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# Molecular dynamics simulation of the surface tension of aqueous sodium chloride: from dilute to highly supersaturated solutions and molten salt

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**Abstract.** Sodium chloride (NaCl) is one of the key components of atmospheric aerosols. The surface tension of aqueous NaCl solution ( $\sigma_{\text{NaCl,sol}}$ ) and its concentration dependence are essential to determine the equilibrium water vapor pressure of aqueous NaCl droplets. Supersaturated NaCl solution droplets are observed in laboratory experiments and under atmospheric conditions, but the experimental data for  $\sigma_{\text{NaCl,sol}}$  are mostly limited up to subsaturated solutions. In this study, the surface tension of aqueous NaCl is investigated by molecular dynamics (MD) simulations and the pressure tensor method from dilute to highly supersaturated solutions. We show that the linear approximation of concentration dependence of  $\sigma_{NaCl,sol}$  at molality scale can be extended to the supersaturated NaCl solution until a molality of  $\sim 10.7 \,\mathrm{mol\,kg^{-1}}$  (i.e., solute mass fraction  $(x_{\mathrm{NaCl}})$  of  $\sim 0.39$ ). Energetic analyses show that this monotonic increase in surface tension is driven by the increase in excess surface enthalpy  $(\Delta H)$  as the solution becomes concentrated. After that, the simulated  $\sigma_{\text{NaCl,sol}}$  remains almost unchanged until  $x_{\text{NaCl}}$  of  $\sim 0.47$  (near the concentration upon efflorescence). The existence of the "inflection point" at  $x_{\text{NaCl}}$ of  $\sim 0.39$  and the stable surface tension of  $x_{\text{NaCl}}$  between  $\sim$  0.39 and  $\sim$  0.47 can be attributed to the nearly unchanged excess surface entropy term  $(T \cdot \Delta S)$  and the excess surface enthalpy term  $(\Delta H)$ . After a "second inflection point" at  $x_{\text{NaCl}}$  of  $\sim 0.47$ , the simulated  $\sigma_{\text{NaCl,sol}}$  gradually regains the growing momentum with a tendency to approach the surface tension of molten NaCl ( $\sim 175.58 \,\mathrm{mN \, m^{-1}}$  at 298.15 K, MD simulation-based extrapolation). This fast increase in  $\sigma_{\text{NaCl,sol}}$  at  $x_{\text{NaCl}} > 0.47$  is a process driven by excess surface

enthalpy and excess surface entropy. Our results reveal different regimes of concentration dependence of the surface tension of aqueous NaCl at 298.15 K: a water-dominated regime ( $x_{\text{NaCl}}$  from 0 to  $\sim$  0.39), a transition regime ( $x_{\text{NaCl}}$  from  $\sim$  0.39 to  $\sim$  0.47) and a molten NaCl-dominated regime ( $x_{\text{NaCl}}$  from  $\sim$  0.47 to 1).

## 1 Introduction

Sodium chloride (NaCl) is one of the most important components of atmospheric aerosol particles (Finlayson-Pitts, 2003; Lewis and Schwartz, 2004). The aqueous NaCl solution droplet could participate in many atmospheric processes, such as phase transition, cloud activation, ice crystallization, long-range transport and chemical aging (Martin, 2000; Finlayson-Pitts, 2003; Ghorai et al., 2014; Wagner et al., 2015; Chen et al., 2016). To better understand these processes, the concentration-dependent surface tension of aqueous NaCl solution ( $\sigma_{\text{NaCl},\text{sol}}$ ) is essential to determine the equilibrium between NaCl solution droplet and water vapor (Jarvis and Scheiman, 1968; Dutcher et al., 2010).

Below the saturation point ( $\sim 6.15 \, \mathrm{mol \, kg^{-1}}$ ),  $\sigma_{\mathrm{NaCl, sol}}$  shows a near-linear dependence on molality (Jarvis and Scheiman, 1968; Johansson and Eriksson, 1974; Aveyard and Saleem, 1976; Weissenborn and Pugh, 1995; Matubayasi et al., 2001) with a slope of  $1.73 \pm 0.17$  (Pegram and Record, 2006, 2007). Because of the energy barrier of crystallization during dehydration and size effects at the nanoscale (Martin,

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2000; Biskos et al., 2006; Cheng et al., 2015), supersaturated aqueous NaCl solution droplets can exist under atmospheric conditions. However, direct measurements of surface tension of supersaturated droplets are challenging due to technical difficulties (Harkins and Brown, 1919; Vargaftik et al., 1983; Richardson and Snyder, 1994; Kumar, 2001). Only recently, Bzdek et al. (2016) overcame these limitations with an optical tweezer method and extended the concentration range to  $\sim 8 \, \rm mol\, kg^{-1}$ , where the near-linear relationship still holds (Bzdek et al., 2016).

It is a matter of debate to what extent the approximation of a near-linear dependence of surface tension on molality can still be used for NaCl droplets. Cheng et al. (2015) used the differential Köhler analyses (DKA) method to retrieve the surface tension of NaCl aqueous droplets, and revealed a large deviation from the near-linear increase at a molality of  $\sim 10 \, \text{mol} \, \text{kg}^{-1}$ . In literature, such a deviation in concentrated solution has also been found for other compounds, such as HNO3 (Weissenborn and Pugh, 1996), and it is believed to be typically true for most highly soluble electrolytes (Dutcher et al., 2010). The reason for such deviation remains unclear.

Several models about surface tension have been developed for highly concentrated solutions, e.g., Li and Lu (2001), Li et al. (1999) and Levin and Flores-Mena (2001). Li and Lu (2001) developed a model based on the Gibbs dividing surface concept, where the adsorption and desorption rate constants, saturated surface excess, stoichiometric coefficient of ions and mean ionic activity coefficient are needed. For NaCl aqueous solutions, this model is suitable for solutions with concentrations up to  $\sim 5.5 \,\mathrm{mol\,kg^{-1}}$ . Li et al. (1999) uses a Debye-Hückel parameter, osmotic coefficient and a proportionality constant from the fitting of measured values to calculate the surface tension, which covers the concentration until the saturation point of bulk NaCl aqueous solutions. The remaining models are mostly only suitable for the dilute electrolyte solutions, such as the one proposed by Levin and Flores-Mena (2001). In their valid concentration range, these surface tension models produce linear or near-linear concentration dependence of  $\sigma_{\text{NaCl,sol}}$  that agrees well with currently available observations.

One surface tension model that is able to predict  $\sigma_{\text{NaCl,sol}}$  in the whole concentration range from infinitely dilute  $(x_{\text{NaCl}} = 0)$  to highly supersaturated solution to molten salts  $(x_{\text{NaCl}} = 1)$  was proposed by Dutcher et al. (2010), which has been adopted into the widely used Extended Aerosol Inorganics Model (E-AIM; Wexler and Clegg, 2002). This model is based on the following concept: ions are solvated by the water at low salt concentrations, which means that water molecules form hydration shells around the ions; while at very high salt concentration the water is considered as "solute" that is solvated by the ions, which means that ions form shells around the water molecules (Dutcher et al., 2010). Accordingly, for a diluted solution, the surface tension of water dominates and the surface tension of the solution equals the surface tension of water adjusted by a term that is pro-

portional to the solute concentration. For a highly supersaturated solution, a similar relationship can be applied with the surface tension of molten salt as governing element. Legitimately, the model is then constrained by the surface tensions of water and molten salt. The parameterization of this model is obtained by fitting the data of subsaturated solutions. When the aqueous NaCl solution gets concentrated, this model shows a nonlinear monotonically increasing trend of  $\sigma_{\text{NaCl},\text{sol}}$  generally in good agreement with observations, but no inflection point was introduced. It should be noted that the surface tension as a function of mole fraction of NaCl according to the Dutcher et al. (2010) model is essentially a linear interpolation between the surface tensions of water and molten NaCl.

In this study, we applied molecular dynamics (MD) simulations and the pressure tensor method to calculate the concentration dependence of  $\sigma_{\text{NaCl,sol}}$  from infinitely dilute  $(x_{\text{NaCl}}=0)$  to highly supersaturated solution to molten salt  $(x_{\text{NaCl}}=1)$ . The concentration dependence of  $\sigma_{\text{NaCl,sol}}$  is divided into 3 regimes: a water-dominated regime, a transition regime and a molten NaCl-dominated regime. We compare our results with the Dutcher et al. (2010) model, and present the principal underlying physical chemistry (driving forces) behind the change of surface tension along concentration changes.

## 2 Methods

# 2.1 MD simulation

MD simulations were carried out with the GROMACS 5.1 package (Abraham et al., 2015). The Na<sup>+</sup> ions, Cl<sup>-</sup> ions and water molecules were added into a cubic box ( $L=5\,\mathrm{nm}$ ) to imitate the NaCl solution. The concentrations of simulated solutions are summarized in Table 1. To simulate the surface tension of supersaturated NaCl aqueous solution, we make use of the time window in the MD simulations before the crystallization starts in the system. The highest  $x_{\mathrm{NaCl}}$  we can reach is  $\sim 0.64$  (the corresponding concentration is  $\sim 30.39\,\mathrm{mol\,kg^{-1}}$ ), below which the simulated surface tensions in three independent runs stably converge after 50 to 100 ns (Fig. 1). For more concentrated solutions, stable convergence cannot be reached, e.g., large fluctuations are shown in Fig. 1d at  $x_{\mathrm{NaCl}}$  of 0.75.

According to Dutcher et al. (2010), surface tension of liquid or molten NaCl at 298.15 K (corresponding  $x_{\text{NaCl}}$  is 1, infinite concentrated solution) can be regarded as the upper boundary of  $\sigma_{\text{NaCl,sol}}$ . However, a direct simulation of surface tension of molten NaCl at 298.15 K would not be possible, due to excessively large relaxation times of this system at this temperature. It has been found that surface tensions of a very wide range of molten salts can be well described by linear functions of temperature (Sada et al., 1984; Horvath, 1985; Janz, 1988; Dutcher et al., 2010). We thus follow

Table 1. Concentrations of solution studied in our simulation and the calculated values of surface tension.

Number of water         Number of NaCl           1         4142         0           2         4058         42           3         3976         83           4         3824         159           5         3728         207           6         3656         243           7         3550         296           8         3452         345           9         3388         377           10         3314         414           11         3222         460           12         3108         517           13         3038         552           14         2960         591           15         2868         637           16         2762         690	in bulk region <sup>b</sup> 0 0.657 1.235 2.41 3.16 3.85 4.8	x <sub>NaCl</sub> in bulk region 0 0.037 0.067 0.123 0.156 0.184 0.219	Concentration (mol kg <sup>-1</sup> ) of whole solution  0 0.575 1.159 2.309 3.08 3.69 4.63	x <sub>NaCl</sub> of whole solution  0 0.0325 0.0635 0.119 0.1528 0.1776 0.213	Surface tension $(\text{mN m}^{-1})$ $62.24 \pm 0.044$ $63.48 \pm 0.03$ $64.8 \pm 0.014$ $67.41 \pm 0.089$ $69.49 \pm 0.006$ $70.76 \pm 0.1$
1     4142     0       2     4058     42       3     3976     83       4     3824     159       5     3728     207       6     3656     243       7     3550     296       8     3452     345       9     3388     377       10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	0 0.657 1.235 2.41 3.16 3.85 4.8	0 0.037 0.067 0.123 0.156 0.184 0.219	0 0.575 1.159 2.309 3.08 3.69	whole solution  0 0.0325 0.0635 0.119 0.1528 0.1776	$62.24 \pm 0.044$ $63.48 \pm 0.03$ $64.8 \pm 0.014$ $67.41 \pm 0.089$ $69.49 \pm 0.006$ $70.76 \pm 0.1$
2     4058     42       3     3976     83       4     3824     159       5     3728     207       6     3656     243       7     3550     296       8     3452     345       9     3388     377       10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	0.657 1.235 2.41 3.16 3.85 4.8	0.037 0.067 0.123 0.156 0.184 0.219	0.575 1.159 2.309 3.08 3.69	0.0325 0.0635 0.119 0.1528 0.1776	$63.48 \pm 0.03$ $64.8 \pm 0.014$ $67.41 \pm 0.089$ $69.49 \pm 0.006$ $70.76 \pm 0.1$
3     3976     83       4     3824     159       5     3728     207       6     3656     243       7     3550     296       8     3452     345       9     3388     377       10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	1.235 2.41 3.16 3.85 4.8	0.067 0.123 0.156 0.184 0.219	1.159 2.309 3.08 3.69	0.0635 0.119 0.1528 0.1776	$64.8 \pm 0.014$ $67.41 \pm 0.089$ $69.49 \pm 0.006$ $70.76 \pm 0.1$
4     3824     159       5     3728     207       6     3656     243       7     3550     296       8     3452     345       9     3388     377       10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	2.41 3.16 3.85 4.8	0.123 0.156 0.184 0.219	2.309 3.08 3.69	0.119 0.1528 0.1776	$67.41 \pm 0.089$ $69.49 \pm 0.006$ $70.76 \pm 0.1$
5     3728     207       6     3656     243       7     3550     296       8     3452     345       9     3388     377       10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	3.16 3.85 4.8	0.156 0.184 0.219	3.08 3.69	0.1528 0.1776	$69.49 \pm 0.006$ $70.76 \pm 0.1$
6 3656 243 7 3550 296 8 3452 345 9 3388 377 10 3314 414 11 3222 460 12 3108 517 13 3038 552 14 2960 591 15 2868 637 16 2762 690	3.85 4.8	0.184 0.219	3.69	0.1776	$70.76 \pm 0.1$
7 3550 296 8 3452 345 9 3388 377 10 3314 414 11 3222 460 12 3108 517 13 3038 552 14 2960 591 15 2868 637 16 2762 690	4.8	0.219			
8     3452     345       9     3388     377       10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690			4.63	0.213	
9 3388 377 10 3314 414 11 3222 460 12 3108 517 13 3038 552 14 2960 591 15 2868 637 16 2762 690	6.04	0.261		0.213	$73.61 \pm 0.055$
10     3314     414       11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690		0.261	5.552	0.245	$76.06 \pm 0.14$
11     3222     460       12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	6.75	0.283	6.182	0.265	$77.5 \pm 0.11$
12     3108     517       13     3038     552       14     2960     591       15     2868     637       16     2762     690	7.47	0.304	6.94	0.288	$79.7 \pm 0.19$
13     3038     552       14     2960     591       15     2868     637       16     2762     690	8.57	0.334	7.931	0.317	$82.06 \pm 0.25$
14     2960     591       15     2868     637       16     2762     690	9.745	0.36	9.24	0.351	$84.35 \pm 0.143$
15 2868 637 16 2762 690	10.66	0.384	10.09	0.371	$85.67 \pm 0.183$
16 2762 690	11.83	0.409	11.09	0.3935	$86.9 \pm 0.04$
	13.49	0.44	12.339	0.419	$87.83 \pm 0.25$
	15.34	0.47	13.879	0.448	$88.03 \pm 0.88$
17 2636 753	17.37	0.504	15.87	0.481	$88.77 \pm 0.42$
18 2486 828	19.98	0.54	18.503	0.519	$90.35 \pm 0.6$
19 2368 887	24.6	0.59	20.81	0.549	$93.4 \pm 2.157$
20 2232 955	26.74	0.61	23.77	0.581	$97.6 \pm 1.46$
21 2122 1010		0.64	26.44	0.607	$102.53 \pm 0.46$
22 <sup>a</sup> 2109 421	30.396	0.4018	11.09	0.3935	$86.9 \pm 0.59$

<sup>&</sup>lt;sup>a</sup> The solution slab in this system is  $3 \text{ nm} \times 3 \text{ nm} \times 10 \text{ nm}$  and the simulation box is  $3 \text{ nm} \times 3 \text{ nm} \times 30 \text{ nm}$ .

b There is a little difference between the concentration in the bulk region and the one of the whole system due to surface effects. The values used in the main text are the ones in the bulk region.

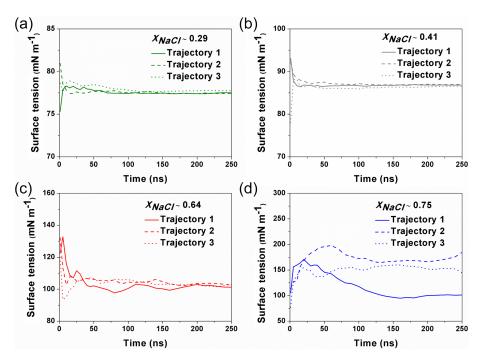
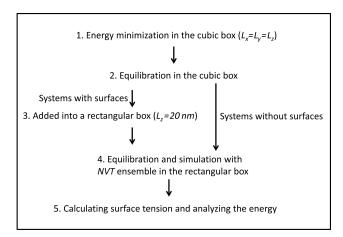


Figure 1. The calculated surface tension at different simulation time from different trajectories. For the solution with  $x_{\text{NaCl}} \le 0.64$  (**a-c**), the surface tension become steadily stabilized after  $\sim 100-150\,\text{ns}$ , and different individual simulation runs converge to a similar result. When  $x_{\text{NaCl}} > 0.64$  (**d**; here  $x_{\text{NaCl}} = 0.75$ ), the surface tension keeps fluctuating and the final values from different individual simulations cannot be converged even after 250 ns.



**Figure 2.** Schematic diagram of the different steps performed in the MD simulation.

the approach of Dutcher et al. (2010) assuming a linear relationship between surface tension of molten NaCl and temperature. With this approach, we retrieve the surface tension of molten NaCl at 298.15 K by extrapolating the simulated surface tension of molten NaCl in the temperature range of 1000 to 1700 K. Note that, in principle, non-linearity could still be possible at very high degrees of supercooling (e.g., close to or at room temperature) for the molten salts, which may introduce uncertainties to the offset obtained by the extrapolation.

The simulation procedure we followed is the following (Fig. 2): (1) systems were firstly energetically minimized by the steepest descent method (Stillinger and Weber, 1985). (2) Solutions were equilibrated in the NVT ensemble (constant-temperature, constant-volume) and NPT ensemble (constant-temperature, constant-pressure) (pressure = 1 bar) with periodic boundary conditions in three directions. The temperature was controlled by using the Nosé-Hoover thermostat (Nosé, 1984; Hoover, 1985). The box volume change due to the variation in density at different temperatures, and in our case the length of the cubic box varied from 4.9 to 5.1 nm. (3) The box was elongated along the z direction with  $L_7 = 20 \,\mathrm{nm}$  to create two interfacial regions. (4) The solution was equilibrated and simulated with the NVT ensemble in the rectangular parallelepiped box at the corresponding temperature. (5) Systems without surfaces were also simulated for further energy analysis, and the trajectories obtained from step 2 were simulated with NPT ensemble. (6) All simulations were carried out for at least 200 ns, which is much longer than that in previous studies (a few nanoseconds; Jungwirth and Tobias, 2000; Neyt et al., 2013), because the system that we were dealing with is much more concentrated. A 1 fs time step was adopted and conformations for analysis were saved every 2 ps. Both electrostatic interactions and van der Waals interactions were calculated using the particle mesh Ewald (PME) algorithm, which has been proven to be a good choice for accurate calculation of long-range interactions (Essmann et al., 1995; Fischer et al., 2015). To test the reproducibility, all the systems were simulated 3 times, and the respective statistical error bars were provided.

In our simulation, the Joung–Cheatham (JC) force field for NaCl (Joung and Cheatham III, 2009) with SPC/E water model (Berendsen et al., 1987) was applied to simulate the NaCl solution and molten NaCl. The solubility at 298.15 K based on the JC force field with SPC/E model has been determined as  $3.7\pm0.2\,\mathrm{mol\,kg^{-1}}$  (Moučka et al., 2013; Mester and Panagiotopoulos, 2015; Espinosa et al., 2016), which to the best of our knowledge is the value closest to the experimental value of solubility ( $\sim6.15\,\mathrm{mol\,kg^{-1}}$ ). Therefore, this force field is appropriate to use to study the concentration dependence of properties. More details about the history of the attempts to correctly calculate the quantity by molecular simulation can be found in the review by Nezbeda et al. (2016).

## 2.2 Calculation of surface tension

Based on results from MD simulations, the surface tension was calculated by using the mechanical definition of the atomic pressure (Alejandre et al., 1995):

$$\sigma_{\text{MD}} = 0.5L_z \left[ \langle P_{zz} \rangle - 0.5 \left( \langle P_{xx} \rangle + \langle P_{yy} \rangle \right) \right], \tag{1}$$

where  $\sigma_{\text{MD}}$  can represent the surface tension of molten NaCl  $(\sigma_{\text{NaCl}})$ , NaCl solution  $(\sigma_{\text{NaCl},\text{sol}})$  or pure water  $(\sigma_{\text{water}})$ ;  $L_z$  is the length of the simulation cell in the longest direction (along z axis) and  $P_{aa}$  (a=x, y, z) denotes the diagonal component of the pressure tensor. The  $\langle \ldots \rangle$  refers to the time average. The factor 0.5 outside the squared brackets takes into account the two interfaces in the system. Only the stable values were taken as our calculated surface tension.

## 2.3 Energy analysis

The excess surface enthalpy denotes the additional enthalpy in the system due to the creation of surfaces. It can be calculated as the difference of enthalpy between solutions with and without surfaces (Bahadur et al., 2007),

$$\Delta H = H_{b \ s} - H_b,\tag{2}$$

where  $H_{b\_s}$  is the total enthalpy of simulated systems with surfaces and  $H_b$  is the total enthalpy of simulated systems without surfaces. As the kinetic energy is the same for systems with or without surfaces and the difference of pV can be ignored,  $\Delta H$  can be presented as

$$\Delta H = E_{b,s} - E_b,\tag{3}$$

where  $E_{b\_s}$  and  $E_b$  are the potential energy of the system with and without surfaces.

Then the surface tension can be determined by the excess surface free energy per unit area as in Eq. (4) (Davidchack

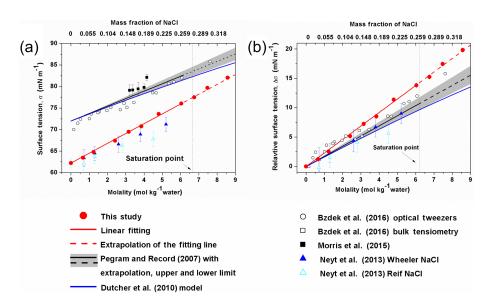


Figure 3. Surface tension (a) and relative surface tension (b) defined as  $\Delta \sigma = \sigma_{\text{solution}} - \sigma_{\text{water}}$  as a function of the concentration of NaCl. The  $\sigma_{\text{water}}$  in the Morris et al. (2015) study was not determined, thus the corresponding  $\Delta \sigma$  is not shown in (b).

and Laird, 2003):

$$\sigma = \frac{\Delta G}{A} = \frac{\Delta H - T \cdot \Delta S}{A},\tag{4}$$

where  $\Delta G$  is the increased part of free energy due to the creation of surfaces, A is the total area of the surface we created, so  $A = 2 \times a$  and a is the area of each created surface.  $\Delta S$  is the excess surface entropy. We then can retrieve  $\Delta S$  by using the data of enthalpy and surface tension:

$$\Delta S = \frac{\Delta H - \sigma \cdot A}{T},\tag{5}$$

where  $\Delta H$  and  $T \cdot \Delta S$  per unit area  $(\frac{\Delta H}{A})$  and  $\frac{T \cdot \Delta S}{A}$ ) are obtained as the enthalpic and entropic part of the contributions to the net surface tension, which will be used to explain the change of surface tension along with the mass fraction of NaCl  $(x_{\text{NaCl}})$ .

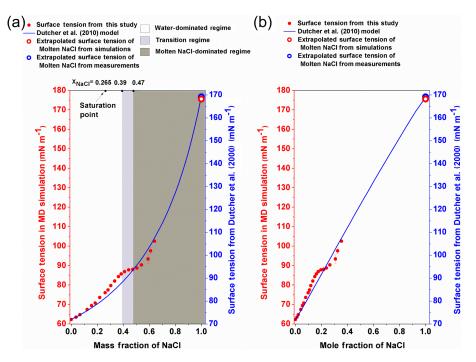
# 3 Results and discussion

# 3.1 Water-dominated regime ( $x_{NaCl} < \sim 0.39$ )

In Fig. 3a, the calculated surface tension of NaCl aqueous solution ( $\sigma_{\text{NaCl,sol}}$ ) is compared with experimentally determined values (Jarvis and Scheiman, 1968; Johansson and Eriksson, 1974; Aveyard and Saleem, 1976; Weissenborn and Pugh, 1995; Matubayasi et al., 2001; Pegram and Record, 2006, 2007; Morris et al., 2015; Bzdek et al., 2016) in the subsaturated concentration range (molality of NaCl solution from 0 to 6.15 mol kg<sup>-1</sup> and  $x_{\text{NaCl}}$  from 0 to  $\sim$  0.265). At 298.15 K, both model simulation (red solid points and fit line in Fig. 3a) and experimental observation (black line in

Fig. 3a) reveal a linear dependence of surface tension on solution concentration at molality scale, with a very similar slope (2.1 versus  $1.73 \pm 0.17$ , respectively). Systematic underestimation, however, exists in the simulated  $\sigma_{\text{NaCl,sol}}$ . The previous MD simulations by Neyt et al. (2013) have also reported a similar result for the solution whose concentration ranges from 0 to 5.2 molkg<sup>-1</sup> by using the same water model (SPC/E) but two different NaCl force fields, i.e., Wheeler NaCl (solid dark-blue triangle in Fig. 3a) and Relf NaCl (open light-blue triangle in Fig. 3a). Bhatt et al. (2004) also used the Wheeler NaCl model and SPC/E water model revealing a linear dependence and underestimation. We also subtracted the experimentally determined and the MD-simulated surface tension of pure water ( $\sigma_{\text{water}}$ ) from the observed and modeled  $\sigma_{\text{NaCl,sol}}$ , respectively. The relative increase in surface tension ( $\Delta \sigma = \sigma_{\text{NaCl,sol}} - \sigma_{\text{water}}$ ) from models and experiments converge nicely (Fig. 3b), and the former is only a little higher than the latter. The MD simulation is able to reproduce the increment in the growth of surface tension from pure water due to the addition of solute NaCl, although the predicted absolute value of  $\sigma_{\text{NaCl,sol}}$ is systematically underestimated, which may mainly be attributed to the discrepancy between observed  $\sigma_{\text{water}}$  and the modeled ones from the SPC/E water model.

By performing MD simulations in the supersaturated concentration range, we found that this linear relationship still holds beyond the saturation point until  $x_{\rm NaCl}$  of  $\sim 0.39$  (Fig. 4). As mentioned above, the laboratory experiments with elevated NaCl aqueous droplet and the optical tweezer method show that the linear relationship between  $\sigma_{\rm NaCl,sol}$  and NaCl concentration (molality scale) can be extended to  $\sim 8~{\rm mol\,kg^{-1}}$  (Fig. 3; Bzdek et al., 2016), corresponding to



**Figure 4.** The surface tension of different-concentration NaCl solution. (a) The surface tension of NaCl solution against the mass fraction of NaCl. The left red y axis is for the data from MD simulation (red circle), and the right blue y axis is for the Dutcher et al. (2010) model (blue solid line). The white, light grey and dark grey areas shade the water-dominated, transition and molten NaCl-dominated regimes, respectively. (b) The surface tension of NaCl solution is plotted against the mole fraction of NaCl.

 $x_{\text{NaCl}}$  of  $\sim 0.33$  (Fig. 4), which is consistent with our simulations.

## 3.2 Transition regime ( $x_{\text{NaCl}}$ from $\sim 0.39$ to $\sim 0.47$ )

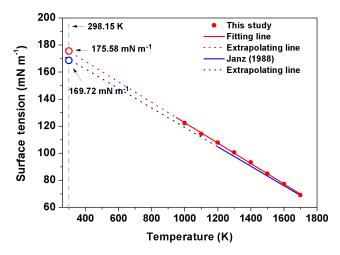
It was often found that surface tensions of single inorganic electrolyte aqueous solutions were linear functions of concentration (at the molality scale) over the moderate concentration range (Horvath, 1985; Dutcher et al., 2010). However, these simple relationships may not hold when the solutions become more concentrated. As shown in Fig. 4, starting from  $x_{\text{NaCl}} \sim 0.39$ , the simulated  $\sigma_{\text{NaCl,sol}}$  remains almost unchanged until  $x_{\text{NaCl}}$  of  $\sim 0.47$  (concentration upon efflorescence). This inflection point of  $\sigma_{\text{NaCl,sol}}$  at  $x_{\text{NaCl}}$  of  $\sim 0.39$  is supported by those determined by the DKA approach (Cheng et al., 2015), where there is a large deviation of surface tension from the monotonic linear increase. Note that beyond  $x_{\text{NaCl}}$  of  $\sim 0.47$ , the simulated surface tension increases again (Fig. 4). This second inflection point, right at the concentration upon efflorescence, may imply a potential correlation with crystallization processes.

## 3.3 Molten NaCl-dominated regime ( $x_{NaCl} > \sim 0.47$ )

Beyond the second inflection point ( $x_{NaCl} > 0.47$ ), the simulated  $\sigma_{NaCl,sol}$  gradually increases more and more strongly (Fig. 4). Unfortunately, due to the large fluctuation in the surface tension simulation (Fig. 1), we are not able to ex-

tend our surface tension calculation in this way beyond  $x_{\text{NaCl}}$  of  $\sim$  0.64. However, according to Dutcher et al. (2010), it is expected that the surface tension of the solution would ultimately approach the surface tension of the hypothetical molten solute (i.e.,  $x_{\text{NaCl}} = 1$ ) at the same temperature. This hypothesis has been found to be consistent with the DKA retrieval for a highly concentrated ammonium sulfate aqueous solution with molality of  $\sim$  380 mol kg $^{-1}$  (Cheng et al., 2015). We thus also try to constrain the growth of  $\sigma_{\text{NaCl},\text{sol}}$  by MD-simulated surface tension of molten NaCl ( $\sigma_{\text{NaCl}}$ ) at 298.15 K.

Similar to the experimental results of Janz (1988), the simulated  $\sigma_{\text{NaCl}}$  is also linearly correlated with temperature from 1000 K (the simulated melting point of NaCl) to 1700 K, as shown in Fig. 5. Following Dutcher et al. (2010), a surface tension of  $\sim 175.58\,\mathrm{mN\,m^{-1}}$  is obtained for the hypothetical molten NaCl at 298.15 K by linear extrapolation of the MD simulated  $\sigma_{\text{NaCl}}$  at higher temperature, which is very close to the  $\sim 169.7\,\mathrm{mN\,m^{-1}}$  extrapolated from the experimental results (Dutcher et al., 2010). Combined with  $\sigma_{\text{NaCl}} = \sigma_{\text{NaCl,sol}}(x_{\text{NaCl}} = 1) = \sim 175.58\,\mathrm{mN\,m^{-1}}$ , the simulated  $\sigma_{\text{NaCl,sol}}$  in the concentration range of  $x_{\text{NaCl}} > 0.47$  shows the tendency to ultimately approach the surface tension of melting NaCl at 298.15 K, similar to the blue curve in Fig. 4 from the Dutcher et al. (2000) study.



**Figure 5.** The surface tension of molten NaCl at different temperatures. The equation in Janz's study (1988) is  $\sigma_{\text{NaCl}} = -0.07188 \cdot T + 191$  (blue solid line). The fitting line based on our data is  $\sigma_{\text{NaCl}} = -0.0755 \cdot T + 198.09$  (red solid line). The red and blue open circles represent the extrapolated value of surface tension in simulation and reality, respectively.

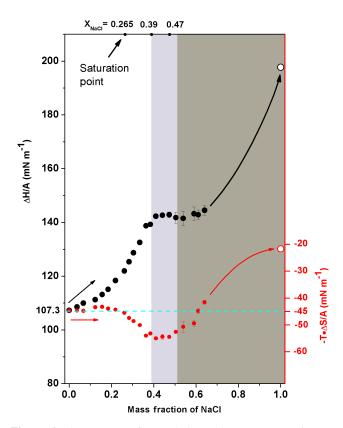
# 3.4 Physical chemistry behind the regimes

In energetic analyses, surface tension was decomposed into excess surface enthalpy  $(\frac{\Delta H}{A})$  and excess surface entropy  $(\frac{T\cdot\Delta S}{A})$ . Note that the increase in excess surface entropy  $(\frac{T\cdot\Delta S}{A})$  or decrease in  $-\frac{T\cdot\Delta S}{A}$  will negatively contribute to the growth of  $\sigma_{\text{NaCl,sol}}.$  The analyses show that the monotonic increase in surface tension in water-dominated concentration ranges  $(x_{\text{NaCl}}$  from 0 to  $\sim 0.39)$  is driven by the increase in  $\frac{\Delta H}{A}$  when the solution becomes concentrated (Fig. 6). When the solution gets concentrated,  $\frac{\Delta H}{A}$  first increases slightly with enhanced increasing rate at  $x_{\text{NaCl}} > \sim 0.2$  and in the supersaturated regime up to  $x_{\text{NaCl}}$  of  $\sim 0.39$ .  $-\frac{T\cdot\Delta S}{A}$  behaves differently, it remains almost constant at about  $-45~\text{mN m}^{-1}$  first and only starts to decrease at  $x_{\text{NaCl}} \sim 0.2$ . This way, in this concentration range  $(x_{\text{NaCl}}$  from 0 to  $\sim 0.39$ ), the increase in excess surface enthalpy outnumbers the increase in excess surface entropy and thus this physicochemical regime can be understood as an excess surface enthalpy-driving process.

The stable surface tension in the transition-regime concentration range ( $x_{\text{NaCl}}$  from  $\sim 0.39$  to  $\sim 0.47$ ) is attributed to the fact that  $-\frac{T \cdot \Delta S}{A}$  and  $\frac{\Delta H}{A}$  are both almost unchanged. Figure 6 shows that in the concentration above  $x_{\text{NaCl}}$  of  $\sim 0.39$ , the increase in  $\frac{\Delta H}{A}$  significantly slows down and stabilizes at  $\sim 145 \text{ mN m}^{-1}$  when the mass fraction approaches the efflorescence point. During this period,  $-\frac{T \cdot \Delta S}{A}$  keeps nearly unchanged, which results in a corresponding  $\sigma_{\text{NaCl,sol}}$  almost independent of the solution concentration change.

Here, we present a potential explanation for the stability of surface tension in this region from the structural analysis.





**Figure 6.** The excess surface enthalpy and entropy per unit area  $(\frac{\Delta H}{A} \text{ and } \frac{T \cdot \Delta S}{A})$  of different NaCl solution concentrations.  $\frac{\Delta H}{A}$  (black circles) and  $-\frac{T \cdot \Delta S}{A}$  (red circles) are shown as a function of mass fraction of NaCl. The solid circles are obtained from simulation directly, and the open circles are obtained from the extrapolation of corresponding properties of molten NaCl. The cyan dashed line is only an auxiliary line for clearer view. Shaded areas are the same as in Fig. 4.

The ratio of Na<sup>+</sup> concentration at different positions to the average concentration of the whole system  $(C_z/C_{average})$  in different solutions is shown in Fig. 7a. The three blue-toned lines represent the ratio of solution in the transition regime with  $x_{\text{NaCl}}$  from  $\sim 0.39$  to  $\sim 0.47$ . All of them have apophyses (significant rise) near the surface and these apophyses almost overlap with each other. This phenomenon suggests that the solute in these solutions enriches close to the surface and the degree of enrichment is almost the same for the different-concentration solution. Here, we denote the significant difference of the solute concentration in bulk region and on surface as a type of liquid–liquid partitioning. To check if this partitioning is dependent on the size of the solution slab, we calculate the corresponding value of a 3 nm  $\times$  3 nm  $\times$  10 nm

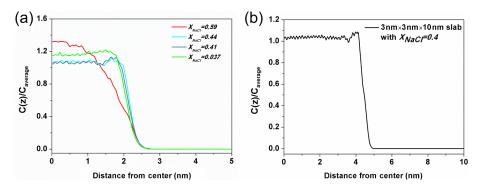


Figure 7. The ratio of Na<sup>+</sup> concentration at different positions ( $C_z$ ) to the average concentration of the whole system ( $C_{average}$ ). (a) The solution with  $x_{NaCl} = 0.59$  (red line) is on behalf of the solution in the molten NaCl-dominated regime (red line), the solution  $x_{NaCl} = 0.44$  and 0.41 (blue lines) represent the solution in transition regime and the solution  $x_{NaCl} = 0.037$  (green line) represents the solution in the water-dominated regime. (b) The density profile obtained from a 3 nm × 3 nm × 10 nm solution slab in which NaCl mass fraction is about 0.4.

solution slab with  $x_{\text{NaCl}}$  of 0.4 (Fig. 7b). There is still an apophysis near the surface, thus we can claim that the partitioning is independent of the size of the solution slab in the simulation. Note that this surface enrichment of NaCl does not mean that NaCl is enriched right on top of the solution surface. Actually the density profile of water extends about 0.2 nm beyond that of NaCl towards the vapor region. By contrast, the solution with  $x_{\text{NaCl}} > 0.47$  or < 0.39 do not have this type of partitioning as shown by the red and green lines. This comparison implies that the stability of surface tension of solution with  $x_{\text{NaCl}}$  from  $\sim 0.39$  to  $\sim 0.47$  is related to the "bulk-surface" partitioning. This interpretation is only a conjecture, and more studies are needed to further examine this phenomenon and interpretation. The shallow minimum in the density profile for  $x_{\text{NaCl}}$  between 0.39 and 0.47 to the left of the maximum is somewhat unexpected, and one might expect equilibration problems. However, we have checked that this structural feature develops already during the first 10 ns of the MD simulation, and does not change at all during the residual 200 ns. Surface enrichment of NaCl can be expected, however, when the solubility limit of the water-rich solution in the bulk is reached. Very roughly, such phenomena are analogous to interfacial wetting phenomena such as surface melting of crystals (Frenken and Van der Veen, 1985), which is sometimes observed when the temperature is raised towards the triple point. In our case, the enrichment zone of NaCl (which is about 0.4 nm thick in Fig. 7) would be a precursor effect to the (metastable) NaClrich bulk solution. Tentatively, one may correlate the formation of the enrichment zone with the stability of the surface entropy in this region via the entropy of mixing. At the same time, the surface enhancement of ions may be related to the phenomenon of efflorescence.

As shown in Fig. 6, when a solution gets more concentrated from  $x_{\text{NaCl}}$  of  $\sim 0.47$  to  $\sim 0.64$ , the  $\frac{\Delta H}{A}$  slightly increases from the plateau of  $\sim 145 \, \text{mN m}^{-1}$  but the change is only  $\sim 5 \, \text{mN m}^{-1}$ . The  $-\frac{T \cdot \Delta S}{A}$  keeps increasing. So dur-

ing this period, both the surface excess enthalpy and entropy terms contribute to the growth of  $\sigma_{\text{NaCl,sol}}$ . To constrain the energetic analyses, the  $\frac{T \cdot \Delta S}{A}$  and  $\frac{\Delta H}{A}$  were also calculated for the molten NaCl at 298.15 K. According to Fig. 5, we have  $\sigma_{\text{NaCl}} = -0.0755 \cdot T + 198.09$ ; then we can get  $\frac{\Delta S_{\text{NaCl}}}{A} = 0.0755 \, \text{mN m}^{-1} \, \text{K}^{-1}$  because of  $\frac{\Delta S(T)}{A} = \frac{-\text{d}\sigma(T)}{\text{d}T}$  (Landau and Lifshitz, 1969). Therefore, for molten NaCl  $(x_{\text{NaCl}} = 1.0)$ ,  $\frac{T \cdot \Delta S_{\text{NaCl}}}{A}$  at 298.16 K is 22.15 mN m<sup>-1</sup>, and  $\frac{\Delta H_{\text{NaCl}}}{A}$  at 298.15 K is 198.09 mN m<sup>-1</sup> (Fig. 6). Here, we used the derivative of the temperature–surface tension relation to calculate the excess surface entropy, and more discussions about the comparison of these methods can be found in the Supplement (Fig. S1). As can be seen in Fig. 6, it is expected that the excess surface enthalpy term will still have a large amount (about more than 50 mN m<sup>-1</sup>) to grow until approaching  $\frac{\Delta H}{A}$  of molten NaCl at 298.15 K. It is similar for the surface excess entropy term while the increment is smaller. Thus, the fast increase in  $\sigma_{\text{NaCl,sol}}$  in the concentration of  $x_{\text{NaCl}}$  from  $\sim$  0.47 to 1 can be assumed to be a process driven by excess surface enthalpy and excess surface entropy.

#### 4 Conclusion

The analysis based on the calculated surface tension confirms the basic concept of the Dutcher et al. (2010) semiempirical model, while unfolding a more detailed global landscape of concentration dependence of surface tension of aqueous NaCl solution and its driving forces: (1) a water-dominated regime ( $x_{\text{NaCl}}$  from 0 to  $\sim$  0.39; at low concentrations ions are solvated by the water molecules, which means that water-structures/hydration shells are formed around ions); (2) a transition regime ( $x_{\text{NaCl}}$  from  $\sim$  0.39 to  $\sim$  0.47); and (3) a molten NaCl-dominated regime ( $x_{\text{NaCl}}$  from  $\sim$  0.47 to 1, at very high salt concentration water molecules are solvated by the ions, which means that a salt-structure is formed around the water molecules). Note that our result may not exactly reflect the real mode of surface tension of NaCl solution along

the concentration, but it does imply the concept of a nonmonotonic change of surface tension. One must be aware that for nucleation processes in the atmosphere other chemical compounds also matter, and will require future study. Also, mixed salt solutions would be very interesting, and can in principle be studied with similar simulation methods as applied here; however, this task must be left to future work.

Data availability. Readers who are interested in the data should contact the authors: Yafang Cheng (yafang.cheng@mpic.de), Hang Su (h.su@mpic.de) or Xiaoxiang Wang (xiaoxiang.wang@mpic.de).

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Author contributions. YC and HS conceived and led the study. XW performed the MD simulation and analyzed the data. XW, YC, KB and HS interpreted the results. UP and CC discussed the results and commented on the manuscript. XW, KB, YC, CC and HS wrote the manuscript with input from all coauthors.

Competing interests. The authors declare that they have no conflict of interest.

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