



*Supplement of*

## **Predicting photooxidant concentrations in aerosol liquid water based on laboratory extracts of ambient particles**

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**Table S1.** Particle sample collection and PME information

Sample ID <sup>a</sup>	Collection dates <sup>b</sup>	Sampling duration for each filter <sup>c</sup> (h)	Avg. PM <sub>2.5</sub> conc. <sup>d</sup> (μg/m <sup>3</sup> -air)	Particle mass/water ratio <sup>e</sup> (10 <sup>-4</sup> μg PM/μg H <sub>2</sub> O)	α <sub>300</sub> <sup>f</sup> (cm <sup>-1</sup> )	R <sub>abs</sub> (300-450 nm) (10 <sup>-6</sup> mol-photons L <sup>-1</sup> s <sup>-1</sup> ) <sup>g</sup>	R <sub>abs</sub> (300-450nm) / R <sub>abs</sub> (300-λ <sub>end</sub> ) <sup>h</sup>	AAE <sup>i</sup>	MAC <sub>DOC</sub> (m <sup>2</sup> (g C) <sup>-1</sup> ) <sup>j</sup>		DOC (mg C L <sup>-1</sup> )	Light screening factor <sup>k</sup>	
									300 nm	365 nm		PME	PME+DMB
WIN-10	2/5/20 – 2/28/20	168 (one week)	9.2	0.51 (±0.09)	0.086	1.5	0.84	7.58	2.0	0.57	10.1	0.98	0.75
WIN-2				2.6 (±0.4)	0.446	7.8	0.79	7.28	2.2	0.65	47.2	0.88	N.A.
WIN-0.7				5.5 (±0.9)	1.089	19	0.75	7.23	2.5	0.74	102.1	0.74	0.64
WIN-0.4				10 (±1.5)	1.820	33	0.74	7.02	2.0	0.63	206.3	0.61	N.A.
WIN-0.3				16 (±2.4)	3.029	56	0.74	7.00	2.1	0.65	335.6	0.48	0.40 <sup>l</sup>
WIN-0.3D <sup>m</sup>				2.4 (±0.4)	0.452	8.1	0.78	7.16	2.1	0.64	50.2	0.88	0.73
SUM-10	8/21/20 – 8/24/20	28.8	54.5	0.42 (±0.07)	0.220	3.9	0.83	7.42	3.1	0.96	16.4	0.94	0.75
SUM-2				2.1 (±0.4)	1.062	20	0.79	7.17	3.4	1.07	72.7	0.74	N.A.
SUM-0.7				5.5 (±1.3)	2.780	51	0.77	7.17	3.1	0.97	208.9	0.50	0.46
SUM-0.4				11 (±2.3)	5.147	97	0.77	7.05	3.1	0.99	383.4	0.32	N.A.
SUM-0.3				14 (±2.4)	6.679	128	0.74	6.93	3.1	1.01	495.4	0.26	0.23 <sup>l</sup>
PME-NR <sup>n</sup>	10/6/20 – 10/8/20	48	30.9	6.4 (±0.2)	1.504	22	0.75	7.57	1.7	0.40	209.9	0.70	0.61
PME-R <sup>n</sup>				6.4 (±0.3)	1.579	23	0.81	7.74	1.8	0.44	204.3	0.68	0.60
Field blanks <sup>o</sup>													
FB1	8/4/20	3 min	6.9	0.16 (±0.06)	0.0022	0.017	1.0				2.1	1	
FB2	1/2/20	3 min	15.6	0.13 (±0.06)	0.0015	0.0013	1.0				2.0	1	
FB3	10/5/20	3 min	39.6	0.47 (±0.38)	0.0065	0.086	1.0				3.0	1	

<sup>a</sup> Samples were named as “PME-water volume” (e.g., WIN-0.7) to denote the sample and extraction volume. WIN-0.3D is the WIN-0.3 sample diluted to an equivalent extract volume of 2 mL/square (i.e., to the equivalent dilution of WIN-2).

<sup>b</sup> For the WIN and SUM samples, we collected three separate, consecutive filters during each collection period and then composited them during extraction. Each winter filter was collected for a week, while each summer filter was collected for approximately 29 hrs. The 10/6/20-10/8/20 sample was just one filter collected for 48 h.

<sup>c</sup> The average sampling duration for each filter within a given composite.

<sup>d</sup> Average PM<sub>2.5</sub> concentration for each sampling period measured at the UC Davis sampling site by the California Air Resources as reported on the iADAM online database (California Air Resources Board, 2019 –2020; <https://www.arb.ca.gov/adam>).

<sup>e</sup> Particle mass/water mass ratio (±1 σ) is calculated as the extracted particle mass per filter square (determined as the difference of filter weights before and after extraction) divided by the volume of water used for extraction.

<sup>f</sup> Base-10 absorbance coefficient of the extract (in cm<sup>-1</sup>) at 300 nm. This is determined as the sample absorbance divided by the cell pathlength.

<sup>g</sup> Rate of sunlight absorption by PME in the 300-450 nm wavelength range, calculated by equation 2 in Kaur et al. (2019), using the actinic flux at midday on the winter solstice in Davis (photons cm<sup>-2</sup> s<sup>-1</sup> nm<sup>-1</sup>) obtained from the Tropospheric Ultraviolet and Visible (TUV) Radiation Model version 4.1. If we apply the actinic flux at midday on the summer solstice, the rate of light absorption is larger by a factor 1.9.

<sup>h</sup> Ratio of the rate of light absorption calculated over a range of 300 to 450 nm to the rate of light absorption calculated from 300 nm to the longest wavelength before the absorbance goes to zero (λ<sub>end</sub>).

<sup>i</sup> AAE, the Angstrom Absorption Exponent, is calculated as the negative slope of a linear regression between ln(absorbance) vs. ln(wavelength) in the 300 – 450 nm wavelength range.

20 <sup>j</sup> Mass absorption coefficients at 300 or 365 nm, normalized to dissolved organic carbon, calculated as  $MAC_{DOC,300nm} = \frac{\alpha_{300nm} \times \ln(10) \times 10^6}{[DOC]}$  (Kaur et al., 2019).

The contributions of nitrate and nitrite to the total absorbance of PME samples are negligible (< 2 %) for both wavelengths.

25 <sup>k</sup> Light-absorption-weighted internal screening factor, calculated with equation 2 in Smith et al. (2016) using a wavelength range of 280-364 nm. A value of 1 indicates no light screening, while a low value represents a strong screening effect. “PME” column shows light screening factors in PME samples, while “PME+DMB” column shows values in the PME with added 80 μM DMB (used for inhibition factor measurements; see Section S1). The cell pathlength was 0.5 cm. To save sample volume, *IF* values were not measured for the -2 and -0.4 extracts, so screening factors are not available for these dilutions.

<sup>l</sup> For these very concentrated PME samples, 160 μM DMB was used for inhibition factor measurements. Values shown here are light screening factors of PME with 160 μM DMB.

<sup>m</sup> To test the impact of rotary evaporation on sample composition and photochemistry, this extract was prepared by taking the rotovapped WIN-0.3 extract and diluting it to the same PM mass/water mass ratio as the WIN-2 sample, which was not rotovapped.

30 <sup>n</sup> To test the impact of rotovapping, this pair of extracts was prepared using portions of the same filter. For the PME-NR sample, the filter was extracted with 0.7 mL water/square and was not rotovapped. For the PME-R sample, the filter was extracted with 2 mL water/square, and was then rotovapped to an equivalent extract volume of 0.7 mL/square.

<sup>o</sup> Field blank samples were extracted with 1.0 mL water/square. Field blank results were not subtracted from sample results.

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**Table S2.** Ion concentrations in PME

Sample ID	[NO <sup>3-</sup> ] (μM)	[NO <sub>2</sub> <sup>-</sup> ] (μM)	[SO <sub>4</sub> <sup>2-</sup> ] (μM) <sup>a</sup>	[Cl <sup>-</sup> ] (μM)	[HCOO <sup>-</sup> ] (μM)	[NH <sub>4</sub> <sup>+</sup> ] (μM)	[Na <sup>+</sup> ] (μM)	[K <sup>+</sup> ] (μM)	[Ca <sup>2+</sup> ] (μM)
WIN-10	179.1	< DL <sup>e</sup>	25.0	5.21	2.65	160.8	196.3	34.0	68.8
WIN-2	793.1	3.49	346.9	29.3	30.3	590.4	612.1	98.4	240.3
WIN-0.7	1535	6.49	538.8	20.5	45.9	1826.7	1238.3	261.4	449.9
WIN-0.4	3215	13.6	1435	89.7	116.4	2558.6	2543.9	457.3	149.4
WIN-0.3	5221	21.3	2347	129.2	193.6	3898.2	3601.5	658.4	1214
WIN-0.3D <sup>b</sup>									
SUM-10	27.4	< DL	21.4	5.21	3.53	100.8	134.2	31.5	50.4
SUM-2	137.6	1.95	90.3	23.4	46.0	208.1	276.0	101.1	98.1
SUM-0.7	325.9	2.49	194.1	64.2	92.8	676.4	607.5	315.8	70.5
SUM-0.4	777.7	< DL	478.0	144.7	145.5	1125	1360	561.3	578.6
SUM-0.3	1018	7.85	618.2	184.2	187.9	1330	1717	676.4	696.7
PME-NR	487.0	8.00	352.7	5.21	3.53	1565	1458	356.5	606.6
PME-R	479.7	8.00	349.1	23.4	46.0	1496	1201	517.0	526.7
Field blanks <sup>c</sup>									
FB1 <sup>d</sup>	3.12	<DL		2458	3.03	0.12	96.0	-0.02	7.01
FB2	4.58	<DL		1.07	2.94	1.42	93.8	5.92	7.02
FB3	1.99	<DL	12.4	0.65	5.54	1.11	124.6	8.88	7.08

<sup>a</sup> Sulfate from the sulfuric acid added to adjust the sample to pH 4.2 has been subtracted. The added trace-metal grade sulfuric acid contributed an average ( $\pm \sigma$ ) of 40 ( $\pm$  47) μM sulfate.

<sup>b</sup> Ion concentrations were not measured in this sample.

<sup>c</sup> Field blank results were not subtracted from sample results.

<sup>d</sup> This field blank sample was contaminated by the pH electrode filling solution, resulting in extremely high concentrations of Cl<sup>-</sup> and possible other, uncharacterized, contaminants.

<sup>e</sup> Below detection limit.

**Table S3.** Hydroxyl radical measurements

Sample ID	$P_{OH}$ ( $10^{-9}$ M $^{-1}$ s $^{-1}$ ) <sup>a</sup>	$k'_{OH}$ ( $10^6$ s $^{-1}$ ) <sup>b</sup>	[•OH] ( $10^{-15}$ M) <sup>c</sup>	$10^4 \times \Phi_{OH}$ <sup>d</sup>	$k_{DOC+OH}$ ( $10^8$ L (mol-C) $^{-1}$ s $^{-1}$ ) <sup>e</sup>	% $P_{OH,NO_3^-}$ <sup>f</sup>
WIN-10	0.24 ( $\pm$ 0.01)	0.20 ( $\pm$ 0.03)	1.2 ( $\pm$ 0.2)	1.7 ( $\pm$ 0.1)	4.5 ( $\pm$ 0.4)	10.4
WIN-2	4.6 ( $\pm$ 0.4)	8.82 ( $\pm$ 0.09)	5.6 ( $\pm$ 0.4)	5.8 ( $\pm$ 0.5)	3.1 ( $\pm$ 0.3)	2.4
WIN-0.7	16.4 ( $\pm$ 1.5)	2.2 ( $\pm$ 0.2)	7.4 ( $\pm$ 0.2)	8.6 ( $\pm$ 0.8)	1.6 ( $\pm$ 0.8)	1.3
WIN-0.4	21.3 ( $\pm$ 5.3)	2.6 ( $\pm$ 0.7)	6.8 ( $\pm$ 0.5)	6.3 ( $\pm$ 1.6)	2.5 ( $\pm$ 0.5)	2.1
WIN-0.3	47.5 ( $\pm$ 41.2)	9.9 ( $\pm$ 8.6)	4.8 ( $\pm$ 0.3)	8.5 ( $\pm$ 7.4)	2.6 ( $\pm$ 3.1)	1.5
WIN-0.3D			4.1 ( $\pm$ 0.4)			
SUM-10	0.26 ( $\pm$ 0.01)	0.61 ( $\pm$ 0.06)	0.43 ( $\pm$ 0.01)	0.67 ( $\pm$ 0.03)	2.4 ( $\pm$ 0.4)	1.5
SUM-2	1.8 ( $\pm$ 0.1)	1.9 ( $\pm$ 0.2)	1.0 ( $\pm$ 0.01)	0.94 ( $\pm$ 0.07)	2.1 ( $\pm$ 0.2)	1.0
SUM-0.7	12.3 ( $\pm$ 5.7)	2.8 ( $\pm$ 1.4)	4.4 ( $\pm$ 0.6)	2.4 ( $\pm$ 1.1)	2.6 ( $\pm$ 0.3)	0.4
SUM-0.4	57.3 ( $\pm$ 10.7)	8.0 ( $\pm$ 1.5)	7.2 ( $\pm$ 0.1)	5.9 ( $\pm$ 1.1)	1.5 ( $\pm$ 0.4)	0.2
SUM-0.3	81.5 ( $\pm$ 98.4)	10.6 ( $\pm$ 12.8)	7.7 ( $\pm$ 0.7)	6.4 ( $\pm$ 7.7)	3.5 ( $\pm$ 3.1)	0.2
PME-NR			4.2 ( $\pm$ 0.3)			
PME-R			4.6 ( $\pm$ 0.8)			
Field blanks <sup>g</sup>						
FB1 <sup>h</sup>			0.57 ( $\pm$ 0.03)			
FB2 <sup>i</sup>	0.0011 ( $\pm$ 0.0001)	0.20 ( $\pm$ 0.02)	0.06 ( $\pm$ 0.01)			5.7
FB3 <sup>i</sup>	0.0008 ( $\pm$ 0.0001)	0.05 ( $\pm$ 0.02)	0.15 ( $\pm$ 0.01)			3.6

<sup>a</sup> Davis winter solstice-normalized rate of •OH photoproduction.

<sup>b</sup> Apparent pseudo-first-order rate constant for destruction of •OH due to natural sinks.

<sup>c</sup> Winter solstice-normalized steady-state concentration of •OH.

<sup>d</sup> Apparent quantum yield of •OH during simulated sunlight illumination, calculated as  $\Phi_{OH} = P_{OH}/R_{abs}(300-450)$ .

<sup>e</sup> Second-order rate constant of dissolved organic carbon scavenging •OH, calculated as  $k_{DOC+OH} = k'_{OH}/DOC$ . The average ( $\pm 1\sigma$ ) values for this rate constant in WIN and SUM dilutions were  $2.4 \times (\pm 0.7) \times 10^8$  L (mol-C) $^{-1}$  s $^{-1}$  and  $2.9 \times (\pm 1.1) \times 10^8$  L (mol-C) $^{-1}$  s $^{-1}$ , respectively.

<sup>f</sup> Fraction of nitrate contribution to the •OH photoproduction rate, calculated as  $(j_{NO_3 \rightarrow OH} \times [NO_3^-])/P_{OH}$  using the aqueous nitrate photolysis rate constant,  $j_{NO_3 \rightarrow OH} = 1.4 \times 10^{-7}$  s $^{-1}$  (Anastasio and McGregor, 2001) and the molar concentration of  $NO_3^-$ . We also calculated the fraction of •OH production rate due to nitrite: it is negligible, with an average value of 1 %.

<sup>g</sup> Field blank results were not subtracted from sample results.

<sup>h</sup> This field blank sample was contaminated by the pH electrode.

<sup>i</sup> The •OH production rate in field blanks was determined by adding 1.2 mM benzoic acid to 1.0 mL FB sample and monitoring the formation of *p*-hydroxybenzoic acid, assuming that all •OH produced reacts with benzoic acid.

**Table S4.** Rate constants of SYR and PTA reacting with triplet excited states, singlet oxygen, and hydroxyl radical at pH 4.2

Oxidants	$k_{\text{SYR+Ox}} (\text{M}^{-1} \text{s}^{-1})$	Reference	$k_{\text{PTA+Ox}} (\text{M}^{-1} \text{s}^{-1})$	Reference
$\bullet\text{OH}$	$20 (\pm 4) \times 10^9$	(Smith et al., 2015)	$10.3 (\pm 0.6) \times 10^9$	(Ma et al., 2023)
$^1\text{O}_2^*$	$3.6 (\pm 0.7) \times 10^7$	(Tratnyek and Hoigne, 1991)	$8.8 (\pm 0.6) \times 10^6$	
$^3\text{DMB}^*$	$3.9 (\pm 0.7) \times 10^9$	(Smith et al., 2015)	$2.5 (\pm 0.6) \times 10^9$	
Direct photodegradation	$j_{\text{SYR}} (\text{s}^{-1})$		$j_{\text{PTA}} (\text{s}^{-1})$	
	$< 4.3 \times 10^{-6}$	(Kaur and Anastasio, 2018)	$6.2 (\pm 0.2) \times 10^{-4}$	(Ma et al., 2023)

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**Table S5.** Syringol loss kinetics and resulting triplet excited state concentrations

Sample ID	$k'_{\text{SYR}}^{\text{a}}$ ( $10^{-2} \text{ min}^{-1}$ )	$f_{\text{SYR,OH}}^{\text{b}}$	$f_{\text{SYR,1O2}^*}^{\text{c}}$	$f_{\text{SYR,3C}^*}^{\text{d}}$	$[\text{}^3\text{C}^*]_{\text{SYR,uncorr}}^{\text{e}}$ ( $10^{-14} \text{ M}$ )	$[\text{}^3\text{C}^*]_{\text{SYR}}^{\text{f}}$ ( $10^{-14} \text{ M}$ )	$k'_{\text{3C}^*,\text{SYR}}^{\text{g}}$ ( $10^6 \text{ s}^{-1}$ )	$P_{\text{3C}^*,\text{SYR}}^{\text{h}}$ ( $10^{-7} \text{ M s}^{-1}$ )	$10^2 \times \Phi_{\text{3C}^*,\text{SYR}}^{\text{i}}$
WIN-10	0.63 ( $\pm 0.03$ )	0.23 ( $\pm 0.06$ )	0.07 ( $\pm 0.02$ )	0.70 ( $\pm 0.07$ )	1.9 ( $\pm 0.4$ )	4.8 ( $\pm 1.0$ )	0.85	0.40 ( $\pm 0.09$ )	2.8 ( $\pm 0.6$ )
WIN-2	1.9 ( $\pm 0.1$ )	0.35 ( $\pm 0.08$ )	0.13 ( $\pm 0.03$ )	0.52 ( $\pm 0.09$ )	4.2 ( $\pm 1.0$ )	15 ( $\pm 4$ )	1.1	1.6 ( $\pm 0.5$ )	2.1 ( $\pm 0.6$ )
WIN-0.7	3.7 ( $\pm 0.2$ )	0.24 ( $\pm 0.05$ )	0.14 ( $\pm 0.04$ )	0.62 ( $\pm 0.09$ )	9.8 ( $\pm 2.3$ )	50 ( $\pm 16$ )	1.4	7.2 ( $\pm 2.4$ )	3.7 ( $\pm 1.2$ )
WIN-0.4	4.6 ( $\pm 0.2$ )	0.18 ( $\pm 0.04$ )	0.20 ( $\pm 0.06$ )	0.62 ( $\pm 0.08$ )	12 ( $\pm 3$ )	71 ( $\pm 22$ )	2.1	15 ( $\pm 5$ )	4.4 ( $\pm 1.3$ )
WIN-0.3	3.9 ( $\pm 0.2$ )	0.15 ( $\pm 0.03$ )	0.45 ( $\pm 0.10$ )	0.40 ( $\pm 0.11$ )	6.7 ( $\pm 2.3$ )	50 ( $\pm 20$ )	2.9	15 ( $\pm 6$ )	2.6 ( $\pm 1.0$ )
WIN-0.3D	1.7 ( $\pm 0.1$ )	0.28 ( $\pm 0.06$ )	0.12 ( $\pm 0.03$ )	0.60 ( $\pm 0.09$ )	4.5 ( $\pm 1.0$ )	16 ( $\pm 5$ )	1.1	1.8 ( $\pm 0.5$ )	2.2 ( $\pm 0.6$ )
SUM-10	2.2 ( $\pm 0.1$ )	0.02 ( $\pm 0.01$ )	0.03 ( $\pm 0.01$ )	0.95 ( $\pm 0.03$ )	8.9 ( $\pm 1.6$ )	16 ( $\pm 3$ )	0.94	1.5 ( $\pm 0.3$ )	3.8 ( $\pm 0.7$ )
SUM-2	4.5 ( $\pm 0.1$ )	0.03 ( $\pm 0.01$ )	0.10 ( $\pm 0.02$ )	0.87 ( $\pm 0.03$ )	17 ( $\pm 3$ )	32 ( $\pm 7$ )	1.5	4.8 ( $\pm 1.1$ )	2.4 ( $\pm 0.5$ )
SUM-0.7	8.7 ( $\pm 0.3$ )	0.06 ( $\pm 0.01$ )	0.13 ( $\pm 0.03$ )	0.81 ( $\pm 0.04$ )	31 ( $\pm 6$ )	68 ( $\pm 18$ )	2.8	19 ( $\pm 5$ )	3.7 ( $\pm 1.0$ )
SUM-0.4	7.9 ( $\pm 0.1$ )	0.11 ( $\pm 0.02$ )	0.21 ( $\pm 0.04$ )	0.68 ( $\pm 0.05$ )	23 ( $\pm 5$ )	68 ( $\pm 18$ )	4.5	31 ( $\pm 8$ )	3.2 ( $\pm 0.9$ )
SUM-0.3	7.3 ( $\pm 0.1$ )	0.13 ( $\pm 0.03$ )	0.25 ( $\pm 0.09$ )	0.62 ( $\pm 0.10$ )	20 ( $\pm 6$ )	65 ( $\pm 20$ )	5.6	36 ( $\pm 11$ )	2.8 ( $\pm 0.9$ )
PME-NR	10.7 ( $\pm 0.3$ )	0.05 ( $\pm 0.01$ )	0.06 ( $\pm 0.01$ )	0.89 ( $\pm 0.03$ )	41 ( $\pm 8$ )	54 ( $\pm 28$ )	2.0	11 ( $\pm 6$ )	5.0 ( $\pm 2.6$ )
PME-R	11.2 ( $\pm 0.4$ )	0.05 ( $\pm 0.01$ )	0.05 ( $\pm 0.01$ )	0.90 ( $\pm 0.04$ )	43 ( $\pm 8$ )	69 ( $\pm 15$ )	2.0	14 ( $\pm 3$ )	5.9 ( $\pm 1.3$ )
Field blanks <sup>j</sup>									
FB1 <sup>k</sup>	0.031 ( $\pm 0.002$ )	2.20 ( $\pm 1.34$ )	0.11 ( $\pm 0.02$ )	-1.31 ( $\pm 1.34$ )	-0.018 ( $\pm 0.018$ )	-0.32 ( $\pm 0.33$ )			
FB2	0.008 ( $\pm 0.001$ )	0.09 ( $\pm 0.02$ )	0.05 ( $\pm 0.01$ )	0.86 ( $\pm 0.03$ )	0.30 ( $\pm 0.05$ )	0.32 ( $\pm 0.08$ )			
FB3	0.12 ( $\pm 0.01$ )	0.15 ( $\pm 0.04$ )	0.05 ( $\pm 0.01$ )	0.80 ( $\pm 0.06$ )	0.42 ( $\pm 0.08$ )	0.42 ( $\pm 0.08$ )			

<sup>a</sup> Davis winter-solstice-normalized pseudo-first-order rate constant for loss of syringol (SYR).

<sup>b</sup> Fraction of SYR loss due to hydroxyl radical, calculated as  $f_{\text{SYR,OH}} = (k_{\text{SYR+OH}} \times [\text{}^{\bullet}\text{OH}]) / k'_{\text{SYR}}$ . Hydroxyl radical concentrations are in Table S5.

<sup>c</sup> Fraction of SYR loss due to singlet oxygen, calculated as  $f_{\text{SYR,1O2}^*} = (k_{\text{SYR+1O2}^*} \times [{}^1\text{O}_2^*]) / k'_{\text{SYR}}$ . Singlet oxygen concentrations are in Table S8.

<sup>d</sup> Fraction of SYR loss due to triplets, calculated as  $f_{\text{SYR,3C}^*} = (1 - f_{\text{SYR,OH}} - f_{\text{SYR,1O2}^*})$ .

<sup>e</sup> Uncorrected triplet steady-state concentration calculated from syringol loss as  $k'_{\text{SYR,3C}^*} / k_{\text{SYR+3DMB}^*}$ .

<sup>f</sup> Triplet concentration after correction for inhibition of SYR loss, calculated as  $[\text{}^3\text{C}^*]_{\text{SYR,uncorr}} / IF_{\text{SYR,corr}}$ .

<sup>g</sup> Apparent pseudo-first-order rate constant for quenching of  ${}^3\text{C}^*$  due to natural organic sinks and dissolved oxygen, as determined by SYR. This was calculated as  $k'_{\text{3C}^*,\text{SYR}} = k_{\text{rxn+Q,3C}^*}[\text{DOC}] + k_{\text{3C}^*+\text{O}_2}[\text{O}_2]$ , where  $k_{\text{rxn+Q,3C}^*}$  is estimated from the fitting between  $[\text{}^3\text{C}^*]_{\text{SYR}}$  and DOC using equation (11) in the main text (see values in Table S9), and  $k_{\text{3C}^*+\text{O}_2} = 2.8 (\pm 0.4) \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$  from Kaur et al. (2019).

<sup>h</sup> Production rate of triplets determined by SYR, calculated as  $P_{\text{3C}^*,\text{SYR}} = [\text{}^3\text{C}^*]_{\text{SYR}} \times k'_{\text{3C}^*,\text{SYR}}$ .

<sup>i</sup> Apparent quantum yield of  ${}^3\text{C}^*$  determined by SYR during simulated sunlight illumination, calculated as  $\Phi_{\text{3C}^*,\text{SYR}} = P_{\text{3C}^*,\text{SYR}} / R_{\text{abs}}$ .

<sup>j</sup> Field blank results were not subtracted from sample results.

<sup>k</sup> This field blank sample was contaminated by filling solution from a pH electrode.



**Table S6.** (Phenylthio)acetic acid (PTA) loss kinetics and resulting triplet excited state concentrations

Sample ID	$k'_{\text{PTA}}^{\text{a}}$ ( $10^{-2} \text{ min}^{-1}$ )	$f_{\text{PTA,OH}}^{\text{b}}$	$f_{\text{PTA,1O2}^{\text{c}}}$	$f_{\text{PTA,3C}^{\text{d}}}$	$[\text{}^3\text{C}^*]_{\text{PTA,uncorr}}^{\text{e}}$ ( $10^{-14} \text{ M}$ )	$[\text{}^3\text{C}^*]_{\text{PTA}}^{\text{f}}$ ( $10^{-14} \text{ M}$ )	$k'_{\text{3C}^*,\text{PTA}}^{\text{g}}$ ( $10^6 \text{ s}^{-1}$ )	$P_{\text{3C}^*,\text{PTA}}^{\text{h}}$ ( $10^{-7} \text{ M s}^{-1}$ )	$10^2 \times \Phi_{\text{3C}^*,\text{PTA}}^{\text{i}}$	$[\text{}^3\text{C}^*]_{\text{PTA}} / [\text{}^3\text{C}^*]_{\text{SYR}}^{\text{j}}$
WIN-10	0.45 ( $\pm 0.02$ )	0.17 ( $\pm 0.03$ )	0.02 ( $\pm 0.01$ )	0.81 ( $\pm 0.06$ )	2.4 ( $\pm 0.06$ )	2.4 ( $\pm 0.06$ )	0.83	0.20 ( $\pm 0.05$ )	1.4 ( $\pm 0.3$ )	0.51 ( $\pm 0.17$ )
WIN-2	2.3 ( $\pm 0.1$ )	0.15 ( $\pm 0.01$ )	0.03 ( $\pm 0.01$ )	0.82 ( $\pm 0.02$ )	13 ( $\pm 3$ )	13 ( $\pm 3$ )	1.0	1.3 ( $\pm 0.3$ )	1.6 ( $\pm 0.4$ )	0.84 ( $\pm 0.31$ )
WIN-0.7	3.8 ( $\pm 0.1$ )	0.12 ( $\pm 0.01$ )	0.03 ( $\pm 0.01$ )	0.85 ( $\pm 0.04$ )	22 ( $\pm 5$ )	22 ( $\pm 5$ )	1.3	2.8 ( $\pm 0.7$ )	1.4 ( $\pm 0.4$ )	0.43 ( $\pm 0.18$ )
WIN-0.4	6.1 ( $\pm 0.3$ )	0.07 ( $\pm 0.01$ )	0.04 ( $\pm 0.01$ )	0.89 ( $\pm 0.05$ )	36 ( $\pm 9$ )	36 ( $\pm 9$ )	1.8	6.4 ( $\pm 1.6$ )	1.9 ( $\pm 0.5$ )	0.51 ( $\pm 0.20$ )
WIN-0.3	6.6 ( $\pm 0.3$ )	0.05 ( $\pm 0.01$ )	0.06 ( $\pm 0.01$ )	0.89 ( $\pm 0.03$ )	39 ( $\pm 10$ )	39 ( $\pm 10$ )	2.4	9.3 ( $\pm 3.0$ )	1.8 ( $\pm 0.5$ )	0.78 ( $\pm 0.39$ )
WIN-0.3D	2.5 ( $\pm 0.1$ )	0.10 ( $\pm 0.01$ )	0.02 ( $\pm 0.01$ )	0.88 ( $\pm 0.02$ )	15 ( $\pm 4$ )	15 ( $\pm 4$ )	1.0	1.6 ( $\pm 0.5$ )	1.9 ( $\pm 0.6$ )	0.95 ( $\pm 0.39$ )
SUM-10	0.57 ( $\pm 0.02$ )	0.05 ( $\pm 0.01$ )	0.03 ( $\pm 0.02$ )	0.92 ( $\pm 0.04$ )	0.35 ( $\pm 0.09$ )	0.37 ( $\pm 0.10$ )	0.87	0.33 ( $\pm 0.08$ )	0.85 ( $\pm 0.21$ )	0.23 ( $\pm 0.07$ )
SUM-2	2.1 ( $\pm 0.1$ )	0.03 ( $\pm 0.01$ )	0.06 ( $\pm 0.01$ )	0.91 ( $\pm 0.03$ )	13 ( $\pm 3$ )	13 ( $\pm 4$ )	1.2	1.6 ( $\pm 0.4$ )	0.80 ( $\pm 0.22$ )	0.41 ( $\pm 0.15$ )
SUM-0.7	3.5 ( $\pm 0.1$ )	0.08 ( $\pm 0.01$ )	0.08 ( $\pm 0.01$ )	0.84 ( $\pm 0.02$ )	20 ( $\pm 5$ )	21 ( $\pm 6$ )	1.9	4.0 ( $\pm 1.1$ )	0.78 ( $\pm 0.22$ )	0.30 ( $\pm 0.12$ )
SUM-0.4	4.9 ( $\pm 0.1$ )	0.10 ( $\pm 0.01$ )	0.08 ( $\pm 0.01$ )	0.82 ( $\pm 0.03$ )	27 ( $\pm 7$ )	27 ( $\pm 8$ )	2.9	7.9 ( $\pm 2.2$ )	0.81 ( $\pm 0.23$ )	0.40 ( $\pm 0.16$ )
SUM-0.3	5.2 ( $\pm 0.2$ )	0.09 ( $\pm 0.01$ )	0.09 ( $\pm 0.03$ )	0.82 ( $\pm 0.03$ )	29 ( $\pm 7$ )	29 ( $\pm 8$ )	3.5	10 ( $\pm 3$ )	0.78 ( $\pm 0.22$ )	0.44 ( $\pm 0.19$ )
PME-NR	4.4 ( $\pm 0.1$ )	0.06 ( $\pm 0.01$ )	0.03 ( $\pm 0.01$ )	0.91 ( $\pm 0.03$ )	27 ( $\pm 7$ )	28 ( $\pm 16$ )	2.1	5.8 ( $\pm 3.2$ )	2.6 ( $\pm 1.5$ )	0.52 ( $\pm 0.40$ )
PME-R	4.8 ( $\pm 0.1$ )	0.06 ( $\pm 0.01$ )	0.03 ( $\pm 0.01$ )	0.91 ( $\pm 0.02$ )	29 ( $\pm 7$ )	41 ( $\pm 10$ )	2.0	8.4 ( $\pm 2.1$ )	3.6 ( $\pm 0.1$ )	0.60 ( $\pm 0.20$ )
Field blanks <sup>k</sup>										
FB1 <sup>l</sup>	2.75 ( $\pm 0.04$ )	0.01 ( $\pm 0.01$ )	0.00 ( $\pm 0.01$ )	0.99 ( $\pm 0.14$ )	18.1 ( $\pm 5.0$ )	20.1 ( $\pm 7.0$ )				
FB2	0.016 ( $\pm 0.005$ )	0.22 ( $\pm 0.03$ )	0.07 ( $\pm 0.01$ )	0.71 ( $\pm 0.32$ )	0.078 ( $\pm 0.040$ )	0.084 ( $\pm 0.043$ )				
FB3	0.030 ( $\pm 0.012$ )	0.31 ( $\pm 0.04$ )	0.05 ( $\pm 0.01$ )	0.64 ( $\pm 0.38$ )	0.13 ( $\pm 0.08$ )	0.13 ( $\pm 0.08$ )				

<sup>a</sup> Davis winter-solstice-normalized value of the measured pseudo-first-order rate constant for loss of PTA after correction for PTA direct photodegradation. PTA direct photodegradation accounted for (0.9-12) % of PTA total decay in PME samples, with an average of 3%. It accounted for (2-79) % of PTA total decay in field blanks.

<sup>b</sup> Contribution of hydroxyl radical to the loss of PTA, calculated as  $f_{\text{PTA,OH}} = (k_{\text{PTA+OH}} \times [\bullet\text{OH}]) / k'_{\text{PTA}}$ . Hydroxyl radical concentrations are in Table S5.

<sup>c</sup> Contribution of singlet oxygen to the loss of PTA, calculated as  $f_{\text{PTA,1O2}^*} = (k_{\text{PTA+1O2}^*} \times [{}^1\text{O}_2^*]) / k'_{\text{PTA}}$ . Singlet oxygen concentration is in the Table S8.

<sup>d</sup> Fraction of PTA loss due to triplets, calculated as  $f_{\text{PTA,3C}^*} = (1 - f_{\text{PTA,OH}} - f_{\text{PTA,1O2}^*})$ .

<sup>e</sup> Uncorrected triplet steady-state concentration calculated from PTA loss as  $k'_{\text{PTA,3C}^*} / k_{\text{PTA+3DMB}^*}$ .

<sup>f</sup> Triplet concentration after correction for inhibition of PTA loss, calculated as  $[\text{}^3\text{C}^*]_{\text{PTA,uncorr}} / IF_{\text{PTA,corr}}$ .

<sup>g</sup> Apparent pseudo-first-order rate constant for quenching of  ${}^3\text{C}^*$  determined by PTA due to natural organic sinks and dissolved oxygen. This was calculated as  $k'_{\text{3C}^*,\text{PTA}} = k_{\text{rxn+Q,3C}^*}[\text{DOC}] + k_{\text{3C}^*+\text{O}_2}[\text{O}_2]$ , where  $k_{\text{rxn+Q,3C}^*}$  is estimated from the fitting between  $[\text{}^3\text{C}^*]_{\text{PTA}}$  and DOC using equation (10) in the main text (values are in Table S9), and  $k_{\text{3C}^*+\text{O}_2} = 2.8 (\pm 0.4) \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$  from Kaur et al. (2019).

<sup>h</sup> Production rate of triplet determined by PTA, calculated as  $P_{\text{3C}^*,\text{PTA}} = [\text{}^3\text{C}^*]_{\text{PTA}} \times k'_{\text{3C}^*,\text{PTA}}$ .

<sup>i</sup> Apparent quantum yield of  ${}^3\text{C}^*$  determined by PTA during simulated sunlight illumination, calculated as  $\Phi_{\text{3C}^*,\text{PTA}} = P_{\text{3C}^*,\text{PTA}} / R_{\text{abs}}$ .

<sup>j</sup> Ratio of triplet concentration determined by PTA to that determined by SYR.

<sup>k</sup> Field blank results were not subtracted from sample results.

100 <sup>l</sup> This field blank sample was contaminated by a pH electrode, leading to fast decay of PTA.

## Section S1. Inhibition factor determination and $^3\text{C}^*$ concentration correction

Dissolved organic matter in PME may inhibit the decay of SYR or PTA by triplets, leading to an underestimation of triplet concentration. Based on our previous research, SYR is more strongly inhibited than PTA (Ma et al., 2023). To investigate and quantify the inhibition effect of PME on these two triplet probes, we measured inhibition factors ( $IF$ s) of FFA, SYR, and PTA for the -10, -0.7 and -0.3 extracts of the WIN and SUM composites, and used the  $IF$  values to correct measured  $^3\text{C}^*$  concentrations in PME. Details of inhibition factors are described in Canonica et al. (2008), Wenk et al. (2011), and Ma et al. (2023). To measure  $IF$ , we monitored the loss of 10  $\mu\text{M}$  probe in three illuminated solutions: (1) in the pH 4.2 PME; (2) in pH 4.2 Milli-Q water containing 80  $\mu\text{M}$  of triplet precursor 3,4-dimethoxybenzaldehyde (DMB); and (3) in the PME with added DMB (80  $\mu\text{M}$  DMB for the -10 extract and 160  $\mu\text{M}$  DMB for the -0.7 and -0.3 extracts). For each illumination, we determined the first-order rate constant of probe decay. The inhibition factor for the probe in that extract was calculated using

$$IF_P = \frac{k'_{DMB,PME} - k'_{PME}}{k'_{DMB}} \quad (S1)$$

where  $k'_{DMB,PME}$  is the first-order decay rate constant of probe in solution containing both DMB and PME, while  $k'_{PME}$  and  $k'_{DMB}$  are the probe loss rate constants in PME alone and in Milli-Q water with DMB, respectively. All  $k'$  values were corrected for internal light screening with screening factors ( $S_\lambda$ ); the PME and PME+DMB values are listed in Table S1, while the light screening factors for 80 and 160  $\mu\text{M}$  DMB are 0.75 and 0.59, respectively. An  $IF$  value of 1 indicates there is no DOM inhibition on probe decay, while  $IF = 0$  indicates complete inhibition of probe decay. Since  $IF_P$  can also be affected by DOM suppressing the  $^3\text{DMB}^*$  concentration, we use  $IF_{FFA}$  to quantify this triplet suppression (Ma et al., 2023). To exclude the effect of triplet suppression on  $IF_{SYR}$  and  $IF_{PTA}$  (i.e., to quantify only inhibition due to probe regeneration), we use corrected inhibition factors,  $IF_{SYR,corr}$  and  $IF_{PTA,corr}$ :

$$IF_{P,corr} = \frac{IF_P}{IF_{FFA}} \quad (S2)$$

Theoretically,  $IF$  should not exceed 1, but we sometimes see this result. When  $IF_{FFA}$  or  $IF_P$  is greater than 1, it suggests there is interaction between DOM in PME with DMB to form reactive species, and thus indicates no inhibition or suppression. Therefore, when  $IF_{FFA}$  and/or  $IF_P$  is greater than 1, we assume that  $IF_{P,corr} = IF_P$ , but we do not correct the  $^3\text{C}^*$  concentration if  $IF_{P,corr} \geq 1$ ; i.e., in this latter case  $[^3\text{C}^*]_P = [^3\text{C}^*]_{P,uncorr}$ . More details are provided in Ma et al. (2023).  $IF_{PTA}$  and  $IF_{SYR}$  values are expected to be lower than  $IF_{FFA}$  because  $IF_{PTA}$  and  $IF_{SYR}$  are affected by both triplet suppression by DOC and probe inhibition by DOC, while  $IF_{FFA}$  is only impacted by triplet suppression. However, in some samples  $IF_{PTA}$  was

greater than  $IF_{\text{FFA}}$ ; we suspect this might be due to the sometimes large errors in  $IF_{\text{FFA}}$  measurement, i.e., when the difference between  $k'_{\text{DMB,PME}}$  and  $k'_{\text{PME}}$  is small. In this case, we assume  $IF_{\text{FFA}} = IF_{\text{PTA}}$  (since PTA is very resistant to suppression) and use this value to calculate  $IF_{\text{P,corr}}$ . The determined  $IF$  and  $IF_{\text{P,corr}}$  values are shown in Table S4. Due to limited PME volumes, we did not measure  $IF$  values for the -2 and -0.4 extracts. Instead, their  $IF_{\text{SYR,corr}}$  and  $IF_{\text{PTA,corr}}$  values were estimated from the linear regression of  $1/IF_{\text{P,corr}}$  from the -10, -0.7, and -0.3 extracts versus DOC (Ma et al., 2023; Wenk et al., 2011).

The uncorrected  $^3\text{C}^*$  concentration is calculated with:

$$[{}^3\text{C}^*]_{\text{P,uncorr}} = \frac{k'_{\text{P,}^3\text{C}^*}}{k_{\text{P}+^3\text{DMB}^*}} \quad (\text{S3})$$

where  $k'_{\text{P,}^3\text{C}^*}$  is the measured first-order rate constant of probe loss due to triplets and  $k_{\text{P}+^3\text{DMB}^*}$  is the second-order rate constant of probe reacting with  $^3\text{DMB}^*$ . This assumes that the DMB triplet is a reasonable proxy for triplets in atmospheric particles and drops in Davis, as we have shown previously (Kaur and Anastasio, 2018; Kaur et al., 2019). To correct for the probe inhibition effect,  $[{}^3\text{C}^*]$  is calculated using

$$[{}^3\text{C}^*]_{\text{P}} = \frac{[{}^3\text{C}^*]_{\text{P,uncorr}}}{IF_{\text{P,corr}}} \quad (\text{S4})$$

The  $^3\text{C}^*$  concentrations shown in the main text are the values after  $IF$  correction.

**Table S7.** Inhibition factors for FFA, SYR, and PTA

Sample ID	$IF_{\text{FFA}}$	$IF_{\text{SYR}}$	$IF_{\text{PTA}}$	$IF_{\text{SYR,corr}}$	$IF_{\text{PTA,corr}}$
WIN-10	0.91 ( $\pm 0.06$ )	0.40 ( $\pm 0.02$ )	1.00 ( $\pm 0.04$ )	0.41 ( $\pm 0.03$ )	1.00 ( $\pm 0.06$ )
WIN-2 <sup>a</sup>				0.28 ( $\pm 0.04$ )	1.00 ( $\pm 0.09$ )
WIN-0.7	0.62 ( $\pm 0.10$ )	0.18 ( $\pm 0.03$ )	0.90 ( $\pm 0.07$ )	0.20 ( $\pm 0.04$ )	1.00 ( $\pm 0.11$ )
WIN-0.4 <sup>a</sup>				0.17 ( $\pm 0.04$ )	1.00 ( $\pm 0.16$ )
WIN-0.3	0.28 ( $\pm 0.08$ )	0.09 ( $\pm 0.01$ )	0.67 ( $\pm 0.10$ )	0.13 ( $\pm 0.03$ )	1.00 ( $\pm 0.21$ )
WIN-0.3D <sup>b</sup>	0.89 ( $\pm 0.13$ )	0.25 ( $\pm 0.02$ )	0.85 ( $\pm 0.06$ )	0.28 ( $\pm 0.05$ )	0.97 ( $\pm 0.17$ )
SUM-10	1.08 ( $\pm 0.09$ )	0.56 ( $\pm 0.02$ )	0.95 ( $\pm 0.08$ )	0.56 ( $\pm 0.02$ )	0.94 ( $\pm 0.07$ )
SUM-2 <sup>a</sup>				0.53 ( $\pm 0.07$ )	0.95 ( $\pm 0.12$ )
SUM-0.7	0.48 ( $\pm 0.06$ )	0.22 ( $\pm 0.03$ )	0.46 ( $\pm 0.04$ )	0.45 ( $\pm 0.09$ )	0.96 ( $\pm 0.14$ )
SUM-0.4 <sup>a</sup>				0.35 ( $\pm 0.06$ )	0.98 ( $\pm 0.14$ )
SUM-0.3	0.19 ( $\pm 0.12$ )	0.10 ( $\pm 0.02$ )	0.32 ( $\pm 0.03$ )	0.30 ( $\pm 0.06$ )	1.00 ( $\pm 0.14$ )
PME-NR <sup>c</sup>	0.68 ( $\pm 0.32$ )	0.52 ( $\pm 0.05$ )	0.65 ( $\pm 0.04$ )	0.77 ( $\pm 0.37$ )	0.95 ( $\pm 0.48$ )
PME-R <sup>c</sup>	1.29 ( $\pm 0.22$ )	0.63 ( $\pm 0.07$ )	0.71 ( $\pm 0.05$ )	0.63 ( $\pm 0.07$ )	0.71 ( $\pm 0.05$ )
Field blanks <sup>d</sup>					
FB1	0.95 ( $\pm 0.12$ )	0.52 ( $\pm 0.05$ )	0.86 ( $\pm 0.13$ )	0.54 ( $\pm 0.08$ )	0.90 ( $\pm 0.19$ )
FB2	1.10 ( $\pm 0.05$ )	0.95 ( $\pm 0.19$ )	0.93 ( $\pm 0.06$ )	0.95 ( $\pm 0.19$ )	0.93 ( $\pm 0.06$ )
FB3	1.21 ( $\pm 0.06$ )	1.20 ( $\pm 0.08$ )	1.15 ( $\pm 0.09$ )	1.20 ( $\pm 0.08$ )	1.15 ( $\pm 0.09$ )

<sup>a</sup>  $IF$  values in these samples were not measured.  $IF_{\text{SYR,corr}}$  and  $IF_{\text{PTA,corr}}$  for these samples were estimated from the linear regressions of  $1/IF_{\text{P,corr}}$  vs. DOC in each dilution series.

<sup>b</sup> The  $IF$  values were measured for WIN-0.3D, which had an equivalent dilution to the WIN-2 sample.

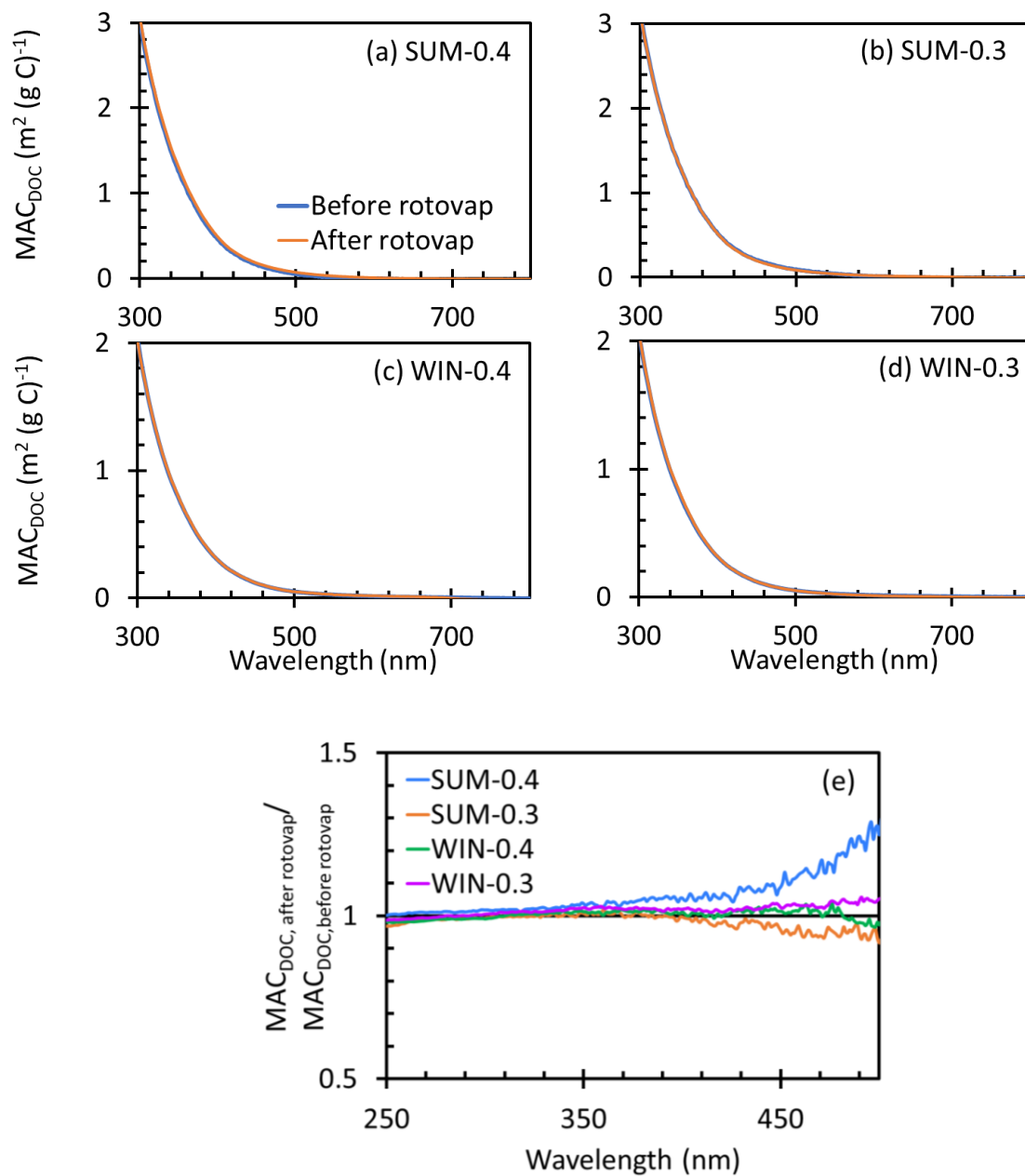
<sup>c</sup>  $IF_{\text{FFA}}$  values for PME-NR and PME-R have large uncertainties because there were very small differences between  $k'_{\text{PME,DMB}}$  and  $k'_{\text{PME}}$  for a given extract. In this case a small difference in  $k'_{\text{PME,DMB}}$  can lead to significant change of  $IF_{\text{FFA}}$ , likely explaining the very different values of  $IF_{\text{FFA}}$  in PME-R and PME-NR.

<sup>d</sup> Field blank results were not subtracted from sample results.

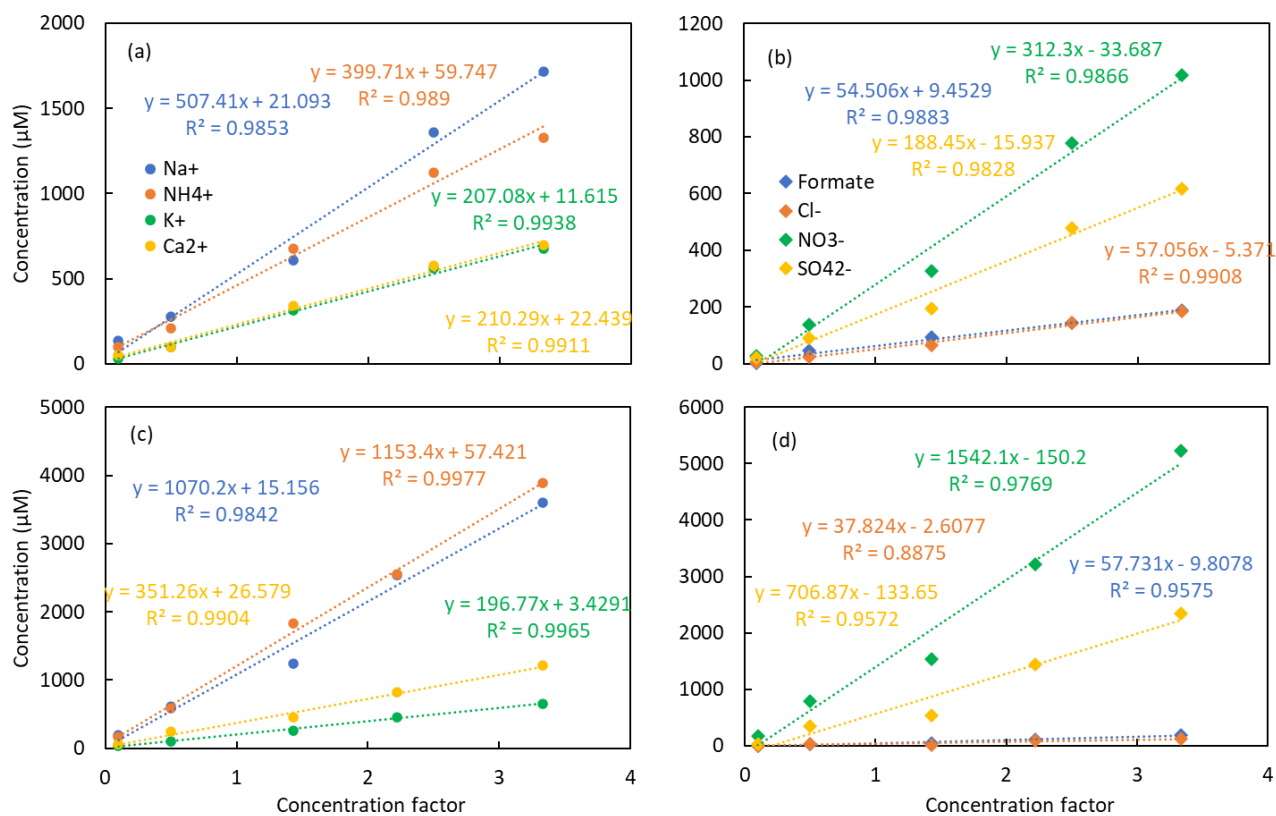
150

155

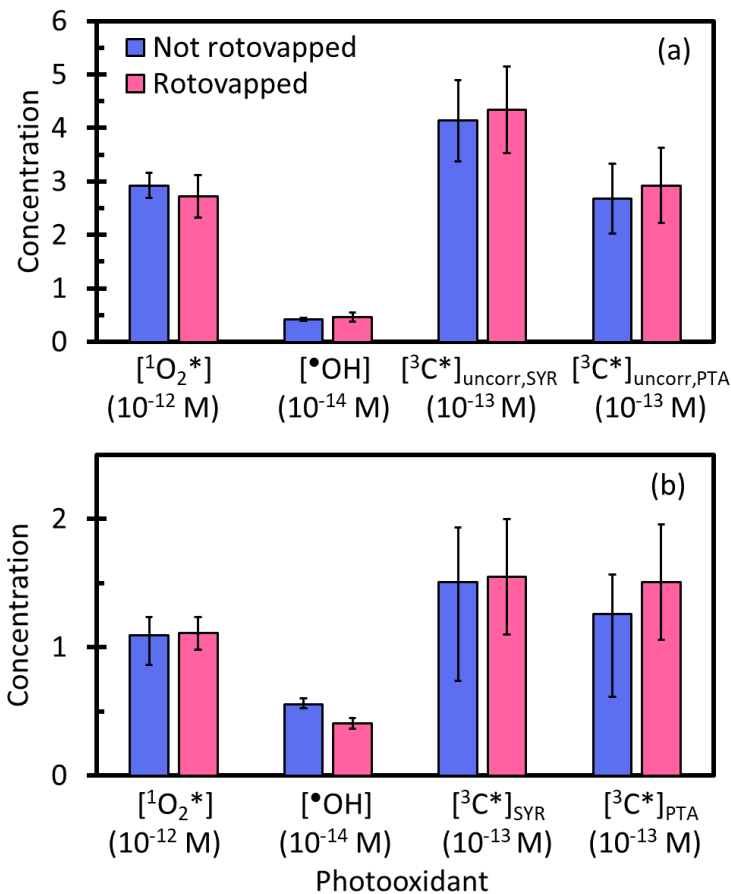
160



**Figure S1.** Mass absorption coefficients in particle extracts normalized by dissolved organic carbon before (blue) and after (orange) rotary evaporation for (a) SUM-0.4, (b) SUM-0.3, (c) WIN-0.4, and (d) WIN-0.3. (e) The ratio of MAC<sub>DOC</sub> after and before rotary evaporation for the four extracts.



**Figure S2.** Dependence of concentrations of cations (panel a for SUM and panel c for WIN) and anions (panel b for SUM and panel d for WIN) in particle extracts on concentration factor.



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**Figure S3.** Influence of roto-vapping on steady-state concentrations of  $^1\text{O}_2^*$ ,  $\cdot\text{OH}$ , and  $^3\text{C}^*$  in not rotovapped (blue) and rotovapped (red) particle extracts of (a) PME-NR vs. PME-R and (b) WIN-2 vs. WIN-0.3D. In each case, the rotovapped sample was concentrated to the concentration factor (i.e., PM mass/water mass ratio) of the not rotovapped sample. Error bars represents  $\pm 1$  standard error propagated from uncertainties in the kinetic regression and rate constants. In (a) we show  $^3\text{C}^*$  concentrations that are not *IF*-corrected because *IF*<sub>FFA</sub> values for PME-NR and PME-R differ by a factor of nearly two but have large uncertainties (Table S7).

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**Table S8.** Singlet oxygen measurements

Sample ID	$[^1\text{O}_2^*]^a$ ( $10^{-12}$ M)	$P_{1\text{O}_2^*}^b$ ( $10^{-7}$ M s $^{-1}$ )	$f_{\text{FFA},1\text{O}_2^*}^c$	$f_{\text{FFA},\text{OH}}^d$	$10^2 \times \Phi_{1\text{O}_2^*}^e$	$\Phi_{3\text{C}^*,\text{SYR}}/(\Phi_{1\text{O}_2^*}/f_\Delta)^f$	$\Phi_{3\text{C}^*,\text{PTA}}/(\Phi_{1\text{O}_2^*}/f_\Delta)^g$	$[^3\text{C}^*]_{\text{SYR}}/[^1\text{O}_2^*]^h$	$[^3\text{C}^*]_{\text{PTA}}/[^1\text{O}_2^*]^i$
WIN-10	0.21 ( $\pm 0.04$ )	0.45 ( $\pm 0.08$ )	0.53 ( $\pm 0.10$ )	0.87 ( $\pm 0.14$ )	3.1 ( $\pm 0.5$ )	0.47 ( $\pm 0.13$ )	0.24 ( $\pm 0.07$ )	0.23 ( $\pm 0.07$ )	0.12 ( $\pm 0.04$ )
WIN-2	1.1 ( $\pm 0.1$ )	2.4 ( $\pm 0.3$ )	0.62 ( $\pm 0.09$ )	0.45 ( $\pm 0.03$ )	3.1 ( $\pm 0.4$ )	0.36 ( $\pm 0.11$ )	0.28 ( $\pm 0.08$ )	0.14 ( $\pm 0.04$ )	0.12 ( $\pm 0.03$ )
WIN-0.7	2.3 ( $\pm 0.4$ )	5.0 ( $\pm 0.9$ )	0.65 ( $\pm 0.12$ )	0.61 ( $\pm 0.02$ )	2.6 ( $\pm 0.4$ )	0.76 ( $\pm 0.27$ )	0.29 ( $\pm 0.09$ )	0.22 ( $\pm 0.08$ )	0.10 ( $\pm 0.03$ )
WIN-0.4	4.3 ( $\pm 0.8$ )	9.4 ( $\pm 1.9$ )	0.69 ( $\pm 0.14$ )	0.31 ( $\pm 0.03$ )	2.8 ( $\pm 0.5$ )	0.84 ( $\pm 0.30$ )	0.36 ( $\pm 0.11$ )	0.17 ( $\pm 0.06$ )	0.09 ( $\pm 0.03$ )
WIN-0.3	8.2 ( $\pm 0.8$ )	18 ( $\pm 2$ )	0.83 ( $\pm 0.09$ )	0.14 ( $\pm 0.01$ )	3.2 ( $\pm 0.3$ )	0.43 ( $\pm 0.17$ )	0.27 ( $\pm 0.09$ )	0.06 ( $\pm 0.02$ )	0.05 ( $\pm 0.02$ )
WIN-0.3D	0.98 ( $\pm 0.13$ )	2.2 ( $\pm 0.3$ )	0.62 ( $\pm 0.08$ )	0.64 ( $\pm 0.07$ )	2.7 ( $\pm 0.3$ )	0.43 ( $\pm 0.14$ )	0.38 ( $\pm 0.12$ )	0.16 ( $\pm 0.05$ )	0.15 ( $\pm 0.05$ )
SUM-10	0.33 ( $\pm 0.19$ )	0.72 ( $\pm 0.04$ )	0.54 ( $\pm 0.32$ )	0.20 ( $\pm 0.02$ )	1.9 ( $\pm 1.1$ )	1.10 ( $\pm 0.67$ )	0.24 ( $\pm 0.15$ )	0.48 ( $\pm 0.30$ )	0.11 ( $\pm 0.07$ )
SUM-2	2.2 ( $\pm 0.2$ )	4.9 ( $\pm 0.4$ )	0.94 ( $\pm 0.10$ )	0.12 ( $\pm 0.01$ )	2.5 ( $\pm 0.2$ )	0.52 ( $\pm 0.13$ )	0.17 ( $\pm 0.05$ )	0.15 ( $\pm 0.04$ )	0.06 ( $\pm 0.02$ )
SUM-0.7	5.3 ( $\pm 0.4$ )	12 ( $\pm 1$ )	1.03 ( $\pm 0.10$ )	0.24 ( $\pm 0.03$ )	2.3 ( $\pm 0.2$ )	0.86 ( $\pm 0.24$ )	0.18 ( $\pm 0.05$ )	0.13 ( $\pm 0.04$ )	0.04 ( $\pm 0.01$ )
SUM-0.4	7.7 ( $\pm 0.6$ )	17 ( $\pm 1$ )	0.91 ( $\pm 0.09$ )	0.24 ( $\pm 0.01$ )	1.8 ( $\pm 0.1$ )	0.96 ( $\pm 0.27$ )	0.25 ( $\pm 0.07$ )	0.09 ( $\pm 0.02$ )	0.04 ( $\pm 0.01$ )
SUM-0.3	8.5 ( $\pm 2.7$ )	19 ( $\pm 6$ )	0.79 ( $\pm 0.25$ )	0.20 ( $\pm 0.02$ )	1.5 ( $\pm 0.5$ )	1.02 ( $\pm 0.45$ )	0.28 ( $\pm 0.12$ )	0.08 ( $\pm 0.03$ )	0.03 ( $\pm 0.01$ )
PME-NR	2.9 ( $\pm 0.2$ )	6.4 ( $\pm 0.5$ )	0.62 ( $\pm 0.06$ )	0.25 ( $\pm 0.02$ )	2.9 ( $\pm 0.2$ )	0.90 ( $\pm 0.47$ )	0.48 ( $\pm 0.27$ )	0.18 ( $\pm 0.10$ )	0.10 ( $\pm 0.05$ )
PME-R	2.7 ( $\pm 0.4$ )	6.0 ( $\pm 0.9$ )	0.59 ( $\pm 0.09$ )	0.28 ( $\pm 0.05$ )	2.6 ( $\pm 0.4$ )	1.22 ( $\pm 0.32$ )	0.75 ( $\pm 0.22$ )	0.25 ( $\pm 0.07$ )	0.15 ( $\pm 0.04$ )
Averages									
WIN					2.9 ( $\pm 0.3$ )	0.55 ( $\pm 0.20$ )	0.22 ( $\pm 0.05$ )	0.16 ( $\pm 0.06$ )	0.10 ( $\pm 0.04$ )
SUM					2.0 ( $\pm 0.4$ )	0.89 ( $\pm 0.23$ )	0.30 ( $\pm 0.06$ )	0.18 ( $\pm 0.17$ )	0.06 ( $\pm 0.03$ )
Field blanks <sup>j</sup>									
FB1 <sup>k</sup>	0.016 ( $\pm 0.001$ )		0.81 ( $\pm 0.15$ )	8.3 ( $\pm 4.8$ )					
FB2	0.021 ( $\pm 0.001$ )		0.66 ( $\pm 0.33$ )	0.54 ( $\pm 0.07$ )					
FB3	0.028 ( $\pm 0.001$ )		0.97 ( $\pm 0.17$ )	0.73 ( $\pm 0.09$ )					

<sup>a</sup> Davis winter solstice sunlight-normalized steady-state concentration of  $^1\text{O}_2^*$ .

180 <sup>b</sup> Production rate of  $^1\text{O}_2^*$ , calculated as  $P_{1\text{O}_2^*} = [^1\text{O}_2^*] \times k'_{\text{H}_2\text{O}}$ , where  $k'_{\text{H}_2\text{O}}$  is the first-order rate constant for loss of  $^1\text{O}_2^*$  in  $\text{H}_2\text{O}$  ( $2.2 \times 10^5 \text{ s}^{-1}$ ) (Bilski et al., 1997).

<sup>c</sup> Fraction of probe FFA lost due to  $^1\text{O}_2^*$  in PME diluted with  $\text{H}_2\text{O}$ , calculated as  $f_{\text{FFA},1\text{O}_2^*} = ([^1\text{O}_2^*]/2 \times k_{\text{FFA}+1\text{O}_2^*})/k'_{\text{FFA},\text{H}_2\text{O}}$ , where  $k_{\text{FFA}+1\text{O}_2^*}$  is the second-order rate constant of FFA reacting with  $^1\text{O}_2^*$  and  $k'_{\text{FFA},\text{H}_2\text{O}}$  is the normalized first-order decay rate of FFA in the PME diluted with  $\text{H}_2\text{O}$ .

185 <sup>d</sup> Fraction of probe FFA lost due to  $^{\bullet}\text{OH}$  in PME diluted with  $\text{H}_2\text{O}$ , calculated as  $f_{\text{FFA},\text{OH}} = ([^{\bullet}\text{OH}] \times k_{\text{FFA}+\text{OH}})/k'_{\text{FFA},\text{H}_2\text{O}}$ , where  $k_{\text{FFA}+\text{OH}}$  is the second-order rate constant of FFA reacting with  $^{\bullet}\text{OH}$  ( $1.5 \times 10^{10} \text{ M}^{-1} \text{ s}^{-1}$ ) (Ross and Ross, 1977), assuming the  $^{\bullet}\text{OH}$  concentration is the same in the diluted and undiluted portions of PME.

<sup>e</sup> Apparent quantum yield of  $^1\text{O}_2^*$ , calculated as  $\Phi_{1\text{O}_2^*} = P_{1\text{O}_2^*}/R_{\text{abs}}$ .

<sup>f</sup> Fraction of oxidizing triplets (determined by SYR) in the total triplet pool (Kaur and Anastasio, 2018).  $f_\Delta$  is the yield of singlet oxygen from the quenching of triplet states by dissolved oxygen, which we assume is 0.53 (McNeill and Canonica, 2016).

<sup>g</sup> Fraction of oxidizing triplets determined by PTA to the total triplet pool.

190 <sup>h</sup> Ratio of triplet concentration determined by SYR to the singlet oxygen concentration.

<sup>i</sup> Ratio of triplet concentration determined by PTA to the singlet oxygen concentration.

<sup>j</sup> Field blank results were not subtracted from sample results.

<sup>k</sup> This field blank sample was contaminated by a pH electrode and other unknown sources.

**Table S9.** Parameters in hyperbolic fitting between photooxidant concentration and DOC using Eqn. 11

	WIN		SUM	
	<i>a</i>	<i>b</i> (M <sup>-1</sup> )	<i>a</i>	<i>b</i> (M <sup>-1</sup> )
<sup>1</sup> O <sub>2</sub> *	2.8 (± 0.1) × 10 <sup>-10a</sup>	6 <sup>a</sup>	4.4 (± 0.3) × 10 <sup>-10</sup>	27 (± 4)
<sup>3</sup> C* <sub>SYR</sub>	0.85 (± 0.46) × 10 <sup>-10</sup>	97 (± 86)	1.2 (± 0.4) × 10 <sup>-10</sup>	149 (± 65)
<sup>3</sup> C* <sub>PTA</sub>	0.44 (± 0.05) × 10 <sup>-10</sup>	73 (± 15)	0.31 (± 0.03) × 10 <sup>-10</sup>	84 (± 13)

195 <sup>a</sup> Since winter samples show no curvature for [<sup>1</sup>O<sub>2</sub>\*] with DOC, to fit data with equation 11, *a* was obtained as the slope of linear regression between [<sup>1</sup>O<sub>2</sub>\*] and DOC, while *b* was obtained by using a fitted line that passed through only the first 4 data points (Figure S5).

**Table S10.** Second-order rate constants of triplet quenching and reaction with dissolved organic carbon<sup>a</sup>

	<i>k</i> <sub>rxn+Q,3C*</sub> (L (mol C) <sup>-1</sup> s <sup>-1</sup> )		<sup>3</sup> C* probe used
	WIN	SUM	
This work	0.47 × 10 <sup>7b</sup>	2.1 (± 0.3) × 10 <sup>7</sup>	FFA
	7.6 (± 6.8) × 10 <sup>7</sup>	12 (± 5) × 10 <sup>7</sup>	SYR
	5.7 (± 1.2) × 10 <sup>7</sup>	6.6 (± 1.0) × 10 <sup>7</sup>	PTA
Kaur et al. (2019) <sup>c</sup>	9.3 (± 1.3) × 10 <sup>7</sup>		SYR
Wenk et al. (2013) <sup>d</sup>	(1.3 – 3.9) × 10 <sup>7</sup>		-

200 <sup>a</sup> Rate constants are for DOM quenching and reaction with the pool of triplets that are seen by a given probe. FFA, by reacting with <sup>1</sup>O<sub>2</sub>\*, is likely seeing the DOM reactivity of the entire triplet pool (i.e., both oxidizing and non-oxidizing triplets), SYR is probing the reactivity of both strongly and weakly oxidizing triplets, while PTA is probing only the strongly oxidizing triplets.

205 <sup>b</sup> This value was calculated using the *b* value (Table S9) that was estimated by fitting the line of equation 11 between [<sup>1</sup>O<sub>2</sub>\*] and DOC through only the first 4 data points (Figure S5).

<sup>c</sup> Value is uncertain because triplet concentrations were not corrected for inhibition of SYR loss caused by DOM.

<sup>d</sup> Rate constant measured for quenching of triplets of 2-acetonaphthone and 3-methoxyacetophenone by surface water dissolved organic matter as determined using laser flash photolysis.

210 **Section S2. Kinetic model for singlet oxygen**

We first consider a modified equation for the steady-state  $^1O_2^*$  concentration from McNeill et al. (2016) by adding DOC as an additional sink for  $^1O_2^*$ :

$$[^1O_2^*] = \frac{k_{O_2+3C^*}[^3C^*][O_2]f_{\Delta}}{k'_{H_2O} + k_{rxn+Q,1O_2^*}[DOC]} \quad (S5)$$

215 where  $k_{O_2+3C^*}$  is the bimolecular rate constant of  $O_2$  quenching  $^3C^*$ ,  $[^3C^*]$  is the concentration of triplets that can transfer energy to  $O_2$  (i.e., essentially all triplets),  $[O_2]$  is the dissolved oxygen concentration,  $f_{\Delta}$  is the fraction of oxygen quenching triplets that produces  $^1O_2^*$ ,  $k'_{H_2O}$  is the first-order rate constant for loss of  $^1O_2^*$  by  $H_2O$  ( $2.2 \times 10^5 \text{ s}^{-1}$ ) (Bilski et al., 1997), and  $k_{rxn+Q,1O_2^*}$  is the bimolecular rate constant of DOC reacting and quenching  $^1O_2^*$ .

220 While DOC will be an important sink for  $^1O_2^*$  under ALW conditions (Kaur et al., 2019), in our PM extracts it appears the curvature of  $[^1O_2^*]$  with increasing DOC observed in SUM (Fig. 2) is only due to  $^3C^*$  since triplets are more sensitive to the presence of organics than is  $^1O_2^*$ . Therefore,  $H_2O$  is the dominant sink, and the quenching of  $^1O_2^*$  by DOC is negligible (i.e.,  $k_{rxn+Q,1O_2^*}[DOC] \ll k'_{H_2O}$ ). From Kaur et al. (2019),  $^3C^*$  in PME can be expressed as

$$[^3C^*] = \frac{\left(\frac{j_{abs}\Phi_{ISC}f}{k_{O_2+3C^*}[O_2]}\right)[DOC]}{1 + \left(\frac{k_{rxn+Q,3C^*}}{k_{O_2+3C^*}[O_2]}\right)[DOC]} \quad (S6)$$

225 where  $j_{abs}$  is the rate constant for light absorption,  $\Phi_{ISC}$  is the quantum yield of intersystem crossing,  $f$  is the fraction of DOC that is in chromophores, and  $k_{rxn+Q,3C^*}$  is the bimolecular rate constant of DOC reacting with and quenching  $^3C^*$ .

Substituting this equation for  $[^3C^*]$  into equation S5 (after applying  $k_{rxn+Q,1O_2^*}[DOC] \ll k'_{H_2O}$ ) yields

$$[^1O_2^*] = \frac{\frac{\left(\frac{j_{abs}\Phi_{ISC}f}{k_{O_2+3C^*}[O_2]}\right)[DOC]}{1 + \left(\frac{k_{rxn+Q,3C^*}}{k_{O_2+3C^*}[O_2]}\right)[DOC]} \times k_{O_2+3C^*}[O_2]f_{\Delta}}{k'_{H_2O}} = \frac{\frac{j_{abs}\Phi_{ISC}f \times f_{\Delta}}{k'_{H_2O}}[DOC]}{1 + \left(\frac{k_{rxn+Q,3C^*}}{k_{O_2+3C^*}[O_2]}\right)[DOC]} \quad (S7)$$

230 This equation is of the form

$$[^1O_2^*] = \frac{a[DOC]}{1 + b[DOC]} \quad (S8)$$

where

$$a = \frac{j_{abs}\Phi_{ISC}f \times f_{\Delta}}{k'_{H2O}} \quad (S9)$$

$$b = \frac{k_{rxn+Q,3C*}}{k_{O2+3C*}[O_2]} \quad (S10)$$

235 Since  $[^1O_2^*] = P_{1O2^*} / k'_{H2O}$  when DOC is a negligible sink of  $^1O_2^*$  (i.e. H<sub>2</sub>O is the only sink), the production rate of singlet oxygen can be calculated by

$$P_{1O2^*} = \frac{a[DOC]}{1 + b[DOC]} \times k'_{H2O} \quad (S11)$$

Thus, in our relatively dilute extracts we calculate  $P_{1O2^*}$  as  $[^1O_2^*] \times k'_{H2O}$  (Eq.10), while for extrapolating to ALW conditions we use Eq. S11 to calculate the  $^1O_2^*$  production rate.

240

**Table S11.** Parameters used for photooxidant concentration extrapolation

Parameters		WIN	SUM
Average DOC/(PM/H <sub>2</sub> O) <sup>a</sup> (mol C L <sup>-1</sup> )/(μg PM/μg H <sub>2</sub> O)		16.5	30.7
•OH	$\Delta P_{OH, aq} / \Delta DOC$ (M s <sup>-1</sup> /(mol C L <sup>-1</sup> ) <sup>b</sup> )	$1.6 \times 10^{-6}$	-
	$\Delta k'_{OH} / \Delta DOC$ (M s <sup>-1</sup> /(mol C L <sup>-1</sup> ) <sup>b</sup> )	$2.9 \times 10^8$	$2.5 \times 10^8$
<sup>1</sup> O <sub>2</sub> <sup>*</sup>	$a^c$	$2.8 \times 10^{-10}$	$4.4 \times 10^{-10}$
	$b$ (M <sup>-1</sup> ) <sup>c</sup>	6	27
	$k_{DOC+1O2^*}$ (L (mol C) <sup>-1</sup> s <sup>-1</sup> ) <sup>d</sup>	$1.0 \times 10^5$	
<sup>3</sup> C <sup>*</sup> <sub>SYR</sub>	$\Delta P_{3C^*} / \Delta DOC$ (M s <sup>-1</sup> /(mol C L <sup>-1</sup> ) <sup>b</sup> )	$6.2 \times 10^{-5}$	$9.2 \times 10^{-5}$
	$k_{rxn+Q,3C^*}$ (L (mol C) <sup>-1</sup> s <sup>-1</sup> ) <sup>e</sup>	$7.6 \times 10^7$	$12 \times 10^8$
<sup>3</sup> C <sup>*</sup> <sub>PTA</sub>	$\Delta P_{3C^*} / \Delta DOC$ (M s <sup>-1</sup> /(mol C L <sup>-1</sup> ) <sup>b</sup> )	$3.4 \times 10^{-5}$	$2.4 \times 10^{-5}$
	$k_{rxn+Q,3C^*}$ (L (mol C) <sup>-1</sup> s <sup>-1</sup> ) <sup>e</sup>	$5.7 \times 10^7$ <sup>a</sup>	$6.6 \times 10^7$

<sup>a</sup> Average ratio of DOC to particle mass/water mass ratio for each sample.

245 <sup>b</sup> Slope of linear regression between production rates or sinks for photooxidant and DOC.

<sup>c</sup> Parameters in regression fit between  $[^1O_2^*]$  and DOC using Eqn. 11 in the main text. Production rates of  $^1O_2^*$  were calculated using these parameters in Eqn. S11.

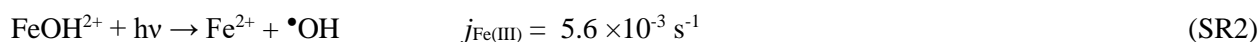
<sup>d</sup> Second-order rate constant for loss of  $^1O_2^*$  by DOC. The value is estimated using the same approach from Kaur et al. (2019) but is lower than their value of  $8.2 \times 10^5$  (L (mol C)<sup>-1</sup> s<sup>-1</sup>).

250 <sup>e</sup> Second-order rate constant for reaction and quenching of oxidizing triplets (as determined by SYR or PTA) by DOC.

### Section S3. Modeling the •OH production rate in SUM by photo-Fenton reactions

To simulate bimolecular •OH production as a function of particle mass/water mass ratio in SUM, we  
255 assume that photo-Fenton reactions are the dominant sources for •OH. We modeled this using two  
reactions (SR1 and SR2) and tuned the reactant concentrations so that calculated •OH production rates  
match measured values.

We simplified the suite of photo-Fenton reactions that produce •OH from hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>)  
using two reactions (Benkelberg and Warneck, 1995; Christensen et al., 1993; Mao et al., 2013):



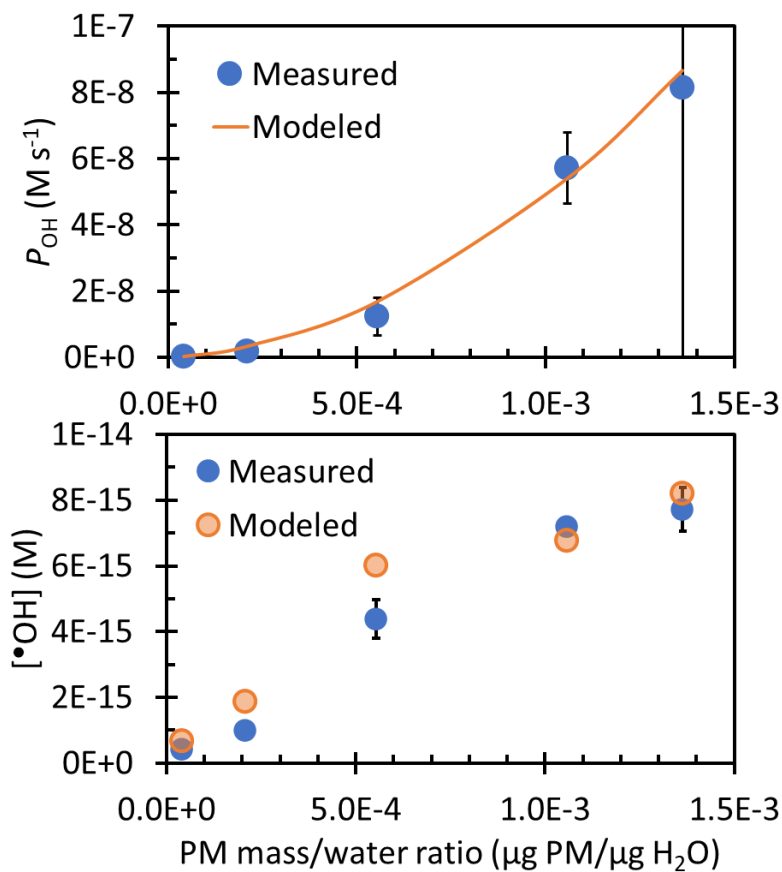
We assume that Fe<sup>2+</sup> and FeOH<sup>2+</sup> are the dominant Fe(II) and Fe(III) hydroxide species, respectively,  
which is reasonable at pH 4.2 or lower (Faust and Hoigné, 1990; Morgan and Lahav, 2007).

Fe(III)–carboxylate complexes can also undergo photolysis to produce •OH (Southworth and Voelker,  
265 2003; Weller et al., 2014), but we neglect them here. The •OH production rate from SR1 and SR2 is

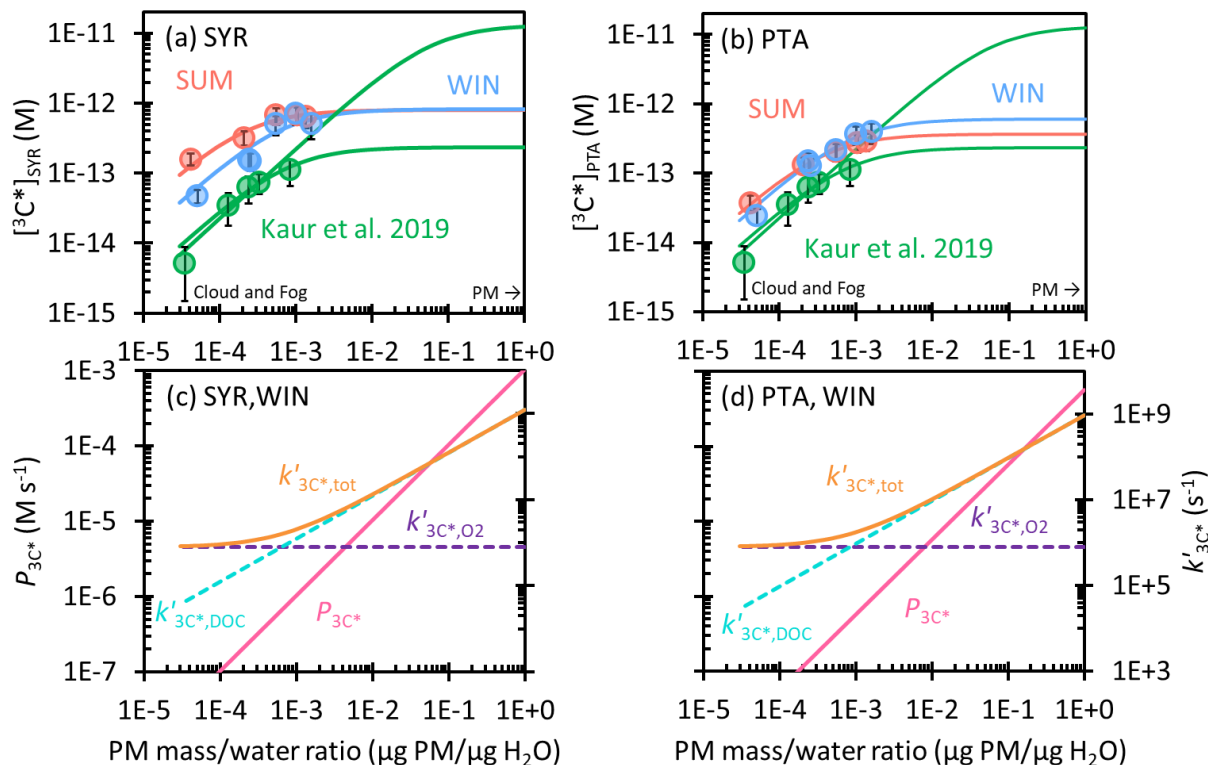
$$P_{\text{OH}} = k_1[\text{Fe}^{2+}][\text{H}_2\text{O}_2] + j_{\text{Fe(III)}}[\text{FeOH}^{2+}] \quad (\text{S12})$$

Next, we estimate the total dissolved iron and H<sub>2</sub>O<sub>2</sub> concentrations so that our calculated  $P_{\text{OH}}$   
approximately matches the measured values in SUM. To do this, we assume that: (1) The ratio of  
[Fe(II)]/([Fe(II)]+Fe(III)) is a constant 0.85 during daytime (i.e. during our illumination), (Deguillaume  
270 et al., 2005; Weller et al., 2014); (2) H<sub>2</sub>O<sub>2</sub> reaches a steady-state concentration during the illumination; (3)  
The concentrations of dissolved iron and H<sub>2</sub>O<sub>2</sub> increase proportionally with concentration factor (PM  
mass/water mass ratio) in our extracts. By setting dissolved iron and H<sub>2</sub>O<sub>2</sub> concentrations to 0.4 μM and 3  
μM in SUM-10, respectively, the simulated  $P_{\text{OH}}$  and [•OH] fit well with the measured values across all  
dilutions (Figure S4). Meanwhile, the estimated concentrations in SUM-10 are in a reasonable range for  
275 dilute cloud/fog water (Anastasio et al., 1994; Deguillaume et al., 2005; Faust et al., 1993). We next  
extrapolate this simple model to ambient PM conditions with one modification: since the aqueous H<sub>2</sub>O<sub>2</sub>  
concentration cannot increase with the particle mass/water mass ratio without limitation (because H<sub>2</sub>O<sub>2(aq)</sub>  
can partition into the gas phase), we set an upper limit for H<sub>2</sub>O<sub>2(aq)</sub> of 100 μM, which corresponds to a  
typical gas-phase H<sub>2</sub>O<sub>2</sub> mixing ratio of 1 ppb (Tilgner et al., 2021; Vione et al., 2003) assuming Henry's  
280 law equilibrium ( $K_{\text{H}} = 10^5 \text{ M atm}^{-1}$ ) (Seinfeld and Pandis, 2008). We assume that the H<sub>2</sub>O<sub>2(aq)</sub>  
concentration increases proportionally with PM mass/water mass ratio until it reaches 100 μM and then is  
constant at this value under more concentrated conditions. Our estimated soluble iron concentration of 0.4  
μM in SUM-10 predicts a dissolved Fe concentration under ALW conditions (1 μg PM/μg H<sub>2</sub>O) of 9.6

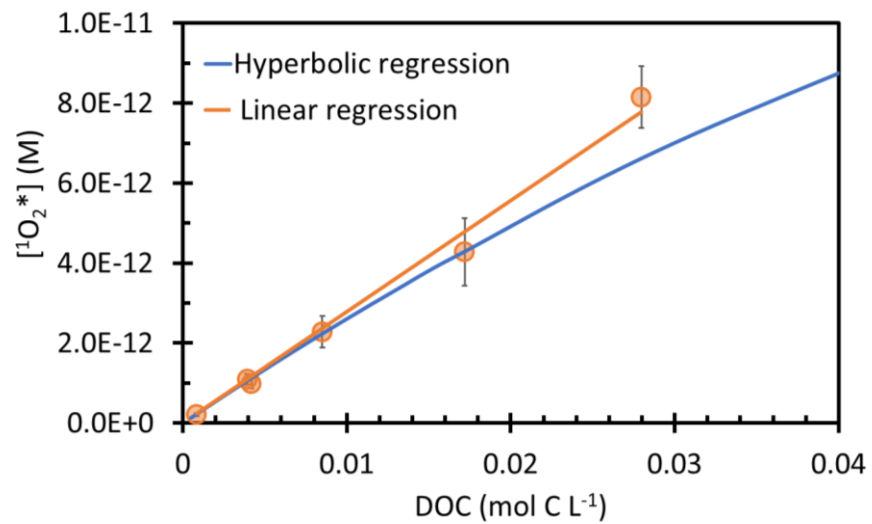
285 mM; we assume this is all dissolved, with no precipitation. This soluble iron concentration is similar to expected dissolved iron concentrations in aqueous aerosols (Gen et al., 2020; Tilgner et al., 2021).



290 **Figure S4.** Comparison of measured (blue) and modeled (orange)  $\text{OH}^\bullet$  production rates (top panel) and concentrations (bottom panel) in SUM as a function of particle mass/water mass ratio. The modeled  $\text{OH}^\bullet$  concentration is calculated using the modeled production rate divided by the measured  $\text{OH}^\bullet$  sink ( $k'_{\text{OH}}$ ) at each dilution.

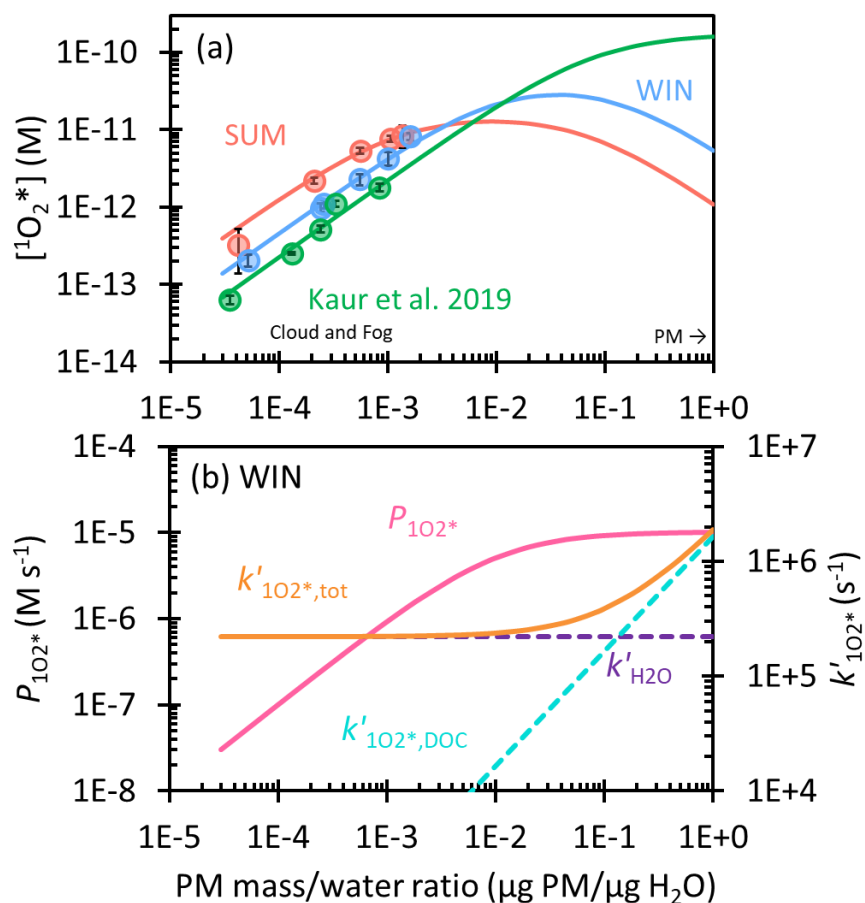


**Figure S5.** Top row: Triplet excited state concentrations determined by (a) SYR and (b) PTA as a function of particle mass/water mass ratio in WIN extracts (blue) and SUM (red). Solid circles are measured values in dilution experiments, while lines are extrapolations to ALW conditions. Previous measurements and extrapolations (best fit and high estimate) for Davis winter particle extracts are in green (Kaur et al., 2019). Bottom row: Dependence of triplet production rate (red line), and rate constants for  $^3\text{C}^*$  loss, including quenching by oxygen ( $k'_{3\text{C}^*,\text{O}_2}$ , purple dashed line), dissolved organic carbon ( $k'_{3\text{C}^*,\text{DOC}}$ , blue dashed line), and total sinks ( $k'_{3\text{C}^*,\text{tot}} = k'_{3\text{C}^*,\text{O}_2} + k'_{3\text{C}^*,\text{DOC}}$ , orange solid line), on particle mass/water mass ratio for the WIN sample. Panels (c) and (d) show data determined using SYR and PTA, respectively.

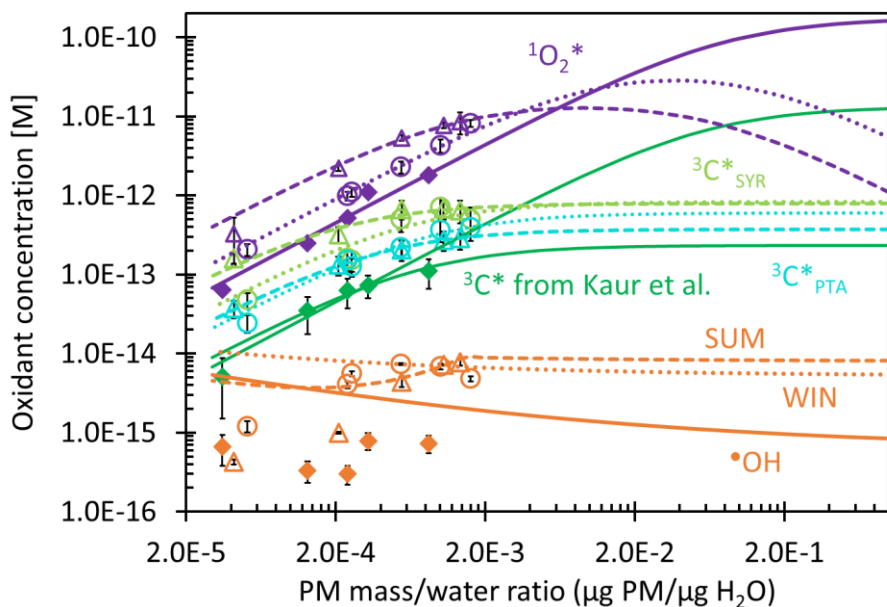


305 **Figure S6.** <sup>1</sup>O<sub>2</sub>\* concentration as a function of DOC in winter samples (circles). The orange line represents a linear regression fit to all points, while the blue line represents a hyperbolic regression fit to the first 4 data points using equation 11 in the main text.





310 **Figure S7.** (a) Dependence of singlet molecular oxygen concentration on particle mass/water mass ratio  
 315 in winter extracts (blue) and summer (red) samples. Solid circles are measured values in dilution  
 experiments, while lines are extrapolations to ALW conditions. Previous measurements and extrapolation  
 with Davis winter particle extracts are in green (Kaur et al., 2019). (b) Singlet oxygen production rate,  
 ( $P_{102^*}$ , red line) and rate constants for  $^1\text{O}_2^*$  loss, including deactivation by water ( $k'_{\text{H}_2\text{O}}$ , purple),  
 quenching by dissolved organic carbon ( $k'_{102^*,\text{DOC}}$ , blue), and total sinks ( $k'_{102^*,\text{tot}} = k'_{\text{H}_2\text{O}} + k'_{102^*,\text{DOC}}$ ,  
 orange), as a function of particle mass/water mass ratio for winter samples.



**Figure S8.** Dependence of photooxidant concentrations on particle mass/water mass ratio in WIN, SUM, and previous Davis winter particle extracts from Kaur et al. (2019). Symbols represent measured values under lab dilution conditions for WIN (open circles), SUM (open triangles), and Kaur et al. (filled diamonds), respectively. Lines represent extrapolations of experimental data to aerosol liquid water conditions for WIN (dotted lines), SUM (dashed lines), and Kaur et al. (solid lines) samples. Singlet oxygen concentrations are in purple; triplet concentrations are in light green for SYR-determined values, blue for PTA-determined values, and dark green for data from Kaur et al.; hydroxyl radical concentrations are in orange. The lines for  $\bullet\text{OH}$  are generally higher than the experimental measurements because the extrapolations include mass transfer of gas-phase hydroxyl radical to the drop/particle. The gas phase does not appear to be a significant source or sink of particle-phase  $^3\text{C}^*$  or  $^1\text{O}_2^*$ .

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