



Supplement of

Dependency of particle size distribution at dust emission on friction velocity and atmospheric boundary-layer stability

Yaping Shao et al.

Correspondence to: Jie Zhang (zhang-j@lzu.edu.cn) and Ning Huang (huangn@lzu.edu.cn)

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We use a Lagrangian stochastic model for saltation in turbulent flow to examine the intensity of saltation bombardment.
 The model combines the equation of sand motion with a stochastic equation for fluid velocity fluctuations along the saltation trajectories. Following Thomson (1987, 1990), the turbulent motion of fluid elements can be modelled with

 $dU_i = a_i(U, X, t)dt + b_{ii}(U, X, t)d\omega_{ii}$ (s1)

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$$dX_i = U_i(X, t)dt \tag{s2}$$

6 where *U* is fluid element Lagrangian velocity (U_i its *i* component), *X* fluid element position, a_i drift coefficient, b_{ij} 7 diffusion coefficient and $d\omega_{ij}$ increment of the Wiener process. Sand particle and fluid element follow different 8 trajectories due to the trajectory-crossing effect (Yudine, 1959; Csanady, 1963).

9 The model used in this study is two dimensional, with x_1 aligned in the horizontal mean wind direction and x_3 in the 10 vertical direction. We denote the sand particle position as *Y*, its velocity as *V*, and the fluid element velocity at *Y* as U^* . 11 The sand-particle to fluid-element relative velocity is $V_R = V - U^*$.

12 The equation of sand particle motion is written as

$$\frac{dV_i}{dt} = -\frac{V_{Ri}}{\tau_p} - \delta_{i3}g \qquad (i = 1, 3)$$
(s3)

15 with τ_p being the sand particle response time (Morsi and Alexander, 1972). V_{Ri} is given by $V_{R1} = V_1 - \overline{U_1^*} - u_1^*$ and 16 $V_{R3} = V_3 - u_3^*$, where $\overline{U_1^*}$ is the mean wind speed at sand particle location. The influences of turbulence on sand particle 17 motion are embedded in u_1^* and u_3^* . These are calculated using a modified Thomson (1987) model. Note that $U = \overline{U} + u$ 18 and $u = (u_1, u_3)$. \overline{U} is assumed to beknown, and the fluid element motion fluctuations (u_1, u_3) are calculated by using 19 Equations (a1) and (a2). The diffusion coefficients b_{ij} are given by

 $b_{ii} = \delta_{ii} \sqrt{C_0 \varepsilon} \tag{s4}$

21 where δ_{ij} is Kronecker delta, C_0 a constant and ε the dissipation rate for turbulent kinetic energy. The determination of a_i 22 uses the well-mixed condition of Thomson (1987), which leads to

- 23 $a_i P = \frac{1_i}{2} \frac{\partial C_0 \varepsilon P}{\partial U_i} + \varphi_i$ (s5)
- 24 and

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$$\frac{\partial \varphi_i}{\partial U_i} = -\frac{\partial P}{\partial t} - \frac{\partial U_i P}{\partial X_i} \tag{s6}$$

with *P* being the phase-space probability density function P(U, X, t). The well-mixed condition requires that *P* equals to the probability density function of the Eulerian velocity U(x=X, t).

28 The increment du_i^* is expressed as

 $du_i^* = du_i + \delta u_i \tag{s7}$

(s9)

- 30 where du_i is the fluid-element velocity increment between *t* and *t*+*dt*, computed using Equation (s1), and δu_i the spatial 31 velocity increment at *t*+*dt* between the two points separated by $V_R dt$. While the structure function of du_i satisfies
 - $\langle du_i du_i \rangle = C_0 \varepsilon dt, \tag{88}$

33 that of δu_i satisfies

- 34
 - 35 Due to its fractional nature, δu_i is difficult to generate stochastically and it is in this study assumed to be

 $\langle \delta u_i \delta u_i \rangle = C_1 \varepsilon^{2/3} V_R^{2/3} dt^{2/3}.$

- 36 $\langle \delta u_i \delta u_i \rangle = C_1 \varepsilon^{2/3} V_R l^{-1/3} dt$ (s10) 37 with *l* being a fixed scaling length. Following Hanna (1981) and Stull (1988), $C_0 = 5$ and $C_1 = 2$. 38 Sand particles are randomly lifted from the surface with velocity (V_{Io} , V_{3o}). The PDF of V_{Io} is assumed to be Gaussian
- 39 and that of V_{3o} Weibull (to avoid negative liftoff speed). The sand-particle liftoff angle is confined to 0° and 180° and
- 40 Gaussian distributed with a mean lift off angle of 55° and a standard deviation of 5° . The sand particles are allowed to
- 41 rebound from the surface with the rebounding kinetic energy half the impacting kinetic energy and a mean rebounding
- 42 angle of 40° . If the kinetic energy of a sand particle becomes lower than a critical value, its motion is stopped.

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