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*Supplement of*

## **Multiphase oxidation of SO<sub>2</sub> by NO<sub>2</sub> on CaCO<sub>3</sub> particles**

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## 8 S1. Deriving the reactive uptake coefficient from aqueous reaction rate constant

9 The reaction rate constant in the literature was used to derive the reactive uptake coefficient to particles under the  
10 same conditions as in this study using the method in Davidovits et al. (2006).

$$11 \quad \frac{1}{\gamma} = \frac{1}{\Gamma_{diff}} + \frac{1}{\alpha} + \frac{1}{\Gamma_{sat} + \Gamma_{rxn}} \quad (S1)$$

12 where  $\Gamma_{diff}$  is the transport coefficient in the gas phase,  $1/\Gamma_{diff}$  is the resistance due to the diffusion in the gas phase.  
13 Similarly,  $1/\Gamma_{sat}$  and  $1/\Gamma_{rxn}$  are the resistance due to liquid phase saturation and liquid phase reaction, respectively.  
14  $\alpha$  is the mass accommodation coefficient of  $SO_2$ .

15  $1/\Gamma_{diff}$  can be derived using the following equation:

$$16 \quad \frac{1}{\Gamma_{diff}} = \frac{0.75 + 0.238Kn}{Kn(1 + Kn)} \quad (S2)$$

17 where Kn is the Knudsen number. Knudsen number is defined as

$$18 \quad Kn = \frac{\lambda}{a} \quad (S3)$$

19 where  $\lambda$  is the mean free path of molecule in the gas phase and  $a$  is the radius of the particle.

20  $\lambda$  can be derived from

$$21 \quad \lambda = \frac{3D_g}{c} \quad (S4)$$

22 where  $D_g$  is the diffusion coefficient in the gas phase and  $c$  is the mean molecular velocity.

23  $c$  is derived from

$$24 \quad c = \sqrt{\frac{8RT}{\pi M}} \quad (S5)$$

25 where  $R$  is the gas constant,  $T$  is temperature, and  $M$  is the molecular mass of  $SO_2$ .

26  $1/\Gamma_{sat}$  can be derived from

$$27 \quad \frac{1}{\Gamma_{sat}} = \frac{c}{4HRT} \sqrt{\frac{t\pi}{D_l}} \quad (S6)$$

28 where  $H$  is the Henry constant of  $SO_2$ ,  $t$  is time, and  $D_l$  is the diffusion coefficient of  $SO_2$  in the liquid phase.

29  $1/\Gamma_{rxn}$  can be derived from

$$30 \quad \frac{1}{\Gamma_{rxn}} = \frac{c}{4HRT} \sqrt{\frac{1}{k_{rxn}D_l}} \quad (S7)$$

31 where  $k_{rxn}$  is the first order rate constant of the reaction in the liquid phase.

$$32 \quad k_{rxn} = k[NO_2(aq)] \quad (S8)$$

33 where  $k$  is the second order rate constant of the reaction of S(IV) with  $NO_2$  and  $[NO_2(aq)]$  is the  $NO_2$   
34 concentration in the liquid phase.

$$35 \quad [NO_2(aq)] = H_{NO_2}P_{NO_2} \quad (S9)$$

36 where  $H_{NO_2}$  is the Henry constant of  $NO_2$  and  $P_{NO_2}$  is the concentration of  $NO_2$  in the gas phase.

37 **S2. Characteristic time for aqueous reaction and gas-particle equilibrium**

38 The characteristic time to achieve the equilibrium in the gas-particle interface and for aqueous reaction  
39 of SO<sub>2</sub> with NO<sub>2</sub> were derived using the method in Seinfeld and Pandis (2006).

40 
$$\tau_p \cong \frac{aH^* \sqrt{2\pi MRT}}{3\alpha} \quad (S10)$$

41 
$$\tau_{ra} = \frac{1}{k_{rxn}} \quad (S11)$$

42 a is the radius of the particle, H\* is the effective Henry constant, M is the molecular weight, R is the gas constant,  
43 T is temperature, α is the mass accommodation coefficient of SO<sub>2</sub>. k<sub>rxn</sub> is the first-order rate constant of the  
44 reaction in the liquid phase (see Equation S8). The values of the constants are shown in Table S1.

45 The characteristic time to achieve the equilibrium in the gas-particle interface is around 4×10<sup>-5</sup> s. The  
46 characteristic time for aqueous reaction is 0.5 and 0.08 s using the reaction rate constant of 2×10<sup>6</sup> mol<sup>-1</sup> L s<sup>-1</sup> (Lee  
47 and Schwartz, 1983) and 1.24×10<sup>7</sup> mol<sup>-1</sup> L s<sup>-1</sup> (Clifton et al., 1988), respectively.

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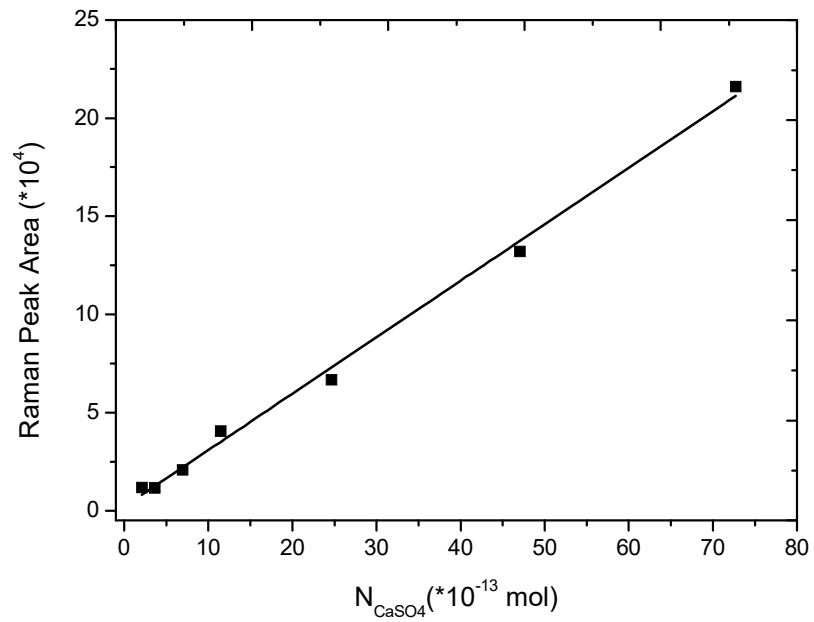
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**Table S1** Constants used for deriving uptake coefficients from reaction rates and deriving characteristic time

Parameter	Value	Reference
$D_g$ ( $\text{m}^2 \text{s}^{-1}$ )	$10^{-5}$	-
a (m)	$8.3 \times 10^{-6}$	-
R ( $\text{J mol}^{-1} \text{K}^{-1}$ )	8.314	-
T (K)	298	-
$M_{\text{SO}_2}$ ( $\text{Kg mol}^{-1}$ )	$6.4 \times 10^{-2}$	-
$\alpha$	0.35	Davidovits et al. (2006)
$D_l$ ( $\text{m}^2 \text{s}^{-1}$ )	$8.3 \times 10^{-12\text{a}}$	Mahiuddin and Ismail (1983)
$H_{\text{SO}_2}$ ( $\text{mol L}^{-1} \text{atm}^{-1}$ )	1.23	Seinfeld and Pandis (2006)
$H_{\text{NO}_2}$ ( $\text{mol L}^{-1} \text{atm}^{-1}$ )	$1 \times 10^{-2}$	Seinfeld and Pandis (2006)
k ( $\text{mol}^{-1} \text{L s}^{-1}$ )	$2 \times 10^6$ $1.24 \times 10^7$	Lee and Schwartz (1983); Clifton et al. (1988)

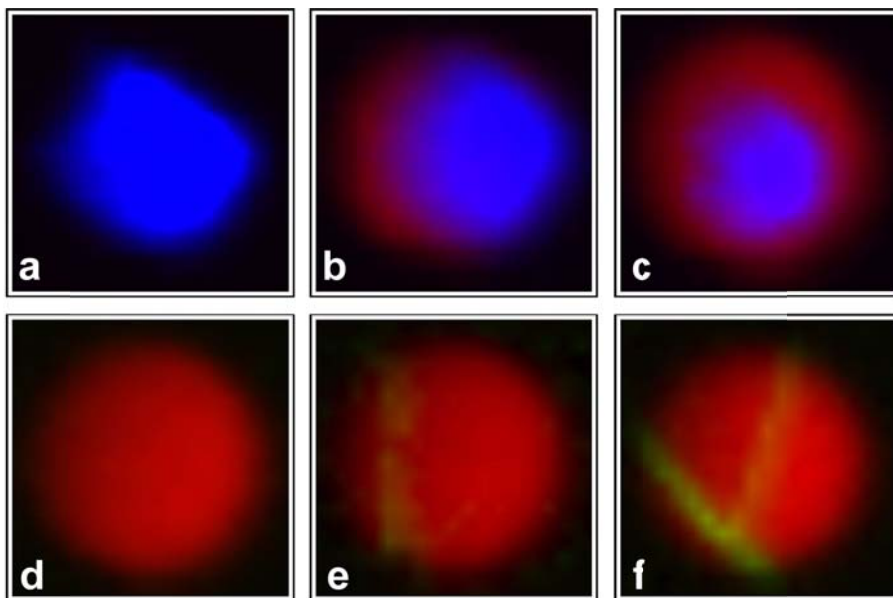
68 <sup>a</sup>The aqueous phase diffusion coefficient was derived from the viscosity of  $\text{Ca}(\text{NO}_3)_2$  solution providing that  
69 diffusion coefficient is inversely proportional to viscosity according to the Stokes–Einstein equation (Bones et al.,  
70 2012) and assuming that the diffusion coefficient in water is  $10^{-9} \text{ m}^2 \text{ s}^{-1}$ .



72

73 Figure S1. Calibration curve for sulfate showing the peak area of sulfate at 1016 cm<sup>-1</sup> in Raman spectra versus the

74 amount of CaSO<sub>4</sub>.



75

76 Figure S2. Raman mapping analysis of a  $\text{CaCO}_3$  particle during the reaction with  $\text{NO}_2$  (75 ppm) and  $\text{SO}_2$  (75 ppm)  
77 at 72% RH at the reaction time of 0, 8, 26, 40, 97, and 1053 min. Blue, red, and green indicate the Raman peak  
78 intensity of carbonate, nitrate, and sulfate at 1087, 1050, and 1013  $\text{cm}^{-1}$ , respectively.

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