



Supplement of

A dynamic parameterization of sulfuric acid–dimethylamine nucleation and its application in three-dimensional modeling

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25 Table S1. Lookup table for G(i,j) and H(i) in the parameterization

G(i,j)		i						26	
		1	2	3	4	5	6	7	27
j	1	0.71	0.96	0.86	0.91	1.01	1.15	1.28	
	2	0.96	1.20	1.20	1.31	1.47	1.70	1.90	
	3	0.86	1.20	1.00	1.01	1.11	1.22	1.32	
	4	0.91	1.31	1.01	0.99	1.06	1.13	1.20	
	5	1.01	1.47	1.11	1.06	1.12	1.18	1.24	
	6	1.15	1.70	1.22	1.13	1.18	1.20	1.24	
	7	1.28	1.90	1.32	1.20	1.24	1.24	1.26	
H(i)		1.00	0.89	0.63	0.51	0.43	0.34	0.29	

28 2 Derivation of the Explicit Formula

Based on the kinetic model presented by Cai et al. (Cai et al., 2021), the formula of pseudo-steady-state cluster concentrations and nucleation rates is as follows:

31
$$[A_1B_1] = [SA_{tot}] - [A],$$
 (S1)

32
$$[A_1B_1] = \frac{\beta_{1-2}[A][B]}{\beta_{1-3}[A] + \beta_{3-3}[A_1B_1] + \beta_{3-5}[A_2B_2] + \beta_{3-6}[A_3B_3] + \beta_{3-7}[A_4B_4] + \text{CoagS}_{3+\gamma}},$$
(S2)

33
$$[A_2B_1] = \frac{\beta_{1,3}[A][A_1B_1]}{\beta_{2,4}[B] + \text{CoagS}_4},$$
 (S3)

34
$$[A_2B_2] = \frac{\frac{1}{2}\beta_{3,3}[A_1B_1][A_1B_1] + \beta_{2,4}[A_2B_1][B]}{\beta_{3,5}[A_1B_1] + \beta_{5,5}[A_2B_2] + \operatorname{CoagS}_5},$$
(S4)

35
$$[A_3B_3] = \frac{\beta_{3.5}[A_2B_2][A_1B_1]}{\beta_{3.6}[A_1B_1] + \text{CoagS}_6},$$
 (S5)

36
$$[A_4B_4] = \frac{\beta_{3,6}[A_3B_3][A_1B_1] + \frac{1}{2}\beta_{5,5}[A_2B_2][A_2B_2]}{\beta_{3,7}[A_1B_1] + \text{CoagS}_7},$$
(S6)

37
$$J_{A_4B_4} = \beta_{3,6}[A_3B_3][A_1B_1] + \frac{1}{2}\beta_{5,5}[A_2B_2][A_2B_2],$$
 (S7)

where [SA_{tot}] represents the concentrations of sulfuric acid (SA) molecules or clusters containing one SA molecule, *A* is SA molecules, *B* is dimethylamine (DMA) molecules, and A_mB_n is the clusters consisting of m SA molecules and n DMA molecules. $\beta_{i,j}$ (m³ s⁻¹) represents the collision coefficients (β) between molecules or clusters *i* and *j*, and 1-7 represent *A*, *B*, $A_1B_1, A_2B_1, A_2B_2, A_3B_3$, and A_4B_4 , respectively. Similarly, CoagS_i represents the coagulation sinks of molecules or clusters *i*. γ (s⁻¹) is the evaporation rate of A_1B_1 clusters. Here the concentrations of clusters are shown as [A_mB_n] in m⁻³.

The analytical solution should be simplified based on proper approximations. For typical polluted urban areas, the sink of A_1B_1 is mainly due to the coagulation scavenging and evaporation, that is,

45
$$[A_1B_1] \approx \frac{\beta_{1,2}[A][B]}{\text{CoagS}_3 + \gamma}$$
, (S8)

however, for a wider range of atmospheric environments with lower CS and temperatures, the above approximations might lead to an overestimation of SA-DMA nucleation rates. Thus in this study, the self-coagulation of A_1B_1 and coagulation with A would also be taken into account as a sink of A_1B_1 :

49
$$[A_1B_1] \approx \frac{\beta_{1-2}[A][B]}{\beta_{1-3}[A]+\beta_{3-3}[A_1B_1]+\operatorname{CoagS}_{3+\gamma}} \approx \frac{\beta_{1-2}[A][B]}{\beta_{1-3}[\operatorname{SA}_{tot}]+\operatorname{CoagS}_{3+\gamma}},$$
 (S9)

50 Putting the above assumption together with the pseudo-steady-state nucleation rates formula, the explicit formula could be 51 simplified to the version in the main text (Eqs. 8-11).



Figure S1. Simulated $J_{1.4}$ (blue) and characteristic equilibrium time (red) of A_3B_3 and A_1B_1 . The typical conditions are [DMA]=3.0 pptv with *CS*=0.0001 s⁻¹ and *T*=255 K in (a) and *CS*=0.01 s⁻¹ and *T*=315 K in (b). The variation of SA

57 concentrations is equal to the averaged diurnal variations.

58 **3** Dimethylamine Emission inventory for marine area

Similar to the continental emission inventory for DMA, the maritime part is also built by combination of NH₃ emission inventory and DMA/NH₃ emission ratio. The maritime NH₃ emission is adopted from the results of Paulot et al with a grid transformation. The DMA/NH₃ emission ratio is estimated by the measured data from a previous study (Chen et al., 2021). During their maritime campaign, mean gaseous DMA and NH3 concentrations are 0.006 μ g cm⁻³ and 0.5300 μ g cm⁻³, of which 16% and 34% come from continental transport, respectively. Hence we can obtain the marine-originated DMA (0.0050 μ g cm⁻

64 ³) and NH₃ (0.34980 µg cm⁻³) concentrations and an approximate DMA/NH₃ emission ratio of 0.0144.

65 Table S2. Key parameters in simulating atmospheric sinks of dimethylamine

Sinks	This study	Variation range
Wet deposition (Henry Law's constant/mol m ⁻³ Pa ⁻¹)	0.56	0.3-0.6 (Sander, 2015)
Gas-phase reaction (•OH oxidation rate constant/cm ⁻³ s ⁻¹)	6.49 ×10 ⁻¹¹	(5.85-7.13) ×10 ⁻¹¹ (Carl and Crowley, 1998)
Aerosol uptake (Uptake coefficient)	0.001	5.9 ×10 ⁻⁴ -4.4×10 ⁻² (Qiu et al., 2011; Wang et al., 2010)



Figure S2. Simulated Evolution of PNSDs and Timeseries of CS (violet line) from scenario DMA1.4_Mech8.



Figure S3. Comparison of observed and simulated averaged particle number size distribution from scenarios with parameterizations from Dunne et al., 2016 (CLOUD) the original scenario (DMA1.4_Mech8).





75 76 Figure S4. Comparison of observed and simulated DMA (a) and SA (b) concentrations from scenarios with parameterizations from Dunne et al., 2016 (CLOUD) the original scenario (DMA1.4_Mech8).





Figure S5. Comparison of observed and simulated averaged particle number size distribution from scenarios with
 parameterizations from Dunne et al., 2016 (CLOUD) the original scenario (DMA1.4_Mech8).



Figure S6. Comparison of observed and simulated [SA]⁴/CS² to show the combined effect of simulated input parameters
 in DMA1.4_Mech8.





Figure S7. Comparison of observed $J_{1.4}$ and simulated nucleation rates from scenarios with parameterizations from Dunne et al., 2016 (CLOUD).



Figure S8. Comparison of observed and simulated averaged particle number size distribution (from DMA1.4_Mech8
 scenario) for 25 NPF days.



95 Figure S9. Variation of parameterized J1.4 with DMA concentrations at 281 K with different ΔG values applied of -15.40, -14.00, -13.54, and -11.02 kcal mol-1, respectively.



97 98 99 Figure S10. Comparison of observed and simulated DMA concentrations from sensitivity scenarios of halving (SenDMA0.5) and doubling (SenDMA2) the DMA emission and the original scenario (DMA1.4_Mech8).



101 Figure S11. Comparison of observed and simulated particle number size distribution from sensitivity scenarios of 102 halving (SenDMA0.5) and doubling (SenDMA2) the DMA emission and the original scenario (DMA1.4_Mech8).



103 104 Figure S12. Comparison of observed and simulated averaged particle number size distribution from sensitivity scenarios of halving (SenDMA0.5) and doubling (SenDMA2) the DMA emission and the original scenario 105 106 (DMA1.4_Mech8).



107Date108Figure S13. Comparison of observed J1.4 and simulated nucleation rate from sensitivity scenarios of halving109(SenDMA0.5) (a) and doubling (SenDMA2) (b) the DMA emission.



Figure S14. Comparison of observed and simulated DMA concentrations from sensitivity scenarios using lowest (SenUpt5.9E-4) and highest (SenUpt4.4E-2) aerosol uptake coefficient of DMA and the original scenario (DMA1.4_Mech8).



- 114 115
- Figure S15. Comparison of observed and simulated particle number size distribution from sensitivity scenarios using
- 116 lowest (SenUpt5.9E-4) and highest (SenUpt4.4E-2) aerosol uptake coefficient of DMA and the original scenario
- 117 (DMA1.4_Mech8).



119

Figure S16. Comparison of observed and simulated averaged particle number size distribution from sensitivity scenarios using lowest (SenUpt5.9E-4) and highest (SenUpt4.4E-2) aerosol uptake coefficient of DMA and the original

scenario (DMA1.4_Mech8).



122 123

Figure S17. Comparison of observed $J_{1.4}$ and simulated nucleation rate from sensitivity scenarios using lowest (SenUpt5.9E-4) (a) and highest (SenUpt4.4E-2) (b) aerosol uptake coefficient of DMA and the original scenario

124 125 (DMA1.4_Mech8).



Date 127 Figure S18. Comparison of observed and simulated DMA concentrations from sensitivity scenarios using $\Delta G = -15.4$ 128 kcal mol⁻¹ (SenDeltaG15.4) and the original scenario (DMA1.4_Mech8).



129 130 Figure S19. Comparison of observed and simulated particle number size distribution from sensitivity scenario using

131 $\Delta G = -15.4$ kcal mol⁻¹ (SenDeltaG15.4) and the original scenario (DMA1.4_Mech8).





133 Figure S20. Comparison of observed and simulated averaged particle number size distribution from sensitivity scenarios using $\Delta G = -15.4$ kcal mol⁻¹ (SenDeltaG15.4) and the original scenario (DMA1.4_Mech8).



Date135Date136Figure S21. Comparison of observed $J_{1.4}$ and simulated nucleation rates from sensitivity scenarios using $\Delta G = -15.4$ 137kcal mol⁻¹ (SenDeltaG15.4).

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