

Impact of dust on tropospheric chemistry over polluted regions: a case study of the Beijing megacity

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Abstract. The box model MECCA (Module Efficiently Calculating the Chemistry of the Atmosphere) is extended by incorporating detailed heterogeneous chemistry occurring on mineral aerosol surfaces. The model is used to investigate the impact of dust on tropospheric photochemistry, when the dust is transported to a polluted region, focusing on the example of Beijing. The impacts of dust via heterogeneous removal of gases are analyzed for different hypothetical transport rates, which are described by four different exchange rate coefficients K_t in the model. Along with the dust, airmasses with trace gas levels characteristic for regions upwind of Beijing are transported with the same rate (K_t) . Substantial impacts are found for many gases, including O_x (O₃+O(³P)), NO_x (NO+NO₂) and OH. The O_x daily average mixing ratio decreases due to heterogeneous reactions on dust. The change ranges from -2.5to $-18.4 \text{ nmol mol}^{-1}$, and is larger for faster mixing with upwind air masses (i.e. greater K_t). This translates into a large relative change in $O_x,$ ranging from -44% to -55%,depending on K_t . By assuming an artificial 50% decrease of all photolysis rates, the impacts of dust via perturbation of the photolysis rates in the polluted region are also estimated. Furthermore, the uncertainties in the results due to the uncertainties in the uptake coefficients are evaluated. It is found that for all gases which are heterogeneously removed, the self-removal results in the largest uncertainty (e.g. -49%for O₃, -76% for NO₂, -47% for HNO₃, -92% for HCHO, -64% for CH₃OH and -93% for SO₂). The heterogeneous removal of NO₂ is found to be particularly important, because it results in significant levels of uncertainty not only for



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itself, but also for OH (340%) and HO₂ (365%). Moreover, the heterogeneous removal rates of HCHO and O₃ also have farther-reaching effects on the OH concentration (resulting in changes of -55% and 45%, respectively), and the heterogeneous removal of HCHO results in an uncertainty of -38%in the HO₂ concentration. The limitations of MECCA due to its missing oxidation mechanism for aromatics and other higher VOC species has also been considered, and shown to be potentially important in the quantitative results, though not likely to change the qualitative results of this study.

1 Introduction

The dust aerosol plays an important role in the physical, chemical, and ecological processes in the earth's system: it is suspected to play a large role in the earth's radiation budget (IPCC, 2007; Haywood et al., 2003; Highwood et al., 2003; Kaufman et al., 2002; Reddy et al., 2005; Stier et al., 2007); it influences ocean and terrestrial biogeochemistry by transporting nutrients like iron (Jickells et al., 2005); and it influences atmospheric chemistry by providing large surfaces for heterogeneous reactions and deposition and mixing with other smaller aerosols (e.g., Dentener et al., 1996.)

Chemical box models as well as global and regional chemistry-transport models have been used to calculate the changes in trace gas mixing ratios due to heterogeneous reactions on mineral dust aerosols. Zhang et al. (1994) and Zhang and Carmichael (1999), for example, used a box model to simulate the loss of SO₂, NO_x, HO₂ and O₃ due to heterogeneous reactions on mineral dust aerosol. They found that the presence of dust resulted in decreases in the concentrations of SO₂ (10%–53%), NO^P_v (16%–100%,

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Fig. 1. The distribution map of Chinese Loess Plateau and surrounding primary desert dust source areas (Maher et al., 2009).

defined as NO₃+N₂O₅+HNO₃), H_xO_y (11%–59%, defined as $OH+HO_2+H_2O_2$), and O_3 (11%–40%) under model conditions representative of spring dust storms in East Asia. Dentener et al. (1996) performed simulations with a global chemistry-transport model and calculated an O₃ reduction up to 10% in and nearby dust source areas. De Reus et al. (2000) calculated a 30-40% reduction of O₃ in a Saharan dust plume near the coast of Africa, attributed to the direct removal of O3 and HNO3. Bian and Zender (2003) found a very small effect (less than 1%) on the global mean O₃ burden while Bauer et al. (2004) predicted a decrease in the O₃ burden of 5% due to heterogeneous reactions on mineral dust. Tie et al. (2005) calculated a maximum reduction of HO_x and O₃ concentrations of 30% and 20%, respectively, over the Sahara desert. In general the effect on surface O₃ concentrations is found to be globally small, but can be significant in dust aerosol source regions such as eastern Asia, the western United States and central Africa.

Mineral dust can affect the tropospheric ozone concentration directly by adsorption of ozone and indirectly by the heterogeneous reactions of ozone precursors (e.g., NO₂ and RO₂). The relationships between tropospheric ozone and its precursors are quite non-linear. Consequently, when dust encounters fresh pollutants, these heterogeneous reactions can lead to a series of complex responses of the photochemical system (Tang et al., 2004). Moreover, mineral dust aerosols can influence tropospheric ozone by changing the photolysis rates of O₃, NO₂, etc.

Although all studies indicate a strong regional influence of mineral dust aerosols on tropospheric chemistry, the results vary greatly. This is mainly due to the large uncertainty in the uptake coefficients for the different trace gases on mineral dust aerosols (e.g., De Reus et al. (2000) calculated that the O_3 mixing ratio ranged from 29 to 45 nmol mol⁻¹ using an accommodation coefficient of 10^{-4} and 10^{-5} , respectively) and the representation of aerosols (e.g., bulk approach versus size resolved and internally mixed aerosols). Moreover, for box model calculations it is difficult to provide realistic initial and boundary conditions, while for 3-D models the

resolution is a challenge, and for all models the comparison with observations is a major challenge.

In this paper we further explore the potential impact of mineral aerosol on tropospheric chemistry, under conditions characteristic of a polluted region. We focus on the example of Beijing city (39.92° N, 116.46° E), the capital city of China. In addition to high anthropogenic emissions, Beijing is also frequently affected by dust storms in spring, which originate from dry regions like the Taklimakan Desert, the Gobi Desert and the Loess areas (Gong et al., 2006) (Fig. 1). For this study, the chemistry box model MECCA (Module Efficiently Calculating the Chemistry of the Atmosphere) is extended by combining dust surface uptake processes with detailed gas-phase chemistry. We assume that the upwind air masses including dust and gases are transported into the polluted region at various mean velocities. The influences of dust via heterogeneous removal of gases and perturbations of the photolysis rates are investigated. In particular, considering the above-mentioned complex responses of the photochemical system, we focus on determining the contributions of the various effects, using chemical budget equations together with the box model outputs, and on qualifying the uncertainty due to the lack of exact knowledge of uptake coefficients.

Section 2 describes the heterogeneous removal processes considered in this study and our modeling setup. In Sect. 3 the results of our model runs are discussed and the uncertainties in the uptake coefficients are analyzed. Section 4 provides a summary of the main results with conclusions.

2 Model description

To investigate the influence of dust aerosol on the mixing ratios of ozone and other reactive gases, model calculations are performed with the chemistry box model MECCA. The chemical reaction scheme has been described by Sander et al. (2005) and includes detailed chemistry of organic species with up to four C-atoms and isoprene (von Kuhlmann et al., 2003). The reaction rates have generally been adopted from the Jet Propulsion Laboratory (JPL) 2003 database (Sander et al., 2003) and the Master Chemical Mechanism (MCM) (http://mcm.leeds.ac.uk/MCM/).

For this study 12 heterogeneous removal reactions on mineral dust (listed in Table 1) have been added to the chemical scheme. In order to describe the transport of dust and gases over polluted regions, three physical processes have been incorporated, including: (1) inflow of upwind dust-rich air masses, (2) deposition and (3) emissions. Sensitivity simulations have been performed with four different exchange coefficients which are used to represent a range of transport velocities. These aspects of the model setup are described in detail in the following subsections.

No.	Heterogeneous reactions	"Best Guess"	Lower Limit	Upper Limit
HR1	$O_3 \rightarrow Dummy$	2.7×10^{-5}	1×10^{-6}	1×10^{-4}
HR2	$HNO_3 \rightarrow Dummy$	0.17	1×10^{-5}	0.2
HR3	$NO_2 \rightarrow Dummy$	2.1×10^{-6}	4×10^{-10}	2×10^{-4}
HR4	$NO_3 \rightarrow Dummy$	0.1	0.01	0.23
HR5	$N_2O_5 \rightarrow Dummy$	0.03	0.01	0.1
HR6	$OH \rightarrow Dummy$	0.1	0.004	1
HR7	$HO_2 \rightarrow H_2O_2$	0.2	0.01	1
HR8	$H_2O_2 \rightarrow Dummy$	2×10^{-3}	8×10^{-4}	0.18
HR9	$SO_2 \rightarrow Dummy$	3×10^{-5}	5×10^{-7}	2.6×10^{-4}
HR10	$CH_3COOH \rightarrow Dummy$	1×10^{-3}	2.4×10^{-4}	2×10^{-3}
HR11	$CH_3OH \rightarrow Dummy$	1×10^{-5}	4×10^{-6}	1.9×10^{-4}
HR12	HCHO → Dummy	1×10^{-5}	2.6×10^{-7}	1.1×10^{-4}

 Table 1. Heterogeneous removal reactions and reactive uptake coefficients.

2.1 Heterogeneous removal reactions

Heterogeneous reactions can deplete gas-phase species by condensation or deposition on aerosol particles. The removal rate of gas-phase species *i* by aerosol particles can be described by a pseudo first-order rate coefficient (s⁻¹), given by Heikes and Thompson (1983):

$$k_i = \int_{r_{\min}}^{r_{\max}} k_{mt,i}(r)n(r)dr,$$
(1)

where n(r)dr (cm⁻³) represents the number concentration of particles with a radius between *r* and r + dr and $k_{mt,i}(r)$ is the size-dependent mass transfer coefficient (m³ s⁻¹), which can be calculated using the formulation given by Fuchs and Sutugin (1970):

$$k_{mt,i} = \frac{4\pi D_i V}{1 + K_n [\chi + 4(1 - \alpha)/3\alpha]},$$
(2)

where D_i (cm² s⁻¹) is the gas phase molecular diffusion coefficient of species i, V is the ventilation coefficient, which is close to unity, and K_n is the dimensionless Knudsen number, which is defined as the ratio of the effective mean free path of a gas molecule in air, λ , to the particle radius r, and χ represents a correction factor for anisotropic movement and is dependent on the Knudsen number. The parameter α is the mass accommodation coefficient (or sticking coefficient), which is a dimensionless number defined as the number of molecules adsorbed by the surface of an aerosol divided by the number of collisions with the aerosol. An alternate parameterization by Schwartz (1986) was used by Dentener et al. (1996), Zhang and Carmichael (1999), de Reus et al. (2000) and de Reus et al. (2005). We have tested using this instead, and find that all results differ by less than 5% compared to using Eq. (B4).

There are two important parameters for interactions of gases with dust surfaces: the mass accommodation coefficient, α , and the reactive uptake coefficient, γ . γ represents the fraction of collisions with a particle that leads to irreversible loss of the gas, whereas α only indicates the reversible adsorption. The value of α usually represents an upper limit of γ . For the calculation of the gas removal rate in the model, we use values of γ based on laboratory studies.

In recent years, numerous measurements of the accommodation or uptake coefficient on mineral aerosol have been performed and have been used in model studies. A discussion of the available measurements for the species of interest and the values used in other model studies, along with those selected for use in our simulations are given in Appendix A. The 12 heterogeneous removal pathways, along with the "best guess" values and the lower and upper limits for the reactive uptake coefficient of the different gases on dust aerosol mentioned above are listed in Table 1.

2.2 Inflow, deposition and emission

In this work, three physical processes are included in the box model MECCA: (1) inflow of upwind dust-rich air masses, (2) deposition and (3) emissions, as described below.

We consider the transport of dust and gases in a highly simplified way, by replacing a fraction of the air mass in the box directly by the incoming air mass, so that the tendency is calculated as:

$$\frac{\partial C_i}{\partial t} = (C'_i - C_i) \cdot f, \tag{3}$$

where C'_i is the concentration of component *i* (dust and gases) in the upwind air masses, *t* is the modeling time step and *f* is the exchange rate coefficient, which is defined as the fraction of air mass in the box replaced per unit time by the incoming air mass (note that *f* is the same for all components *i*).



Fig. 2. Size distribution of dust surface area concentration in upwind air mass and in the box, for the four exchange rates used in the study.

We assume a homogeneous vertical distribution of all the simulated species in the boundary layer. For the emitted species, the increase in concentration C_i (which we call the source term, B_e) can be calculated from the emission flux J_e and the height of the boundary layer Z_{pbl} :

$$B_e = \frac{\partial C_i}{\partial t} = \frac{J_e}{Z_{pbl}}.$$
(4)

The deposition flux J_d for the dry deposition can be parameterized as the product of the concentration C_i and the deposition velocity v_d :

$$J_d = -v_d C_i. \tag{5}$$

To obtain the concentration change, the deposition flux is divided by the height of the boundary layer Z_{pbl} :

$$\frac{\partial C_i}{\partial t} = -\frac{v_d C_i}{Z_{pbl}}.$$
(6)

where v_d/Z_{pbl} is defined as the deposition coefficient K_d . Note that the parameters J_e (and thus B_e) and v_d (and thus K_d) differ for each species *i*; these are discussed further in the following sections, and information on their values is given in Table 2. Wet deposition is not included in this study, considering that dust storm events only occur when it is not raining.

2.3 Input parameters

The air parcel encompasses the boundary layer, which is assumed to be uniformly mixed up to 756 m. Temperature, air pressure, and relative humidity as input parameters are kept constant during the simulations at 284.35 K, 943.17 hPa, and 44%, respectively. These physical parameters, the initial gas-phase species concentrations C_i and the upwind gas-phase species concentrations C'_i are derived from the global atmospheric chemistry general circulation model ECHAM5/MESSy Atmospheric Chemistry (EMAC) (Jöckel et al., 2006). The EMAC simulation from which these parameters were obtained (B. Steil, personal communication, 2008) was performed with a horizontal resolution of T106 on a Gaussian grid (approximately $1.1^{\circ} \times 1.1^{\circ}$ in longitude and latitude, respectively) and 31 levels on a hybrid-pressure grid in the vertical. The output was archived every 5 h. The monthly average values for April 2006 for the boundary layer of the grid covering Beijing are used for the initial concentrations, and the values of the neighboring grid to the west are used for the upwind concentrations. The initial (y_i) and upwind (y'_i) mixing ratios of key gases, along with their deposition velocities, are listed in Table 2. One may note that the values are lower in the upwind airmass than in the "box" for all species except O_3 . This is caused by the strong emission of NO_x in the Beijing area, that results in lower ozone production efficiency in the "box" than in the upwind area, where there is less NO_x. This phenomenon has commonly been observed in and around North American and European cities (e.g. Kleinman et al., 1994; Kleinman, 2000). For the dust size distribution, we have used measurements over Northern China coastal areas during a dust storm episode in April 2006, which are assumed to be generally representative for the dust source regions in North China (Wang et al., 2008). The assumed upwind dust size distribution is shown in Fig. 2.

The emission fluxes of CO, NO_x , NMVOC (non-methane volatile organic compound) and SO_2 for the Beijing urban area are derived from the regional emission inventory of North China for the year 2006 (Zhao, 2007). The calculated emission rates of key gases are listed in Table 2.

The dry deposition velocities of dust in different size classes are taken from Lee et al. (2005). They estimated the dry deposition velocity of Asian dust in spring of 2002 for 11 particle size bins with diameters ranging from 0.2 to 74 μ m. The deposition velocities of gases are derived from the archived output of the EMAC simulation.

2.4 Sensitivity simulations

The wind speed and direction at 10 m above ground observed hourly at one meteorological station located in the Beijing urban area (39.48° N, 116.28° E) show that in April 2006 the wind originating from the west has a average velocity of 2.2 m s⁻¹ and a maximum velocity of 5.0 m s⁻¹, while the wind from the northwest has an average velocity of 5.1 m s⁻¹ and a maximum velocity of about 10.5 m s⁻¹ (Fig. 3). To investigate the impact of dust which is imported to the Beijing region with different transport velocities, four cases are considered with different mixing time lengths. From slow to fast mixing, they are the "T16" case (1/*f*=16 h), "T08" case (1/*f*=8 h), "T04" case (1/*f*=4 h) and "T02" case (1/*f*=2 h), in which the exchange rate coefficients *f* are

gases (nmol mol ⁻¹)	y_i (nmol mol ⁻¹)	y'_i (cm s ⁻¹)	v_d (nmol mol ⁻¹ s ⁻¹)	B _e
O ₃	55.5	59.2	0.18	0
NO ₂	8.6	5.7	0.13	4.3×10^{-4}
NO	1.3	0.9	6.3×10^{-3}	3.8×10^{-3}
CO	245.4	222.1	0	0.04
SO ₂	19.8	13.8	0.19	1.3×10^{-3}
H_2O_2	0.23	0.19	0.29	0
CH ₄	1789.6	1787.8	0	0
НСНО	0.91	0.83	0.07	7.3×10^{-5}
CH ₃ OH	2.13	1.97	0.06	1.4×10^{-4}

Table 2. The initial (y_i) and upwind (y'_i) mixing ratios, deposition velocities (v_d) and emission rates (B_e) of key gases.

 1.7×10^{-5} , 3.5×10^{-5} , 7.0×10^{-5} and 1.4×10^{-4} per second, respectively. According to Gurjar et al. (2008), the surface area of Beijing megacity is about 20 000 km², which would correspond to ~150 km per side. However, this applies to the entire Beijing district; only considering the highly populated central district would be about 10% of this area, or about 50 km per side. If we take a length scale of 100 km as intermediate between these extremes, then we estimate corresponding mean horizontal wind speeds ranging from 1.7 m s^{-1} to 14 m s^{-1} . Thus the T16 case is at the low end of the mean winds originating from the west or northwest, while the T02 case represents an extreme case of very strong inflow from upwind regions. The dust number concentration dN of size bin *i* at time step *t* is calculated in two steps, first:

$$dN_{t,i} = dN_{t-1,i} + (dN_{0,i} - dN_{t-1,i}) \cdot \Delta t \cdot f$$
(7)

where $dN_{0,i}$ is the "upwind dust number concentration" derived from our observation data; Δt is the time step interval length; f is the exchange rate coefficient. This is followed by:

$$dN_{t,i} = dN_{t,i} \cdot (1 - \Delta t \cdot v_{di}/Z_{pbl})$$
(8)

where v_{di} is the deposition velocity of size bin *i*, and Z_{pbl} is the planet boundary layer height. Then the dust surface area concentration $dS_{t,i}$ is estimated by:

$$dS_{t,i} = dN_{t,i} \cdot 4 \cdot \pi \cdot r_i^2 \tag{9}$$

where r_i is the radius of the dust particle of size bin *i*. The combination of the increase in the exchange rate coefficient *f* from the T16 case to the T02 case, and the larger v_{di} for the larger dust particles results in the dust distributions shown in Fig. 2.

The settings of these four cases are listed in Table 3. In each case, four simulations are performed: a simulation without dust (NO_DUST), a simulation with dust but only considering the heterogeneous reactions (DUST_H), a simulation with dust, but only considering a decrease of photolysis rates (DUST_J) and a simulation considering boththe



Fig. 3. Wind rose depicting the monthly average, minimum and maximum wind speed and direction during April 2006 at a station in the Beijing urban area (39.48° N, 116.28° E).

heterogeneous reactions and a decrease of photolysis rates (DUST_H+J). Jeong et al. (2007) calculated a 47.3% decrease in the reactions having photolytic wavelengths in the UV (210–380 nm) at surface, for dust assumed to have a size distribution like that measured during ACE-Asia. In this study, an artificial 50% decrease of all photolysis rates is used for the DUST_J simulation and the DUST_H+J simulation, to examine the basic sensitivity in the context of dust over Beijing.

For the simulations, we allow a spinup time of 96 h. This is sufficient to establish equilibrium with the upwind air mass for the long-lived tracers (e.g. CO and dust), even for the T16 case. In the following sections, analyses are based on the fifth simulation day, after equilibrium has been established.

The difference between the DUST_H and NO_DUST simulations isolates the influence of dust via heterogeneous reactions. The additional dust influence through photolysis

Table 3. The settings used for the sensitivity simulations. The equivalent mean transport speed is estimated based on the assumption of a characteristic spatial scale for Beijing of 100 km.

	T16	T08	T04	T02
Mixing time length λ (hours) Exchange rate coefficient f (s ⁻¹) Mean transport speed v (m s ⁻¹)	16 1.7×10 ⁻⁵ 1.7	8 3.5×10 ⁻⁵ 3.5	$ \begin{array}{l} 4 \\ 7 \times 10^{-5} \\ 7 \end{array} $	$2 \\ 14 \times 10^{-5} \\ 14$

Table 4. Gas phase reaction indices.

Reaction No.	Reaction
R1	$O_3+hv \rightarrow O_2+O(^3P)$
R2	$O(^{3}P)+O_{2} \rightarrow O_{3}$
R3	$O_3+NO \rightarrow NO_2+O_2$
R4	$NO_2+hv \rightarrow NO+O(^{3}P)$
R5	$NO+HO_2 \rightarrow NO_2+OH$
R6	$HONO+hv \rightarrow NO+OH$
R7	$H_2O+O(^1D) \rightarrow 2OH$
R8	NO+OH→HONO
R9	$NO_2+OH \rightarrow HNO_3$
R10	$CO+OH \rightarrow H+CO_2$
R11	$SO_2+OH+O_2+H_2O \rightarrow H_2SO_4+HO_2$
R12	$NO_2+O_3 \rightarrow NO_3+O_2$

rates perturbation is represented by the difference between the DUST_J and NO_DUST simulations. These differences are discussed separately in the following section.

3 Results

3.1 Influence of the exchange rate coefficient

In this section, we will first discuss the influence due to mixing with upwind air mass (without the additional influence of dust), then in Sects. 3.2 and 3.3, we will consider the influence of dust via heterogeneous reactions and photolysis perturbation, respectively. The time series of the mixing ratios of O₃, NO, NO₂ and the concentration of OH for 24 h (beginning at 00:00 of the fifth simulation day) are shown in Fig. 4 (black curves). A positive correlation with the exchange rate coefficient *f* is found for the O₃ mixing ratio and the OH concentration for the NO_DUST simulation, and a negative correlation is found for the NO and NO₂ mixing ratios. We can understand the main factors contributing to these changes by examining the budget equations for each of these gases.

Considering the existence of the null cycle, Reactions (R1) and (R2) in Table 4, the Reaction (R3) is a dominant loss term for O_3 , from which the corresponding loss frequency

will be much larger than the loss frequency due to heterogeneous removal of gases on dust. In order to better display the influence of heterogeneous removal on the tropospheric photochemistry in the following sections, only the family budget of O_x (defined as $O_3+O(^3P)$) will be analyzed. $O(^1D)$ is not included in O_x due to its negligible effect (only ~1%). Similarly, the rapid photochemical equilibrium between NO and NO₂, established by the Reactions (R3), (R4) and (R2), tends to dominate the individual budgets of NO and NO₂, so that it is more enlightening to examine the budget of the family NO_x (defined as NO+NO₂).

Considering that steady state has been reached, we have the equation:

$$K_t \cdot (C'_i - C_i) + B_e - K_d \cdot C_i + B_{cp} - K_{cl} \cdot C_i = 0,$$
(10)

where C'_i is the concentration of component *i* in the upwind air masses, C_i is the daily average concentration of component *i*, K_t represents the exchange rate coefficient (i.e. "*f*" in Eq., B1), B_e is the source term due to direct emission into the box (i.e. " J_e/Z_{pbl} " in Eq. 4), K_d is the deposition coefficient (i.e. " v_d/Z_{pbl} " in Eq. 6), B_{cp} is the daily average gross chemical production rate, and K_{cl} is the daily average gross chemical loss frequency (so that $K_{cl} \cdot C_i$ is the daily average gross chemical loss term in the budget). Based on Eq. (10), we can solve for C_i :

$$C_{i} = \frac{K_{t} \cdot C_{i}' + B_{e} + B_{cp}}{K_{t} + K_{cl} + K_{d}},$$
(11)

where C'_i , B_e and K_d are fixed, while B_{cp} and K_{cl} change with K_t because the tracer concentrations in the box are influenced by the inflowing upwind air mass.

Since the model is nearly in steady state, the change in O_3 mixing ratio during the day (calculated as the mixing ratios at the end of day five minus the beginning of the fifth day) is very small, and a balance between its net production term (i.e. the transport process) and its net loss terms (i.e. the deposition process and the chemistry process) is reached, as listed in Table 5. The emission budget term is zero because no significant direct emission of O_3 occurs. The transport process is the only production term of O_3 and the corresponding major competitive process is the net chemical loss. It is qualitatively similar for O_x . The relationship between O_x mixing ratio and these four processes in steady state is described in Eq. (11). For O_x , no emission is considered, so in



Fig. 4. Time series of (a) O_3 , (b) NO and (c) NO_2 mixing ratios and (d) OH concentration for 24 h of the fifth simulation day. Different exchange rate coefficient cases are shown from left to right: "T16", "T08", "T04" and "T02". Results of the NO_DUST simulations and the DUST_H simulations are shown in black and red, respectively.

Table 5. Changes in O_3 and NO_x mixing ratios (*y*) during the course of the 5th day of NO_DUST simulation, and factors contributing to the budget of each. (unit: nmol mol⁻¹).

Tracer		(D ₃		NO _x			
Rate Contribution Process	T16	T08	T04	T02	T16	T08	T04	T02
Change in y	1.6E-15	3.9E-16	-2.5E-16	2.5E-10	0.2	0.1	0.2	-0.01
Transport	80.6	150.1	231.7	230.9	-341.4	-350.7	-356.4	-355.5
Emission	0	0	0	0	365.1	365.1	365.1	365.1
Deposition	-1.1	-1.9	-4.3	-8.3	-15.5	-11.2	-7.9	-4.3
Chemistry	-79.5	-148.2	-227.4	-222.6	-7.9	-3.2	-0.7	-5.4



Fig. 5. The daily average mixing ratios of (**a**) O_x , (**b**) NO and NO₂, (**c**) NO_x and concentration of (**d**) OH for the NO_DUST simulations, and their gross chemical production rates B_{cp} and gross chemical loss frequencies for O_x and NO_x are multiplied by 10 and 100, respectively, for readability. For each term, the bar sequence from left to right is: "T16", "T08", "T04" and "T02".

Eq. (11), $B_e = 0$. y'_i (and thus C'_i) and K_d are fixed for O₃ as listed in Table 2, and no physical process effects O(³P), while B_{cp} and K_{cl} change with the increasing K_t , as shown in Fig. 5a. From the T16 case to the T02 case, K_t doubles each step from $1.7 \times 10^{-5} \text{ s}^{-1}$ to $1.4 \times 10^{-4} \text{ s}^{-1}$, while B_{cp} and K_{cl} decrease in magnitude. Since no heterogeneous reactions on dust are included yet, the changes in B_{cp} and K_{cl} are due only to the changes in NO_x and other gases. Although K_t doubles each step, B_{cp} and K_{cl} are the dominating factors of the numerator and denominator of Eq. (11), respectively, which causes both the numerator and the denominator to decrease with the doubling K_t . We find that for each step from the T16 case to the T02 case, the relative decrease of the denominator is about 2 times larger than the relative decrease of the numerator. Consequently, the O_x daily average mixing ratio approximately doubles when doubling K_t , although not exactly, as shown in Fig. 5a.

Similar to O_3 , the change in NO_x mixing ratio during the day is very small and a balance between its production term (i.e. the emission process) and its loss terms (i.e. the transport process, the deposition process and the chemistry process) is reached, as listed in Table 5. However, different from O_3 , the emission process is the only production term of NO_x and the corresponding major competitive process is the transport process. In Eq. (11), for NO_x, both the chemical production rate B_{cp} and the chemical loss frequency K_{cl} increase with the doubling K_t as shown in Fig. 5c. Different from O_x , the local emission rate B_e is the largest production term, and K_t is the largest loss frequency, especially when the mixing is slow (i.e. smaller K_t). Both the numerator and the denominator of Eq. (11) increase with the doubling K_t . However, for each step from the T16 case to the T02 case, the relative increase of the denominator is larger than the relative increase of the numerator. Consequently, both the NO and NO₂ daily average mixing ratios decrease with the doubling K_t , as seen in Fig. 5b.

As a short-lived radical, the OH concentration is determined only by its chemical budget. As shown in Fig. 6a, the major source terms of OH are Reactions (R5), (R6) and (R7). As already discussed, when the exchange rate coefficient increases, the NOand NO₂ mixing ratios decrease. Thus, the rates of reactions R5 and R6 decrease with the increasing exchange rate coefficient K_t . This causes the decrease of the OH gross production rate with the increasing K_t , as seen in Fig. 5d. On the other hand, the major loss terms of OH are Reactions (R8), (R9), (R10) and (R11), due to the high mixing ratios of NO, NO₂, CO, and SO₂ from local emissions. The "Miscellaneous" loss term, which represents the loss of OH due to all other reactions, mostly with various hydrocarbons, is also important. It is worth noting that the Reaction (R11) plays an unusually large role over Beijing, due to the high SO₂ mixing ratios originating largely from local emissions. Since the mixing ratios of NO, NO₂, CO, SO_2 and hydrocarbons decrease with the increasing K_t , the gross loss reaction frequency decreases in magnitude, as seen in Fig. 5d. We find that the relative decrease in the gross loss frequency is larger than the relative decrease in the gross production rate. As a result, the daily average OH concentration increases with increasing K_t , as seen in Fig. 5d.

3.2 Influence of heterogeneous uptake on dust

The influence of dust via heterogeneous reactions is discussed in this section. First, following up on the discussion in the previous section, for the DUST_H simulations, when K_t increases, the tendencies of the O_x and NO_x mixing ratios are qualitatively similar to those for the NO_DUST simulations discussed in Sect. 3.1. However, the tendency of the OH concentration is different: it stays nearly constant, decreasing slightly from the T16 case to the T08 case, then increasing again to the T02 case. The OH concentration results from a delicate balance between loss and production terms as discussed above. Introducing losses of several gases on dust, especially NO₂ and SO₂, shifts this balance so that OH responds differently to K_t in the DUST_H case than in the NO_DUST case.

The overall effect of introducing the heterogeneous dust reactions is to decrease the Ox mixing ratio, as seen in Fig. 7a. The change ranges from -2.5 to -18.4 nmol mol⁻¹, and is larger for faster mixing in of upwind air masses (i.e. greater K_t). This translates into a large relative change (in percentage, calculated as $100 \times (DUST_H - NO_DUST)/NO_DUST)$ in O_x, ranging from -44% to -55%, which increases in magnitude slightly from the T16 case to the T04 case, then decreases in magnitude slightly to the T02 case. In order to understand how the various changes due to the inclusion of heterogeneous dust reactions contribute to this decrease in O_x , as well as for other gases (discussed below), we can analyze the budget equations for the DUST_H and NO_DUST cases more closely. Based on Eq. (11), the heterogeneous influence on the tracer daily average concentration is represented as (for any species *i*, leaving out the subscript here for readability):

$$\Delta C = \frac{\Delta B_{cp} - \Delta K_{cl} \cdot C_{(\text{NO},\text{DUST})}}{(K_t + K_{cl}(\text{DUST},\text{H}) + K_d)}.$$
(12)

The derivation of Eq. (12) is explained in Appendix B. Since the denominator in Eq. (12) is always positive, this indicates that the balance between the changes in the gross chemical production rate B_{cp} and the gross chemical loss frequency K_{cl} , determine whether the heterogeneous reactions will cause an increase or decrease in the daily average mixing ratio. Since the direct influence of dust due to heterogeneous uptake of *C* is included in the chemical loss frequency, K_{cl} , and its change, ΔK_{cl} , one would expect this to result in a tendency for the mixing ratios of most gases to decrease, as seen to be the case for O_x, though this is not always the case, as shown below. Equation (12) also shows that, all else being



Fig. 6. (a) The daily average chemical production rates (labels in black) and chemical loss frequencies (labels in red) of OH for the NO_DUST simulation. (b) The differences between the DUST_H and NO_DUST simulations (DUST_H-NO_DUST). "Miscellaneous" represents the sum of all the other source or loss terms. The bar sequence is the same as in Fig. 5. The reactions are listed in Table 4.

equal, the change in *C* becomes smaller as the rate of mixing (K_t) becomes larger (in comparison to $K_{cl(\text{DUST}-\text{H})}$).

As shown in Fig. 7a, for each of the four exchange rate coefficient cases, the gross chemical production rate (B_{cp}) decreases when the dust reactions are included. This is mainly due to the decrease in the NO₂ mixing ratio (Fig. 7b). The relative change in B_{cp} is substantial, ranging from about -37% (T16) to -21% (T02). On the other hand, as K_t increases from the T16 case to the T02 case, the dust surface area concentration also increases as shown in Fig. 2. Consequently, the O_x loss frequency due to the heterogeneous removal (HR1) also increases, as shown in Fig. 7a. This, however, is small compared to the change in K_{cl} , also shown in Fig. 7a. The relative change in K_{cl} is substantial, ranging from 13% (T16) to 61% (T04), as shown in Fig. 8a, and is mostly governed by the change in NO via the Reaction (R3) which increases substantially as shown in Fig. 7b. Because the relative increase of NO is largest in the T04 case, it is thus the T04 case, instead of the T02 case, which has the largest relative increase in the K_{cl} of O_x . This is part of another



Fig. 7. Differences of the daily average mixing ratios and the gross chemical production rates B_{cp} and the gross chemical loss frequencies K_{cl} of (a) O_x , (b) NO and NO₂ (c) NO_x, and (d) OH, between the DUST_H and NO_DUST simulations (DUST_H–NO_DUST). The bar sequence is the same as in Fig. 5.

Fig. 8. Relative differences of the daily average mixing ratios and the gross chemical production rates B_{cp} and the gross chemical loss frequencies K_{cl} of (a) O_x , (b) NO_x , and (c) OH due to the heterogeneous dust reactions. The bar sequence is the same as in Fig. 5.

null cycle (Reactions R3, R4 and R2), which can principally be removed by extending the definition of O_x to include NO₂ (Crutzen and Schmailzl, 1983). When the budget of O_x with this broader definition as $O_3+O(^3P)+NO_2+O(^1D)$ is analyzed, the strong direct effect of the heterogeneous reaction becomes apparent. For example, in the T08 case, the loss frequency of the heterogeneous uptake (HR1+HR3) is 1.6×10^{-5} s⁻¹ and the ΔK_{cl} is 1.2×10^{-5} s⁻¹, which corresponds to a relative increase of 125% (The value of K_{cl} in the NO_DUST run is $0.96 \times 10^{-5} \text{ s}^{-1}$). ΔK_{cl} is a bit smaller than the loss frequency of the heterogeneous uptake, due to the negative response of some gas phase reactions (e.g. the loss frequency of the reaction $NO_2+O_3 \rightarrow NO_3+O_2$ Reaction (R12) decreases by $3.3 \times 10^{-6} \text{ s}^{-1}$). Since, however, O₃ and NO_x more closely correspond to the quantities that are normally reported in observations and other modeling studies, we will mostly employ these standard definitions here, rather than the extended O_x definition.

The overall effect of introducing the heterogeneous dust reactions is to decrease the NO_x mixing ratio, as seen in Fig. 7c. The decrease ranges from -18 to -2.7 nmol mol⁻¹, and is smaller for faster mixing in of upwind air masses (i.e. greater K_t). This translates into a relative decrease ranging from -8% to -9% (Fig. 9b), which changes slightly with increasing values of K_t . For each of the four exchange rate coefficient cases, the gross chemical production rate (B_{cp}) decreases when the dust reactions are included. This is mainly due to the decrease in other gases, e.g. NO₃ and N₂O₅. The relative decrease in B_{cp} is substantial, increasing in magnitude from about -42% (T16) to -93% (T02). From the T16 case to the T02 case, the NO_x loss frequency due to the heterogeneous removal (HR3) increases due to the increasing dust surface area concentration, as shown in Fig. 7c. This translates into a substantial relative change in the gross chemical loss frequency K_{cl} , which is positive for T16 and T08 and negative for the other two cases, as shown in Fig. 8b. This is because the change in K_{cl} is also influenced by the decrease in NO₃ via the reaction NO₃+NO₂ \rightarrow N₂O₅, which changes from $-2.7 \times 10^{-8} \text{ s}^{-1}$ in the T16 case to -9.0×10^{-5} s⁻¹ in the T02 case, and is larger in magnitude than the increase in the loss frequency of the heterogeneous removal HR3 in the T04 and T02 cases.

As shown in Figs. 7d and 8c, the overall influence of the heterogeneous dust reactions is to increase the OH concentration in the T16 case, and reduce OH in the other three cases. The corresponding relative change ranges from 4% in the T16 case to -33% in the T02 case. On the whole, this is due to the balance in the production and loss terms in the chemical budget (see Eq. 11), especially given the short lifetime of OH. For all four cases, both the gross production rate B_{cp} and the gross loss frequency K_{cl} decrease. However, as K_t increases from the T16 case to the T02 case, the relative change in B_{cp} increases in magnitude. In the T16 case, the relative change in B_{cp} is smaller in magnitude than in K_{cl} , leading



Fig. 9. Differences of the daily average chemical production budgets (black bars) and chemical loss frequencies (red bars) of OH, between the DUST_J and NO_DUST simulations (DUST_J-NO_DUST) in the T04 case. "Miscellaneous" (hollow bars) represents the sum of all the other source or loss terms. The reactions are listed in Table 4.

to the increase in OH concentration. In the other three cases the relative change in B_{cp} is larger in magnitude than in K_{cl} , leading to the decrease in OH concentration. For the T08, T04 and T02 cases, the relative change in OH concentration increases in magnitude as K_t increases. The main reactions responsible for these changes are depicted in Fig. 6d. The change in the gross production rate B_{cp} is mainly due to the reaction R5, because of the strong local buildup of NO_x (up to about $150 \text{ nmol mol}^{-1}$ of NO in the T16 case) caused by the strong urban emissions. The change in the gross loss frequency K_{cl} is primarily due to the reactions R9 and R11, especially strongly in the T16 case, again due to the buildup of high local pollution levels, in this case NO₂ and SO₂, where the latter can be expected to be particularly applicable to Chinese megacities (Tang et al, 2004). On the whole, this shows that the OH response to dust reactions is complex and will be difficult to predict for other cities without model simulations (box or 3-D) applicable to their specific conditions.

3.3 Photolysis influence

In order to investigate the influence of dust via photolysis rate perturbations, the simulation DUST_J is performed for the T04 case with an artificial 50% decrease of all photolysis rate coefficients. It is important to note that the actual change in photolysis rates due to dust will vary from species to species, due to the wavelength-dependent effects of dust particles on the actinic flux; the approach here is only meant to establish an order-of-magnitude estimate of this effect, as an indicator of whether or not it is worth continued investigation for characterizing the effects of dust on chemistry in Beijing. The differences in the daily (24 h) mean mixing ratios and the gross chemical production budgets and loss frequencies of O_x , NO_x and OH between the DUST_J and NO_DUST

Table 6. The differences calculated as DUST_J–NO_DUST of the daily average mixing ratios (*y*) and the gross chemical production rates (B_{cp}) and the gross chemical loss frequencies (K_{cl}) of O_x, NO_x and OH due to the decrease of photolysis rate coefficients for the T04 case. The relative differences calculated as (DUST_J–NO_DUST)/NO_DUST are shown in parentheses. For OH, the concentration *C* is shown instead of the mixing ratio *y*.

	у	B _{cp}	K _{cl}
O _x NO _x OH	$\begin{array}{l} -3.7 \mathrm{nmol} \mathrm{mol}^{-1} (-17.8\%) \\ 0.3 \mathrm{nmol} \mathrm{mol}^{-1} (0.5\%) \\ -8.5 \times 10^4 \mathrm{molecules} \mathrm{cm}^{-3} (-54.2\%) \end{array}$	$\begin{array}{l} -0.05 \ \mathrm{nmol} \ \mathrm{mol} \ ^{-1} \ \mathrm{s}^{-1} \ (-42.3\%) \\ -1.5 \times 10^{-4} \ \mathrm{nmol} \ \mathrm{mol} \ ^{-1} \ \mathrm{s}^{-1} \ (-7.5\%) \\ -2.2 \times 10^{6} \ \mathrm{molecules} \ \mathrm{cm}^{-3} \ \mathrm{s}^{-1} \ (-52.3\%) \end{array}$	$\begin{array}{c} -1.8 \times 10^{-3} {\rm s}^{-1} (-28.6\%) \\ -2.4 \times 10^{-6} {\rm s}^{-1} (-10.1\%) \\ 1.1 {\rm s}^{-1} (4.2\%) \end{array}$

Table 7. The linearly summed influences (calculated as $DUST_H-NO_DUST+DUST_J-NO_DUST$) and the nonlinearly combined influences (calculated as $DUST_H+J-NO_DUST$) of dust on the daily average mixing ratios *y* of O_x , NO_x and the daily average concentration *C* of OH through the heterogeneous removal reactions and the photolysis rates decrease for the T04 case. The relative influences (i.e. the influences normalized by NO_DUST) are shown in parentheses.

	$O_x nmol mol^{-1}$	$NO_x nmol mol^{-1}$	$OH molecules cm^{-3}$
Linear	-15.2 (-73.3%)	-5.2 (-8.6%)	$-1.1 \times 10^5 (-69.9\%)$
Nonlinear	-13.2 (-63.8%)	-5.9 (-9.6%)	$-9.6 \times 10^4 (-61.1\%)$

simulations and the relative differences are listed in Table 6. This artificial photolysis rate perturbation causes a large relative decrease in OH (-54%) and O_x (-18%), respectively, while only a small relative increase (0.5%) is computed for NO_x.

When the photolysis rate coefficients are reduced, the rate of the reaction R4 decreases, and thus the B_{cp} of O_x decreases. On the other hand, the values of K_{cl} for O_x also decrease due to the change in NO mixing ratio $(-2.8 \text{ nmol mol}^{-1})$. Since the relative decrease in the B_{cp} is larger than the relative decrease in the K_{cl} , and based on Eq. (12), the O_x mixing ratio decreases due to the dust photolysis perturbation.

For NO_x, as discussed in Sect. 3.1, the numerator and denominator of Eq. (11) are dominated by the emission rate B_e and the exchange rate coefficient K_t , respectively. As a result, although B_{cp} decreases by 7.5% and K_{cl} decreases by 10.1%, the numerator and denominator of Eq. (11) do not change significantly. Consequently, NO_x mixing ratio only decreases slightly.

As shown in Fig. 9, all the production terms of OH decrease due to the decrease in the photolysis rate coefficients, so the B_{cp} of OH decreases. On the other hand, the small increase in the OH loss frequency is due to the balance between large changes in the reactions with NO (Reaction R8) and NO₂ (Reaction R9), with the latter dominating slightly. This combination results in the large decrease in the OH concentration.

In real conditions, the effects of dust on the tropospheric chemistry through the heterogeneous removal and the photolysis perturbations will act simultaneously. To test the degree of nonlinearity, we can compare the results from the DUST_H+J simulation to the sum of individual changes in the DUST_H and the DUST_J simulations, as shown in Table 7. We find that the differences (i.e., the nonlinearities) are small, with the nonlinearly combined influences of dust on O_x and OH being somewhat smaller than the linearly summed influences: the differences in the relative influences are 9.5% for O_x 8.8% for OH, and only 1% for NO_x .

3.4 Uncertainties

As described in Appendix A, due to the different types of mineral dust and different methodologies used in laboratory experiments, the measured accommodation or uptake coefficients have large uncertainties, in some cases several orders of magnitude. This can lead to large uncertainties in the calculated heterogeneous removal influence of dust. We can make use of the numerical model to examine the relative significance of the influence of each heterogeneous removal reaction and the uncertainty in the results. For this purpose, simulations in the T08 case have been performed in which one removal reaction is calculated individually with either the "Lower Limit" or "Upper Limit" coefficient from Table 1, and all the other removal reactions are calculated with the "Best Guess" coefficients. The differences in the tracer mixing ratios calculated with the "Upper Limit" and "Lower Limit" coefficients are normalized by the tracer mixing ratio calculated without dust considered, i.e. $\frac{y_{\text{DUST}} + (\gamma_{\text{Upper}}) - y_{\text{DUST}} + (\gamma_{\text{Lower}})}{y_{\text{NO}} - D_{\text{UST}}}$, and the results are compared in Fig. 10. The absolute differences, i.e. $y_{\text{DUST}}(\gamma_{\text{Upper}}) - y_{\text{DUST}}(\gamma_{\text{Lower}})$, are shown in Appendix C for reference. The uncertainties are negative for the gases which are reduced due to the heterogeneous removals, and positive for the gases which are increased due to the heterogeneous removal. Although the cumulative effect of all reactions can be different, some insight into the effect of each single reaction is provided by this approach.

For all gases which are heterogeneously removed, the self-removal results in the largest uncertainty (e.g. -49.2% for O₃, -75.7% for NO₂, -46.6% for HNO₃, -92.2% for HCHO, -64.3% for CH₃OH and -93.3% for SO₂), except for OH and HO₂, for which the largest uncertainties come from the heterogeneous removal of NO₂. We find that the heterogeneous removal of NO₂ is particularly important, because it results in significant uncertainties not only in itself, but also in OH (340.4\%) and HO₂ (365.6\%). Moreover, the heterogeneous removals of HCHO and O₃ also have farther-reaching effects, causing uncertainties in the OH concentration of -54.8% and 45.0%, respectively; furthermore, the heterogeneous removal of HCHO results in an uncertainty of -38.4% in HO₂ concentration.

If we instead normalize by the tracer mixing ratio calculated with the "Best Guess" coefficients, i.e. $\frac{y_{\text{DUST}-H}(y_{\text{Upper}})-y_{\text{DUST}-H}(y_{\text{Lower}})}{y_{\text{DUST}-H}(y_{\text{Rest}-Guess})}$, we compute larger uncertainties (e.g. -89.8% for O₃) and some with extremely large values (e.g. -558552% for HNO₃). This is because introduction of the heterogeneous removal reactions (i.e., the DUST_H "Best Guess" case) already decreases these tracer mixing ratios as discussed in Sect. 3.2, even to extremely low values for some tracers like HNO₃ due to their rapid uptake. The uncertainties computed with this manner are also shown in Appendix D for reference.

On the whole, the results clearly indicate that the uncertainty in the uptake coefficients result in large uncertainties for the influence of dust under polluted conditions, and point towards where future work should be focused.

The chemical reaction scheme used in this study includes detailed chemistry of organic species with up to four Catoms and isoprene. Uncertainties are expected due to the limited VOC species considered in the model, since aromatic species and other VOC species with more than four C-atoms are also important for the gas-phase photo oxidation chemistry in an urban area. To partially account for this, in the model simulations discussed above we have already distributed the missing VOC (in terms of mass of C) as a surrogate amongst the lower hydrocarbons (including Ethylene, Ethane, Propene, Propane, Butane, Acetaldehyde, Acetone, Acetic acid, Methanol, Methanal, Formic acid and Methyl Ethyl Ketone). To gain a further impression of the uncertainty introduced by this surrogate treatment of the missing VOC, here we perform two additional sensitivity runs in which we redistribute a large fraction of the total VOC into two surrogate species, C₃H₆ and C₄H₁₀ with different reactivities and oxidation pathways (and thus effects on ozone and OH). For this sensitivity study, we have chosen to re-



Fig. 10. Uncertainties of the tracer mixing ratios caused by each heterogeneous removal reaction. The colors red and black represent negative and positive values, respectively. Hollow circle represents the values scaled by 0.1. Corresponding values are shown in Table 8.

distribute 25% of the total VOC in this manner, which we have chosed based on the result of Shao et al. (2009) that the aromatics and the C5 alkenes contributed 17% and 7%, respectively, to the OH radical loss rate of VOCs in the urban area of Beijing in 2006. "S1" and "S2" are used to represent the results from simulations with the VOC emissions redistributed into C₃H₆ and C₄H₁₀, respectively. They are compared to the results from Sect. 3.2 (denoted as "S0"), as listed in Table 9. We find that, on the whole, these drastic changes in the emissions only cause relatively small changes in the result, of the order of 10% or less for O₃, and 20% or less for OH, with the one major exception of the effect of heterogeneous dust reactions on OH, which is found to be about three times as large for the S1 case as in the results discussed above (S0 case). Since NO_DUST simulations have larger burden of O₃ and OH than DUST_H simulations, and larger relative increases in O3 and OH are found in NO_DUST simulations when the additional C_3H_6 is considered, thus the effect of heterogeneous dust reactions (i.e. NO_DUST-DUST_H) are expanded, especially for OH. This indicates that the qualitative results discussed above, especially for ozone, would likely be similar in a model which included a more detailed representation of the higher VOC, though there may be some interesting detailed differences, especially for OH due to the differences in reactivity of various VOCs, which might be interesting to investigate in the future.

HR Un(%)	O ₃	NO ₂	NO ₃	N ₂ O ₅	HNO ₃	OH	HO ₂	H ₂ O ₂	НСНО	CH ₃ OH	CH ₃ COOH	SO ₂
SO ₂	-0.01	-0.08	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	-93.34
CH ₃ COOH	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-2.75	0.00
CH ₃ OH	-0.05	-0.21	0.00	0.00	0.00	0.01	0.01	0.00	0.03	-64.28	0.00	0.00
HCHO	3.16	23.15	0.00	0.03	-0.03	-0.61	-0.84	0.00	-92.16	-0.13	0.00	0.17
H_2O_2	-0.02	1.45	0.00	0.00	0.00	-0.01	0.42	-0.68	-0.15	0.00	0.00	-0.06
HO ₂	-5.66	365.55	0.01	0.14	-0.16	-3.61	-8.18	-0.01	-38.40	-0.26	-0.01	-14.45
OH	45.04	340.42	0.04	0.34	-0.39	-8.62	-11.58	-0.03	-54.75	-0.12	0.00	2.44
HNO ₃	0.00	-0.01	0.00	0.00	-46.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00
N_2O_5	-4.65	-2.98	-0.02	-3.87	0.00	-0.02	-0.05	0.00	-0.26	0.00	0.00	-0.09
NO ₃	-50.90	-34.47	-0.22	-0.40	-0.03	-0.30	-0.64	0.00	-3.12	-0.02	0.00	-1.06
NO ₂	-25.37	-75.67	-0.03	-0.29	-0.01	-0.09	-0.25	0.00	-1.15	-0.01	0.00	-0.56
O ₃	-49.17	-48.08	-0.04	-0.23	-0.02	-0.29	-0.63	0.00	-3.11	-0.02	0.00	-1.04

Table 8. Values of the uncertainties corresponding to Fig. 10. Columns are different heterogeneous removal reactions (HR) and rows are uncertainties in the tracer mixing ratios in percent (Un(%)).

Table 9. Results from the sensitivity simulations with additional surrogate VOC emissions in the NO_DUST and DUST_H simulations. "S1" and "S2" represent the results of the simulations with 25% of total VOC (as C-atoms) emission distributed to C3H6 and C4H10, respectively. "S0" represents the results in Sect. 3.2. Listed in the table are the differences (calculated as S1-S0 and S2-S0) in O3 mixing ratio and OH concentration for the NO_DUST and DUST_H simulations, and the uncertainties in the dust heterogeneous influences calculated as DUST_H–NO_DUST; The relative differences (calculated as (S1-S0)/S0 and (S2-S0)/S0) are shown in parentheses.

Tracer	O_3 nmol mol ⁻¹		ΔO_3 nmol mol ⁻¹	OH mo cm	ΔOH molecules cm ⁻³	
Simulation Difference	NO_DUST	DUST_H		NO_DUST	DUST_H	
\$1-\$0 \$2-\$0	0.78 (8.3%) -0.07 (-0.7%)	0.29 (5.7%) -0.03 (-0.5%)	-0.48 (11.5%) 0.04 (-1%)	3.5×10^4 (27.8%) -7.5 × 10 ³ (-6.1%)	$2.6 \times 10^4 (21.7\%) -7.3 \times 10^3 (-6.1\%)$	$\begin{array}{c} -8.5 \times 10^3 \ (192\%) \\ 2.6 \times 10^2 \ (-5.8\%) \end{array}$

4 Summary and conclusions

In this study, a box model is used in which detailed gas-phase chemistry is combined with dust surface uptake processes. Based on the output from a global atmospheric chemistry general circulation model and a regional emission inventory of North China, we design the "box" to represent the typical polluted condition in urban area of Beijing megacity. Dust is assumed to be transported together with other gas-phase species over the polluted region at various speeds. The influences of dust on tropospheric photochemistry via heterogeneous removal under different assumed transport speeds have been investigated and discussed in detail.

The influences due to mixing with upwind air mass have been discussed first, without considering the heterogeneous reactions on dust (i.e. NO_DUST simulations). It is found that the O_x mixing ratio and OH concentration both increase while the NO_x mixing ratio decreases with the increasing K_t (consistent with upwind levels of O₃ and NO_x). Similar tendencies of the O_x and NO_x mixing ratios are also found when the heterogeneous reactions are considered (i.e., in the DUST_H simulations), while the OH concentration is roughly constant in the simulations with the varying K_t .

The overall effect of introducing the heterogeneous dust reactions is to decrease the O_x mixing ratio. The change ranges from -2.5 to -18.4 nmol mol⁻¹, and is larger for faster mixing in of upwind air masses (i.e. greater K_t). This translates into a large relative change in O_x, ranging from -44% to -55%, which changes slightly with increasing values of K_t . This is comparable to the global results of Dentener et al. (1996), who found changes in the range of -50%to -20%. The NO_x mixing ratio is decreased due to introducing the heterogeneous dust reactions. The decrease ranges from -18 to -2.7 nmol mol⁻¹ (a relative decrease of -8% to -9%), and is smaller for faster mixing in of upwind air masses (i.e. greater K_t). The influence on OH due to the heterogeneous dust reactions on dust is complex. The OH concentration is increased for smaller K_t (4% in the T16 case), but decreased for greater K_t (up to -33% in the T02 case). It would be difficult to predict the anticipated change in OH for other cities without model simulations (box or 3-D) applicable to their specific conditions.

In the T04 case, by introducing an artificial 50% decrease of all photolysis rate coefficients, we estimate that the relative contributions of the heterogeneous removal on dust and the decrease in photolytic rates to the decrease in O_x mixing ratio are 87% (calculated by (y_(DUST H) $y_{(NO_DUST)})/(y_{(DUST_H+J)} - y_{(NO_DUST)}))$ and 28% (calculated by $(y_{(DUST_J)} - y_{(NO_DUST)})/(y_{(DUST_H+J)} - y_{(NO_DUST)})$ $y_{(NO_DUST)})$, respectively (note that this is only an approximate relative apportionment, because combining the two processes in the DUST_H+J run might cause nonlinear effects, which could lead to a smaller influence on O_x than the linearly summed influence, as discussed in Sect. 3.3, so that the sum of the two relative contributions is larger than 100%). They approximately fit to the values reported by Zhang et al. (1999) which are 79.7%-92.9% and 7.1%-20.3%, respectively.

It should be noted that in reality there is a dependence of the dust source on the wind speed (normally faster winds cause larger upwind sources), so the approach of assuming a constant upwind dust mixing ratio and size distribution for all four exchange rate coefficient cases will tend to underestimate the spread in the effects from T16 to T02.

The potential uncertainties due to different uptake coefficients are investigated in the T08 case. It is found that for most of the gases which are heterogeneously removed, the self-removal results in the largest uncertainty (with the important exceptions of OH and HO₂). The heterogeneous removal of NO₂ is particularly important due to its influence on the uncertainties in OH and HO₂; the heterogeneous removal of HCHO and O₃ also have similar farther-reaching effects. The results clearly indicate that the uncertainty in the uptake coefficients result in large uncertainties for the influence of dust under polluted conditions, and suggest that further laboratory work, especially on the uptake of NO₂, HCHO and O₃, will be valuable for reducing the uncertainties in future modeling studies.

This paper provides an analysis of potential influences of dust under the conditions of a typical highly polluted region. For global atmospheric chemistry and climate change studies, the overall O₃ change in the column due to dust is important. In a 3-D model study, Bian and Zender (2003) reported that in the real atmosphere the sensitivity of O_3 to the vertical location of dust is complicated and can change signs depending on the presence of O_3 precursors. Given this complexity, the overall influence of dust over the column will be examined in a follow-up 3-D model study. This study will provide guidance for the incorporation and analysis of heterogeneous dust reactions in a regional 3-D chemistry-transport model, which is being developed to study the impacts of dust on tropospheric photochemistry in different polluted areas of North China. Considering the large uncertainties demonstrated in this study, we will place particular emphasis on using sensitivity studies to evaluate the uptake coefficients appropriate for North China.

Appendix A

Review of the heterogeneous uptake coefficient values measured and adopted in former laboratory and model studies

A1 O₃

Many direct measurements of O₃ uptake on mineral dust were recently performed with contradictory results (Michel et al., 2002, 2003; Hanisch and Crowley, 2003; Usher et al., 2003). Values of γ in the range of approximately $10^{-6} \sim 10^{-4}$ were reported. In recent model studies, 1×10^{-5} was used by Liao et al. (2004), Liao and Seinfeld (2005), Tie et al. (2005), Bauer et al. (2004), and Pozzoli et al. (2008). In this study, the value 2.7×10^{-5} recommended by The International Union of Pure and Applied Chemistry (IUPAC) for China loess is used (http://www.iupac-kinetic.ch.cam.ac.uk).

A2 HNO₃, N₂O₅, NO₃ and NO₂

The reaction of nitric acid with mineral dust aerosols has been recently addressed by several laboratory studies (Hanisch and Crowley, 2001; Goodman et al., 2000; Underwood et al., 2001; Grassian, 2002). This reaction irreversibly removes HNO₃ from the gas phase. The reported γ for HNO₃ varies from approximately 10⁻⁵ to 0.2. In model studies, 10⁻³ was used by Bian and Zender (2003), while 0.1 was used by Liao et al. (2004), Liao and Seinfeld (2005), Tie et al. (2005), Pozzoli et al. (2008), Dentener et al. (1996), and Bauer et al. (2004). A larger value of 0.17 recommended by IUPAC for Chinese dust is adopted for this study.

In recent laboratory work, the uptake of N_2O_5 on mineral dust was investigated by Seisel et al. (2005), Karagulian et al. (2006) and Wagner et al. (2008). Seisel et al. (2005) and Wagner et al. (2008) reported similar values of about 10^{-2} , while Karagulian et al. (2006) reported significantly larger values (about 10^{-1}). In model studies, Dentener et al. (1996), Bian and Zender (2003) used the value 0.1, while values between 0.003 and 0.02 depending on the relative humidity were used by Bauer et al. (2004), Liao et al. (2004), Liao and Seinfeld (2005), and Pozzoli et al. (2008). The value 0.03 is chosen as a compromise for this study.

Some experiments focusing directly on the uptake of NO₃ on mineral dust surfaces have been performed by Karagulian and Rossi (2005). The measured uptake coefficient ranged from roughly 0.01 to 0.23 for different mineral dusts. Tang et al. (2010) determined that γ (NO₃)/ γ (N₂O₅) = 0.9±0.4 for Saharan dust, indicating an uptake coefficient of γ (NO₃) = 9×10^{-3} with an associated uncertainty of at least factor of two. These values are significantly larger than the γ value of 3.0×10^{-3} for NO₃ used by Bauer et al. (2004). An intermediate γ value of 0.1 for NO₃ was used for the modeling studies performed by Bian and Zender (2003) and Pozzoli et al. (2008), and is also used in this study.

The initial uptake coefficients for NO₂ on the surface of different mineral particles were measured by Underwood et al. (2001). The γ value ranges from $<4 \times 10^{-10}$ to 2×10^{-5} , with most values in the 10^{-6} range. Ullerstam et al. (2003) measured the uptake coefficient of NO₂ for Saharan dust. They reported the uptake coefficient as $(2.0\pm0.4)\times10^{-4}$ for geometric area. IUPAC recommends an upper limit of 1×10^{-6} for γ , considering that it will be smaller as the dust aging (e.g. being coated with nitrate from HNO₃ uptake). The modeling study performed by Bian and Zender (2003) used a γ value of 4.4×10^{-5} for NO₂. In this study, we employ a lower value of 2.1×10^{-6} recommended by IUPAC for China loess.

A3 HO₂, OH and H₂O₂

Laboratory experiments on the uptake of OH and HO₂ on sulfuric acid and water surfaces show reactive uptake coefficients which range from 0.004 to 1 for OH, and from 0.01 to 1 for HO₂ (Hanson et al., 1992). Unfortunately no laboratory studies of the uptake of the HO₂ radical on mineral dust aerosol are documented; however, in a review, Jacob (2000) recommends including the uptake of HO₂ by aerosols with $\gamma = 0.2$ in atmospheric chemistry models, and also concludes that although the mechanism for HO₂ uptake is uncertain, H_2O_2 is the likely product. Here we adopt this recommendation for γ , as well as the assumption that H₂O₂ is the only reaction product with a 100% yield. For the uptake coefficient of OH, we adopt the value of 0.1, based on DeMore et al. (1997). This value was also used by Bian and Zender (2003) and Zhang and Carmichael (1999) in their modeling studies of the heterogeneous chemistry on mineral dust.

Measured mass accommodation coefficients of H_2O_2 on sulfuric acid and water surfaces, within a range from 8×10^{-4} to 0.18, are reported by DeMore et al. (1997). In the modeling studies of Dentener et al. (1996), Bian and Zender (2003) and Zhang and Carmichael (1999), $\gamma = 1.0 \times 10^{-4}$ was used for mineral dust surfaces. However, de Reus et al. (2005), employing the assumption that H_2O_2 is formed when HO_2 is taken up in the Saharan dust aerosol, concluded that the heterogeneous removal of HO_2 and H_2O_2 , with accommodation coefficients of 0.2 and 2×10^{-3} , respectively, had to be included in order to obtain agreement between calculated and observed values. In this study, we use the values from de Reus et al. (2005).

A4 Acetic acid, formaldehyde and methanol

The heterogeneous uptake of VOC (volatile organic compound) has rarely been included in modeling studies. In this study, in order to explore the potential sensitivity to these reactions, we use uptake coefficients for acetic acid (CH₃COOH), formaldehyde (HCHO), and methanol (CH₃OH) of 10^{-3} , 10^{-5} and 10^{-5} , respectively, based on the laboratory measurements performed by Carlos-Cuellar et al. (2003).

A5 SO₂

Recently, the heterogeneous reactivity of SO₂ has been studied on metal oxides (Goodman et al., 2001; Usher et al., 2002), China Loess dust (Usher et al., 2002) and Saharan mineral dust (Ullerstam et al., 2002; Ullerstam et al., 2003; Adams et al., 2005). The reported γ values range from roughly 5×10^{-7} to 2.6×10^{-4} . Pozzoli et al. (2008) used a value of 1×10^{-4} in their modeling study. The value of 3×10^{-5} recommended by IUPAC for Chinese dust has been used in this study.

Appendix B

Formula derivation for Eq. (B4)

Based on Eq. (B1):

$$C_{i} = \frac{K_{t} \cdot C_{i}' + B_{e} + B_{cp}}{K_{t} + K_{cl} + K_{d}},$$
(B1)

the heterogeneous influence on the tracer daily average concentration is represented as (for any species *i*, leaving out the subscript here for readability):

$$\Delta C = C_{(\text{DUST}_\text{H})} - C_{(\text{NO}_\text{DUST})}$$

$$= \frac{K_t \cdot C' + B_e + B_{cp(\text{DUST}_\text{H})}}{K_t + K_{cl(\text{DUST}_\text{H})} + K_d} - \frac{K_t \cdot C' + B_e + B_{cp(\text{NO}_\text{DUST})}}{K_t + K_{cl(\text{NO}_\text{DUST})} + K_d}$$

$$= \frac{(K_{cl(\text{NO}_\text{DUST}]} - K_{cl(\text{DUST}_\text{H})}) \cdot (K_t \cdot C' + B_e + B_{cp(\text{NO}_\text{DUST})})}{(K_t + K_{cl(\text{NO}_\text{DUST})} + K_d) \cdot (K_t + K_{cl(\text{DUST}_\text{H})} + K_d)}$$

$$+ \frac{(B_{cp(\text{DUST}_\text{H})} - B_{cp(\text{NO}_\text{DUST})}) \cdot (K_t + K_{cl(\text{NO}_\text{DUST})} + K_d)}{(K_t + K_{cl(\text{NO}_\text{DUST})} + K_d) \cdot (K_t + K_{cl(\text{DUST}_\text{H})} + K_d)}$$
(B2)

where ΔC is the difference in the tracer daily average concentration between the NO_DUST and DUST_H simulations (DUST_H-NO_DUST). Recognizing that

$$\frac{(K_t \cdot C' + B_e + B_{cp(\text{NO}_\text{DUST})})}{(K_t + K_{cl(\text{NO}_\text{DUST})} + K_d)} = C_{(\text{NO}_\text{DUST})},$$
(B3)

and defining $K_{cl(\text{NO}_{DUST})} - K_{cl(\text{DUST}_{H})} = -\Delta K_{cl}$ and $B_{cp(\text{DUST}_{H})} - B_{cp(\text{NO}_{DUST})} = \Delta B_{cp}$, we can simplify the formula to:

$$\Delta C = \frac{\Delta B_{cp} - \Delta K_{cl} \cdot C_{\text{(NO_DUST)}}}{(K_t + K_{cl(\text{DUST_H})} + K_d)}.$$
(B4)

Appendix C

Table C1. The absolute differences in the tracer mixing ratios calculated with the "Upper Limit" and "Lower Limit" coefficients $(y_{\text{DUST}_H}(\gamma_{\text{Upper}}) - y_{\text{DUST}_H}(\gamma_{\text{Lower}}))$. Columns are different heterogeneous removal reactions (HR) and rows are absolute differences in ppbv (AD(nmol mol⁻¹)).

HR AD (nmol mol-1)	O ₃	NO ₂	NO ₃	N ₂ O ₅	HNO ₃	ОН	HO ₂	H ₂ O ₂	НСНО	CH ₃ OH	CH ₃ COOH	SO ₂
SO ₂	-3.9E-02	-2.9E-01	-6.1E-05	-3.1E-04	3.5E-04	7.5E-03	1.0E-02	6.1E-05	4.7E-02	1.2E-04	3.1E-05	-3.2E+02
CH ₃ COOH	2.4E-07	-2.9E-05	0.0E+00	-2.6E-06	-6.9E-06	-1.4E-06	-6.3E-05	-1.5E-05	2.7E-05	0.0E+00	-9.0E-02	4.1E-06
CH ₃ OH	-2.6E-03	-1.2E-02	-2.1E-06	-1.7E-05	1.3E-05	3.0E-04	4.0E-04	1.7E-06	1.9E-03	-3.7E+00	4.8E-07	-1.1E-04
HCHO	7.9E-02	5.8E-01	7.5E-05	6.4E-04	-6.7E-04	-1.5E-02	-2.1E-02	-6.4E-05	-2.3E+00	-3.2E-03	-1.1E-04	4.3E-03
H_2O_2	-4.3E-05	2.8E-03	1.0E-07	1.1E-06	-1.2E-06	-2.8E-05	8.0E-04	-1.3E-03	-3.0E-04	-2.0E-06	2.4E-07	-1.1E-04
HO ₂	-9.3E-07	6.0E-05	2.2E-09	2.4E-08	-2.6E-08	-6.0E-07	-1.3E-06	-2.1E-09	-6.3E-06	-4.2E-08	-1.2E-09	-2.4E-06
OH	2.3E-06	1.8E-05	2.3E-09	1.8E-08	-2.0E-08	-4.5E-07	-6.0E-07	-1.5E-09	-2.8E-06	-6.5E-09	-2.1E-10	1.3E-07
HNO ₃	-3.3E-05	-1.3E-04	0.0E+00	-2.4E-07	-1.2E+00	-1.9E-05	-2.6E-05	0.0E+00	-1.2E-04	-2.4E-07	0.0E+00	2.9E-06
N_2O_5	-1.0E-04	-6.4E-05	-3.6E-07	-8.3E-05	-5.1E-08	-5.0E-07	-1.1E-06	-2.3E-09	-5.5E-06	-3.5E-08	-2.6E-09	-2.0E-06
NO ₃	-4.1E-06	-2.8E-06	-1.8E-08	-3.3E-08	-2.3E-09	-2.4E-08	-5.2E-08	-1.1E-10	-2.5E-07	-1.5E-09	-1.0E-10	-8.6E-08
NO ₂	-1.8E+01	-5.3E+01	-1.9E-02	-2.0E-01	-8.2E-03	-6.6E-02	-1.8E-01	-3.1E-04	-8.1E-01	-6.6E-03	-3.8E-04	-4.0E-01
O ₃	-4.5E+00	-4.4E+00	-3.3E-03	-2.1E-02	-1.8E-03	-2.7E-02	-5.8E-02	-1.2E-04	-2.9E-01	-1.7E-03	-9.9E-05	-9.6E-02

Appendix D

Table D1. The uncertainties computed by normalizing the absolute differences by the tracer mixing ratios calculated with the "Best Guess" coefficients. Columns are different heterogeneous removal reactions (HR) and rows are uncertainties in percent (Un(%)).

HR Un(%)	O ₃	NO ₂	NO ₃	N ₂ O ₅	HNO ₃	ОН	HO ₂	H_2O_2	НСНО	CH ₃ OH	CH ₃ COOH	SO ₂
SO ₂	-0.04	-0.31	0.00	0.00	0.00	0.01	0.01	0.00	0.05	0.00	0.00	-339.96
CH ₃ COOH	0.01	-0.93	0.00	-0.09	-0.23	-0.05	-2.04	-0.49	0.89	0.00	-2921.05	0.13
CH ₃ OH	-0.10	-0.48	0.00	0.00	0.00	0.01	0.02	0.00	0.07	-145.72	0.00	0.00
HCHO	5.83	42.71	0.01	0.05	-0.05	-1.13	-1.54	0.00	-170.00	-0.24	-0.01	0.32
H_2O_2	-9.32	597.80	0.02	0.24	-0.26	-5.99	172.04	-279.25	-63.52	-0.42	0.05	-23.92
HO ₂	-9.42	607.82	0.02	0.24	-0.26	-6.01	-13.60	-0.02	-63.85	-0.43	-0.01	-24.03
OH	46.69	352.89	0.05	0.35	-0.40	-8.94	-12.01	-0.03	-56.75	-0.13	0.00	2.53
HNO ₃	-16.05	-60.74	0.00	-0.12	-558522.12	-9.01	-12.47	0.00	-57.73	-0.12	0.00	1.39
N_2O_5	-222.03	-142.35	-0.80	-184.60	-0.11	-1.11	-2.53	-0.01	-12.26	-0.08	-0.01	-4.51
NO ₃	-172.81	-117.02	-0.74	-1.37	-0.10	-1.00	-2.17	0.00	-10.59	-0.06	0.00	-3.59
NO ₂	-36.77	-109.69	-0.04	-0.42	-0.02	-0.14	-0.37	0.00	-1.67	-0.01	0.00	-0.81
O ₃	-89.76	-87.78	-0.07	-0.42	-0.04	-0.53	-1.15	0.00	-5.68	-0.03	0.00	-1.90

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