slightly faster than the flush out rate due to some deposition.



34

35 Figure S2: Logarithmic fit of particle surface decay timeseries to determine particle lifetime in the chamber

36 S3 Box model input parameters

37 The input parameters into the model are defined by the flows into the reactor and consist of the flows themselves, their humidity 38 and the contained α -pinene, O₃ and CO concentration. Additional inputs are the temperature, pressure, and J(O¹D). The UVC 39 light is characterized by an on/off switch and the gap opening of the shielding. In separate experiments $J(O^{1}D)$ was calculated 40 from O₃ loss as a function of the gap opening. Other necessary input parameters are the OH background reactivity (loss of OH 41 without VOC present) and the wall loss of the RO_2 and HO_2 species in the STAR chamber. It is assumed that the product 42 species in the MCM are too volatile to be lost on the walls, but that the radical species are lost upon wall collision. An OH 43 background reactivity measurement (kOH instrument, see Lou et al. (2010), Fuchs et al. (2017) for more detailed information) 44 was performed in the empty, very clean chamber at the same humidity as in the experiments. This yielded a reactivity of 3 s¹. 45 The background reactivity was adapted to represent the α -pinene consumption in the photooxidation phase correctly, resulting in a maximum $k_{OH Backaround} = 5 s^{-1}$. A possible reason for the discrepancy is that the background reactivity determination 46 47 was done in a very clean chamber while during the experiment series small residual contaminations, resisting flushing over > 48 6 residence times, may have contributed to the background reactivity.

For the estimation of the maximum wall loss the following experiment was performed twice: In a gas phase α -pinene photooxidation steady state the light was turned off and the decay of HOM product signals were observed in the NO₃-MION-CIMS. This approach was used before by Ehn et al. (2014) and Sarrafzadeh et al. (2016) to determine the maximum loss in

52 the JPAC chamber.

53 Only products showing a clear single exponential decay were considered and it is assumed that the chosen HOMs are no longer

54 produced after light off and lost on wall contact. Their timeseries is used to calculate an individual lifetime τ by fitting the

55 decay curve to the function shown in Eq. (S1). From the observation of the decay of C10 products an average lifetime of

56 τ =171 s is determined.

The derived wall loss rate for HOM was also applied to describe the wall loss of RO₂ radicals, and therefore, $k_{RO_2 wall}$ is set as 1/170 s⁻¹. The lifetime is correlated to the transport through the diffusion layer of the chamber thus should scale with the inverse of the square root of the molar mass (under the assumption of perfect mixing of the chamber core). It is therefore expected that the smaller HO₂ radical is lost faster due to its faster transport. Additionally, the removal efficiency for HO₂ and RO₂ radicals might differ further as RO₂ are not lost necessarily on every collision with the wall. The specific RO₂ removal efficiency depends on the radical's molecular structure (Miyazaki, 2012).

63 To estimate a value for the HO₂ wall loss, the expected diffusion constant for a HOM-Mon, HOM-Acc and HO₂ are calculated

by the parametrization developed by Fuller et al. (1966) and recently reviewed by Tang et al. (2015). The results can be found

65 in Table S1.

66 Table S1. Calculated diffusion coefficients of an exemplary HOM-Mon, exemplary HOM-A

Compound	Diffusion constant at 1 bar (cm ² s ⁻¹)
C ₁₀ H ₁₅ O ₆ (HOM-Mon proxy)	0.053
$C_{20}H_{30}O_{10}$ (HOM-Acc proxy)	0.038
HO ₂	0.202

67

If the wall loss is only dependent on the diffusion to the wall (i.e. 100 % loss on wall contact), the lifetime should inversely scale with the diffusion speed. To verify this assumption, the ratio of the average lifetimes of HOM-Mon and HOM-Acc were compared to the ratio of their diffusion constants: The HOM-Acc proxy's diffusion constant is 0.71 of the monomer proxy's diffusion constant. The observed accretion products decay resulted in average lifetime of $\tau = 202$ s, leading to $k_{HOM-Acc wall} / k_{HOM-Mon wall} = 0.85$. Within the uncertainties of the diffusion constants calculation and the lifetime determination, the wall loss seems to depend indeed on the diffusion to the surface layer, thus on the diffusion constant. Therefore, considering the diffusion constant of HO₂, $k_{HO_2 wall} = 1/50$ s⁻¹ is chosen.

- 75 To study the sensitivity of the modelled HO₂/RO₂ ratio to the assumed wall loss rates, a sensitivity study was performed by
- 76 varying the rate coefficients for wall losses. The RO₂ wall loss was varied within 1σ of the determined HOM product wall loss.
- 77 The HO₂ wall loss was varied in a wider range to cover the case that not all collision with the wall lead to loss of HO₂.
- 78 Therefore, the lifetime of HO₂ was either set as 50 s or to a maximum lifetime of 170 s as determined by HOM monomer loss.
- 79 The resulting HO₂/RO₂ ratios of the sensitivity study for the Exp1 experiment are displayed in **Table S2** as an example.

80 Table S2. Box model HO₂/RO₂ ratio results at varying RO₂ and HO₂ wall loss at low HO₂/RO₂ (left) and high HO₂/RO₂ (right) in 81 the <u>Exp1</u> experiment

τ(HO ₂)	low HO ₂ /RO ₂		high H	O ₂ /RO ₂
τ(RO ₂)	<u>50 s</u>	<u>170 s</u>	<u>50 s</u>	<u>170 s</u>
<u>145 s</u>	6.8E-3	7.5E-3	0.7	1.0
<u>170 s</u>	6.4E-3	7.0E-3	0.6	0.9
<u>195 s</u>	6.1E-3	6.7E-3	0.6	0.9

82

83 The sensitivity study shows that independent of the assumed wall loss rate the HO2/RO2 ratio is around 0.007 and near one in

84 the low and high HO₂/RO₂ case, respectively. In any case, the modelling results are only used to qualify the change of chemical

85 regime and not to yield absolute values.

86 S4 Model results for HO₂, RO₂ and pinonaldehyde

Table S3. Overview of modelled steady-state concentrations for HO₂, the peroxy radical sum and pinonaldehyde. Results are presented for all experiments for low HO₂/RO₂ conditions and high HO₂/RO₂ conditions (background highlighted in grey).

Conditions	[HO ₂]ss	[RO ₂]ss sum	Pinonaldehyde
Exp1: Low HO ₂ /RO ₂	3.8E+7 cm ⁻³	6.0E+9 cm ⁻³	1.3E+10 cm ⁻³
<u>Exp1: High HO₂/RO₂</u>	1.2E+9 cm ⁻³	1.9E+9 cm ⁻³	4.8E+9 cm ⁻³
<u>Exp2.1: Low HO₂/RO₂</u>	4.6E+7 cm ⁻³	6.8E+9 cm ⁻³	1.1E+10 cm ⁻³
Exp2.1: High HO ₂ /RO ₂	1.5E+9 cm ⁻³	2.0E+9 cm ⁻³	3.7E+9 cm ⁻³
Exp2.2: Low HO_2/RO_2	4.7E+7 cm ⁻³	6.9E+9 cm ⁻³	1.1E+10 cm ⁻³
<u>Exp2.2: High HO₂/RO₂</u>	$1.5E+9 \text{ cm}^{-3}$	1.9E+9 cm ⁻³	$3.6E+9 \text{ cm}^{-3}$
Exp3: Low HO ₂ /RO ₂	$4.4E+7 \text{ cm}^{-3}$	6.3E+9 cm ⁻³	9.8E+9 cm ⁻³
Exp3: High HO ₂ /RO ₂	1.7E+9 cm ⁻³	1.7E+9 cm ⁻³	3.1E+9 cm ⁻³

89 The box model results expect average HO₂/RO₂ ratios of 6.9E-3 (~1/150) for low HO₂/RO₂ conditions and 0.8 for high

90 HO₂/RO₂ conditions. The modelled pinonaldehyde concentration is reduced to 34 % at high HO₂/RO₂. These calculations

91 only serve as indication of the expected trends as we cannot verify their results.

92 S5 Peaklist of oxidation products identified in NO₃-MION-CIMS

93 Table S4. Peaklist NO₃-MION-CIMS. All compounds were detected as clusters with (NO₃)⁻. The table is sorted into fragments,

94 monomers, and accretion products. Some compounds were just assignable in certain experiments, this is indicated by the superscript,

95 no superscript indicated that the compound was assigned in all experiments.

Fragr	nents	Monomers Accretion products		Accretion products		
$C_5H_6O_4^{E1}$	C ₈ H ₁₀ O ₆	C ₁₀ H ₁₄ O ₅	C ₁₄ H ₂₀ O ₉	C ₁₇ H ₂₄ O ₇	$C_{19}H_{26}O_8^{E1,E2}$	C ₂₀ H ₂₈ O ₉
$C_5H_6O_5$	$C_8H_{10}O_7$	$C_{10}H_{14}O_6$	$C_{14}H_{22}O_{10}$	$C_{17}H_{24}O_9$	$C_{19}H_{28}O_7$	$C_{20}H_{28}O_{11}$
C ₅ H ₆ O ₆	$C_8H_{10}O_{10}^{E1}$	C ₁₀ H ₁₄ O ₇	$C_{14}H_{22}O_{11}{}^{E1,E2}$	$C_{17}H_{24}O_{10}{}^{\text{E1,E2}}$	C19H28O8	C ₂₀ H ₃₀ O ₆
$C_5H_6O_7$	$C_8H_{12}O_5^{E1,E2}$	$C_{10}H_{14}O_8$	$C_{14}H_{26}O_{11}$	$C_{17}H_{24}O_{11}$	$C_{19}H_{28}O_9$	$C_{20}H_{30}O_7$
$C_5H_6O_8^{E_2}$	C ₈ H ₁₂ O ₆	C ₁₀ H ₁₄ O ₉		$C_{17}H_{24}O_{13}^{E1,E2}$	C ₁₉ H ₂₈ O ₁₀	C ₂₀ H ₃₀ O ₈
C ₅ H ₇ O ₈	C ₈ H ₁₂ O ₇	$C_{10}H_{14}O_{10}$	$C_{15}H_{20}O_{14}{}^{E1}$	C17H26O8	C ₁₉ H ₂₈ O ₁₁	C ₂₀ H ₃₀ O ₉
C ₅ H ₈ O ₇	$C_8H_{12}O_8$	$C_{10}H_{14}O_{11}$	$C_{15}H_{22}O_9$	$C_{17}H_{26}O_9$	$C_{19}H_{28}O_{12}{}^{E1,E2}$	$C_{20}H_{30}O_{10}$
	C ₈ H ₁₂ O ₉		C ₁₅ H ₂₂ O ₁₀	$C_{17}H_{26}O_{10}$	C ₁₉ H ₂₈ O ₁₃	C ₂₀ H ₃₀ O ₁₁
$C_6H_6O_4^{E1,E3}$	C ₈ H ₁₃ O ₈	C ₁₀ H ₁₅ O ₅	C15H22O11	$C_{17}H_{26}O_{11}$	$C_{19}H_{28}O_{14}^{E1,E2}$	C ₂₀ H ₃₀ O ₁₂
$C_6H_{10}O_5$	C ₈ H ₁₃ O ₉	$C_{10}H_{15}O_{6}$	$C_{15}H_{22}O_{12}{}^{E1,E2}$	$C_{17}H_{26}O_{12}$	$C_{19}H_{28}O_{15}^{E1}$	C ₂₀ H ₃₀ O ₁₃
$C_6H_{10}O_6$	C ₈ H ₁₄ O ₅	C ₁₀ H ₁₅ O ₇	$C_{15}H_{22}O_{13}^{E1}$	$C_{17}H_{26}O_{13}{}^{E1,E2}$	$C_{19}H_{28}O_{16}{}^{\text{E1,E2}}$	$C_{20}H_{30}O_{14}$
$C_6H_{10}O_7$	$C_8H_{14}O_6$	$C_{10}H_{15}O_8$	$C_{15}H_{22}O_{14}^{E1}$	$C_{17}H_{26}O_{14}{}^{\text{E1,E2}}$	$C_{19}H_{30}O_6$	$C_{20}H_{30}O_{15}$
	C ₈ H ₁₄ O ₇	$C_{10}H_{15}O_9$	$C_{15}H_{24}O_{13}{}^{E1,E2}$	C ₁₇ H ₂₈ O ₈	C ₁₉ H ₃₀ O ₇	$C_{20}H_{30}O_{16}$
$C_7 H_8 O_5^{E3}$	$C_8H_{14}O_8$	$C_{10}H_{15}O_{10}$	$C_{15}H_{26}O_{10}{}^{\text{E1,E2}}$	$C_{17}H_{28}O_9$	$C_{19}H_{30}O_8$	$C_{20}H_{30}O_{18}$
C7H8O6 ^{E3}	C ₈ H ₁₄ O ₉	$C_{10}H_{15}O_{11}$		$C_{17}H_{28}O_{10}$	C ₁₉ H ₃₀ O ₉	C ₂₀ H ₃₂ O ₆
C7H8O7		$C_{10}H_{15}O_{12}$	$C_{16}H_{22}O_9^{E1,E2}$	$C_{17}H_{28}O_{11}$	C ₁₉ H ₃₀ O ₁₀	C ₂₀ H ₃₂ O ₇
C ₇ H ₈ O ₈	C9H12O5		C ₁₆ H ₂₄ O ₉	C ₁₇ H ₂₈ O ₁₂	C ₁₉ H ₃₀ O ₁₁	C ₂₀ H ₃₂ O ₈
$C_7H_{10}O_5^{E1,E3}$	$C_9H_{12}O_6$	$C_{10}H_{16}O_4$	$C_{16}H_{24}O_{10}$		$C_{19}H_{30}O_{12}$	$C_{20}H_{32}O_9$
C7H10O6	C9H12O7	$C_{10}H_{16}O_5$	C ₁₆ H ₂₄ O ₁₁	C ₁₈ H ₂₆ O ₉	C ₁₉ H ₃₀ O ₁₃	C ₂₀ H ₃₂ O ₁₀
C7H10O7	C9H12O8	$C_{10}H_{16}O_{6}$	$C_{16}H_{24}O_{12}{}^{E1,E2}$	$C_{18}H_{26}O_{10}$	$C_{19}H_{30}O_{14}^{E1,E2}$	C ₂₀ H ₃₂ O ₁₁
$C_7H_{10}O_8$	$C_9H_{12}O_9$	$C_{10}H_{16}O_7$	$C_{16}H_{26}O_8$	$C_{18}H_{26}O_{11}$	$C_{19}H_{30}O_{15}{}^{\text{E1,E2}}$	$C_{20}H_{32}O_{12}$
$C_7H_{10}O_9^{E1,E2}$	$C_9H_{12}O_{12}^{E2}$	$C_{10}H_{16}O_8$	$C_{16}H_{26}O_9$	$C_{18}H_{26}O_{15}^{E1}$	$C_{19}H_{30}O_{16}^{E1}$	C ₂₀ H ₃₂ O ₁₃
C7H10O10	C9H13O9	$C_{10}H_{16}O_9$	$C_{16}H_{26}O_{10}$	$C_{18}H_{28}O_6$	C ₁₉ H ₃₂ O ₇	C ₂₀ H ₃₂ O ₁₄
C7H14O5 ^{E1,E2}	C9H13O10	$C_{10}H_{16}O_{10}$	$C_{16}H_{26}O_{11}$	C ₁₈ H ₂₈ O ₈	C19H32O8	C ₂₀ H ₃₂ O ₁₅
C7H14O6	C9H14O4	$C_{10}H_{16}O_{11}$	C ₁₆ H ₂₆ O ₁₂	$C_{18}H_{28}O_9^{E1}$	C19H32O9	C ₂₀ H ₃₄ O ₆
	C9H14O5		$C_{16}H_{26}O_{13}E_{2}$	$C_{18}H_{28}O_{10}$	C ₁₉ H ₃₂ O ₁₀	C ₂₀ H ₃₄ O ₇
	C ₉ H ₁₄ O ₆	C ₁₀ H ₁₇ O ₆	$C_{16}H_{28}O_{18}^{E1,E2}$	C ₁₈ H ₂₈ O ₁₁	C ₁₉ H ₃₂ O ₁₁	C ₂₀ H ₃₄ O ₈
	$C_9H_{14}O_7$	$C_{10}H_{17}O_7$		$C_{18}H_{28}O_{12}^{E1,E2}$	$C_{19}H_{32}O_{12}$	$C_{20}H_{34}O_9$
	C9H14O8	C ₁₀ H ₁₇ O ₈		C ₁₈ H ₂₈ O ₁₃	$C_{19}H_{32}O_{13}^{E1}$	C ₂₀ H ₃₄ O ₁₀
	C9H14O9	C ₁₀ H ₁₇ O ₉		$C_{18}H_{28}O_{14}^{E1,E3}$	C ₁₉ H ₃₂ O ₁₄ ^{E1,E2}	C ₂₀ H ₃₄ O ₁₁
	$C_9H_{14}O_{10}$	$C_{10}H_{17}O_{10}{}^{\text{E1,E3}}$		$C_{18}H_{28}O_{15}^{E1}$		C ₂₀ H ₃₄ O ₁₂
	$C_9H_{16}O_5$	$C_{10}H_{17}O_{11}{}^{\text{E3}}$		$C_{18}H_{28}O_{16}{}^{E1,E3}$		$C_{20}H_{34}O_{13}$
	$C_9H_{16}O_6$			C ₁₈ H ₃₀ O ₇		
	C9H16O7	$C_{10}H_{18}O_4$		C ₁₈ H ₃₀ O ₈		
	C ₉ H ₁₆ O ₈	$C_{10}H_{18}O_5$		$C_{18}H_{30}O_9$		
		$C_{10}H_{18}O_6$		$C_{18}H_{30}O_{10}$		
		C ₁₀ H ₁₈ O ₇		C ₁₈ H ₃₀ O ₁₁		
		C ₁₀ H ₁₈ O ₈		C ₁₈ H ₃₀ O ₁₂		
		C ₁₀ H ₁₈ O ₉		C ₁₈ H ₃₀ O ₁₃		
				$C_{18}H_{30}O_{14}{}^{E1}$		

96 S6 Exemplary reported HO₂/RO₂ ratios from field studies

Conditions	$HO_2 (10^8 cm^{-3})$	$RO_2 (10^8 cm^{-3})$	HO ₂ /RO ₂	Source
Autumn, Pearl Riva Delta, China				(Tan et al., 2019)
(polluted)				
Morning (median)	0.8	0.3	2.7	
Afternoon (median)	2.5	1.7	1.5	
Winter, Beijing, China				(Tan et al., 2018)
(urban)				
Background (24 h average)	1.04 ± 0.62	0.70 ± 0.34	1.5	
Clean (24 h average)	0.93 ± 0.72	0.76 ± 0.46	1.2	
Polluted (24 h average)	0.52 ± 0.23	0.71 ± 0.41	0.7	
Jülich, Germany				(Cho et al., 2023)
(rural)				
Spring & Summer noon (median)	3.0	3.0	1.0	
Summer, Michigan, USA				(Bottorff et al.,
(rural forest)				2023)
Average diurnal maximum	3.5	4.0	1.1	
September, Colorado, USA				(Stevens et al.,
(remote)	(Uncertainty		(Uncertainty factor	1997)
Single measurements:	factor of 2)		of 2)	
$High NO_X (1.9 ppbv)$	0.3	4.7 ± 2.0	0.1	
Low $NO_X(0.5 ppbv)$	1	4 ± 2	0.3	
Schauinsland/Pabsthum, Germany	-	-	Reported ratios	(Mihelcic et al.,
(rural)			around 1 for a	2003)
			range of NO	
			concentrations	
			(0.1 – 1.5 ppbv)	

97 Table S5. Measured HO₂ and RO₂ concentrations from field studies under different atmospheric conditions.

98

99 S7 Estimation of change in peroxy radical steady state concentration between low and high HO₂/RO₂

Starting from the balance equation **Eq. (S2)**, we derived an equation for the steady state concentration (indicated by subscript SS) of an $[RO_2]_i$ (**Eq. (S3)**). The equations assume a primary production term Pri_i for $[RO_2]_i$, as well as only three significant loss pathways: The reaction with the pool of available $[RO_2]$ with a bulk reaction rate constant k_{RO2RO2} , the reaction with $[HO_2]$ with a reaction rate of $k_{RO2HO2}=2.46\cdot10^{-11}$ cm³·s⁻¹ at 20 °C as defined in the MCM (Jenkin et al., 1997; Saunders et al., 2003) and the wall loss. A wall loss rate coefficient of 1/170 s was used, as determined by our measurements for HOM products (see supplement section **S3**). The rate coefficient k_{RO2RO2} was varied in a range 1.0-5.0·10⁻¹² cm³·s⁻¹, typical values expected for substituted organic peroxy radicals (Jenkin et al., 2019), to determine what bulk rate coefficient would be reconcilable with

- 107 our observations. To compare directly to the measured ratio of HOM-RO₂ signal, we calculated the RO₂ concentration ratio at
- 108 high to low HO₂/RO₂ applying Eq. (S4). In Eq. (S4) the primary production term Pri_i could be eliminated as the primary
- 109 production was same at high and low HO₂/RO₂ in our experiments.

$$\frac{d[RO_2]_i}{dt} = Pri_i - k_{RO2RO2}[RO_2][RO_2]_i - k_{HO2}[HO_2][RO_2]_i - k_{wall}[RO_2]_i$$
(S2)

$$[RO_2]_{i,SS} = \frac{Pri_i}{k_{RO2RO2}[RO_2] + k_{HO2}[HO_2] + k_{wall}}$$
(S3)

$$\frac{[RO_2]_{i,SS,highHO2}}{[RO_2]_{i,SS,lowHO2}} = \frac{k_{RO2RO2}[RO_2]_{SS,lowHO2} + k_{HO2}[HO_2]_{SS,lowHO2} + k_{wall}}{k_{RO2RO2}[RO_2]_{SS,highHO2} + k_{HO2}[HO_2]_{SS,highHO2} + k_{wall}}$$
(S4)

Calculation of condensation rate constant k_{cond} 110 **S8**

111 The condensation rate constant k_{cond} of each compound was calculated as shown in Eq. (S5). Here α is the accommodation 112 coefficient and is set to 1. \bar{v} is the mean molecular speed calculated from the molar mass of the compound and S_{Ptot} is the total 113 particle surface measured in the chamber. f_{FS} is the Fuchs-Sutugin factor which is calculated as shown in Eq. (S6), where knn 114 is the Knudsen Number calculated as shown in Eq. (S7). \bar{s} represents the mean free path of the molecule and p_{dia} the particle diameter. For *p*_{dia} we used the median diameter of the particle surface distribution measured (McFiggans et al., 2019). 115

$$k_{cond} = \alpha * f_{FS} * \frac{\bar{\nu}}{4} * S_{Ptot}$$
(S5)

$$f_{FS} = \frac{1 + knn}{1 + (0.75 * \frac{\alpha}{knn}) + knn + (0.283 * \alpha)}$$
(S6)

$$knn = \frac{2 * \bar{s}}{p_{dia}} \tag{S7}$$

116 S9 Error estimation via error propagation

Error propagation was utilized to estimate the error of derived parameters. For a parameter q, the error is defined by the errors of the variables x, ..., z necessary to calculate q. The general equation to calculate the absolute uncertainty δq can be found in **Eq. (S8)**. This equation is only valid if the uncertainties in x, ..., z are independent and random. (Taylor, 1997)

$$\delta q = \sqrt{\left(\frac{\partial q}{\partial x}\delta x\right)^2 + \ldots + \left(\frac{\partial q}{\partial z}\delta z\right)^2}$$
(S8)

For all measured parameters the measured standard deviation in steady state was used as the absolute uncertainty. For parameters that cannot be measured directly their uncertainties were calculated with error propagation as shown in **Eq. (S8)**. For the diffusion coefficient we used uncertainties reported in the literature: Tang et al. (2015) reviewed diffusion coefficient calculation and came to the result that the difference between measurement and estimation via the method of Fuller et al. (1966) are mostly below 10 %. Therefore, we assumed a 10 % uncertainty for the diffusion coefficient of each formula composition.

126 S10 Comparison of approximated (upper limit) HOM particulate mass concentration with measured organic mass



• calculated particle phase HOM mass concentration

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128 Figure S3: Comparison of particulate, organic mass concentration (measured by AMS) and approximation from NO₃-MION-

129 CIMS measurements. Error of AMS measurement is estimated as 20 %. For calculated particle phase HOM mass

130 concentration we assumed an uncertainty of factor 2 in the calibration factor (He et al., 2023).

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